



## Stormwater Management Report

483 – 485 Elizabeth Ave  
Block 507.14, Lots 61 & 62  
Franklin Township, Somerset County, NJ

October 2020

*Prepared For*  
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### **Appendices**

- A. Hydrographs, CN, & Tc Calculations for Existing Conditions
- B. Hydrographs, CN, & Tc Calculations for Developed Conditions, Storage Volume and Stage-Storage Calculations for Stormwater Management Basin
- C. NJDEP Water Quality Storm Routing, Calculations, Dewatering, & Water Budget
- D. Emergency Spillway Calculations (150% of 100 Year Storm Routing)
- E. Pipe Calculations for Stormwater Conveyance System & HGL Profiles
- F. Conduit Outlet Protection & Curb Cut Calculations
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### **Maps**

- 1. Project Location Map – USGS QUAD
- 2. Soils Map
- 3. Existing Drainage Area Map
- 4. Proposed Drainage Area Map
- 5. Inlet Drainage Area Map





## Introduction

On behalf of the applicant, Elizabeth Realty Partners, LLC, Maser Consulting, Inc. is submitting this stormwater management report as part of a major site plan submission. The ±8.40 acre project site ( $\pm 4.8$  acre disturbance area) is located on the northbound side of Elizabeth Ave. The project site is known as Block 507.14, Lots 61 & 62. The proposed development is a warehouse use consisting of an approximate 76,230 SF warehouse including office space. Additional site improvements include, but are not limited to, the construction of loading docks, vehicle parking spaces, site lighting, landscaping, storm sewers, water mains, septic system, and utility laterals. One wet pond and a porous pavement area are proposed for the project. The project includes the demolition of the existing residence on the southeastern side of the site and associated improvements.

To satisfy the current stormwater management regulations, new stormwater management features are proposed. The site has been designed with features that provide stormwater attenuation, address groundwater recharge requirements, and satisfy water quality treatment requirements prior to discharge.

## Hydrologic Methodologies

The Soil Conservation Service Unit Hydrograph (Appendix I) was utilized to calculate the stormwater runoff volumes and rates from the project site. Technical Release No. 55 (TR55) was utilized to obtain runoff curve numbers (CNs) for the various land cover types, and to obtain coefficients to calculate the time of concentration (TC) for each drainage area. The hydrologic model was analyzed and designed with the HydroCAD software program v10. The Type C storm was utilized to analyze the 2, 10, 25, and 100-year storm events.

The following parameters were utilized in the design of the stormwater management system:

**Water Quantity** - NJAC 7:8-5.4(a)3 provides three alternatives for controlling stormwater runoff quantity impacts.

- i. Demonstrate through hydrologic and hydraulic analysis that for stormwater leaving the site, post-construction runoff hydrographs for the two, 10 and 100-year storm events do not exceed, at any point in time, the pre-construction runoff hydrographs for the same storm events;*
- ii. Demonstrate through hydrologic and hydraulic analysis that there is no increase, as compared to the pre-construction condition, in the peak runoff rates of stormwater leaving the site for the two, 10 and 100-year storm events and that the increased volume or change in timing of stormwater runoff will not increase flood damage at or downstream of the site. This analysis shall include the analysis of impacts of existing land uses and projected land uses assuming full development under existing zoning and land use ordinances in the drainage area; or*
- iii. Design stormwater management measures so that the post-construction peak runoff rates for the two, 10 and 100-year storm events are 50, 75 and 80 percent, respectively, of the pre-construction peak runoff rates. The percentages apply only to the post-construction stormwater runoff that is attributable to the portion of the site on which the proposed development or project is to be constructed.*



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**Water Quality** - Treat runoff volume generated by the NJDEP 1.25-inch, 2-hour Water Quality Storm by utilizing stormwater management methods that reduce the developed site's average annual total suspended solids (TSS) load by at least 80% for proposed developed drainage areas, per NJAC 7:8-5.5.

**Groundwater Recharge** - Maintain 100 percent of the existing annual groundwater recharge volume on site under developed conditions, per NJAC 7:8-5.4 and the New Jersey Stormwater BMP Manual, Chapter 6.

## Existing Conditions

The site topography has elevations ranging from 62± to 85±. The site is a combination of open space, wooded areas, wooded wetlands, two residential homes & drives, and an unnamed tributary of the Raritan River with crossings.

Based on the NRCS Web Soil Survey for Somerset County, the following soil types are mapped: Norton Loam (HSG C), Penn Silt Loam (HSG C) and Reaville Silt Loam (HSG C).

The existing drainage areas are broken into three areas, EDA 1, 2 and O.S.

EDA 1, the largest tract drains to an existing unnamed tributary of the Raritan River crossing the site. The existing tributary is located on the southwest portion of the site and runs in front of the southern residence and behind the northern residence. The tributary collects all the runoff from the site and Elizabeth Ave. The tributary flows from southwest to northeast and continues offsite and discharges into the Raritan River about two (2) miles northeast.

EDA-2, the northeasterly portion of the site initially drains to the north off-site. The runoff flows towards the tributary but is not collected by the on-site. The stormwater runoff from EDA-2 is collected by the tributary to the north of the site. The area consists of woods and grass.

EDA-O.S. borders the northwest portion of the tract and mainly consists of woods and grass. This area splits into two different routes. The southern portion of the off-site drainage area flows to a swale along the south property line. The northern portion follows the same path as EDA-2.

EDA-1: 4.44 Acres

EDA-2: 0.37 Acres

EDA-O.S.: 0.68 Acres

All three drainage patterns and areas converge into the existing Raritan River Unnamed Tributary.



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## Proposed Conditions

The project proposes the construction of a one-story warehouse consisting of an office and warehouse floor space. A driveway, car parking area, truck loading area, and a fire access drive are also proposed. The proposed stormwater management was designed so that the developed flow rates for the 2-year, 10-year and 100-year storms would be reduced to at least 50%, 75% and 80% of the existing flow rates for all of the developed drainage areas (PDA 1, O.S., U.D. A & B).

There are four overall post-developed drainage areas.

PDA 1 & O.S. is captured and detained in a proposed wet pond. The wet pond discharges into the existing tributary via a new driveway crossing and culvert also proposed in this project.

PDA U.D A is located on the west end of the proposed development. This area consists of undetained runoff that could not be routed to the basin due to elevation constraints. The large majority of the undetained area is the proposed driveway. All driveway runoff that could be reasonably captured is collected by two inlets on the high end of the driveway. All other undetained runoff from the drive is collected by additional inlets near Elizabeth Avenue and discharged at the proposed culvert into the tributary.

PDA U.D B. is located on the southeast portion of the site. The area consists of a proposed septic field that will treat wastewater from the warehouse. This area drains into the adjacent wetlands on the southern portion of the site. This wetland area discharges into the swale along the southern property line and into the upstream reach of the on-site tributary. This area follows the same path as EDA O.S.



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## Flow Rates & Volumes

The enclosed calculations were performed using the Soil Conservation Service Unit Hydrograph (Appendix I). Below is a comparison of the existing and developed flow rates for the site's drainage areas during a 2-year, 10-year, 25-year, and 100-year storm frequency.

Table 1: Peak Flow Rates for the Existing Drainage Areas (EDAs)

	EDA-1 Peak Flow Rate (cfs)	EDA-2 Peak Flow Rate (cfs)	EDA-O.S. Peak Flow Rate (cfs)
2-year	3.03	0.35	0.99
10-year	6.89	0.82	2.20
25-year	9.90	1.19	3.14
100-year	15.31	1.85	4.81

Table 2: Peak Undetained Flow Rates for the Developed Drainage Areas (PDAs)

	PDA-1 & O.S. (Wet Pond) Peak Flow Rate (cfs)	PDA-1 UD A Peak Flow Rate (cfs)	PDA-1 UD B Peak Flow Rate (cfs)
2-year	0.26	1.05	0.12
10-year	4.12	1.84	0.26
25-year	9.41	2.43	0.37
100-year	10.36	3.45	0.56

Table 3: Permitted Developed Flow Rates (based on NJDEP required reductions)

EDA-1.2 & O.S./PDA-1 & O.S.	2-Year Storm	10-Year Storm	100-Year Storm
EDA-1 & 2 Permitted Discharge Flow Rates	3.38 cfs x 50% = 1.69 cfs	7.71 cfs x 75% = 5.78 cfs	17.16 cfs x 80% = 13.73 cfs
EDA- O.S. Permitted Discharge Flow Rates	0.99 cfs	2.20 cfs	4.81 cfs
Total Permitted Discharge Flow Rates	2.68 cfs	7.98 cfs	18.54 cfs
Basin Discharge, PDA-1, O.S. & PDA-1 UD A&B Combined	0.26 cfs#	4.12 cfs#	10.36 cfs#

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## Storage Systems

The proposed stormwater management wet pond is described above in “Proposed Conditions.”

Table 5: Peak Rates and Storage Volumes for the Stormwater Management Basins

Wet Pond				
Condition	Peak Inflow Rate (cfs)	Peak Outflow Rate (cfs)	Maximum Storage Volume (cf.)	Maximum Water Surface Elevation
2-year	11.64	0.26	33,090	71.10
10-year	18.35	4.12	40,025	71.60
25-year	23.16	9.41	45,216	71.96
100-year	31.45	10.36	59,183	72.89

## Emergency Spillway Calculations

The earthen, broad-crested weir emergency spillway has been designed to safely convey 150% of the 100-year storm if the basin outlet structure orifices, weirs, and grates are blocked.

The emergency spillway is designed as a 50’ wide earthen broad-crested weir. The invert of the spillway is 73.00 and the top of the berm is 74.00. At 150% of the 100-year storm, the spillway will convey the stormwater at 46.56 cfs with a maximum elevation of 73.49. The velocity will be 1.91 fps.

## Water Quality

The proposed wet pond and porous paving has been designed to provide water quality benefits to meet New Jersey Stormwater Quality Requirements per NJAC 7:8-5.5 and the New Jersey Stormwater BMP Manual, Chapter 9.5.

The total required TSS removal rate for the tract has been calculated below taking into consideration an existing driveway area that will be removed and revegetated as a part of the project (0.11 acres) and an existing gravel driveway that will be removed and replaced.

### Required TSS removal rate

Total impervious area to be treated = 1.57 acres

Total paved driveway area to be removed = 0.11 acres

Total gravel driveway area to be removed = 0.01 acres

$[(80\% \times (1.57 \text{ acres} - 0.12 \text{ acres})) + (0\% \times 0.11 \text{ acres}) + (50\% \times 0.01 \text{ acres})]/1.57 \text{ acres} = 74.2\%$

74.2% TSS Removal Rate Required

The Wet Pond utilizes a permanent pool at least three times greater than the water quality storm of the inflow for a 80% TSS removal. The inflow water quality storm volume is 4,051 cf. The permanent pool volume for the wet pond is 28,506 cf which is greater than three times the water quality storm volume. The wet pond also achieves a water quality storm detention time of 46.2 hours and therefore combined with the 3:1 volume achieves a 90% TSS removal rate. See Appendix C.



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The porous paving on a portion of the employee parking area is designed to infiltrate the water quality storm. A minimum of 16" of stone is used throughout the entire porous paving parking lot. A design infiltration rate of 0.5 in/hr was used for exfiltration of the stone. The invert of the stone is 73.85 and the minimum top elevation is 75.19. The water quality storm reaches a peak of 74.64, therefore the stone can detain the water quality storm. Larger storms are collected by an overflow piping system and discharged to the proposed wet pond. Supporting calculations can be found in Appendix C. The porous paving system will provide 80% TSS removal.

A portion of the proposed access driveway cannot be treated in the above systems due to elevation challenges. Since the proposed treatment systems achieve TSS removal rates over the required amount, an average for the project tract has been provided. All area discharge to the downstream side of the proposed culvert within the Raritan River Tributary on-site.

Porous Paver Drainage Area = 80% x 0.23 acres

Wet Pond Drainage Area = 90% x 1.11 acres

Driveway Drainage Area = 0% x 0.23 acres

#### Provided TSS removal rate

$$[(0.23 \times 80) + (1.11 \times 90) + (0.23 \times 0)]/1.57 \text{ acres} = 75.4 \%$$

75.4% TSS Removal Rate Achieved > 74.2% Required

## Groundwater Recharge

The proposed groundwater recharge facility (Porous Paving) has been designed to maintain 100 percent of the existing annual groundwater recharge volume, per by NJAC 7:8-5.4 and the New Jersey BMP Manual, Chapter 6. The site was analyzed utilizing the NJ Annual Groundwater Recharge Spreadsheet (based on GSR-32), described in Chapter 6 of the New Jersey Stormwater BMP Manual, along with existing and proposed impervious/pervious coverage information. See Appendix H for supportive documentation that groundwater recharge is achieved. Also refer to the above noted appendices for infiltration design information.

## Off-Site Stability

### Stability Analysis:

A wet pond has been designed which reduces the peak flow rates to less than 50% of the predevelopment 2-year storm and less than 75% of the predevelopment 10-year storm. A comparison table on page 4 is provided for pre and post development discharges.

## Storm Sewer Collection System

The storm sewer system has been designed in accordance with NJAC 5:21-7.2, 7.3 & 7.4. The 25-year frequency storm event was utilized. The Somerset IDF curve, as determined by NOAA Atlas 14 and specified in NJAC 5:21-7.2(c)5, was utilized to determine the storm intensity. A minimum time of concentration of 10 minutes was utilized in the design, per NJAC 5:21-7.2(c)5. See Appendix E for calculation worksheets.



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## Nonstructural Strategies

According to the NJDEP Stormwater Management Rules at N.J.A.C. 7:8, the groundwater recharge, stormwater quality, and stormwater quantity standards established by the Rules for major land development projects must be met by incorporating nine specific nonstructural stormwater management strategies into the project's design to the maximum extent practicable.

The site remains compliant with NJAC 7:8-5.3 non-structural management strategies by specifically incorporating the following nonstructural stormwater management strategies as follows:

1. Protect areas that provide water quality benefits or areas particularly susceptible to erosion and sediment loss;

*The footprint of the improvements has been minimized. The existing wetland area disturbance has been minimized and transition area compensated for. Stormwater runoff will be discharged in a similar manor of existing conditions.*

2. Minimize impervious surfaces and break up or disconnect the flow of runoff over impervious surfaces;

*The overall impervious coverage is less than 49% and below the Township ordinance of 60% maximum impervious coverage. Porous paving and curb cuts for drainage have been utilized to disconnect impervious surfaces.*

3. Maximize the protection of natural drainage features and vegetation;

*The footprint of the improvements has been minimized to the rear of the site. The clearing of the existing wooded area in the front of the site is minimized. Stormwater runoff will be discharged in a similar manor of existing conditions. Wetland disturbance has been minimized. Soil erosion measures are proposed to be utilized during construction to protect the adjoining properties and wetland area. An existing house and associated impervious improvement will be removed and revegetated.*

4. Minimize the decrease in the "time of concentration" from pre-construction to post construction. "Time of concentration" is defined as the time it takes for runoff to travel from the hydraulically most distant point of the drainage area to the point of interest within a watershed;

*Porous paving and curb cuts for drainage have been utilized to disconnect impervious surfaces and increase time of concentration.*

5. Minimize land disturbance including clearing and grading;

*The proposed land disturbance has been minimized to 4.77AC which is only 57% of the total tract. Disturbance to wetland and tributary areas have been minimized. Retaining walls are proposed along the parking lot, basin and driveway to reduce expanded grading which reduces the overall disturbance area.*

6. Minimize soil compaction;

*Soil compaction has been minimized within the project limits. The site is subject to the decompaction requirements of the from the Soil Erosion & Sediment Control Details for compaction testing details.*

7. Provide low-maintenance landscaping that encourages retention and planting of native vegetation and minimizes the use of lawns, fertilizers and pesticides;

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*Landscaping proposed has been chosen for its native and drought tolerant qualities.*

8. Provide vegetated open-channel conveyance systems discharging into and through stable vegetated areas; and

*The loading area has been designed to discharge through curb cuts to the vegetated basin in lieu of piping.*

9. Provide other source controls to prevent or minimize the use or exposure of pollutants at the site to prevent or minimize the release of those pollutants into stormwater runoff. These source controls include, but are not limited to:

- i. Site design features that help to prevent accumulation of trash and debris in drainage systems;

*In existing conditions, the debris washes directly into the existing tributary. In proposed conditions, the stormwater inlets have been specified with "eco J" type curb pieces indicating the text "Dump No Waste, Drains to Waterways" and trash racks are specified for installation at the outlet control structure. In addition, a "Stormwater Management Facilities Operation & Maintenance Manual" has been prepared for use by contractors and the owners that specify that street sweeping must occur on a bi-monthly schedule.*

- ii. Site design features that help to prevent discharge of trash and debris from drainage systems;

*In existing conditions, the debris washes directly into the tributary. In proposed conditions, the stormwater inlets have been specified with "eco J" type curb pieces indicating the text "Dump No Waste, Drains to Waterways" and trash racks are specified for installation at the outlet control structure. In addition, a "Stormwater Management Facilities Operation & Maintenance Manual" has been prepared for use by contractors and the owners that specify that street sweeping must occur on a bi-monthly schedule.*

- iii. Site design features that help to prevent and/or contain spills or other harmful accumulations of pollutants at industrial or commercial developments; and

*The stormwater management wet pond and porous paving will improve water quality by 80% or more.*

- iv. When establishing vegetation after land disturbance, applying fertilizer in accordance with the requirements established under the Soil Erosion and Sediment Control Act, N.J.S.A. 4:24-39 et seq., and implementing rules.

*The soil erosion and sediment control and landscape plans address the requirement for establishing vegetation.*

Preventative source controls include use of ECO inlet curb pieces, storm drain inlets and trash rack on the OFS. Pollution prevention techniques such as water quality treatment thru infiltration and clearing restrictions have been implemented in the design. The soil erosion and sediment control plan addresses, re-stabilizing vegetation and implementing SESC protection measures. Prevention and maintenance is also addressed in the Stormwater Operations and Maintenance Manual prepared for the project.

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## Conclusion

The proposed development has been designed in accordance with NJAC 5:21, NJAC 7:8 & the New Jersey Stormwater Best Management Practices Manual.





## **APPENDIX A**

Hydrographs, CN, & Tc Calculations for Existing Conditions



## Worksheet 3: Time of Concentration (Tc) or Travel Time (Tt)

Project: Elizabeth Realty Partners LLC

Location: Franklin Township (Somerset)

By: MSB

Date: 10/12/2020

Circle one: Present Developed

Checked: MSY

Date: \_\_\_\_\_

Circle one: Tc Tt through subarea

EDA-1

Notes: Space for as many as two segments per flow type can be used for each worksheet. Include a map, schematic, or description of flow segments.

### Sheet Flow (applicable to Tc only)

1. Surface description (table 3-1)
2. Manning's roughness coefficient, n (table 3-1)
3. Flow Length, L (total L ≤ 300 ft)
4. Two-year 24-hour rainfall, P2
5. Land slope, s
6.  $Tc = \frac{0.007(nL)^{0.8}}{(P2)^{0.5}s^{0.4}}$

Grass (Dense)		
0.24		
ft		
100		
in		
3.3		
ft/ft		
0.025		
hr	0.21	+
	0	+
		=
		0.21

### Shallow Concentrated Flow

7. Surface Description (paved or unpaved)
8. Flow Length, L
9. Watercourse slope, s
10. Average Velocity, V (figure 3-1)
11.  $Tt = \frac{L}{3600V}$

Unpaved		
ft		
702		
ft/ft		
0.024		
ft/sec		
0.77		
hr	0.25	+
	0	+
		=
	0	0.25

### Channel Flow

12. Cross sectional flow area, a
13. Wetted perimeter, pw
14. Hydraulic radius, r (=a/pw)
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49r^{(2/3)}s^{(1/2)}}{n}$
18. Flow length, L
19.  $Tt = \frac{L}{3600V}$

sq ft	27.00		
ft	18.00		
ft	1.5000	0	0
ft/ft	0.005		
	0.03		
ft/s	4.60	0	0
ft	322		
hr	0.02	+	
	0.00	+	
			=
	0.00		0.02

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

$$= \begin{array}{|c|} \hline 0.49 \\ \hline \end{array} \text{ hr}$$

$$= \begin{array}{|c|} \hline 29.1 \\ \hline \end{array} \text{ min}$$

## Worksheet 3: Time of Concentration (Tc) or Travel Time (Tt)

Project: Elizabeth Realty Partners LLC

Location: Franklin Township (Somerset)

By: MSB

Date: 10/12/2020

Circle one: Present Developed

Checked: MSY

Date: \_\_\_\_\_

Circle one: Tc Tt through subarea

EDA-2

Notes: Space for as many as two segments per flow type can be used for each worksheet. Include a map, schematic, or description of flow segments.

### Sheet Flow (applicable to Tc only)

1. Surface description (table 3-1)
2. Manning's roughness coefficient, n (table 3-1)
3. Flow Length, L (total L ≤ 300 ft)
4. Two-year 24-hour rainfall, P2
5. Land slope, s
6.  $Tc = \frac{0.007(nL)^{0.8}}{(P2)^{0.5}s^{0.4}}$

ft	Grass (Short)		
	0.15		
in	42		
	3.3		
ft/ft	0.004		
hr	0.15	+	0
			=
			0.15

### Shallow Concentrated Flow

7. Surface Description (paved or unpaved)
8. Flow Length, L
9. Watercourse slope, s
10. Average Velocity, V (figure 3-1)
11.  $Tt = \frac{L}{3600V}$

ft	Grassed	Woodland	
	20	97	
ft/ft	0.024	0.021	
ft/sec	0.77	0.75	
hr	0.01	0.04	=
			0.04

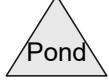
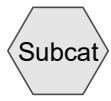
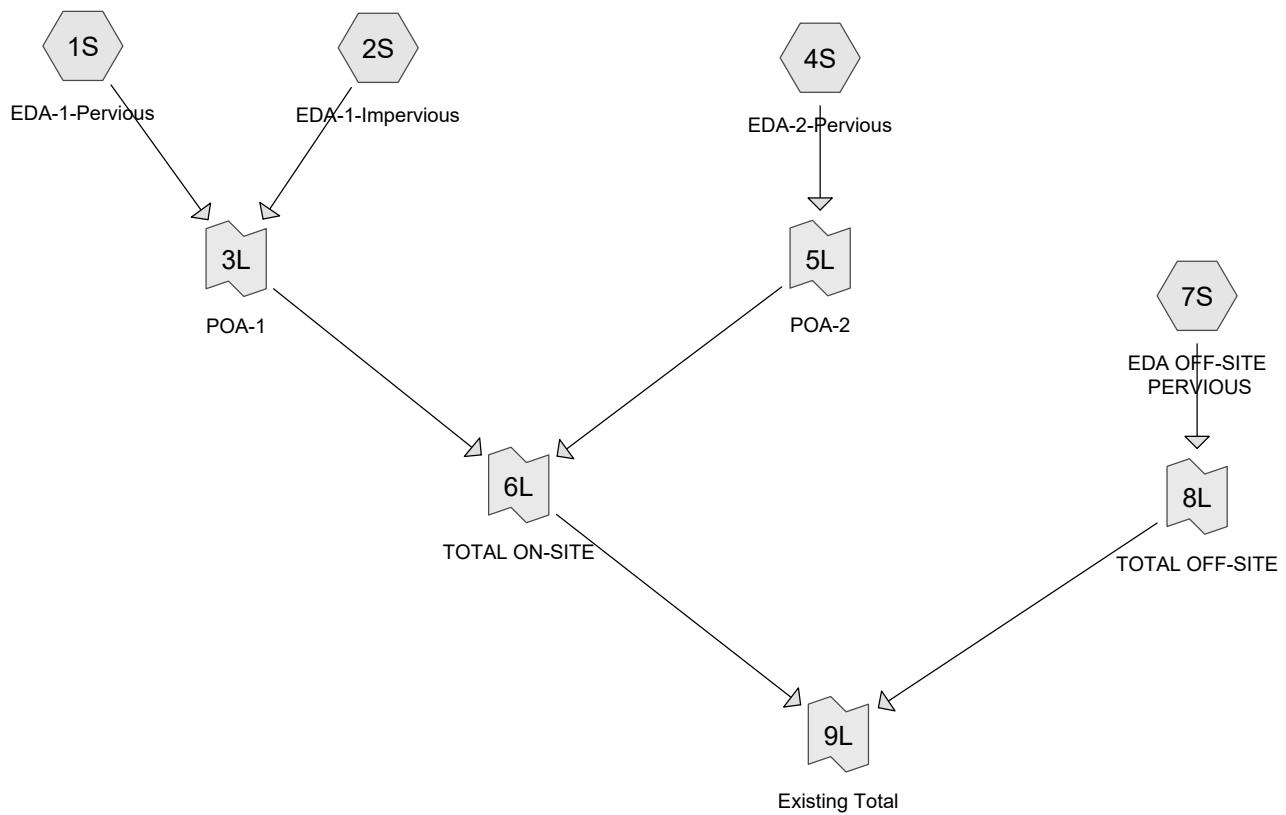
### Channel Flow

12. Cross sectional flow area, a
13. Wetted perimeter, pw
14. Hydraulic radius, r (=a/pw)
15. Channel slope, s
16. Manning's roughness coefficient, n
17.  $V = \frac{1.49r^{(2/3)}s^{(1/2)}}{n}$
18. Flow length, L
19.  $Tt = \frac{L}{3600V}$

sq ft			
ft			
ft			
ft/ft			
ft/s			
ft			
hr			=
			0.00

20. Watershed or subarea Tc or Tt (add Tt in steps 6, 11, and 19)

= 0.20 hr  
11.7 min



**Routing Diagram for Existing**  
 Prepared by Maser Consulting PA, Printed 11/2/2020  
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**Existing**

Prepared by Maser Consulting PA

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**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
2.310	74	>75% Grass cover, Good, HSG C (1S, 4S)
0.060	98	Paved parking, HSG C (2S)
2.440	70	Woods, Good, HSG C (1S, 4S)
0.680	72	Woods/grass comb., Good, HSG C (7S)
<b>5.490</b>	<b>72</b>	<b>TOTAL AREA</b>

**Existing**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
5.490	HSG C	1S, 2S, 4S, 7S
0.000	HSG D	
0.000	Other	
<b>5.490</b>		<b>TOTAL AREA</b>

**Existing**

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	2.310	0.000	0.000	2.310	>75% Grass cover, Good	1S, 4S
0.000	0.000	0.060	0.000	0.000	0.060	Paved parking	2S
0.000	0.000	2.440	0.000	0.000	2.440	Woods, Good	1S, 4S
0.000	0.000	0.680	0.000	0.000	0.680	Woods/grass comb., Good	7S
<b>0.000</b>	<b>0.000</b>	<b>5.490</b>	<b>0.000</b>	<b>0.000</b>	<b>5.490</b>	<b>TOTAL AREA</b>	

**Existing**

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HydroCAD® 10.00-25 s/n 09800 © 2019 HydroCAD Software Solutions LLC

NOAA 24-hr C 2-Year Rainfall=3.34"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment1S: EDA-1-Pervious** Runoff Area=4.380 ac 0.00% Impervious Runoff Depth=1.02"  
Flow Length=1,124' Tc=29.1 min CN=72 Runoff=2.92 cfs 0.371 af

**Subcatchment2S: EDA-1-Impervious** Runoff Area=0.060 ac 100.00% Impervious Runoff Depth=3.11"  
Flow Length=1,124' Tc=25.4 min CN=98 Runoff=0.13 cfs 0.016 af

**Subcatchment4S: EDA-2-Pervious** Runoff Area=0.370 ac 0.00% Impervious Runoff Depth=0.96"  
Flow Length=159' Tc=11.7 min CN=71 Runoff=0.35 cfs 0.030 af

**Subcatchment7S: EDA OFF-SITE PERVIOUS** Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=1.02"  
Tc=0.0 min CN=72 Runoff=0.99 cfs 0.058 af

**Link 3L: POA-1** Inflow=3.03 cfs 0.387 af  
Primary=3.03 cfs 0.387 af

**Link 5L: POA-2** Inflow=0.35 cfs 0.030 af  
Primary=0.35 cfs 0.030 af

**Link 6L: TOTAL ON-SITE** Inflow=3.20 cfs 0.417 af  
Primary=3.20 cfs 0.417 af

**Link 8L: TOTAL OFF-SITE** Inflow=0.99 cfs 0.058 af  
Primary=0.99 cfs 0.058 af

**Link 9L: Existing Total** Inflow=3.44 cfs 0.474 af  
Primary=3.44 cfs 0.474 af

**Total Runoff Area = 5.490 ac Runoff Volume = 0.474 af Average Runoff Depth = 1.04"**  
**98.91% Pervious = 5.430 ac 1.09% Impervious = 0.060 ac**

**Existing**

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NOAA 24-hr C 2-Year Rainfall=3.34"

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**Summary for Subcatchment 1S: EDA-1-Pervious**

Runoff = 2.92 cfs @ 12.44 hrs, Volume= 0.371 af, Depth= 1.02"

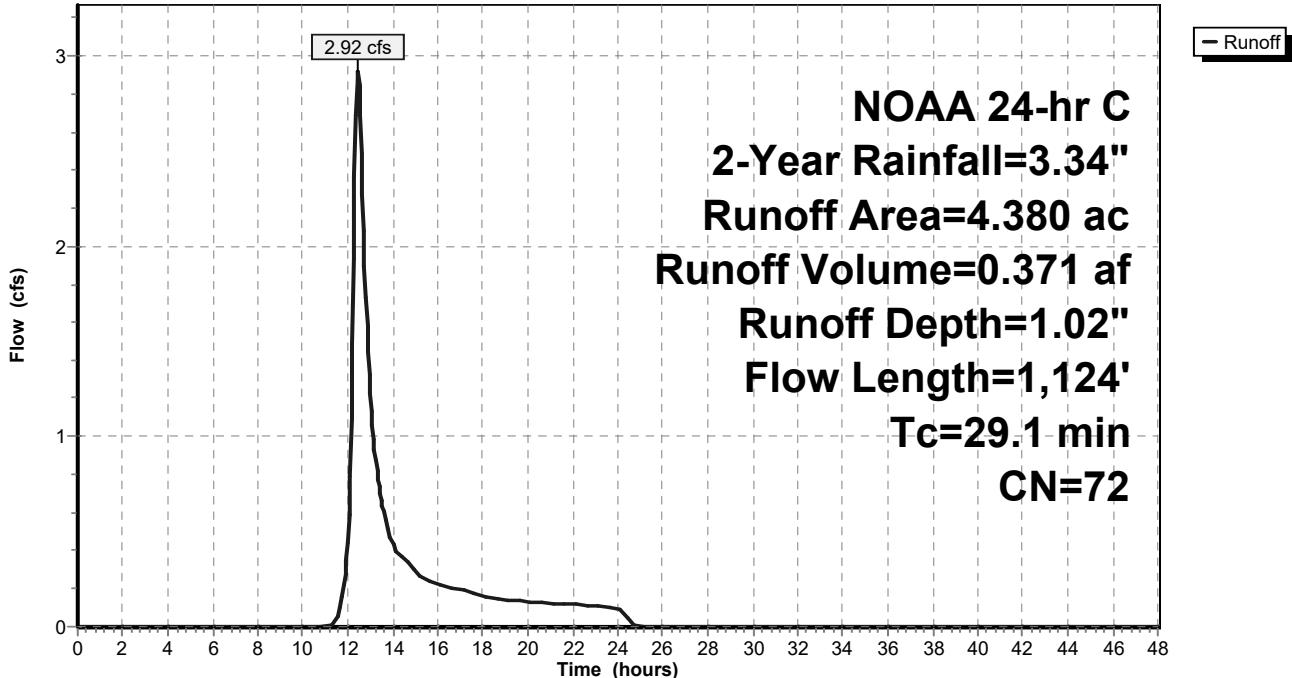
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
2.150	70	Woods, Good, HSG C
2.230	74	>75% Grass cover, Good, HSG C

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.7	100	0.0252	0.13		<b>Sheet Flow, Sheet Flow</b> Grass: Dense n= 0.240 P2= 3.38"
15.2	702	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
29.1	1,124	Total			

**Subcatchment 1S: EDA-1-Pervious**

Hydrograph



**Existing**

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NOAA 24-hr C 2-Year Rainfall=3.34"

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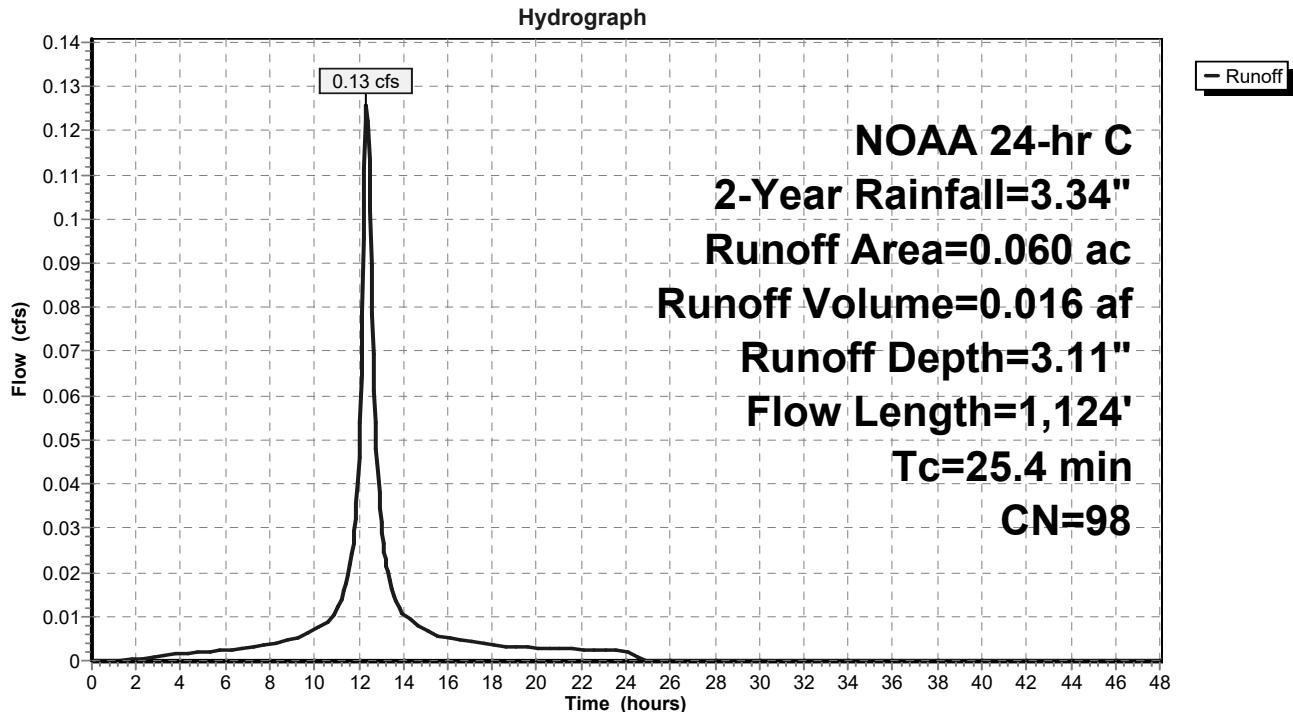
**Summary for Subcatchment 2S: EDA-1-Impervious**

Runoff = 0.13 cfs @ 12.35 hrs, Volume= 0.016 af, Depth= 3.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
0.060	98	Paved parking, HSG C
0.060		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.2	108	0.0252	0.19		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
15.0	694	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
25.4	1,124				Total

**Subcatchment 2S: EDA-1-Impervious**

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NOAA 24-hr C 2-Year Rainfall=3.34"

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**Summary for Subcatchment 4S: EDA-2-Pervious**

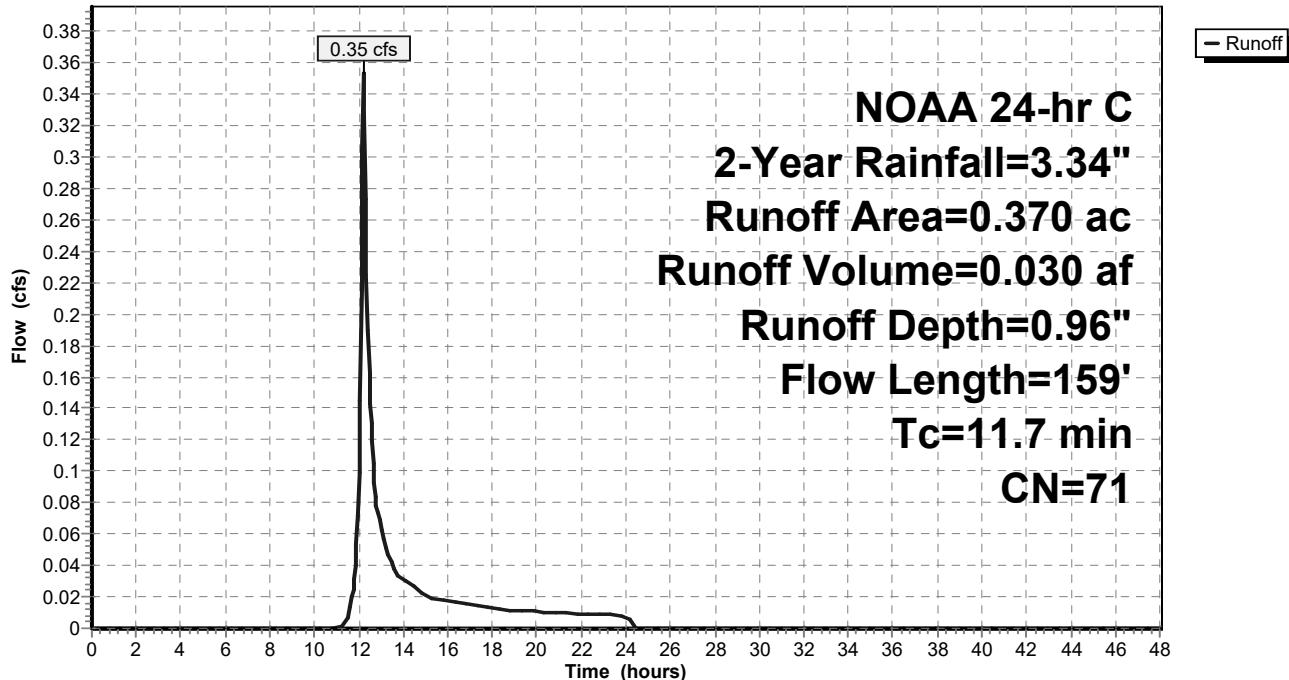
Runoff = 0.35 cfs @ 12.21 hrs, Volume= 0.030 af, Depth= 0.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description			
0.290	70	Woods, Good, HSG C			
0.080	74	>75% Grass cover, Good, HSG C			
0.370	71	Weighted Average			
0.370		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	42	0.0040	0.08		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
0.4	20	0.0040	0.95		<b>Shallow Concentrated Flow, Grass Waterway</b> Grassed Waterway Kv= 15.0 fps
2.2	97	0.0210	0.72		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
11.7	159	Total			

**Subcatchment 4S: EDA-2-Pervious**

Hydrograph



**Existing**

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NOAA 24-hr C 2-Year Rainfall=3.34"

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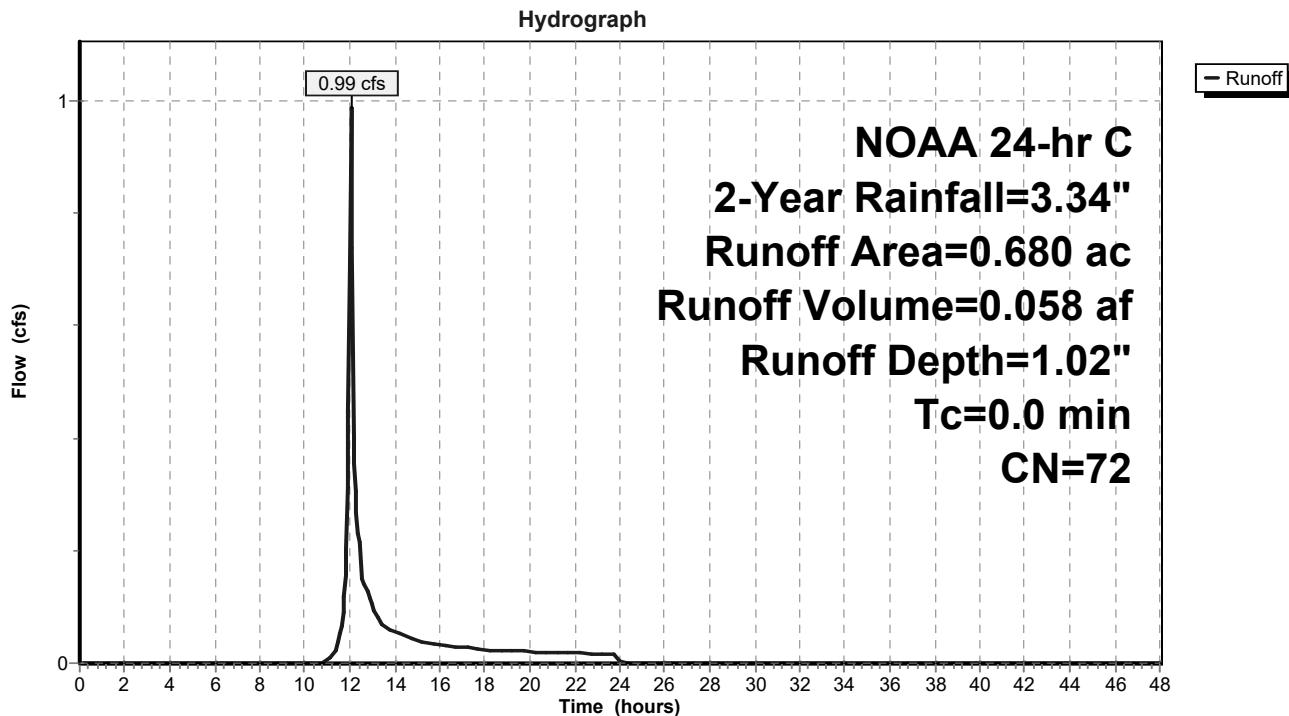
**Summary for Subcatchment 7S: EDA OFF-SITE PERVIOUS**[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 0.99 cfs @ 12.05 hrs, Volume= 0.058 af, Depth= 1.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0				Direct Entry, 10	

**Subcatchment 7S: EDA OFF-SITE PERVIOUS**

**Summary for Link 3L: POA-1**

Inflow Area = 4.440 ac, 1.35% Impervious, Inflow Depth = 1.05" for 2-Year event

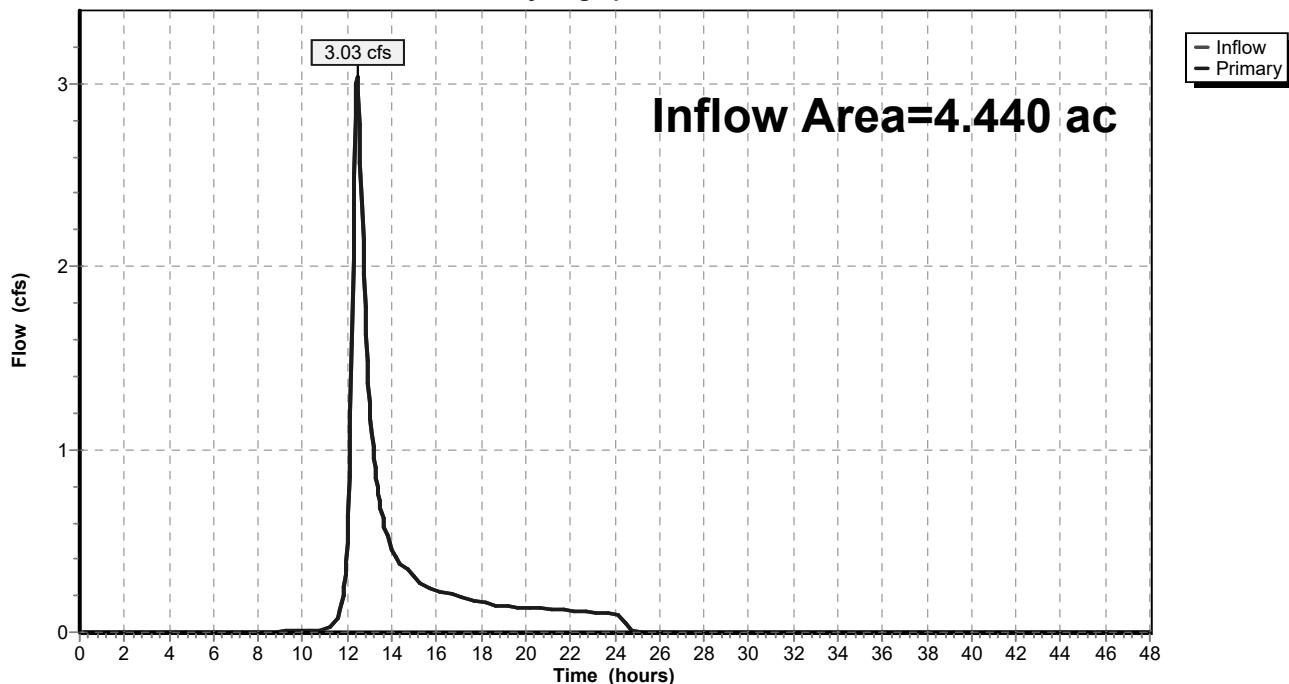
Inflow = 3.03 cfs @ 12.44 hrs, Volume= 0.387 af

Primary = 3.03 cfs @ 12.44 hrs, Volume= 0.387 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 3L: POA-1**

Hydrograph



**Summary for Link 5L: POA-2**

Inflow Area = 0.370 ac, 0.00% Impervious, Inflow Depth = 0.96" for 2-Year event

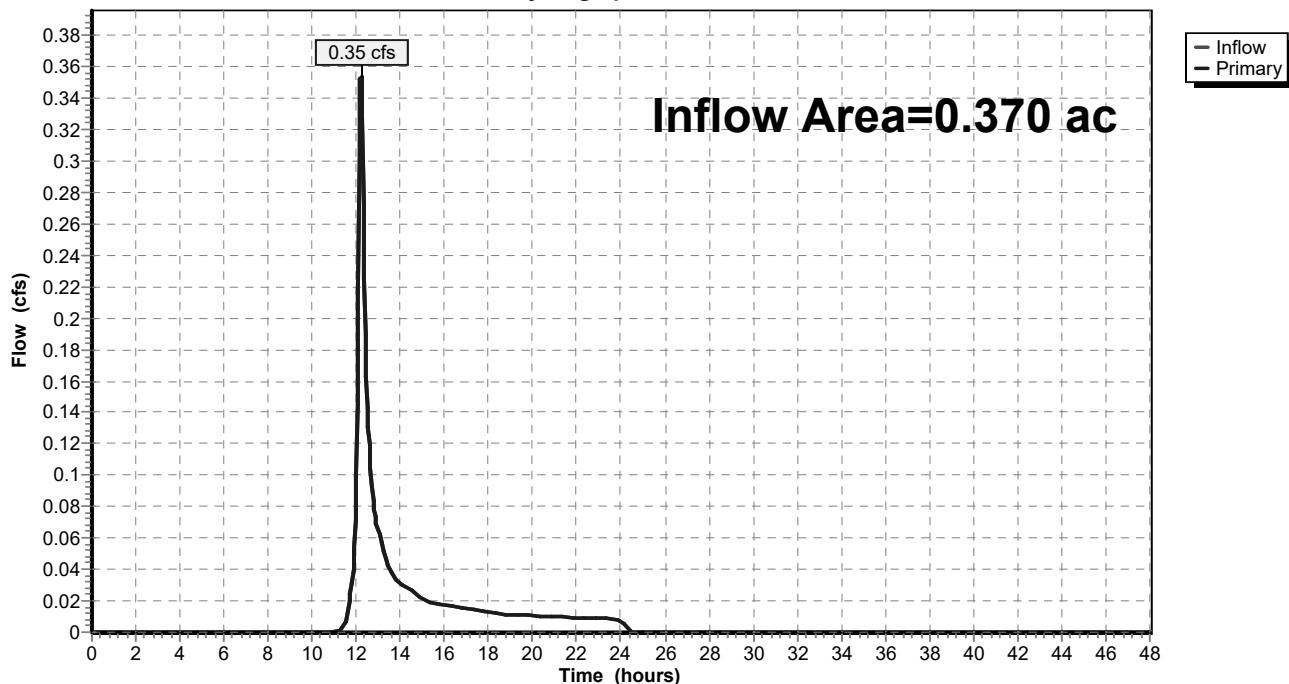
Inflow = 0.35 cfs @ 12.21 hrs, Volume= 0.030 af

Primary = 0.35 cfs @ 12.21 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 5L: POA-2**

Hydrograph



**Summary for Link 6L: TOTAL ON-SITE**

Inflow Area = 4.810 ac, 1.25% Impervious, Inflow Depth = 1.04" for 2-Year event

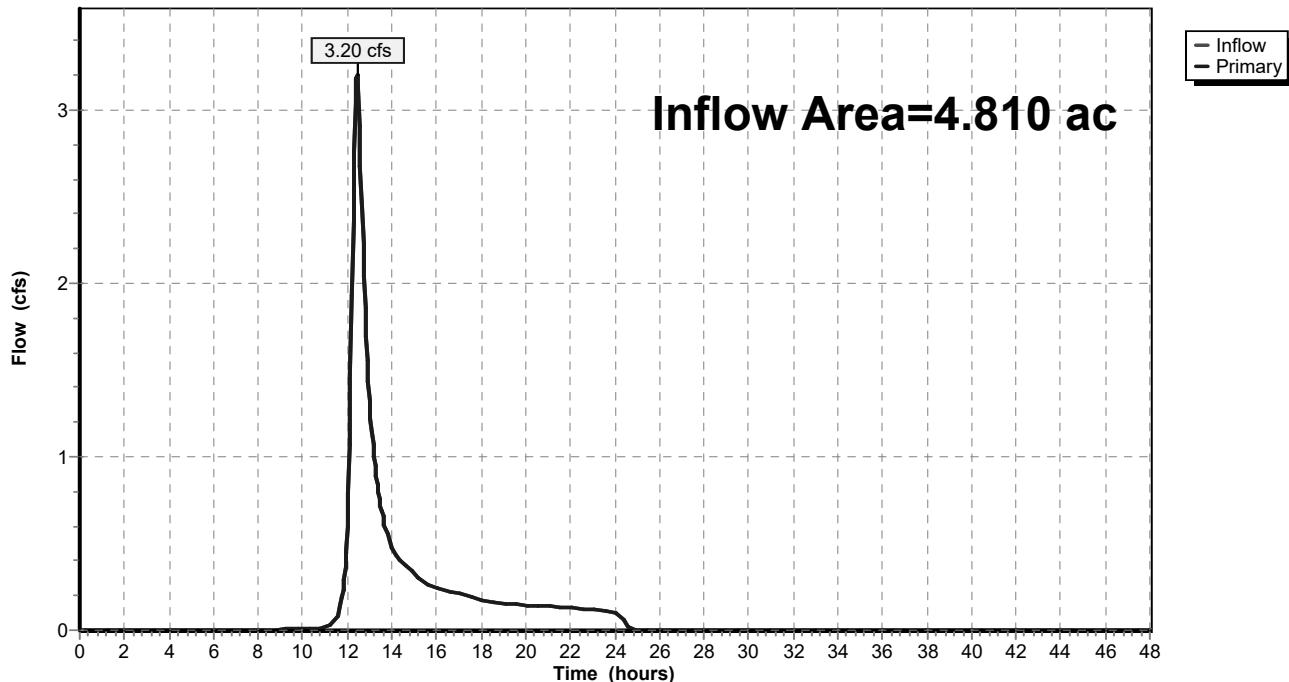
Inflow = 3.20 cfs @ 12.43 hrs, Volume= 0.417 af

Primary = 3.20 cfs @ 12.43 hrs, Volume= 0.417 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 6L: TOTAL ON-SITE**

Hydrograph



**Summary for Link 8L: TOTAL OFF-SITE**

Inflow Area = 0.680 ac, 0.00% Impervious, Inflow Depth = 1.02" for 2-Year event

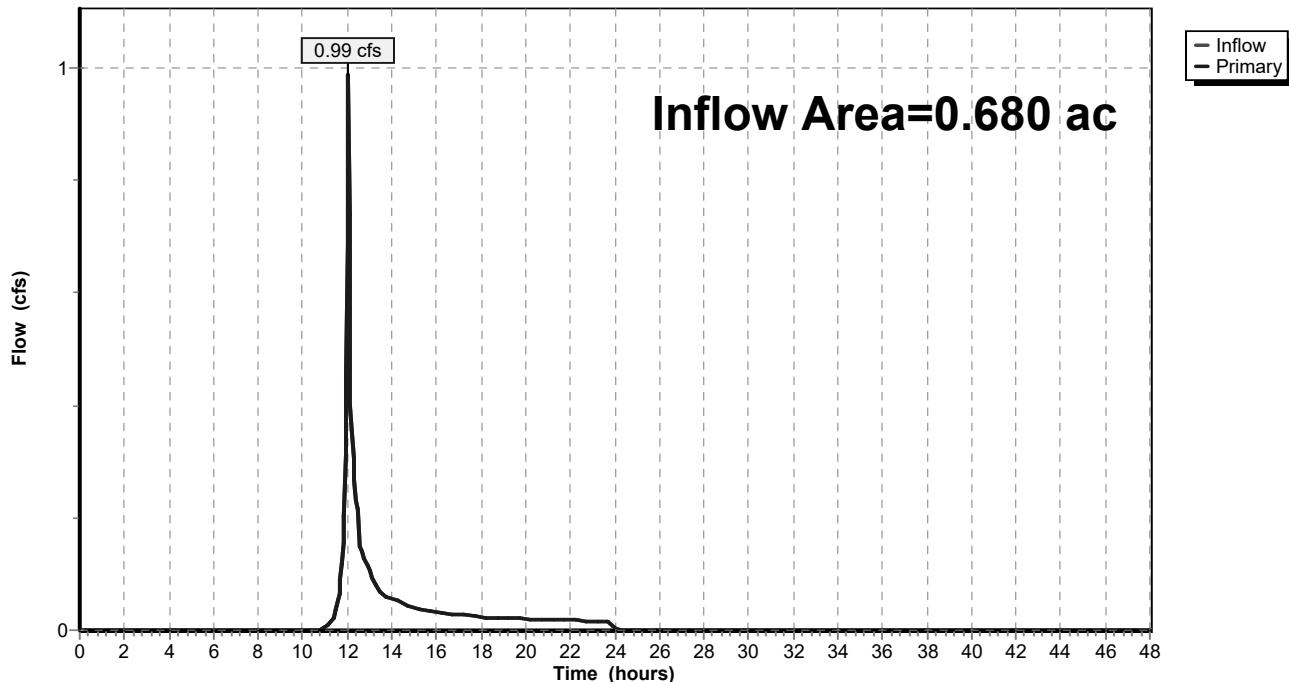
Inflow = 0.99 cfs @ 12.05 hrs, Volume= 0.058 af

Primary = 0.99 cfs @ 12.05 hrs, Volume= 0.058 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 8L: TOTAL OFF-SITE**

Hydrograph



**Summary for Link 9L: Existing Total**

Inflow Area = 5.490 ac, 1.09% Impervious, Inflow Depth = 1.04" for 2-Year event

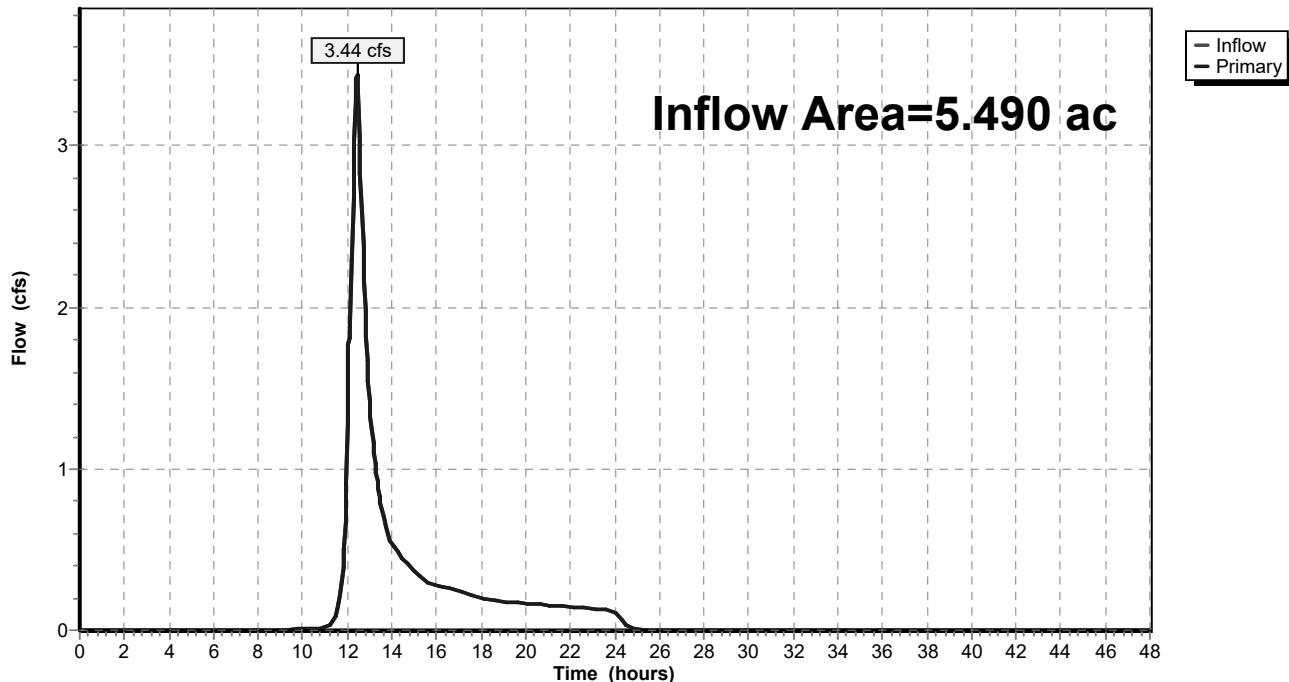
Inflow = 3.44 cfs @ 12.43 hrs, Volume= 0.474 af

Primary = 3.44 cfs @ 12.43 hrs, Volume= 0.474 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 9L: Existing Total**

Hydrograph



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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment1S: EDA-1-Pervious**Runoff Area=4.380 ac 0.00% Impervious Runoff Depth=2.21"  
Flow Length=1,124' Tc=29.1 min CN=72 Runoff=6.71 cfs 0.805 af**Subcatchment2S: EDA-1-Impervious**Runoff Area=0.060 ac 100.00% Impervious Runoff Depth=4.77"  
Flow Length=1,124' Tc=25.4 min CN=98 Runoff=0.19 cfs 0.024 af**Subcatchment4S: EDA-2-Pervious**Runoff Area=0.370 ac 0.00% Impervious Runoff Depth=2.12"  
Flow Length=159' Tc=11.7 min CN=71 Runoff=0.82 cfs 0.065 af**Subcatchment7S: EDA OFF-SITE PERVIOUS**Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=2.21"  
Tc=0.0 min CN=72 Runoff=2.20 cfs 0.125 af**Link 3L: POA-1**Inflow=6.89 cfs 0.829 af  
Primary=6.89 cfs 0.829 af**Link 5L: POA-2**Inflow=0.82 cfs 0.065 af  
Primary=0.82 cfs 0.065 af**Link 6L: TOTAL ON-SITE**Inflow=7.27 cfs 0.894 af  
Primary=7.27 cfs 0.894 af**Link 8L: TOTAL OFF-SITE**Inflow=2.20 cfs 0.125 af  
Primary=2.20 cfs 0.125 af**Link 9L: Existing Total**Inflow=7.73 cfs 1.019 af  
Primary=7.73 cfs 1.019 af**Total Runoff Area = 5.490 ac Runoff Volume = 1.019 af Average Runoff Depth = 2.23"**  
**98.91% Pervious = 5.430 ac 1.09% Impervious = 0.060 ac**

**Existing**

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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Subcatchment 1S: EDA-1-Pervious**

Runoff = 6.71 cfs @ 12.42 hrs, Volume= 0.805 af, Depth= 2.21"

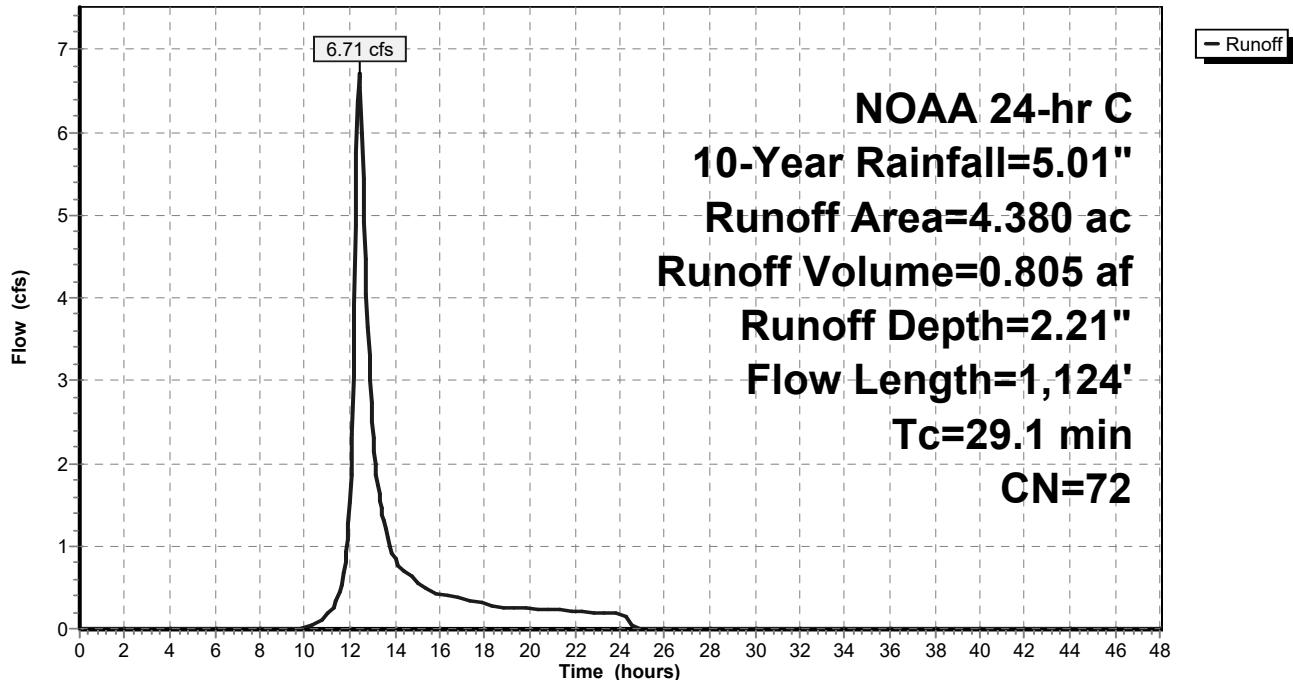
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
2.150	70	Woods, Good, HSG C
2.230	74	>75% Grass cover, Good, HSG C

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.7	100	0.0252	0.13		<b>Sheet Flow, Sheet Flow</b> Grass: Dense n= 0.240 P2= 3.38"
15.2	702	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
29.1	1,124	Total			

**Subcatchment 1S: EDA-1-Pervious**

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.01"

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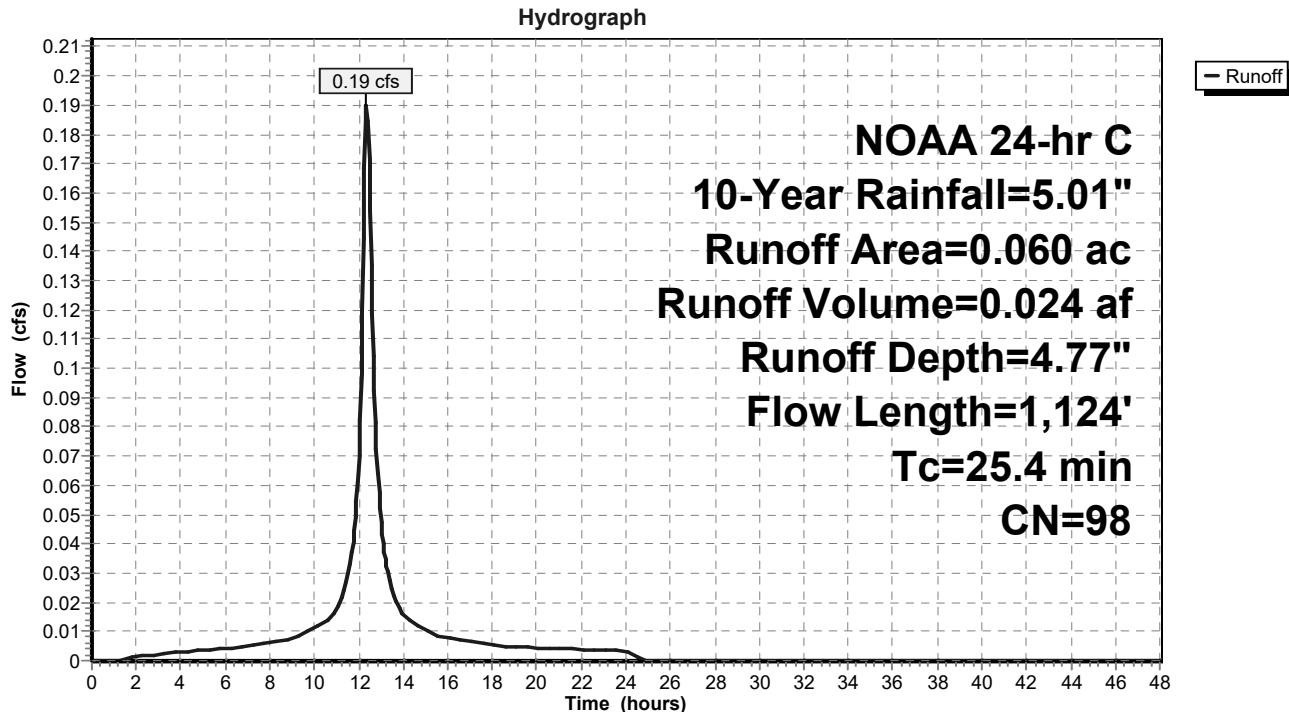
**Summary for Subcatchment 2S: EDA-1-Impervious**

Runoff = 0.19 cfs @ 12.35 hrs, Volume= 0.024 af, Depth= 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
0.060	98	Paved parking, HSG C
0.060		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.2	108	0.0252	0.19		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
15.0	694	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
25.4	1,124				Total

**Subcatchment 2S: EDA-1-Impervious**

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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Subcatchment 4S: EDA-2-Pervious**

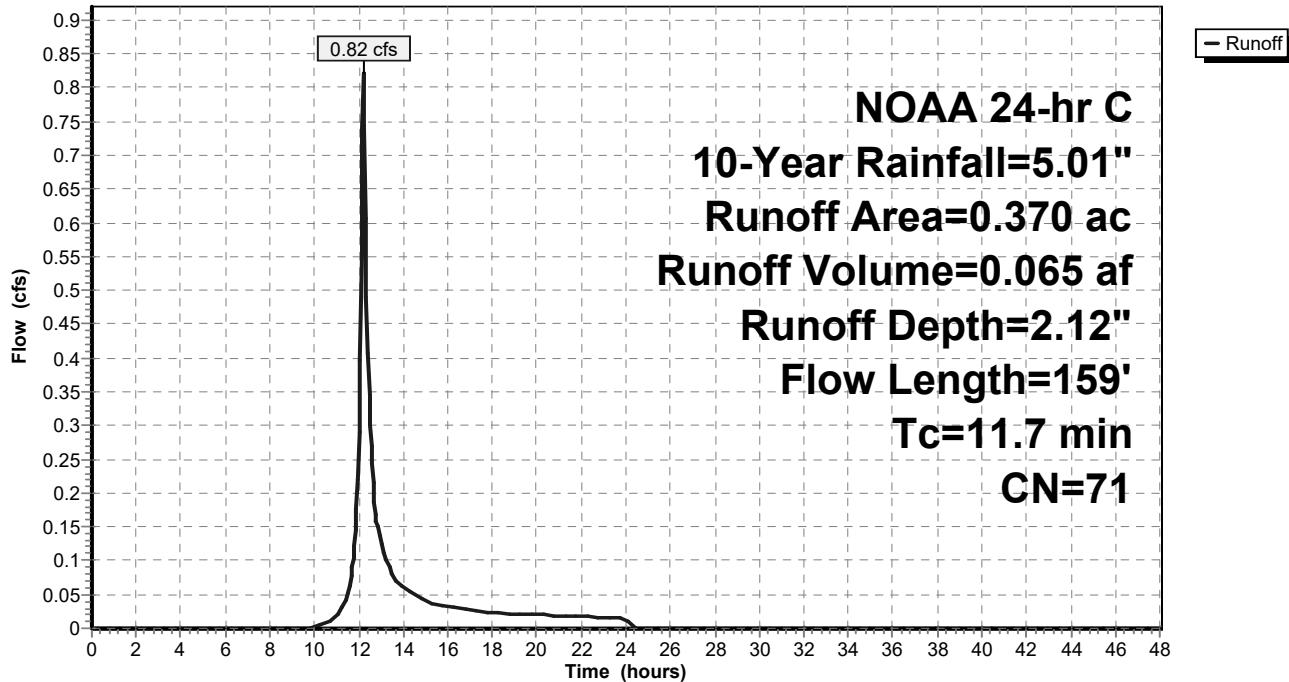
Runoff = 0.82 cfs @ 12.20 hrs, Volume= 0.065 af, Depth= 2.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description			
0.290	70	Woods, Good, HSG C			
0.080	74	>75% Grass cover, Good, HSG C			
0.370	71	Weighted Average			
0.370		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	42	0.0040	0.08		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
0.4	20	0.0040	0.95		<b>Shallow Concentrated Flow, Grass Waterway</b> Grassed Waterway Kv= 15.0 fps
2.2	97	0.0210	0.72		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
11.7	159	Total			

**Subcatchment 4S: EDA-2-Pervious**

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Subcatchment 7S: EDA OFF-SITE PERVIOUS**[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 2.20 cfs @ 12.05 hrs, Volume= 0.125 af, Depth= 2.21"

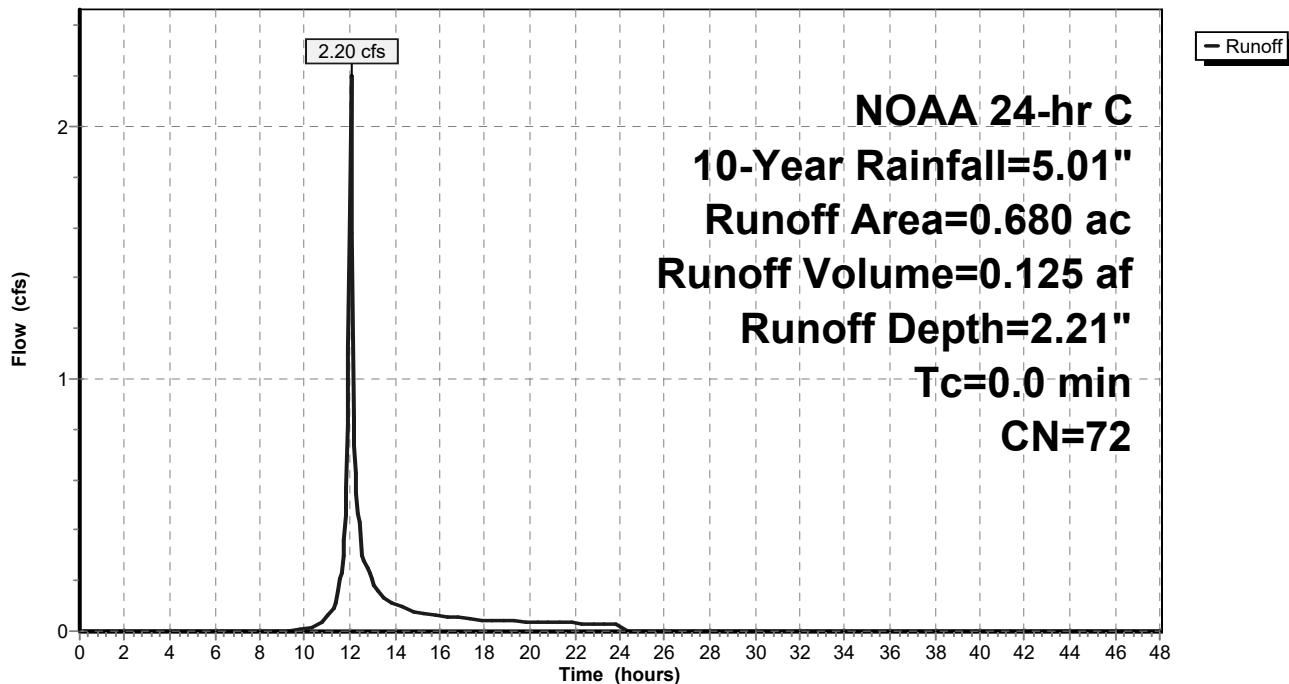
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0	Direct Entry, 10				

**Subcatchment 7S: EDA OFF-SITE PERVIOUS**

Hydrograph



**Summary for Link 3L: POA-1**

Inflow Area = 4.440 ac, 1.35% Impervious, Inflow Depth = 2.24" for 10-Year event

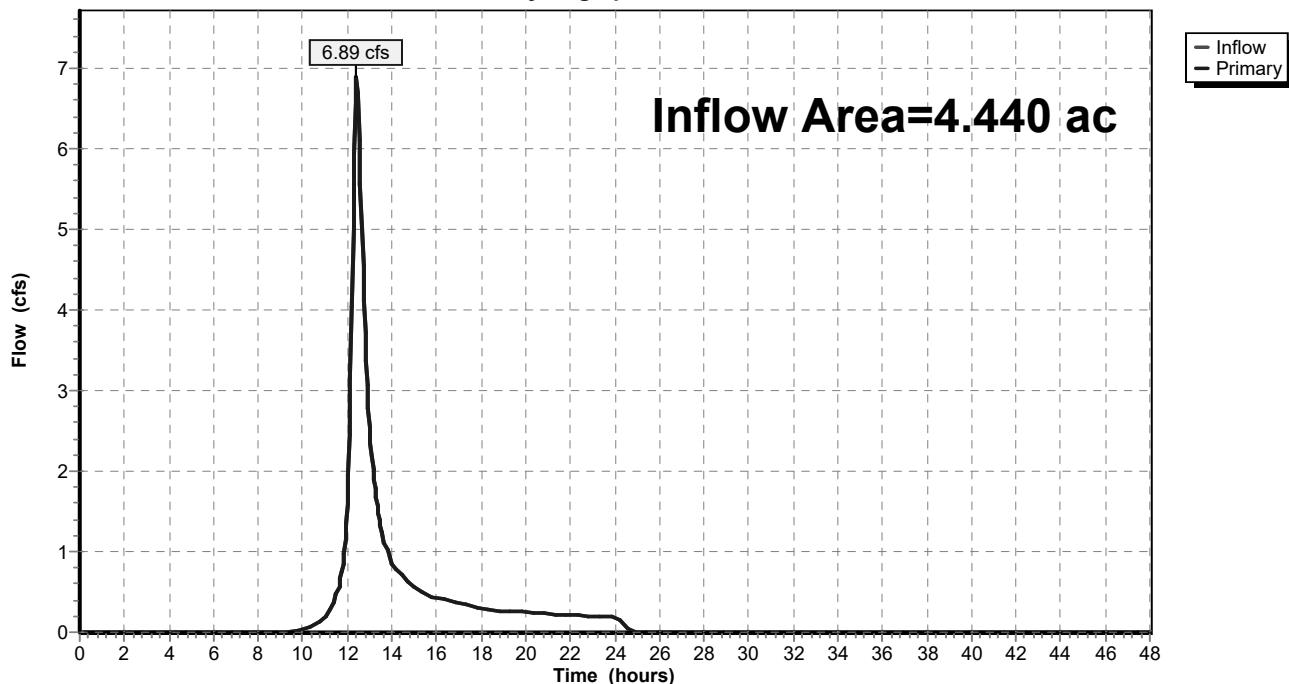
Inflow = 6.89 cfs @ 12.42 hrs, Volume= 0.829 af

Primary = 6.89 cfs @ 12.42 hrs, Volume= 0.829 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 3L: POA-1**

Hydrograph



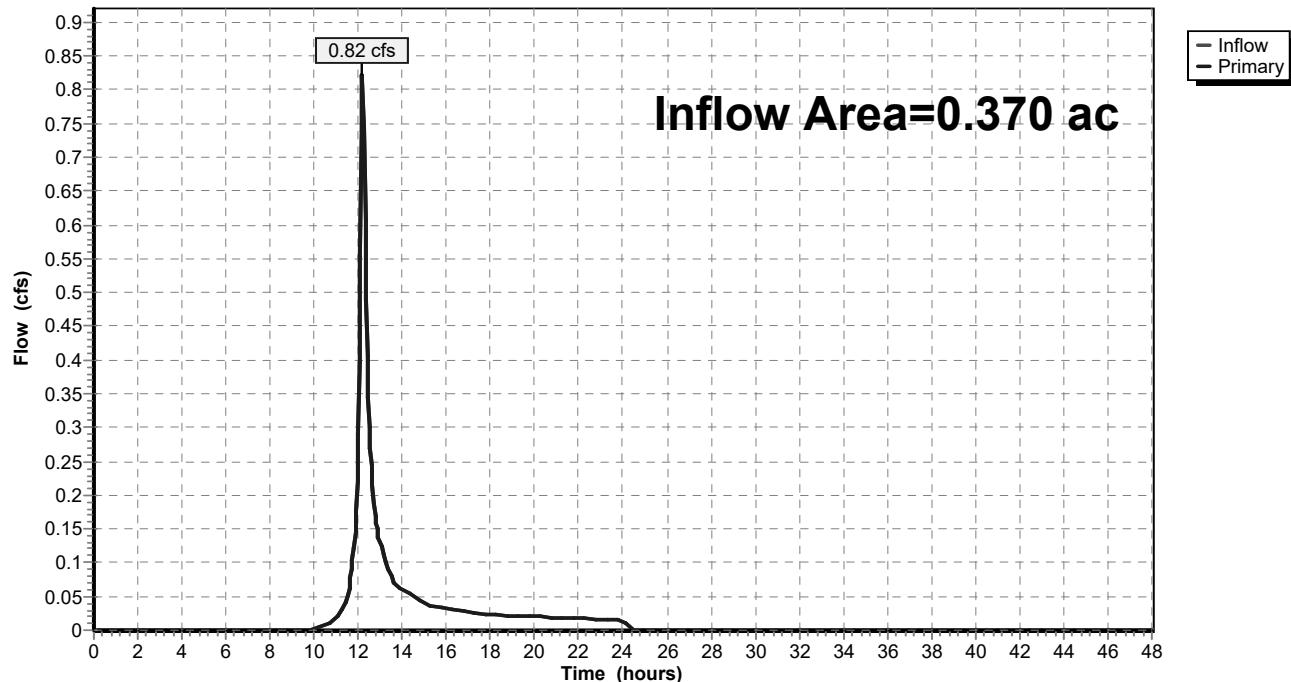
**Summary for Link 5L: POA-2**

Inflow Area = 0.370 ac, 0.00% Impervious, Inflow Depth = 2.12" for 10-Year event

Inflow = 0.82 cfs @ 12.20 hrs, Volume= 0.065 af

Primary = 0.82 cfs @ 12.20 hrs, Volume= 0.065 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 5L: POA-2****Hydrograph**

**Summary for Link 6L: TOTAL ON-SITE**

Inflow Area = 4.810 ac, 1.25% Impervious, Inflow Depth = 2.23" for 10-Year event

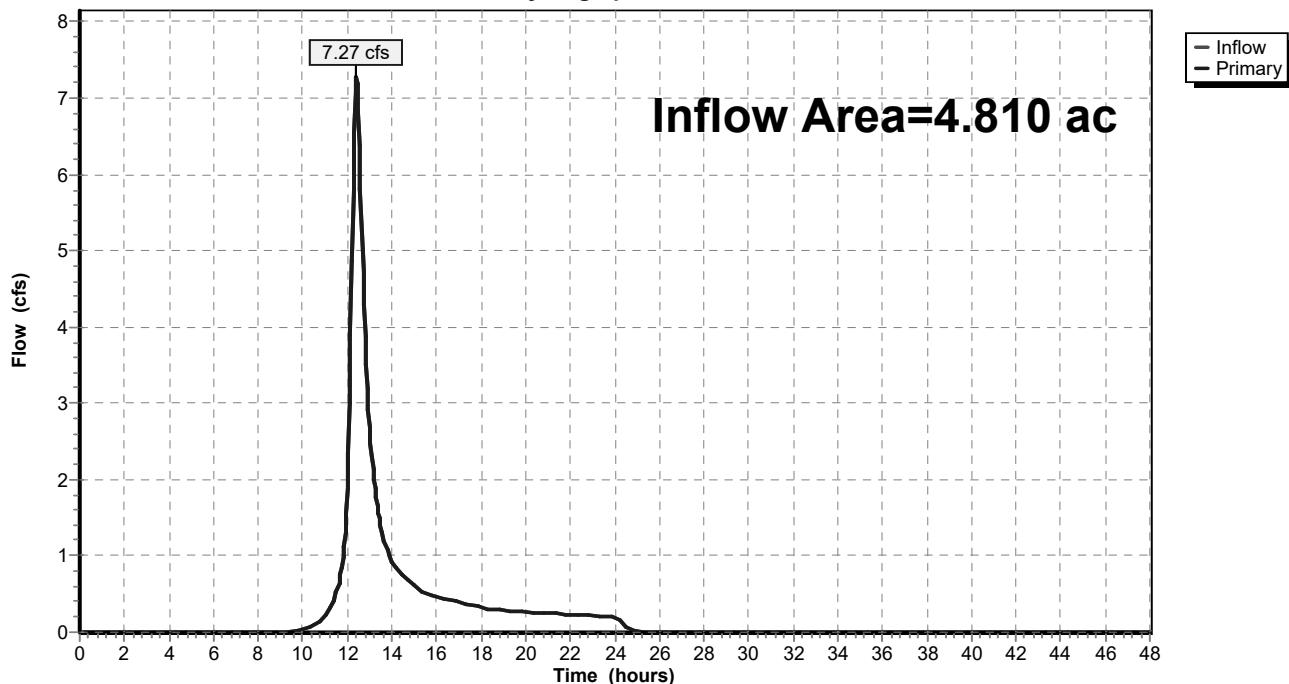
Inflow = 7.27 cfs @ 12.41 hrs, Volume= 0.894 af

Primary = 7.27 cfs @ 12.41 hrs, Volume= 0.894 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 6L: TOTAL ON-SITE**

Hydrograph



**Summary for Link 8L: TOTAL OFF-SITE**

Inflow Area = 0.680 ac, 0.00% Impervious, Inflow Depth = 2.21" for 10-Year event

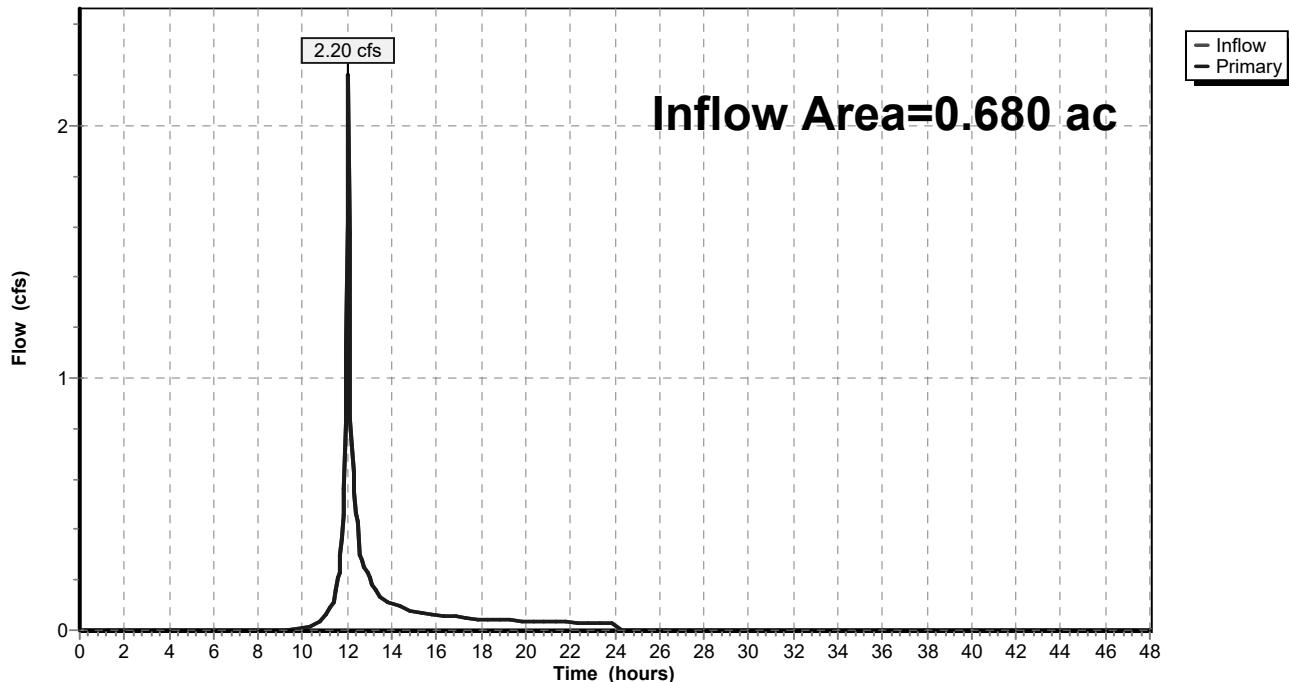
Inflow = 2.20 cfs @ 12.05 hrs, Volume= 0.125 af

Primary = 2.20 cfs @ 12.05 hrs, Volume= 0.125 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 8L: TOTAL OFF-SITE**

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Link 9L: Existing Total**

Inflow Area = 5.490 ac, 1.09% Impervious, Inflow Depth = 2.23" for 10-Year event

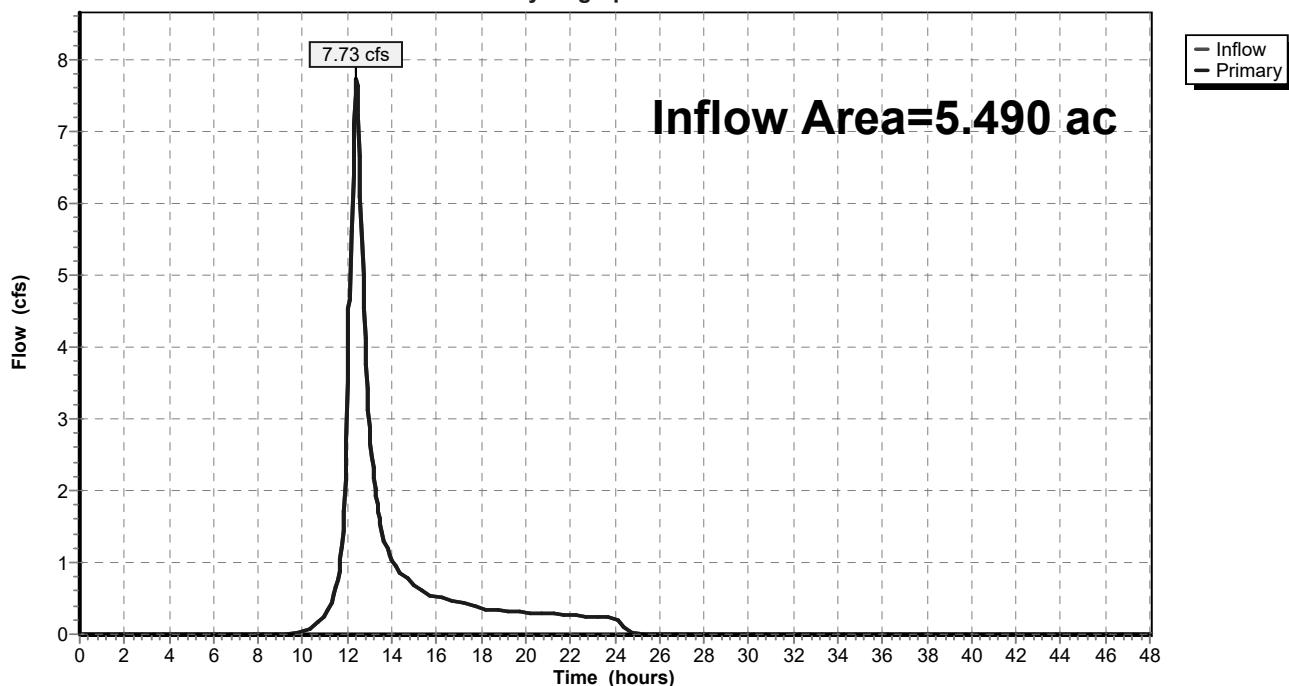
Inflow = 7.73 cfs @ 12.41 hrs, Volume= 1.019 af

Primary = 7.73 cfs @ 12.41 hrs, Volume= 1.019 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 9L: Existing Total**

Hydrograph



**Existing**

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*NOAA 24-hr C 25-Year Rainfall=6.19"*

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment1S: EDA-1-Pervious**Runoff Area=4.380 ac 0.00% Impervious Runoff Depth=3.15"  
Flow Length=1,124' Tc=29.1 min CN=72 Runoff=9.67 cfs 1.150 af**Subcatchment2S: EDA-1-Impervious**Runoff Area=0.060 ac 100.00% Impervious Runoff Depth=5.95"  
Flow Length=1,124' Tc=25.4 min CN=98 Runoff=0.24 cfs 0.030 af**Subcatchment4S: EDA-2-Pervious**Runoff Area=0.370 ac 0.00% Impervious Runoff Depth=3.05"  
Flow Length=159' Tc=11.7 min CN=71 Runoff=1.19 cfs 0.094 af**Subcatchment7S: EDA OFF-SITE PERVIOUS**Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=3.15"  
Tc=0.0 min CN=72 Runoff=3.14 cfs 0.178 af**Link 3L: POA-1**Inflow=9.90 cfs 1.179 af  
Primary=9.90 cfs 1.179 af**Link 5L: POA-2**Inflow=1.19 cfs 0.094 af  
Primary=1.19 cfs 0.094 af**Link 6L: TOTAL ON-SITE**Inflow=10.45 cfs 1.273 af  
Primary=10.45 cfs 1.273 af**Link 8L: TOTAL OFF-SITE**Inflow=3.14 cfs 0.178 af  
Primary=3.14 cfs 0.178 af**Link 9L: Existing Total**Inflow=11.09 cfs 1.452 af  
Primary=11.09 cfs 1.452 af**Total Runoff Area = 5.490 ac Runoff Volume = 1.452 af Average Runoff Depth = 3.17"**  
**98.91% Pervious = 5.430 ac 1.09% Impervious = 0.060 ac**

**Existing**

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NOAA 24-hr C 25-Year Rainfall=6.19"

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**Summary for Subcatchment 1S: EDA-1-Pervious**

Runoff = 9.67 cfs @ 12.42 hrs, Volume= 1.150 af, Depth= 3.15"

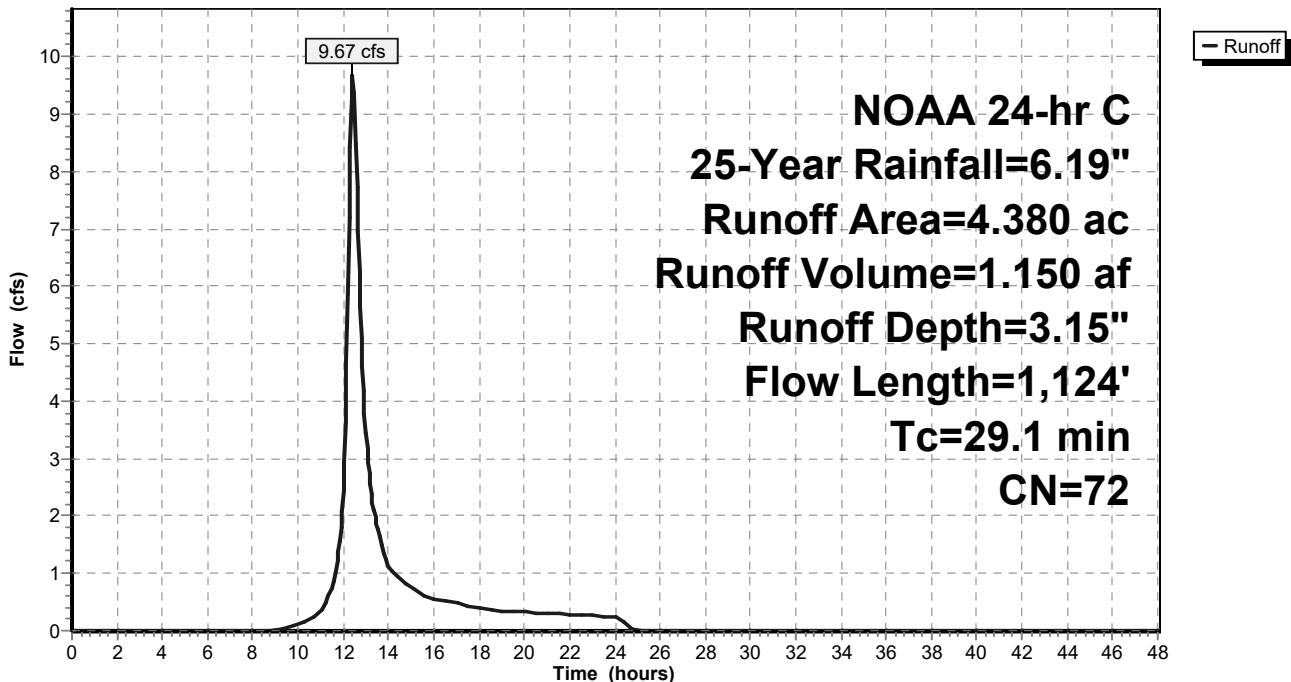
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
2.150	70	Woods, Good, HSG C
2.230	74	>75% Grass cover, Good, HSG C

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.7	100	0.0252	0.13		<b>Sheet Flow, Sheet Flow</b> Grass: Dense n= 0.240 P2= 3.38"
15.2	702	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
29.1	1,124	Total			

**Subcatchment 1S: EDA-1-Pervious**

Hydrograph



**Existing**

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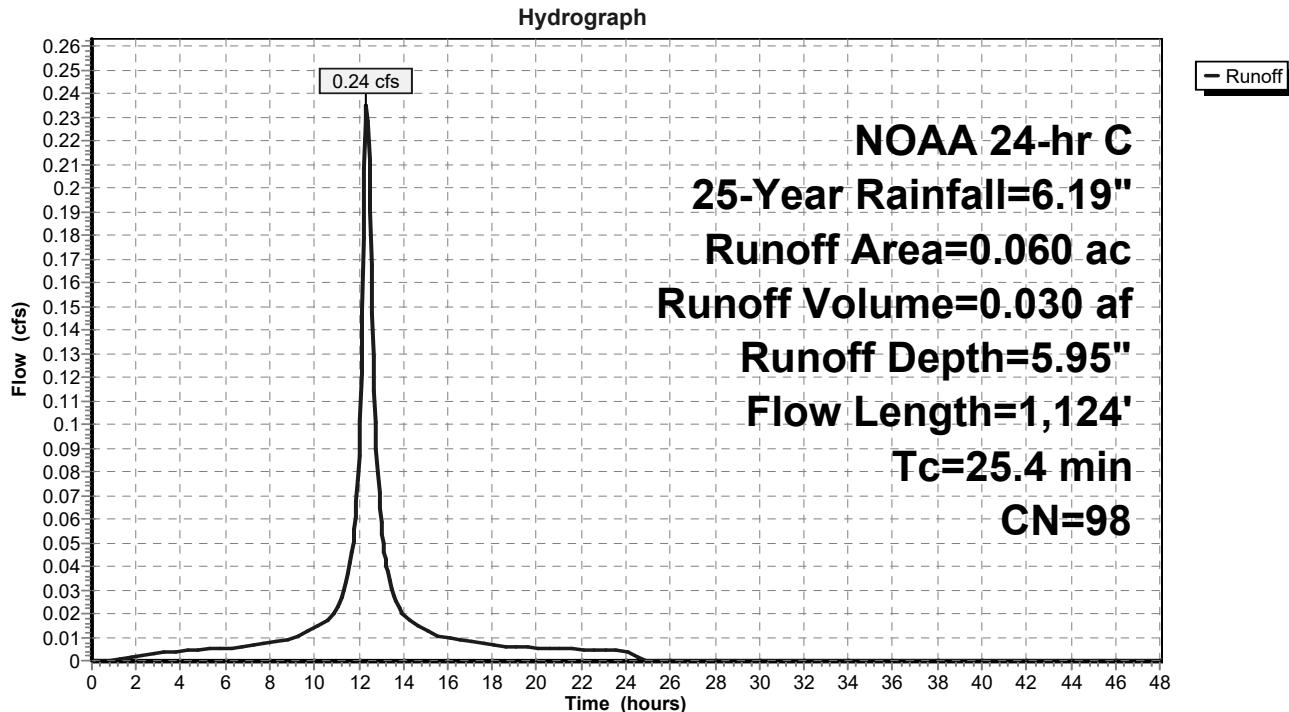
**Summary for Subcatchment 2S: EDA-1-Impervious**

Runoff = 0.24 cfs @ 12.35 hrs, Volume= 0.030 af, Depth= 5.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
0.060	98	Paved parking, HSG C
0.060		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.2	108	0.0252	0.19		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
15.0	694	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
25.4	1,124				Total

**Subcatchment 2S: EDA-1-Impervious**

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**Summary for Subcatchment 4S: EDA-2-Pervious**

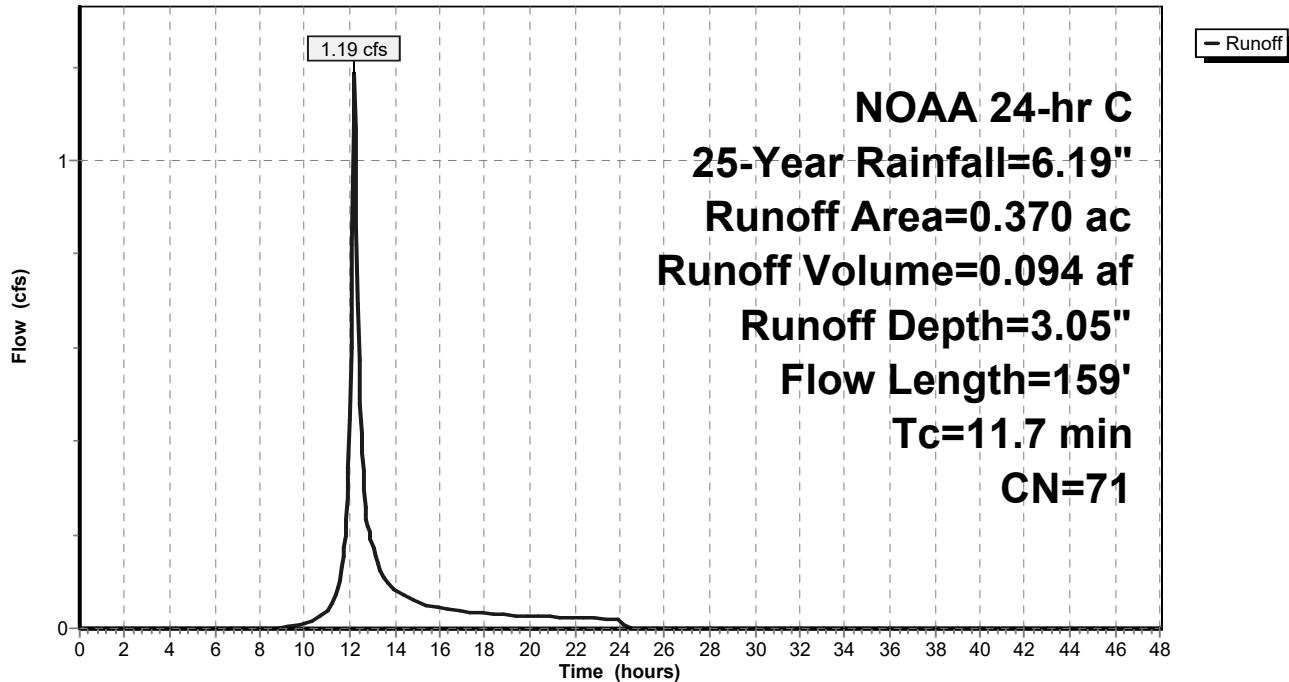
Runoff = 1.19 cfs @ 12.20 hrs, Volume= 0.094 af, Depth= 3.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description			
0.290	70	Woods, Good, HSG C			
0.080	74	>75% Grass cover, Good, HSG C			
0.370	71	Weighted Average			
0.370		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	42	0.0040	0.08		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
0.4	20	0.0040	0.95		<b>Shallow Concentrated Flow, Grass Waterway</b> Grassed Waterway Kv= 15.0 fps
2.2	97	0.0210	0.72		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
11.7	159	Total			

**Subcatchment 4S: EDA-2-Pervious**

Hydrograph



**Summary for Subcatchment 7S: EDA OFF-SITE PERVIOUS**

[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 3.14 cfs @ 12.05 hrs, Volume= 0.178 af, Depth= 3.15"

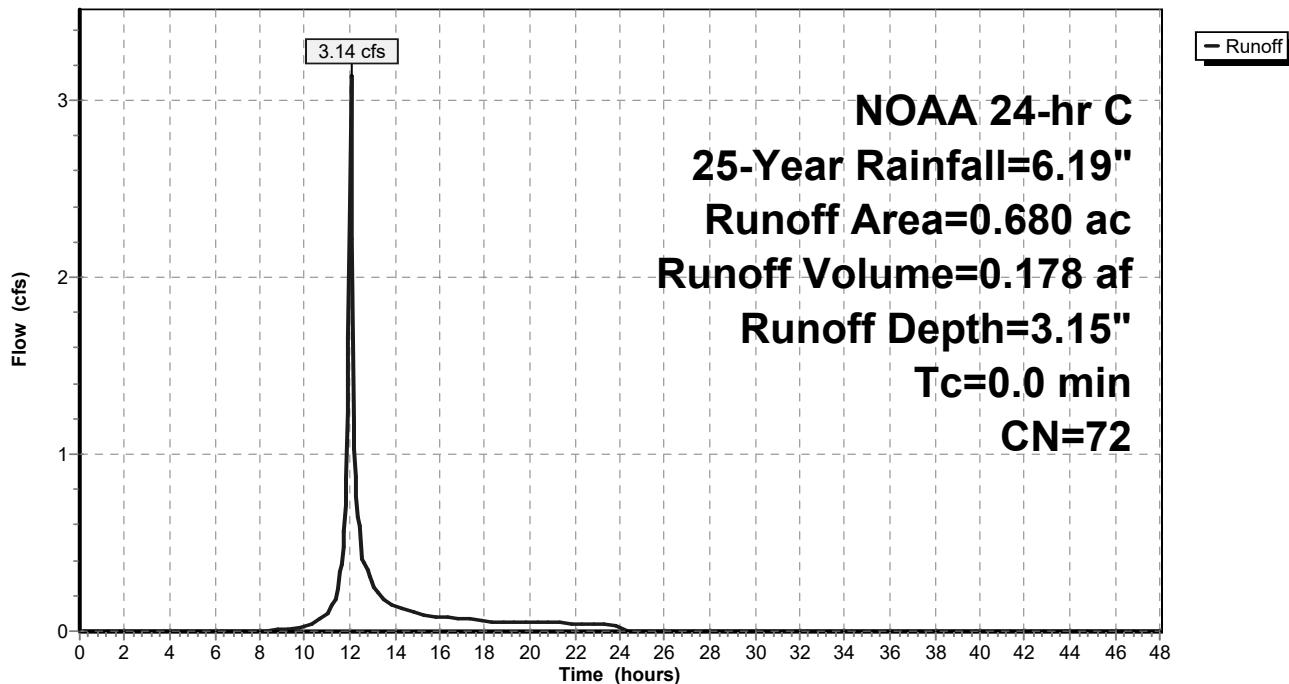
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0				Direct Entry, 10	

**Subcatchment 7S: EDA OFF-SITE PERVIOUS**

Hydrograph



**Summary for Link 3L: POA-1**

Inflow Area = 4.440 ac, 1.35% Impervious, Inflow Depth = 3.19" for 25-Year event

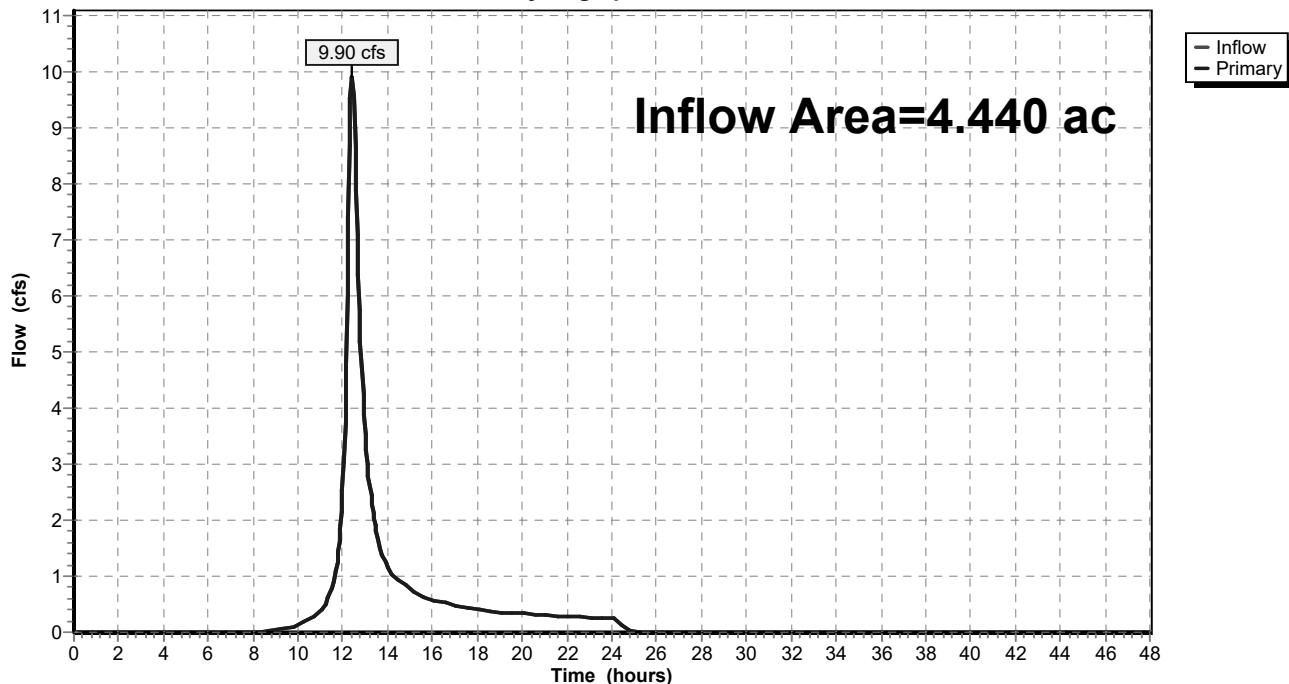
Inflow = 9.90 cfs @ 12.42 hrs, Volume= 1.179 af

Primary = 9.90 cfs @ 12.42 hrs, Volume= 1.179 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 3L: POA-1**

Hydrograph



**Summary for Link 5L: POA-2**

Inflow Area = 0.370 ac, 0.00% Impervious, Inflow Depth = 3.05" for 25-Year event

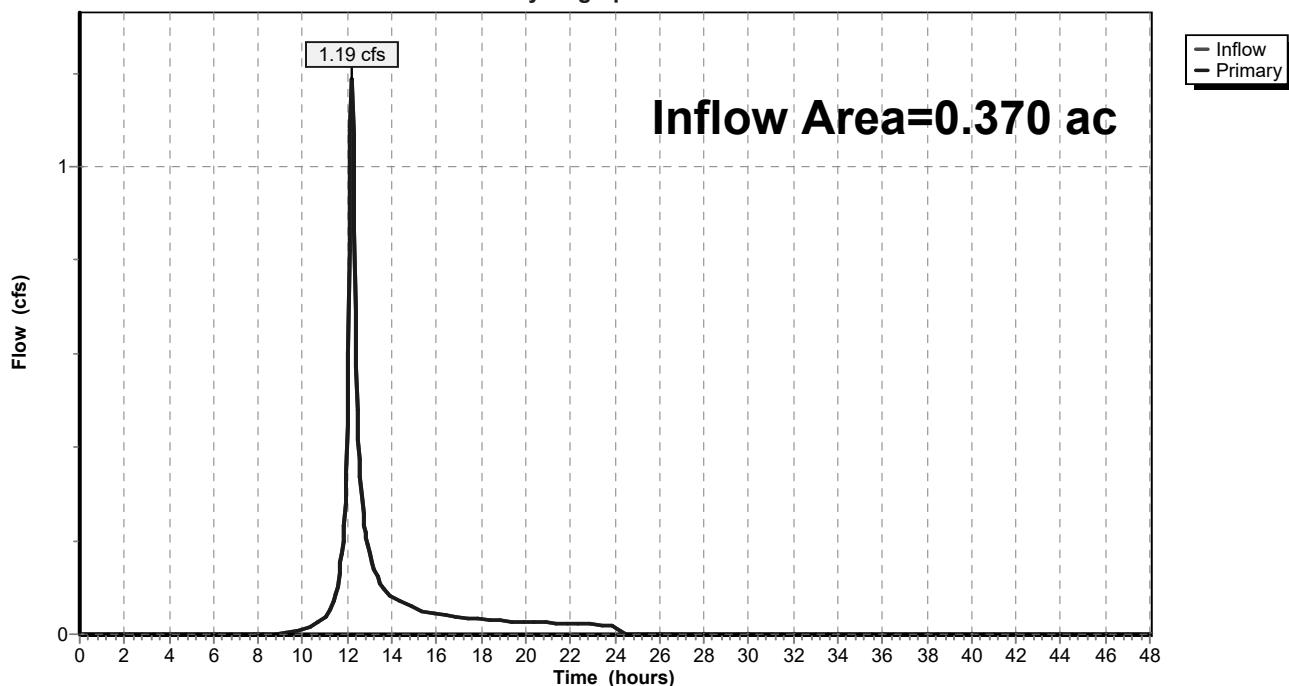
Inflow = 1.19 cfs @ 12.20 hrs, Volume= 0.094 af

Primary = 1.19 cfs @ 12.20 hrs, Volume= 0.094 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 5L: POA-2**

Hydrograph



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**Summary for Link 6L: TOTAL ON-SITE**

Inflow Area = 4.810 ac, 1.25% Impervious, Inflow Depth = 3.18" for 25-Year event

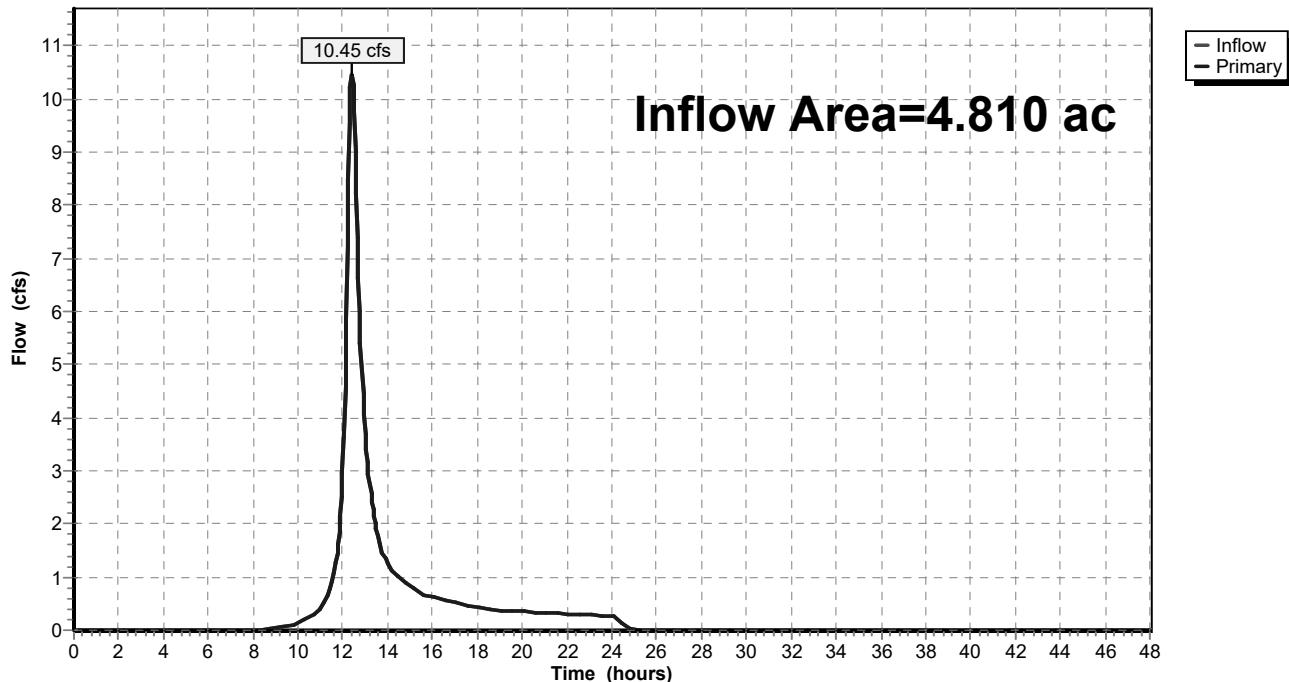
Inflow = 10.45 cfs @ 12.40 hrs, Volume= 1.273 af

Primary = 10.45 cfs @ 12.40 hrs, Volume= 1.273 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 6L: TOTAL ON-SITE**

Hydrograph



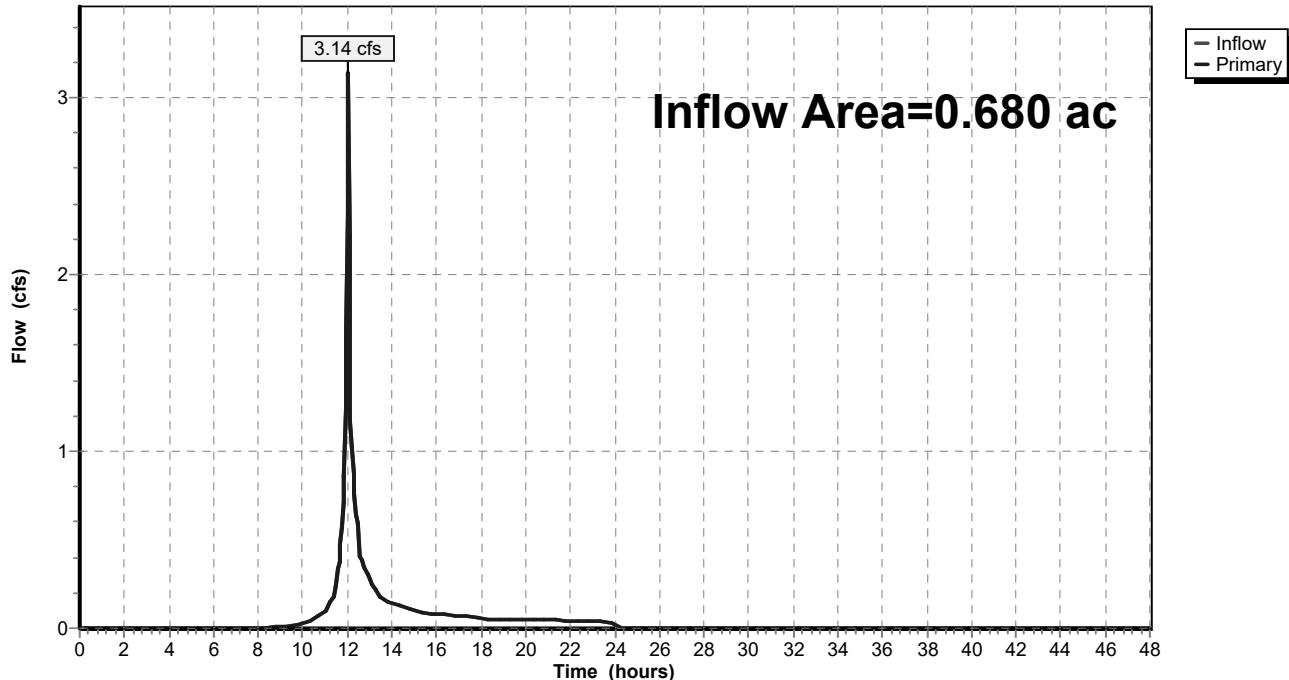
**Summary for Link 8L: TOTAL OFF-SITE**

Inflow Area = 0.680 ac, 0.00% Impervious, Inflow Depth = 3.15" for 25-Year event  
Inflow = 3.14 cfs @ 12.05 hrs, Volume= 0.178 af  
Primary = 3.14 cfs @ 12.05 hrs, Volume= 0.178 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 8L: TOTAL OFF-SITE**

Hydrograph



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**Summary for Link 9L: Existing Total**

Inflow Area = 5.490 ac, 1.09% Impervious, Inflow Depth = 3.17" for 25-Year event

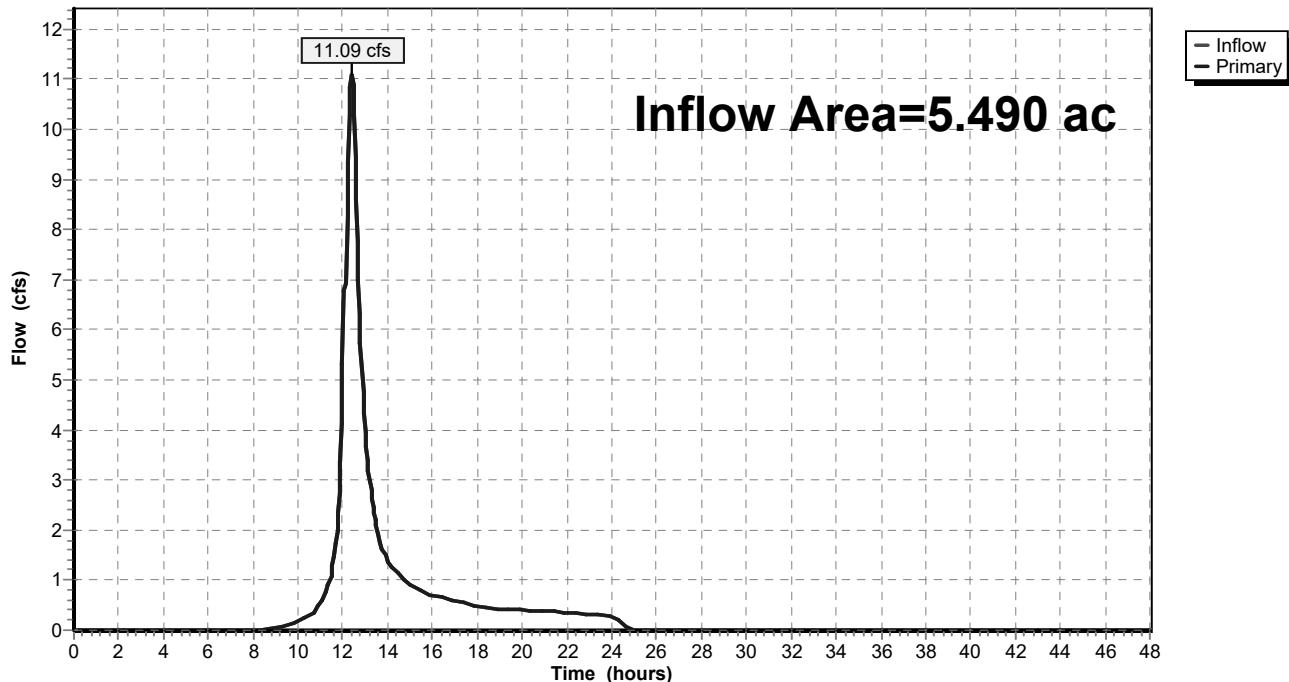
Inflow = 11.09 cfs @ 12.40 hrs, Volume= 1.452 af

Primary = 11.09 cfs @ 12.40 hrs, Volume= 1.452 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 9L: Existing Total**

Hydrograph



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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment1S: EDA-1-Pervious** Runoff Area=4.380 ac 0.00% Impervious Runoff Depth=4.88"  
Flow Length=1,124' Tc=29.1 min CN=72 Runoff=15.01 cfs 1.781 af

**Subcatchment2S: EDA-1-Impervious** Runoff Area=0.060 ac 100.00% Impervious Runoff Depth=7.97"  
Flow Length=1,124' Tc=25.4 min CN=98 Runoff=0.31 cfs 0.040 af

**Subcatchment4S: EDA-2-Pervious** Runoff Area=0.370 ac 0.00% Impervious Runoff Depth=4.76"  
Flow Length=159' Tc=11.7 min CN=71 Runoff=1.85 cfs 0.147 af

**Subcatchment7S: EDA OFF-SITE PERVIOUS** Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=4.88"  
Tc=0.0 min CN=72 Runoff=4.81 cfs 0.276 af

**Link 3L: POA-1** Inflow=15.31 cfs 1.821 af  
Primary=15.31 cfs 1.821 af

**Link 5L: POA-2** Inflow=1.85 cfs 0.147 af  
Primary=1.85 cfs 0.147 af

**Link 6L: TOTAL ON-SITE** Inflow=16.17 cfs 1.968 af  
Primary=16.17 cfs 1.968 af

**Link 8L: TOTAL OFF-SITE** Inflow=4.81 cfs 0.276 af  
Primary=4.81 cfs 0.276 af

**Link 9L: Existing Total** Inflow=17.11 cfs 2.244 af  
Primary=17.11 cfs 2.244 af

**Total Runoff Area = 5.490 ac Runoff Volume = 2.244 af Average Runoff Depth = 4.91"**  
**98.91% Pervious = 5.430 ac 1.09% Impervious = 0.060 ac**

**Existing**

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**Summary for Subcatchment 1S: EDA-1-Pervious**

Runoff = 15.01 cfs @ 12.41 hrs, Volume= 1.781 af, Depth= 4.88"

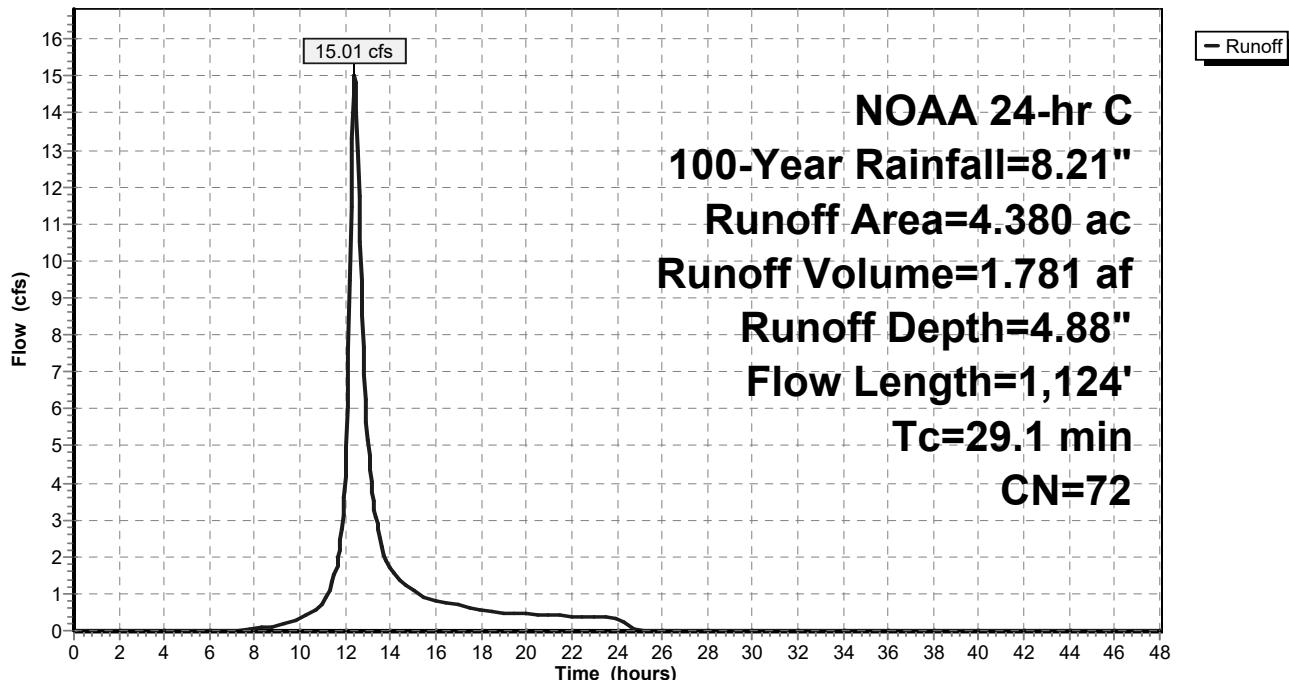
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
2.150	70	Woods, Good, HSG C
2.230	74	>75% Grass cover, Good, HSG C

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.7	100	0.0252	0.13		<b>Sheet Flow, Sheet Flow</b> Grass: Dense n= 0.240 P2= 3.38"
15.2	702	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
29.1	1,124	Total			

**Subcatchment 1S: EDA-1-Pervious**

Hydrograph



**Existing**

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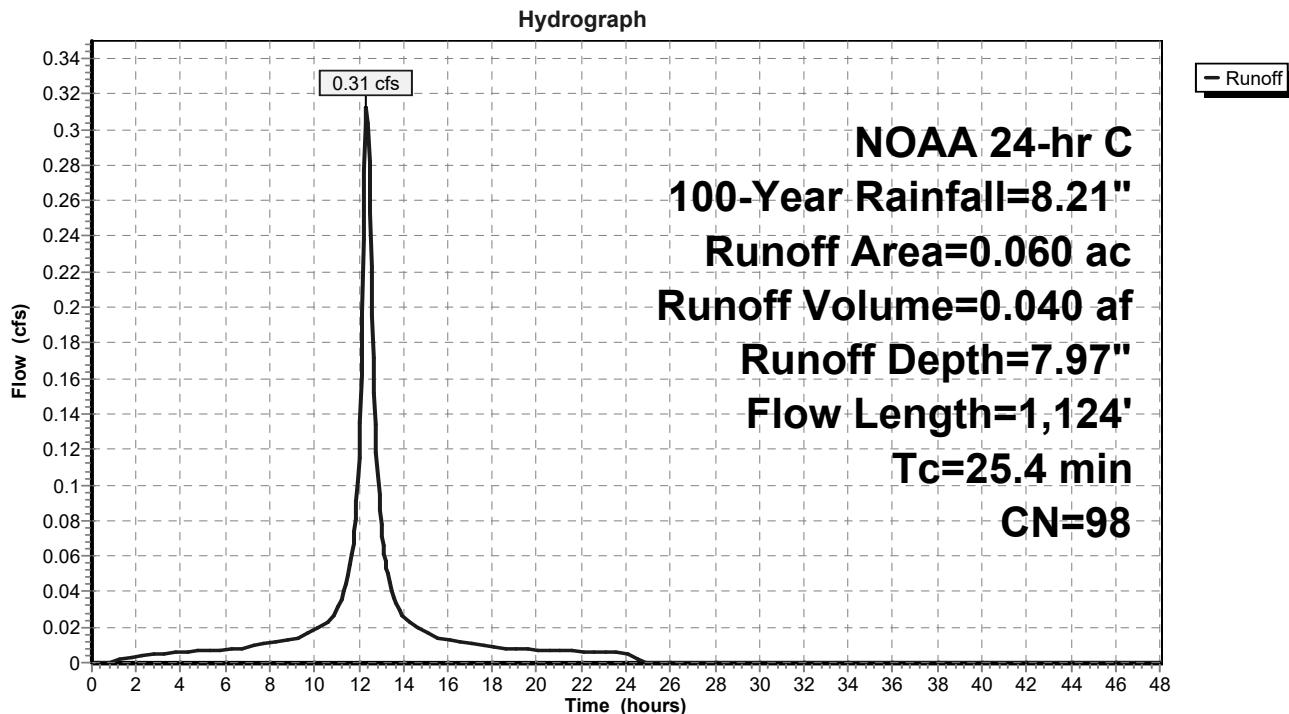
**Summary for Subcatchment 2S: EDA-1-Impervious**

Runoff = 0.31 cfs @ 12.35 hrs, Volume= 0.040 af, Depth= 7.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
0.060	98	Paved parking, HSG C
0.060		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.2	108	0.0252	0.19		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
15.0	694	0.0238	0.77		<b>Shallow Concentrated Flow, Shallow Concentrated Flow</b> Woodland Kv= 5.0 fps
1.2	322	0.0050	4.59	123.92	<b>Channel Flow, Natural Stream</b> Area= 27.0 sf Perim= 18.0' r= 1.50' n= 0.030 Stream, clean & straight
25.4	1,124				Total

**Subcatchment 2S: EDA-1-Impervious**

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**Summary for Subcatchment 4S: EDA-2-Pervious**

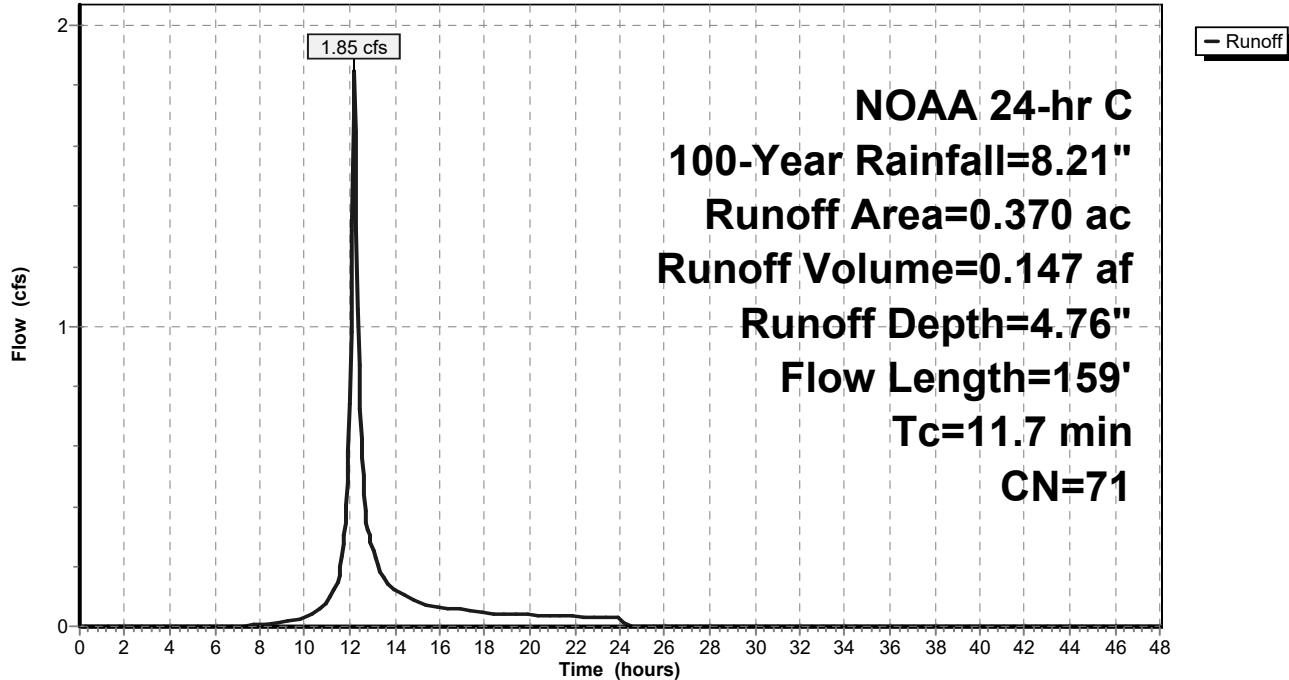
Runoff = 1.85 cfs @ 12.20 hrs, Volume= 0.147 af, Depth= 4.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description			
0.290	70	Woods, Good, HSG C			
0.080	74	>75% Grass cover, Good, HSG C			
0.370	71	Weighted Average			
0.370		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	42	0.0040	0.08		<b>Sheet Flow, Sheet Flow</b> Grass: Short n= 0.150 P2= 3.38"
0.4	20	0.0040	0.95		<b>Shallow Concentrated Flow, Grass Waterway</b> Grassed Waterway Kv= 15.0 fps
2.2	97	0.0210	0.72		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
11.7	159	Total			

**Subcatchment 4S: EDA-2-Pervious**

Hydrograph



**Existing**

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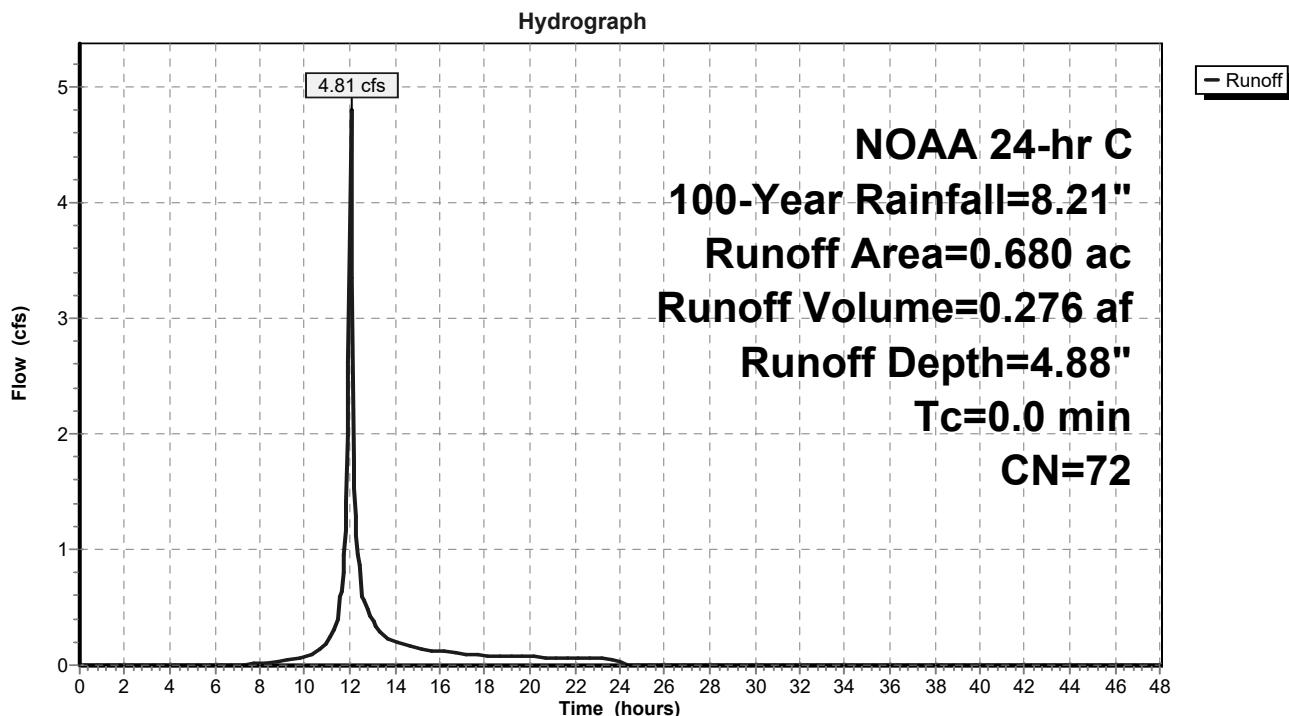
**Summary for Subcatchment 7S: EDA OFF-SITE PERVIOUS**[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 4.81 cfs @ 12.05 hrs, Volume= 0.276 af, Depth= 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0				Direct Entry, 10	

**Subcatchment 7S: EDA OFF-SITE PERVIOUS**

**Summary for Link 3L: POA-1**

Inflow Area = 4.440 ac, 1.35% Impervious, Inflow Depth = 4.92" for 100-Year event

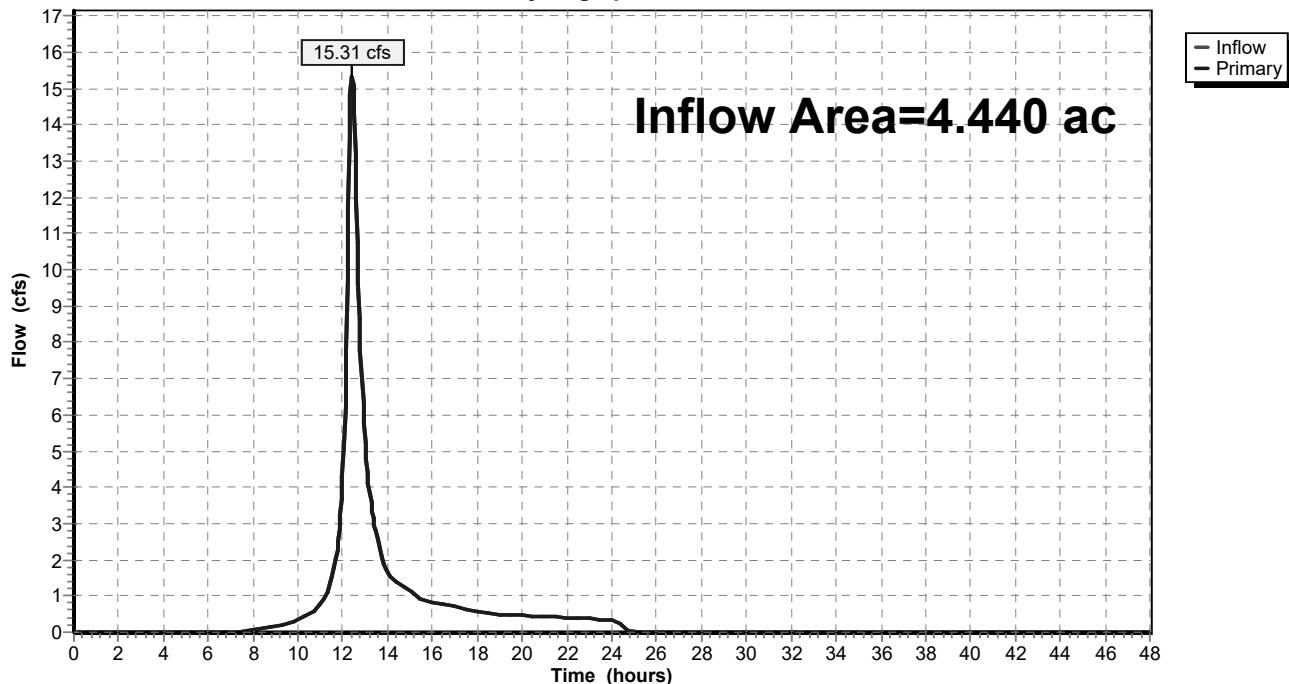
Inflow = 15.31 cfs @ 12.41 hrs, Volume= 1.821 af

Primary = 15.31 cfs @ 12.41 hrs, Volume= 1.821 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 3L: POA-1**

Hydrograph



**Summary for Link 5L: POA-2**

Inflow Area = 0.370 ac, 0.00% Impervious, Inflow Depth = 4.76" for 100-Year event

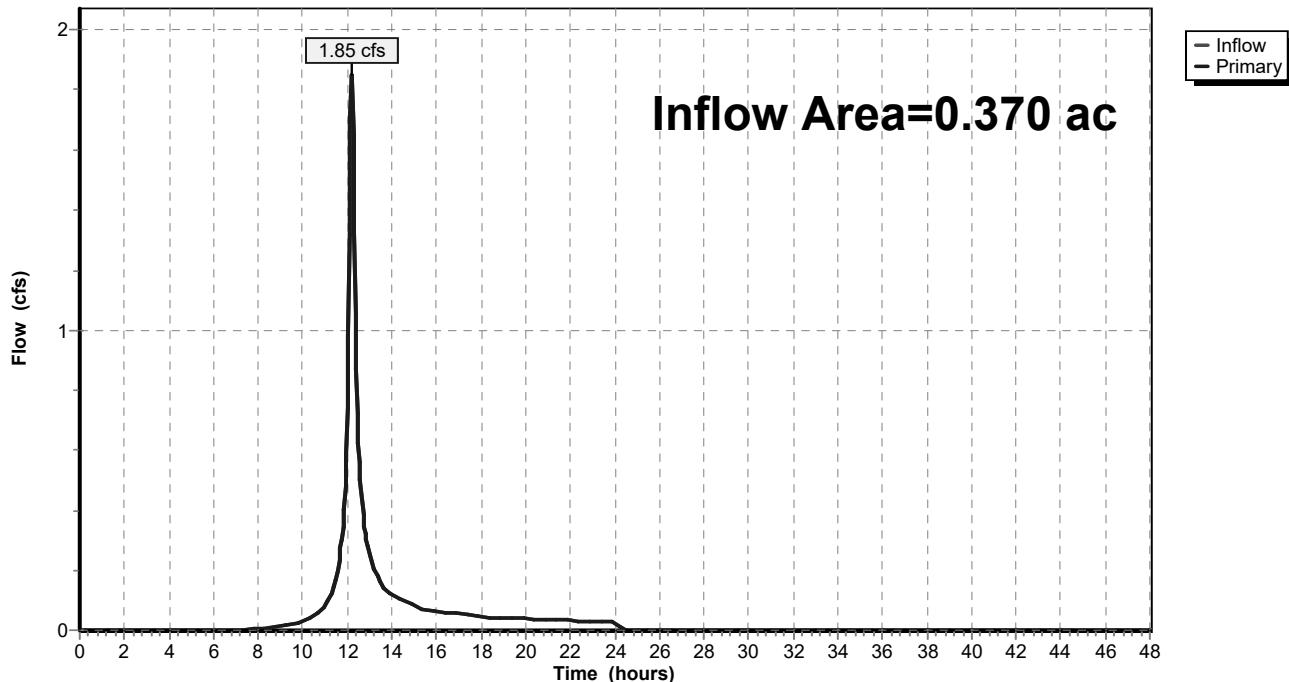
Inflow = 1.85 cfs @ 12.20 hrs, Volume= 0.147 af

Primary = 1.85 cfs @ 12.20 hrs, Volume= 0.147 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 5L: POA-2**

Hydrograph



**Summary for Link 6L: TOTAL ON-SITE**

Inflow Area = 4.810 ac, 1.25% Impervious, Inflow Depth = 4.91" for 100-Year event

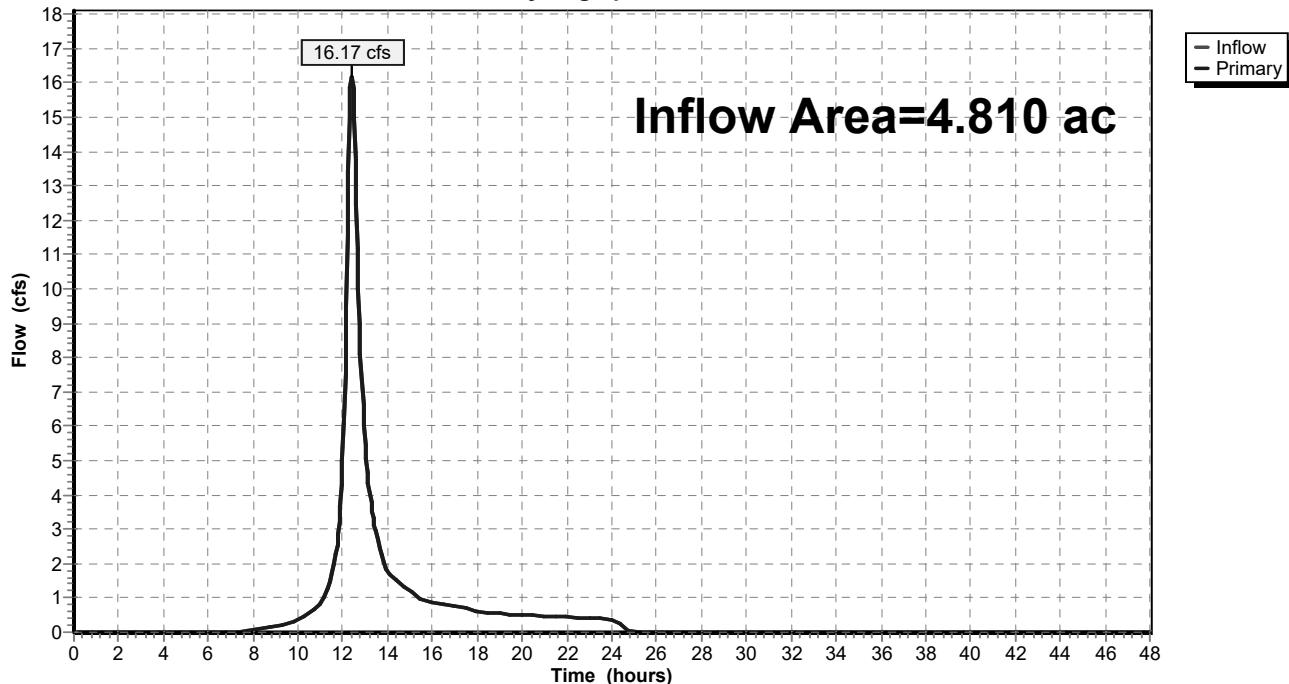
Inflow = 16.17 cfs @ 12.40 hrs, Volume= 1.968 af

Primary = 16.17 cfs @ 12.40 hrs, Volume= 1.968 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 6L: TOTAL ON-SITE**

Hydrograph



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**Summary for Link 8L: TOTAL OFF-SITE**

Inflow Area = 0.680 ac, 0.00% Impervious, Inflow Depth = 4.88" for 100-Year event

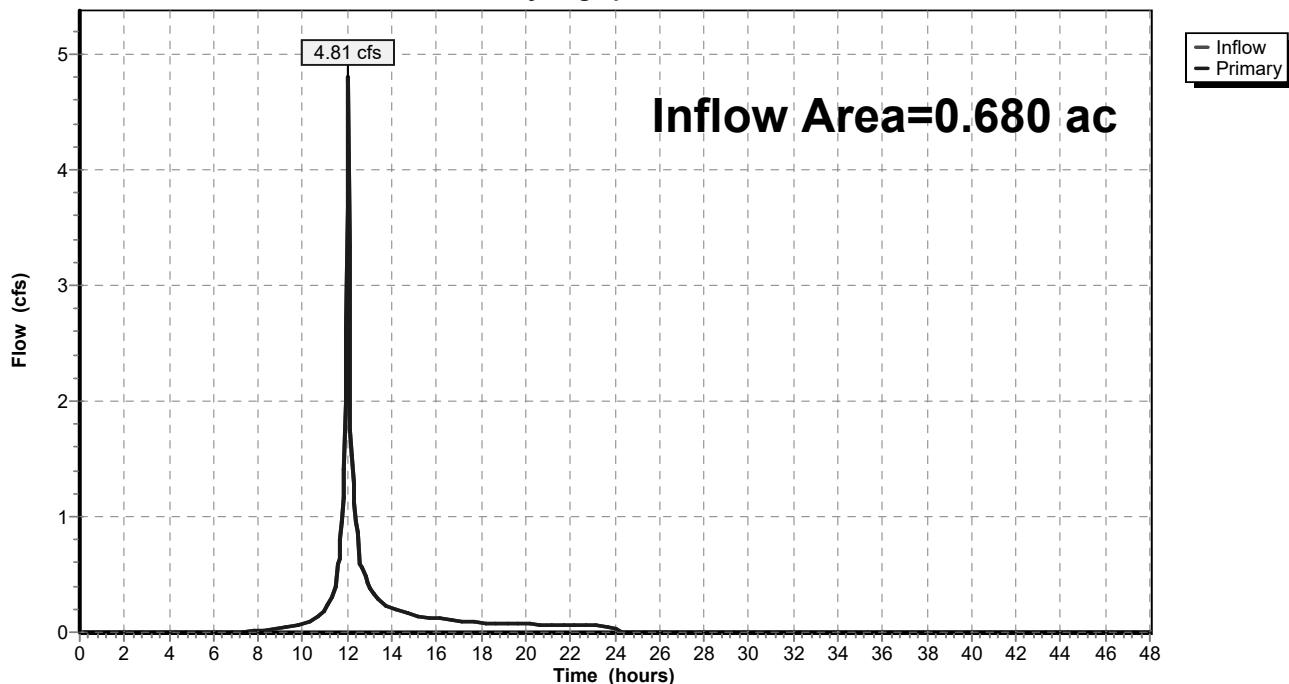
Inflow = 4.81 cfs @ 12.05 hrs, Volume= 0.276 af

Primary = 4.81 cfs @ 12.05 hrs, Volume= 0.276 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 8L: TOTAL OFF-SITE**

Hydrograph



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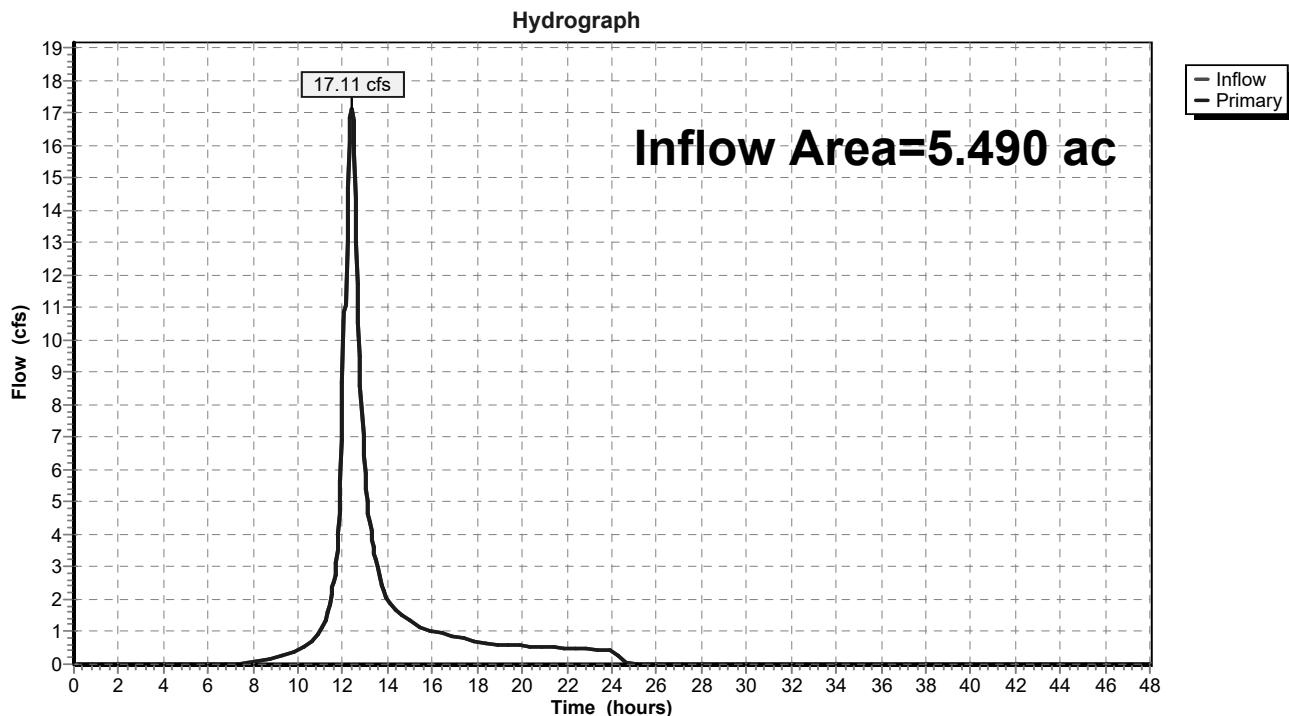
**Summary for Link 9L: Existing Total**

Inflow Area = 5.490 ac, 1.09% Impervious, Inflow Depth = 4.91" for 100-Year event

Inflow = 17.11 cfs @ 12.40 hrs, Volume= 2.244 af

Primary = 17.11 cfs @ 12.40 hrs, Volume= 2.244 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

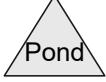
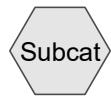
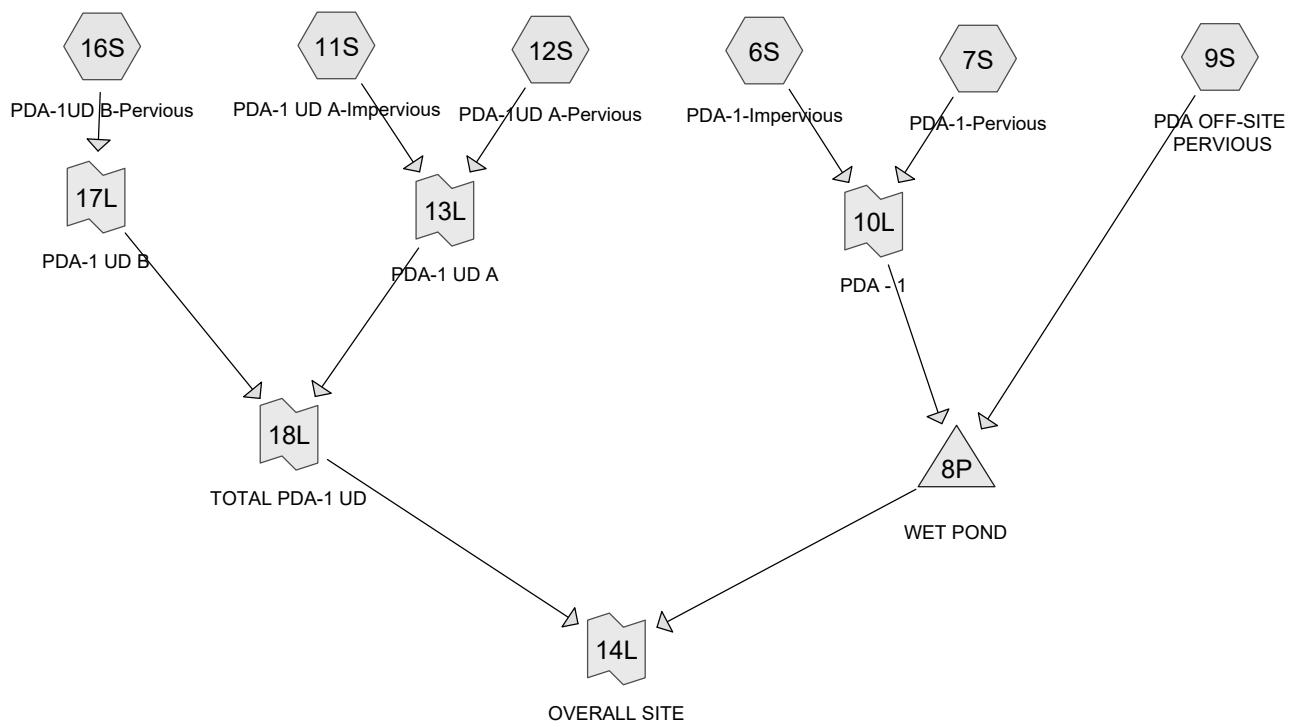
**Link 9L: Existing Total**



## **APPENDIX B**

Hydrographs, CN, & Tc Calculations for Developed Conditions, Storage  
Volume and Stage-Storage Calculations for Stormwater Management Basin





**Routing Diagram for Proposed**  
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**Proposed**

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**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
1.140	74	>75% Grass cover, Good, HSG C (7S, 12S, 16S)
3.670	98	Paved parking, HSG C (6S, 11S)
0.680	72	Woods/grass comb., Good, HSG C (9S)
<b>5.490</b>	<b>90</b>	<b>TOTAL AREA</b>

**Proposed**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
5.490	HSG C	6S, 7S, 9S, 11S, 12S, 16S
0.000	HSG D	
0.000	Other	
<b>5.490</b>		<b>TOTAL AREA</b>

**Proposed**

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	1.140	0.000	0.000	1.140	>75% Grass cover, Good	7S, 12S, 16S
0.000	0.000	3.670	0.000	0.000	3.670	Paved parking	6S, 11S
0.000	0.000	0.680	0.000	0.000	0.680	Woods/grass comb., Good	9S
<b>0.000</b>	<b>0.000</b>	<b>5.490</b>	<b>0.000</b>	<b>0.000</b>	<b>5.490</b>	<b>TOTAL AREA</b>	

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**Pipe Listing (all nodes)**

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	8P	66.50	66.00	100.0	0.0050	0.015	15.0	0.0	0.0

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment6S: PDA-1-Impervious** Runoff Area=3.450 ac 100.00% Impervious Runoff Depth=3.11"  
Tc=10.0 min CN=98 Runoff=10.42 cfs 0.893 af**Subcatchment7S: PDA-1-Pervious** Runoff Area=0.720 ac 0.00% Impervious Runoff Depth=1.13"  
Tc=10.0 min CN=74 Runoff=0.88 cfs 0.068 af**Subcatchment9S: PDA OFF-SITE PERVIOUS** Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=1.02"  
Tc=0.0 min CN=72 Runoff=0.99 cfs 0.058 af**Subcatchment11S: PDA-1 UD** Runoff Area=0.220 ac 100.00% Impervious Runoff Depth=3.11"  
Tc=10.0 min CN=98 Runoff=0.66 cfs 0.057 af**Subcatchment12S: PDA-1UDA-Pervious** Runoff Area=0.320 ac 0.00% Impervious Runoff Depth=1.13"  
Tc=10.0 min CN=74 Runoff=0.39 cfs 0.030 af**Subcatchment16S: PDA-1UDB-Pervious** Runoff Area=0.100 ac 0.00% Impervious Runoff Depth=1.13"  
Tc=10.0 min CN=74 Runoff=0.12 cfs 0.009 af**Pond 8P: WET POND** Peak Elev=71.10' Storage=33,090 cf Inflow=11.64 cfs 1.019 af  
Outflow=0.26 cfs 0.707 af**Link 10L: PDA - 1** Inflow=11.29 cfs 0.961 af  
Primary=11.29 cfs 0.961 af**Link 13L: PDA-1 UD A** Inflow=1.05 cfs 0.087 af  
Primary=1.05 cfs 0.087 af**Link 14L: OVERALL SITE** Inflow=1.36 cfs 0.803 af  
Primary=1.36 cfs 0.803 af**Link 17L: PDA-1 UD B** Inflow=0.12 cfs 0.009 af  
Primary=0.12 cfs 0.009 af**Link 18L: TOTAL PDA-1 UD** Inflow=1.17 cfs 0.097 af  
Primary=1.17 cfs 0.097 af**Total Runoff Area = 5.490 ac Runoff Volume = 1.115 af Average Runoff Depth = 2.44"**  
**33.15% Pervious = 1.820 ac 66.85% Impervious = 3.670 ac**

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NOAA 24-hr C 2-Year Rainfall=3.34"

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**Summary for Subcatchment 6S: PDA-1-Impervious**

Runoff = 10.42 cfs @ 12.17 hrs, Volume= 0.893 af, Depth= 3.11"

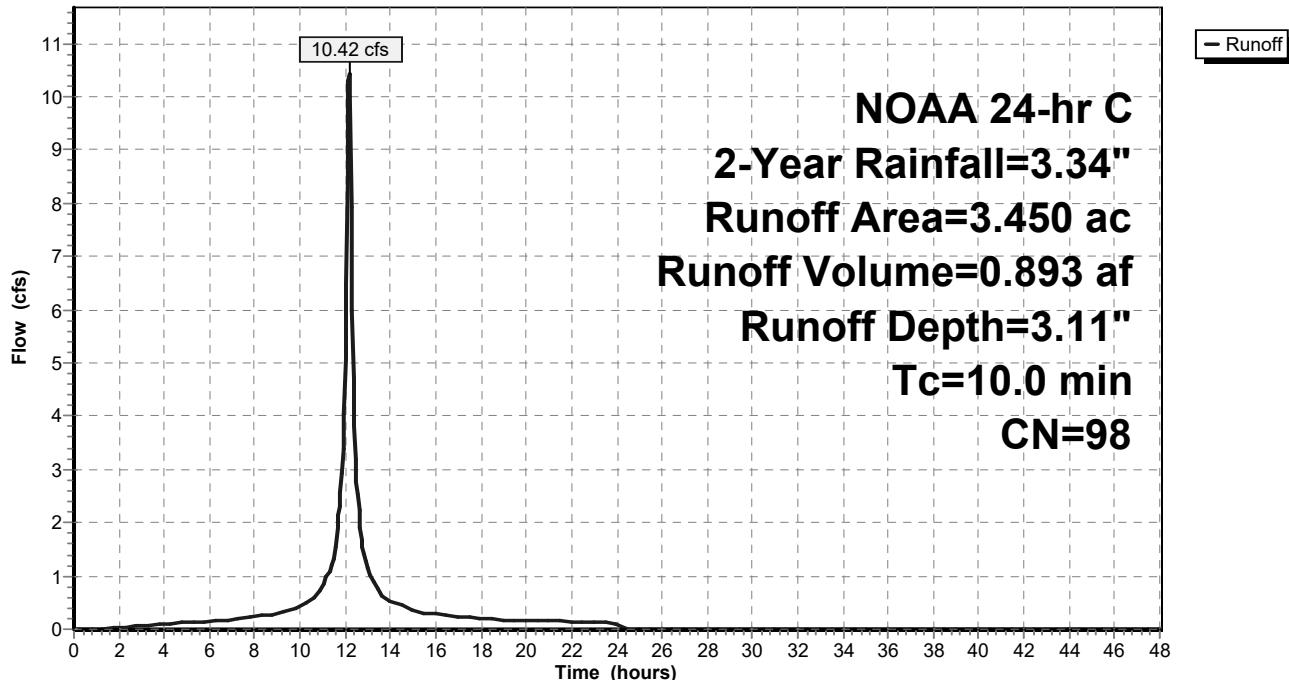
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
3.450	98	Paved parking, HSG C
3.450		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 6S: PDA-1-Impervious**

Hydrograph



**Summary for Subcatchment 7S: PDA-1-Pervious**

Runoff = 0.88 cfs @ 12.18 hrs, Volume= 0.068 af, Depth= 1.13"

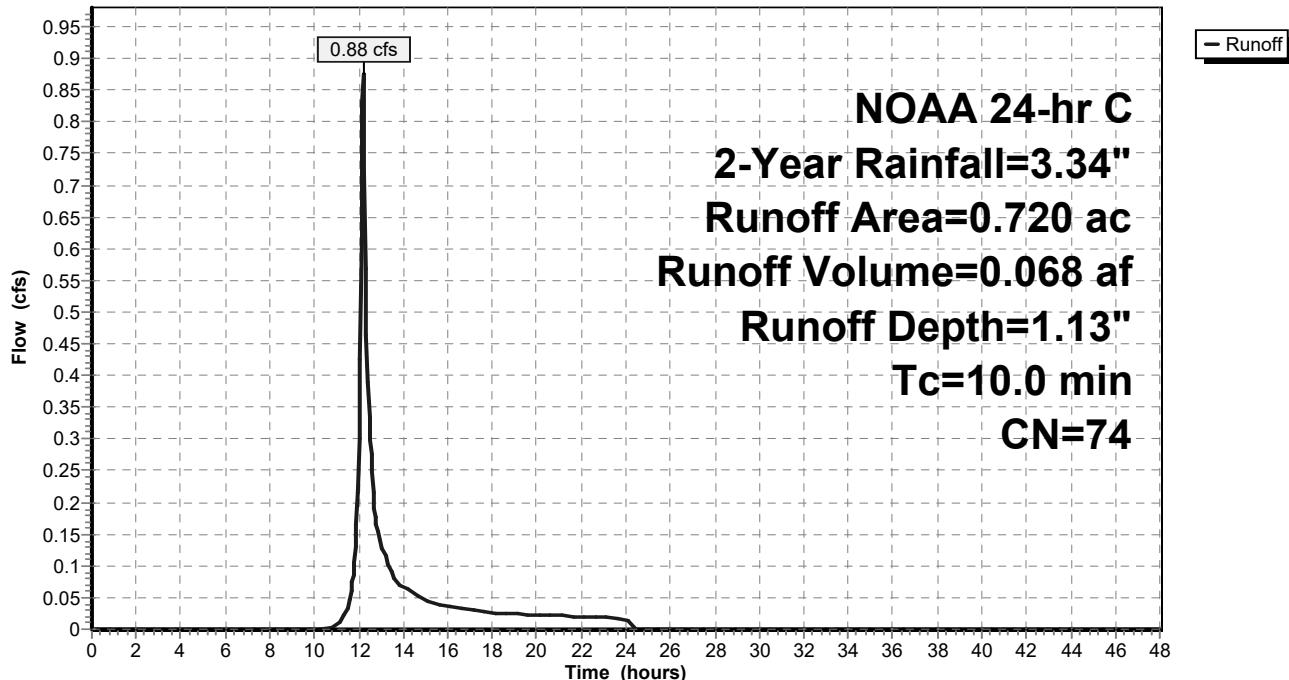
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
0.720	74	>75% Grass cover, Good, HSG C
0.720		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 7S: PDA-1-Pervious**

Hydrograph



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NOAA 24-hr C 2-Year Rainfall=3.34"

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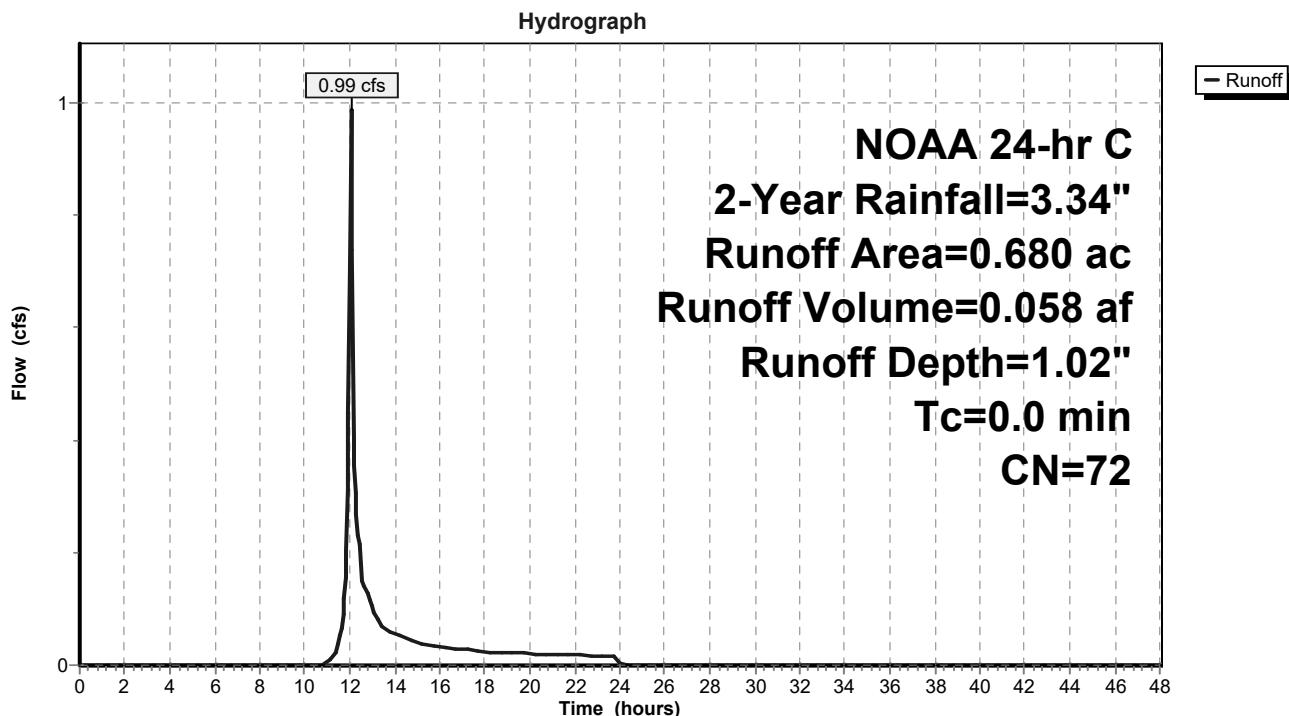
**Summary for Subcatchment 9S: PDA OFF-SITE PERVIOUS**[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 0.99 cfs @ 12.05 hrs, Volume= 0.058 af, Depth= 1.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0				Direct Entry, 10	

**Subcatchment 9S: PDA OFF-SITE PERVIOUS**

**Summary for Subcatchment 11S: PDA-1 UD A-Impervious**

Runoff = 0.66 cfs @ 12.17 hrs, Volume= 0.057 af, Depth= 3.11"

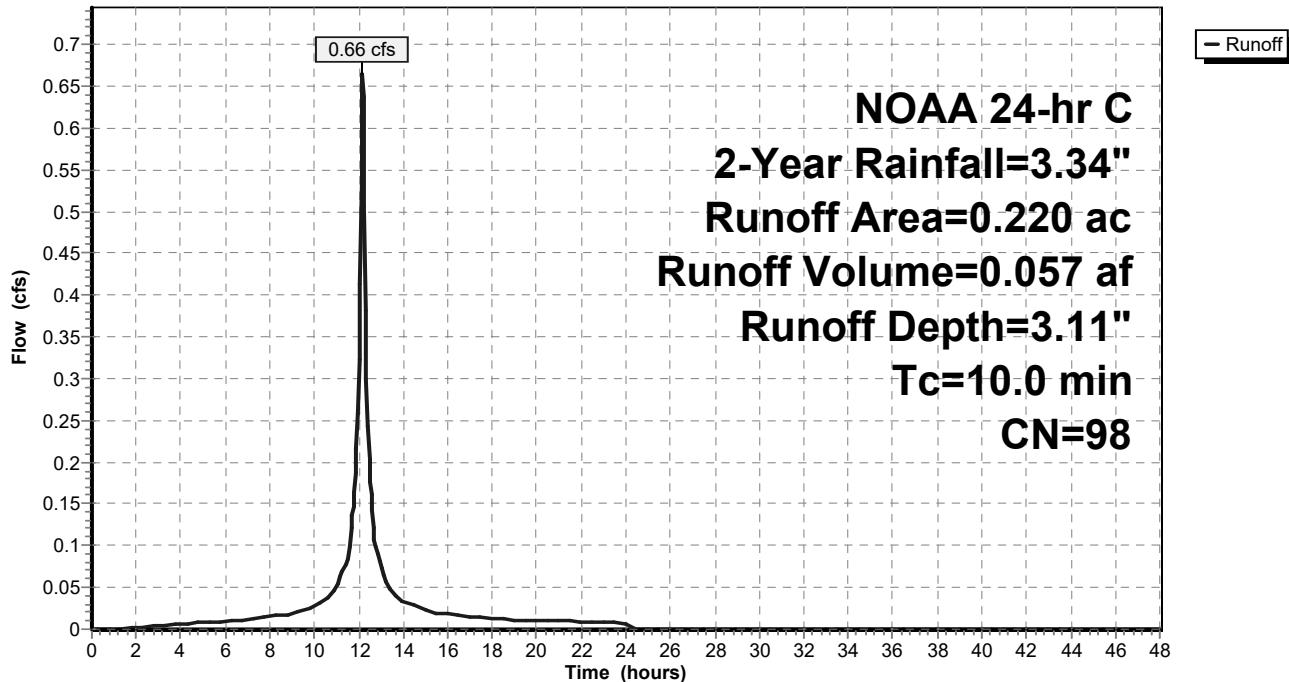
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
0.220	98	Paved parking, HSG C
0.220		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 11S: PDA-1 UD A-Impervious**

Hydrograph



**Summary for Subcatchment 12S: PDA-1UD A-Pervious**

Runoff = 0.39 cfs @ 12.18 hrs, Volume= 0.030 af, Depth= 1.13"

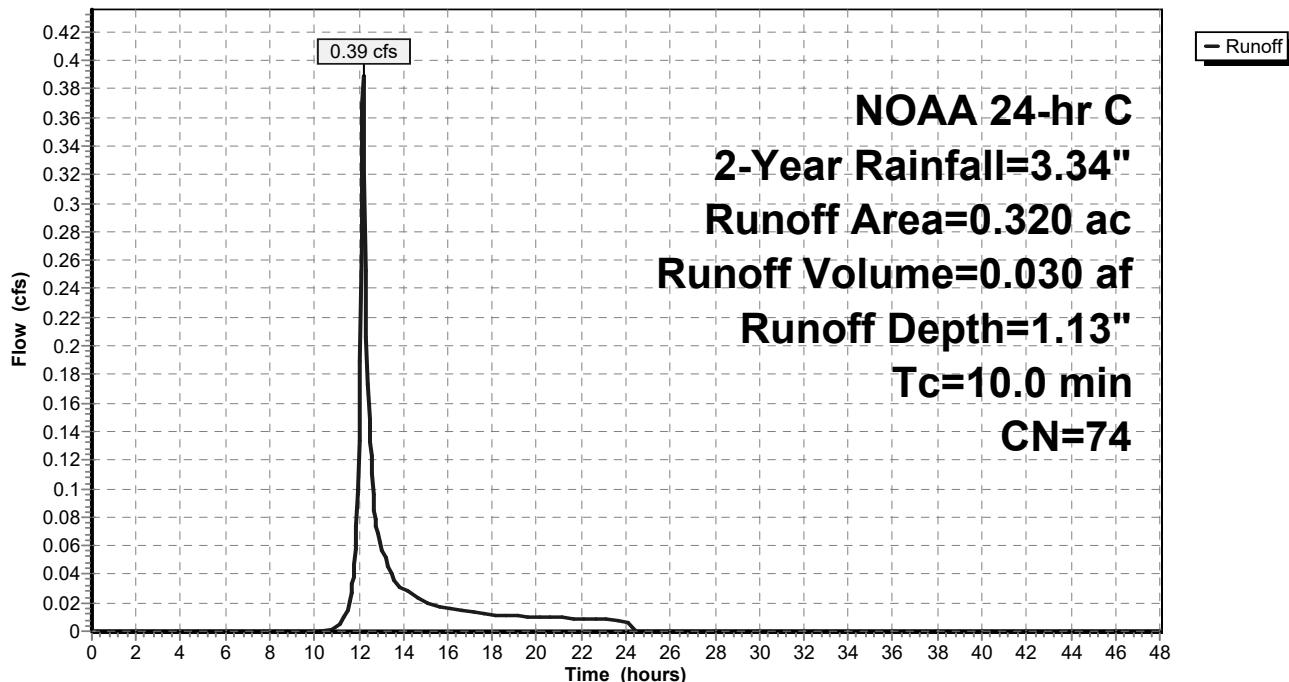
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
0.320	74	>75% Grass cover, Good, HSG C
0.320		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 12S: PDA-1UD A-Pervious**

Hydrograph



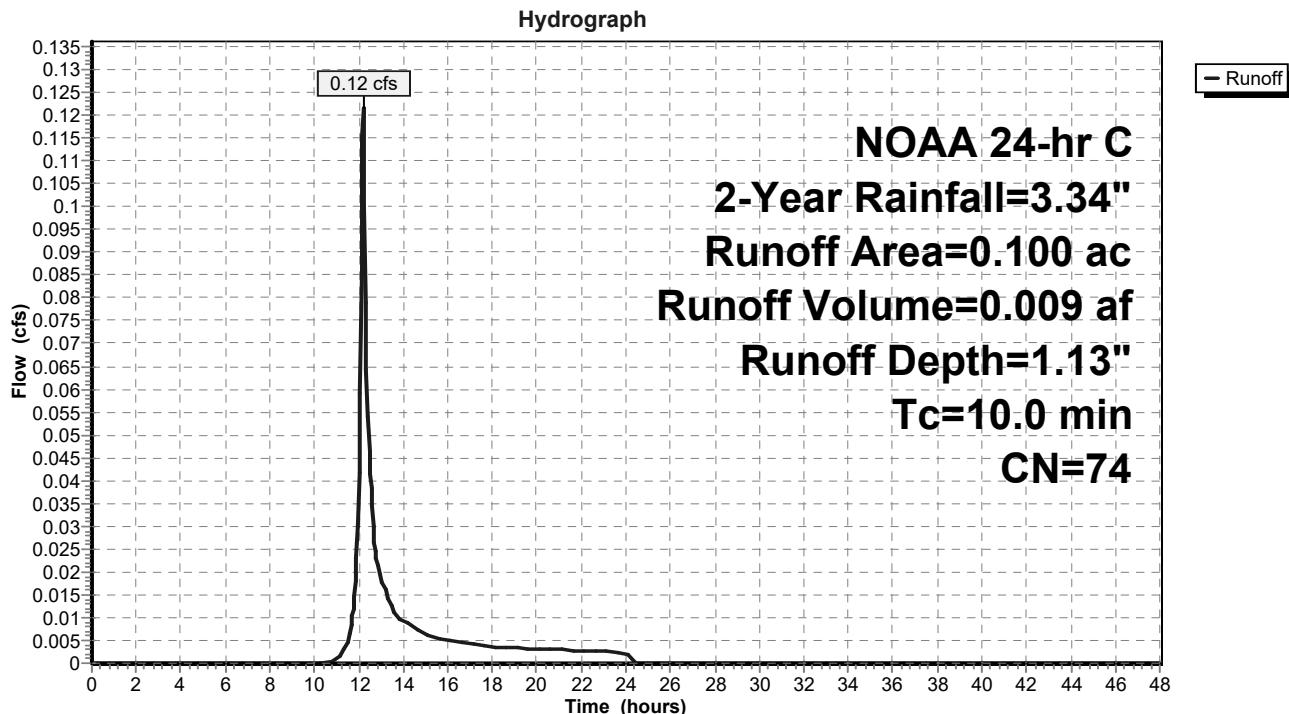
**Summary for Subcatchment 16S: PDA-1UD B-Pervious**

Runoff = 0.12 cfs @ 12.18 hrs, Volume= 0.009 af, Depth= 1.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 2-Year Rainfall=3.34"

Area (ac)	CN	Description
0.100	74	>75% Grass cover, Good, HSG C
0.100		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 16S: PDA-1UD B-Pervious**

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NOAA 24-hr C 2-Year Rainfall=3.34"

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**Summary for Pond 8P: WET POND**

Inflow Area = 4.850 ac, 71.13% Impervious, Inflow Depth = 2.52" for 2-Year event  
 Inflow = 11.64 cfs @ 12.17 hrs, Volume= 1.019 af  
 Outflow = 0.26 cfs @ 17.74 hrs, Volume= 0.707 af, Atten= 98%, Lag= 334.6 min  
 Primary = 0.26 cfs @ 17.74 hrs, Volume= 0.707 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
 Peak Elev= 71.10' @ 17.74 hrs Surf.Area= 13,789 sf Storage= 33,090 cf

Plug-Flow detention time= 990.6 min calculated for 0.706 af (69% of inflow)  
 Center-of-Mass det. time= 891.4 min ( 1,664.7 - 773.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	68.50'	60,825 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
68.50	11,408	0	0
69.00	12,104	5,878	5,878
70.00	12,902	12,503	18,381
71.00	13,711	13,307	31,688
72.00	14,475	14,093	45,781
73.00	15,613	15,044	60,825

Device	Routing	Invert	Outlet Devices
#1	Primary	66.50'	<b>15.0" Round Culvert</b> L= 100.0' Ke= 1.000 Inlet / Outlet Invert= 66.50' / 66.00' S= 0.0050 '/' Cc= 0.900 n= 0.015 Concrete sewer w/manholes & inlets, Flow Area= 1.23 sf
#2	Device 1	68.50'	<b>2.5" Vert. Orifice</b> C= 0.600
#3	Device 1	71.15'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)
#4	Device 1	72.90'	<b>48.0" x 42.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.26 cfs @ 17.74 hrs HW=71.10' (Free Discharge)

↑ 1=Culvert (Passes 0.26 cfs of 8.55 cfs potential flow)

↑ 2=Orifice (Orifice Controls 0.26 cfs @ 7.61 fps)

↑ 3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

↑ 4=Grate (Controls 0.00 cfs)

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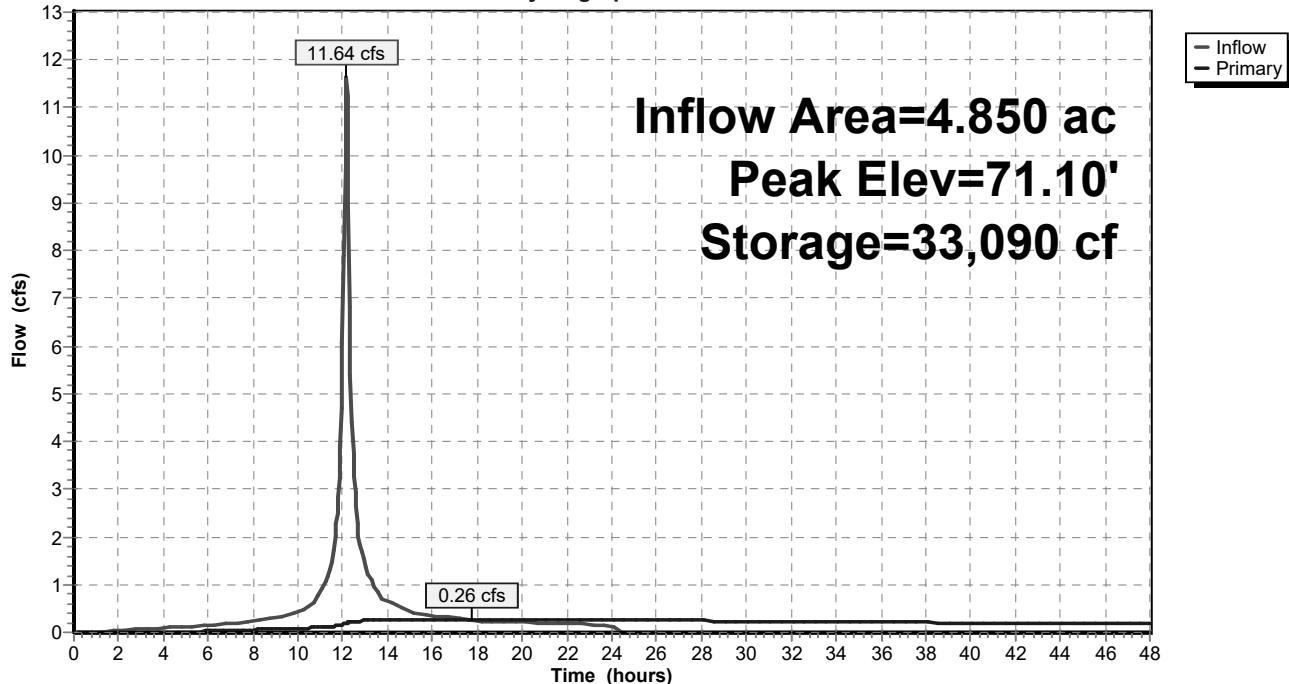
NOAA 24-hr C 2-Year Rainfall=3.34"

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**Pond 8P: WET POND**

Hydrograph



**Summary for Link 10L: PDA - 1**

Inflow Area = 4.170 ac, 82.73% Impervious, Inflow Depth = 2.77" for 2-Year event

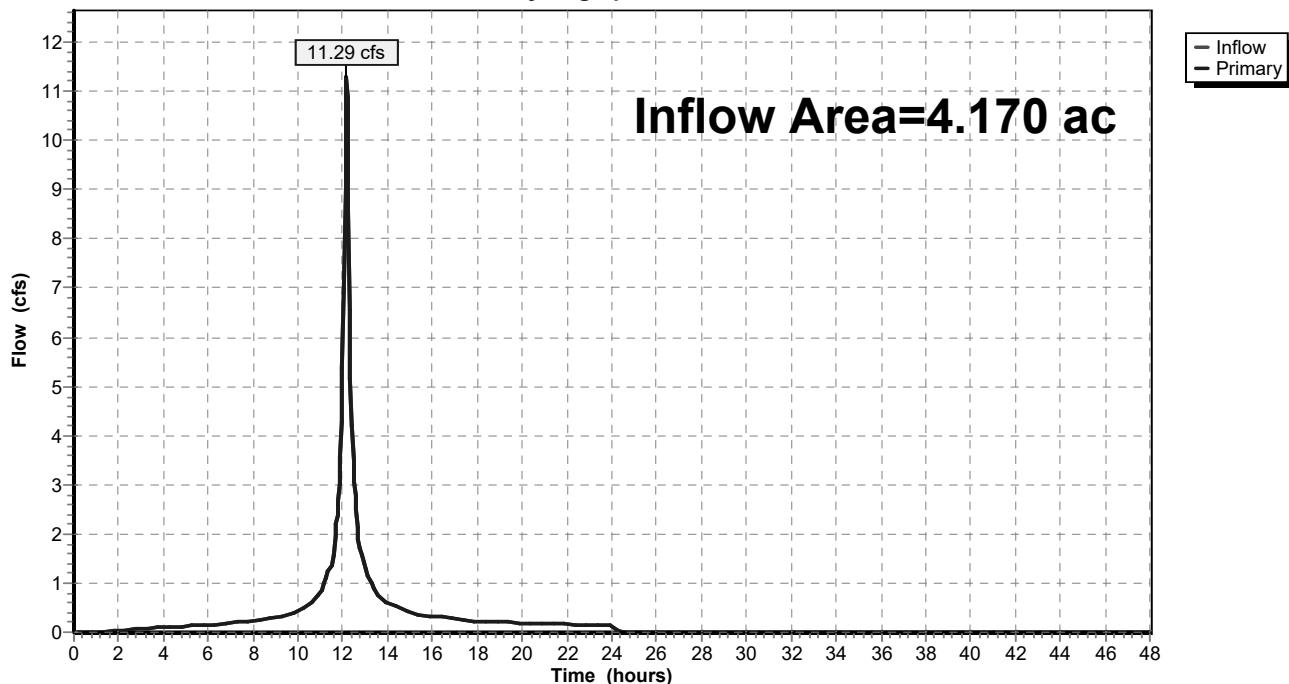
Inflow = 11.29 cfs @ 12.17 hrs, Volume= 0.961 af

Primary = 11.29 cfs @ 12.17 hrs, Volume= 0.961 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 10L: PDA - 1**

Hydrograph



**Summary for Link 13L: PDA-1 UD A**

Inflow Area = 0.540 ac, 40.74% Impervious, Inflow Depth = 1.94" for 2-Year event

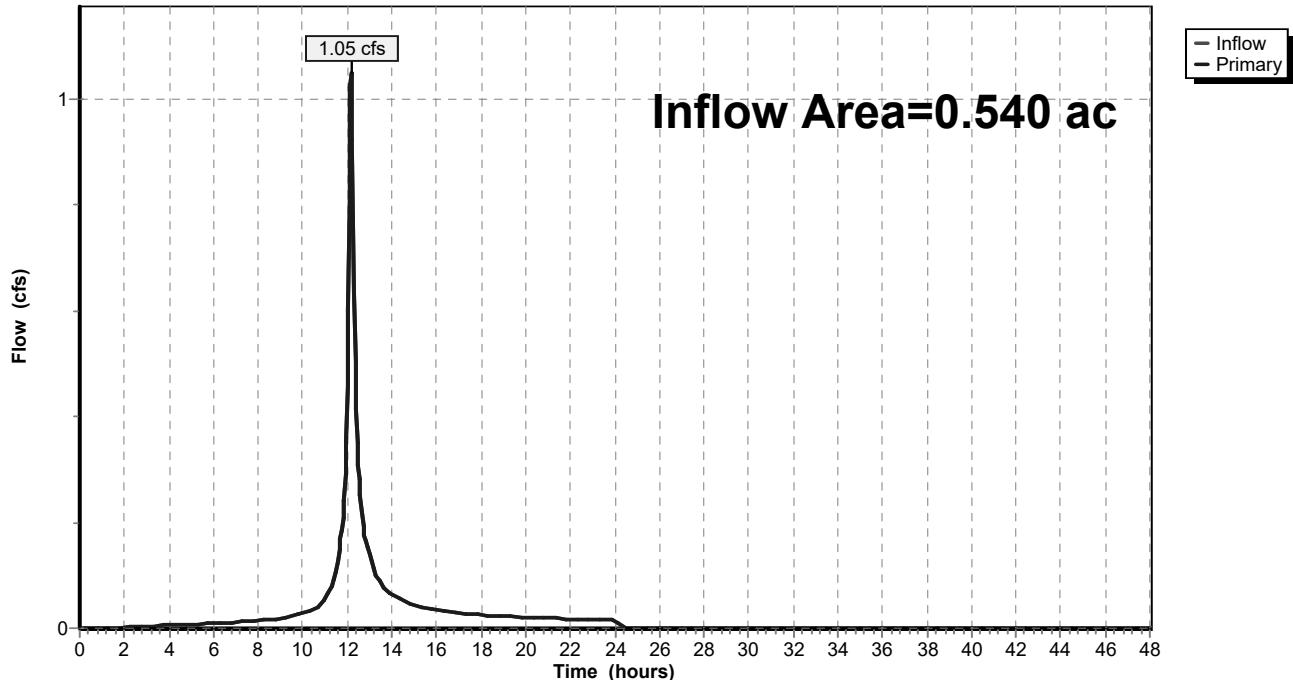
Inflow = 1.05 cfs @ 12.17 hrs, Volume= 0.087 af

Primary = 1.05 cfs @ 12.17 hrs, Volume= 0.087 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 13L: PDA-1 UD A**

Hydrograph



**Summary for Link 14L: OVERALL SITE**

Inflow Area = 5.490 ac, 66.85% Impervious, Inflow Depth > 1.76" for 2-Year event

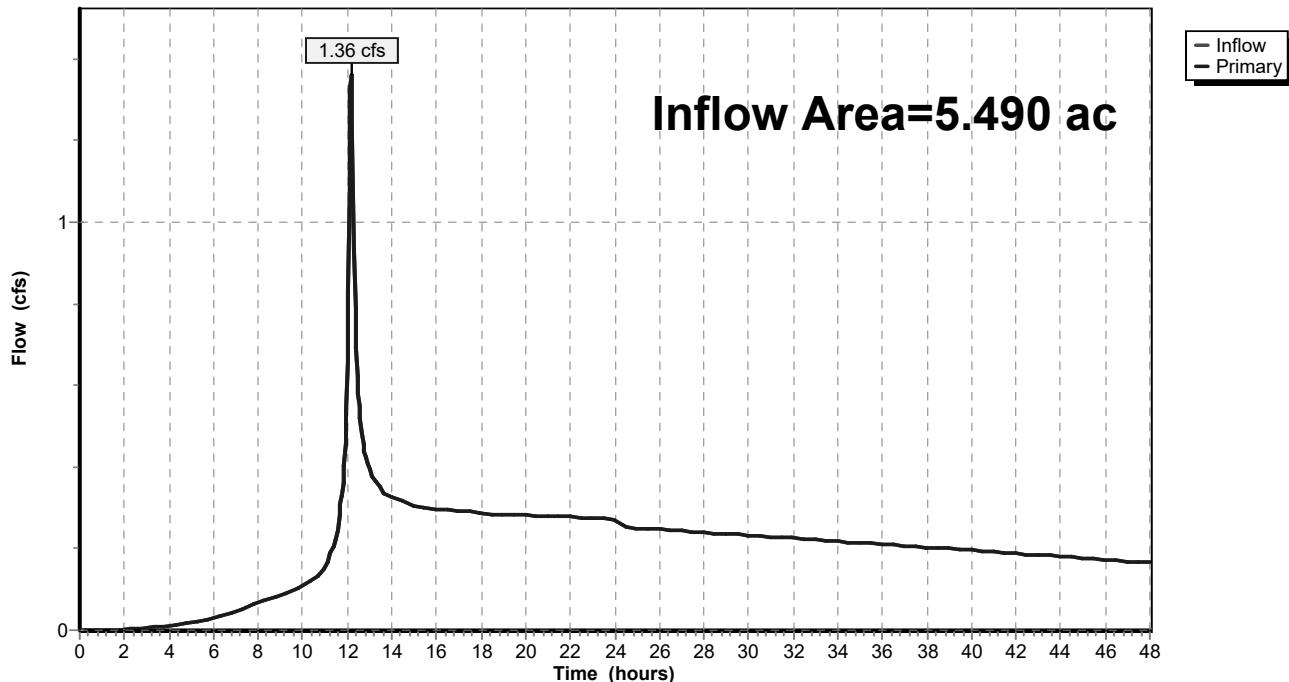
Inflow = 1.36 cfs @ 12.18 hrs, Volume= 0.803 af

Primary = 1.36 cfs @ 12.18 hrs, Volume= 0.803 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 14L: OVERALL SITE**

Hydrograph



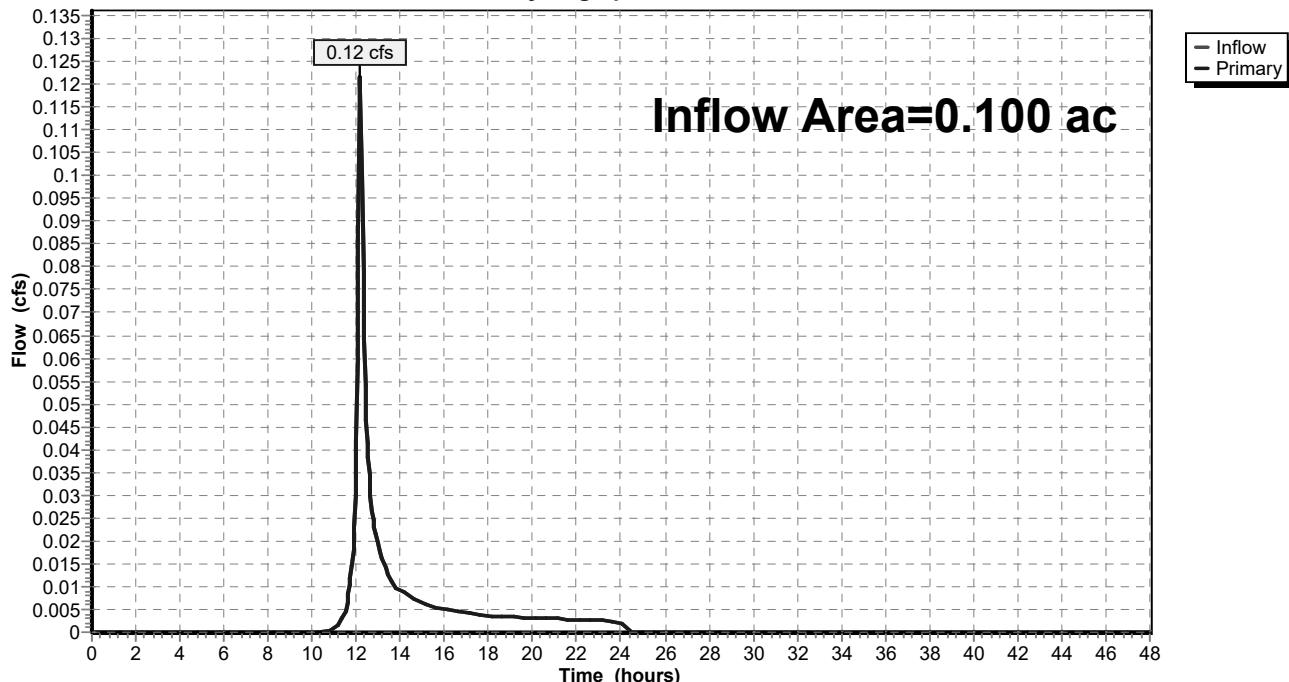
**Summary for Link 17L: PDA-1 UD B**

Inflow Area = 0.100 ac, 0.00% Impervious, Inflow Depth = 1.13" for 2-Year event

Inflow = 0.12 cfs @ 12.18 hrs, Volume= 0.009 af

Primary = 0.12 cfs @ 12.18 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 17L: PDA-1 UD B****Hydrograph**

**Summary for Link 18L: TOTAL PDA-1 UD**

Inflow Area = 0.640 ac, 34.38% Impervious, Inflow Depth = 1.81" for 2-Year event

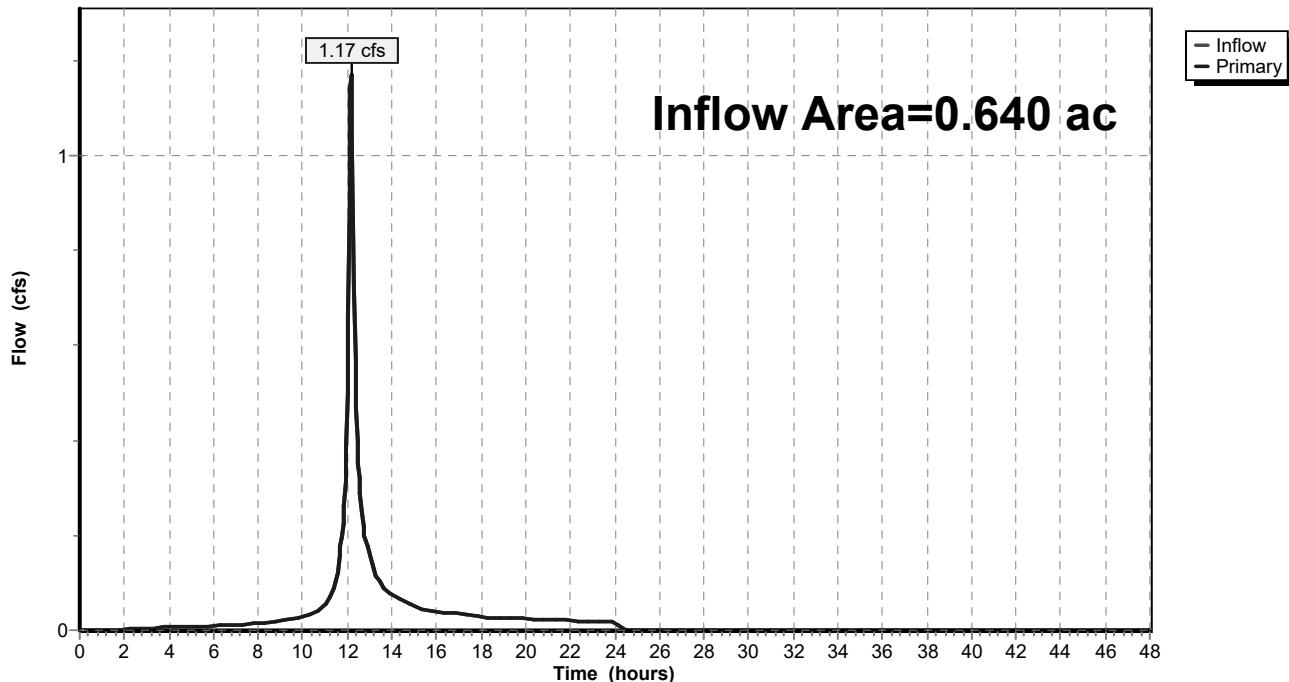
Inflow = 1.17 cfs @ 12.18 hrs, Volume= 0.097 af

Primary = 1.17 cfs @ 12.18 hrs, Volume= 0.097 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 18L: TOTAL PDA-1 UD**

Hydrograph



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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment6S: PDA-1-Impervious** Runoff Area=3.450 ac 100.00% Impervious Runoff Depth=4.77"  
Tc=10.0 min CN=98 Runoff=15.74 cfs 1.372 af**Subcatchment7S: PDA-1-Pervious** Runoff Area=0.720 ac 0.00% Impervious Runoff Depth=2.37"  
Tc=10.0 min CN=74 Runoff=1.89 cfs 0.142 af**Subcatchment9S: PDA OFF-SITE PERVIOUS** Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=2.21"  
Tc=0.0 min CN=72 Runoff=2.20 cfs 0.125 af**Subcatchment11S: PDA-1 UD** Runoff Area=0.220 ac 100.00% Impervious Runoff Depth=4.77"  
Tc=10.0 min CN=98 Runoff=1.00 cfs 0.088 af**Subcatchment12S: PDA-1UDA-Pervious** Runoff Area=0.320 ac 0.00% Impervious Runoff Depth=2.37"  
Tc=10.0 min CN=74 Runoff=0.84 cfs 0.063 af**Subcatchment16S: PDA-1UDB-Pervious** Runoff Area=0.100 ac 0.00% Impervious Runoff Depth=2.37"  
Tc=10.0 min CN=74 Runoff=0.26 cfs 0.020 af**Pond 8P: WET POND** Peak Elev=71.60' Storage=40,025 cf Inflow=18.35 cfs 1.640 af  
Outflow=4.12 cfs 1.296 af**Link 10L: PDA - 1** Inflow=17.62 cfs 1.515 af  
Primary=17.62 cfs 1.515 af**Link 13L: PDA-1 UD A** Inflow=1.84 cfs 0.151 af  
Primary=1.84 cfs 0.151 af**Link 14L: OVERALL SITE** Inflow=4.64 cfs 1.466 af  
Primary=4.64 cfs 1.466 af**Link 17L: PDA-1 UD B** Inflow=0.26 cfs 0.020 af  
Primary=0.26 cfs 0.020 af**Link 18L: TOTAL PDA-1 UD** Inflow=2.10 cfs 0.171 af  
Primary=2.10 cfs 0.171 af**Total Runoff Area = 5.490 ac Runoff Volume = 1.810 af Average Runoff Depth = 3.96"**  
**33.15% Pervious = 1.820 ac 66.85% Impervious = 3.670 ac**

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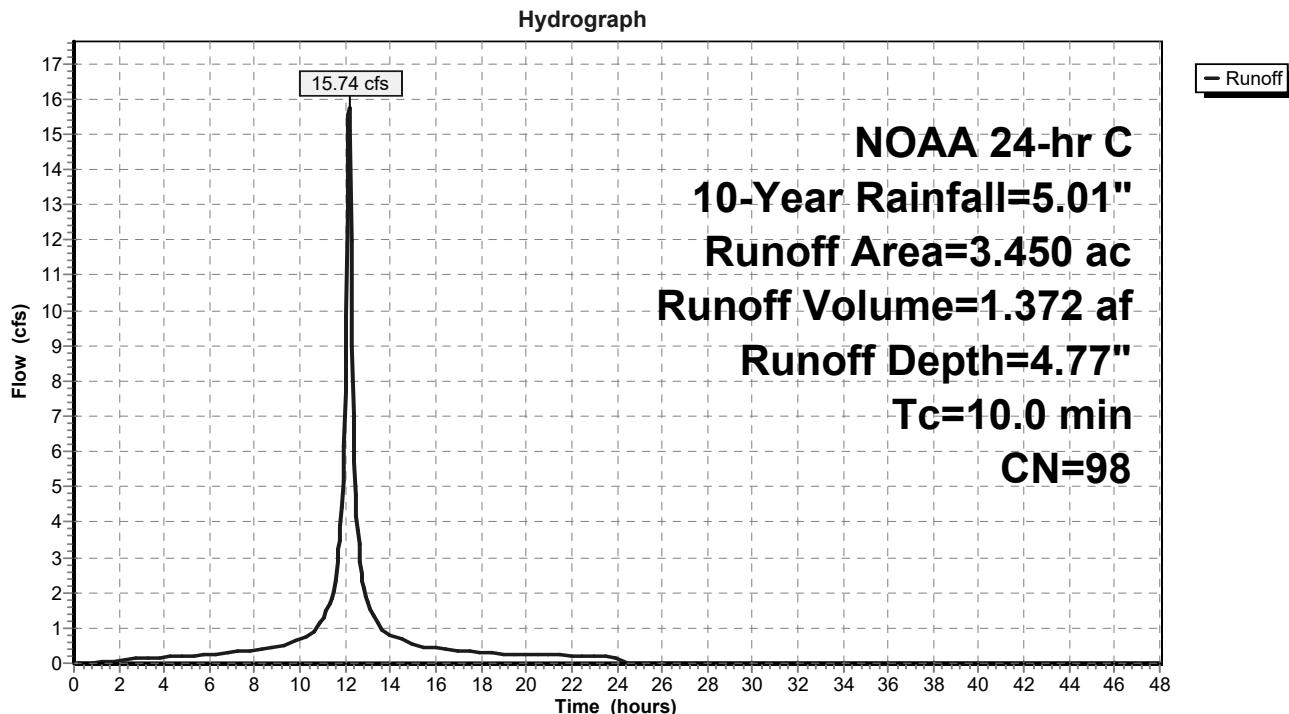
**Summary for Subcatchment 6S: PDA-1-Impervious**

Runoff = 15.74 cfs @ 12.17 hrs, Volume= 1.372 af, Depth= 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
3.450	98	Paved parking, HSG C
3.450		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 6S: PDA-1-Impervious**

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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Subcatchment 7S: PDA-1-Pervious**

Runoff = 1.89 cfs @ 12.18 hrs, Volume= 0.142 af, Depth= 2.37"

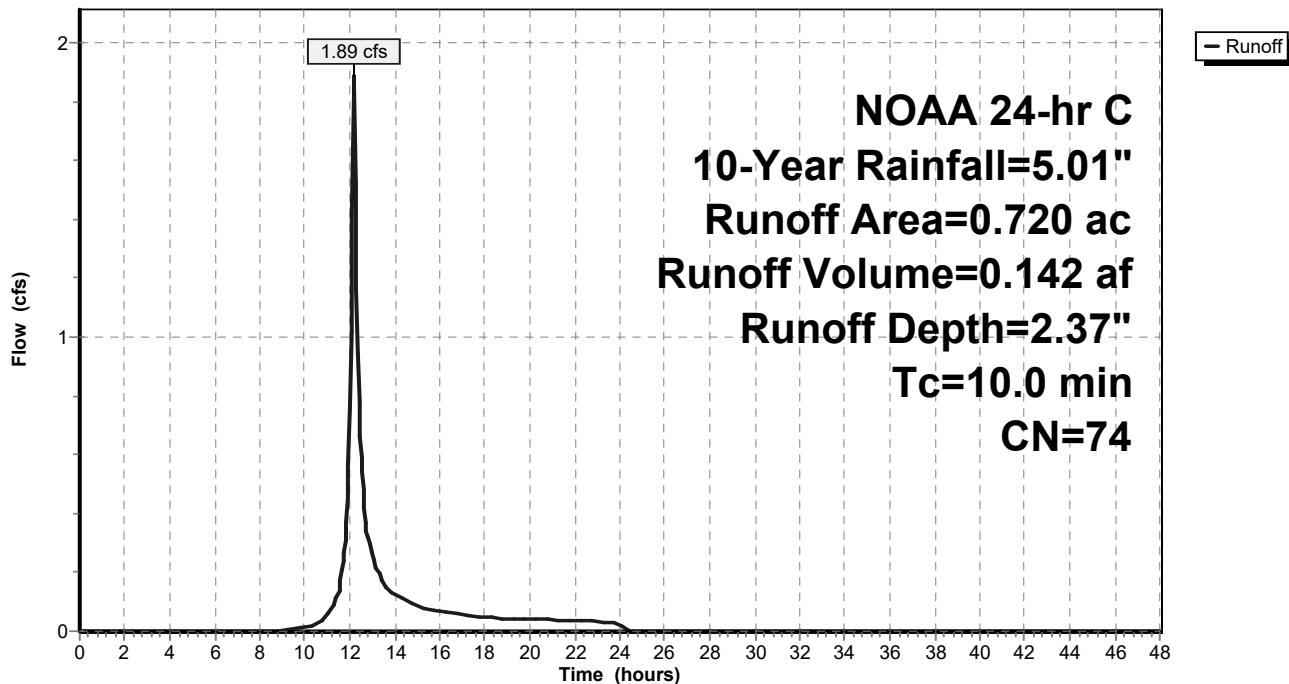
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
0.720	74	>75% Grass cover, Good, HSG C
0.720		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 7S: PDA-1-Pervious**

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Subcatchment 9S: PDA OFF-SITE PERVIOUS**[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 2.20 cfs @ 12.05 hrs, Volume= 0.125 af, Depth= 2.21"

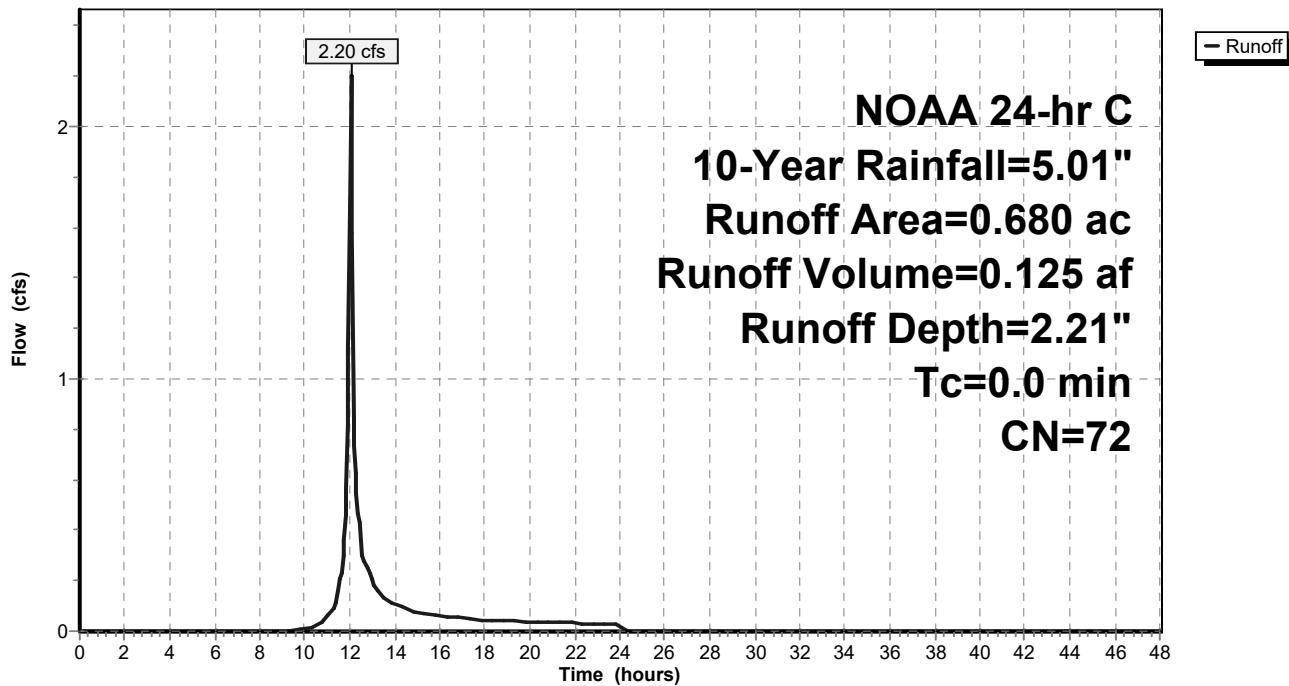
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0				Direct Entry, 10	

**Subcatchment 9S: PDA OFF-SITE PERVIOUS**

Hydrograph



**Summary for Subcatchment 11S: PDA-1 UD A-Impervious**

Runoff = 1.00 cfs @ 12.17 hrs, Volume= 0.088 af, Depth= 4.77"

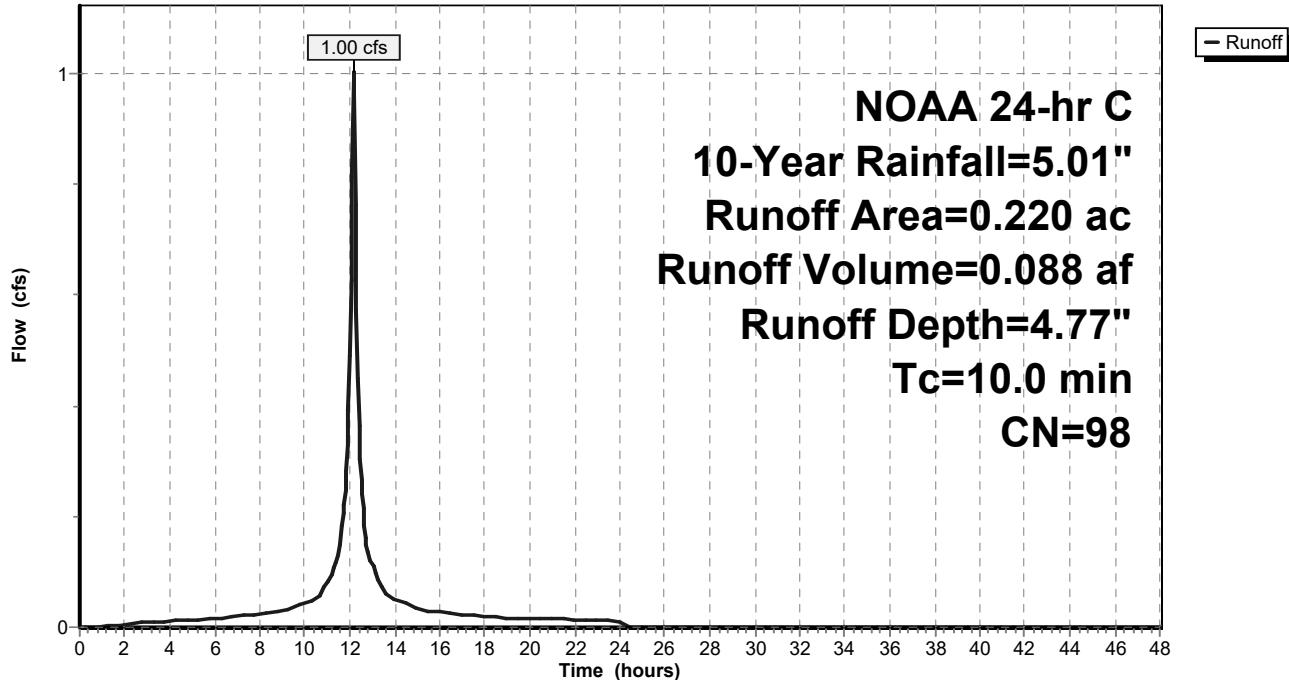
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
0.220	98	Paved parking, HSG C
0.220		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 11S: PDA-1 UD A-Impervious**

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Subcatchment 12S: PDA-1UD A-Pervious**

Runoff = 0.84 cfs @ 12.18 hrs, Volume= 0.063 af, Depth= 2.37"

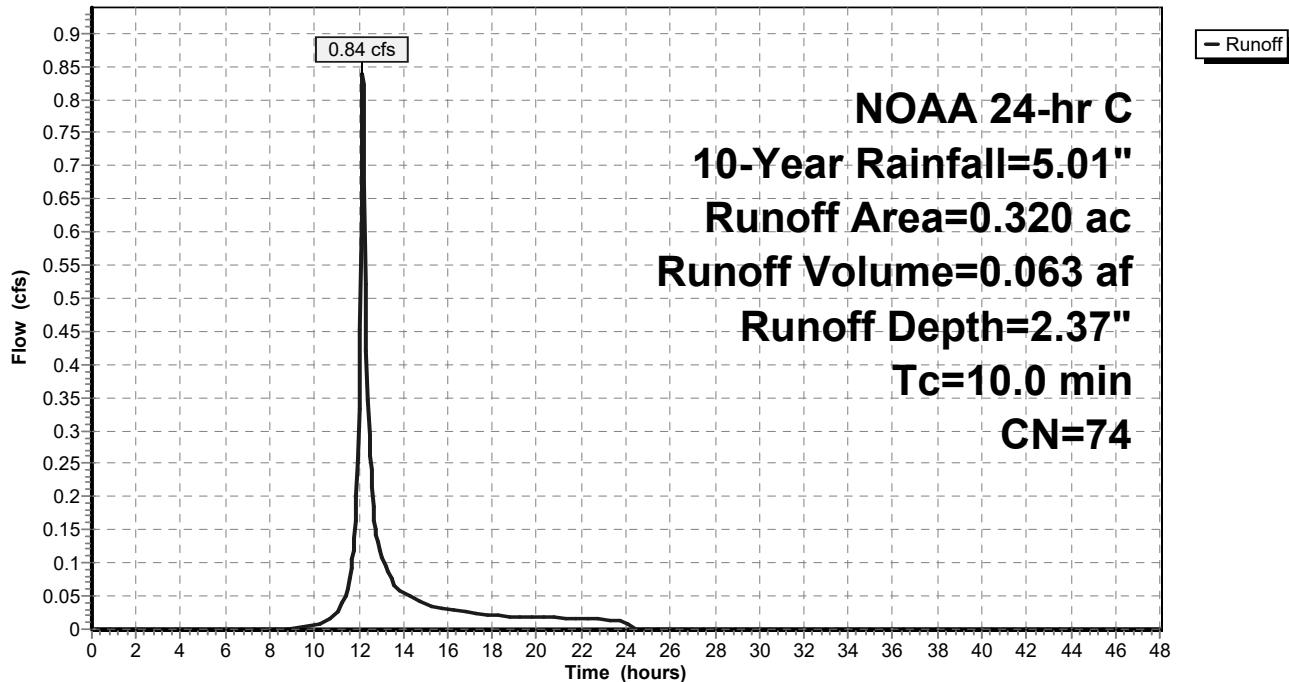
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
0.320	74	>75% Grass cover, Good, HSG C
0.320		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 12S: PDA-1UD A-Pervious**

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Subcatchment 16S: PDA-1UD B-Pervious**

Runoff = 0.26 cfs @ 12.18 hrs, Volume= 0.020 af, Depth= 2.37"

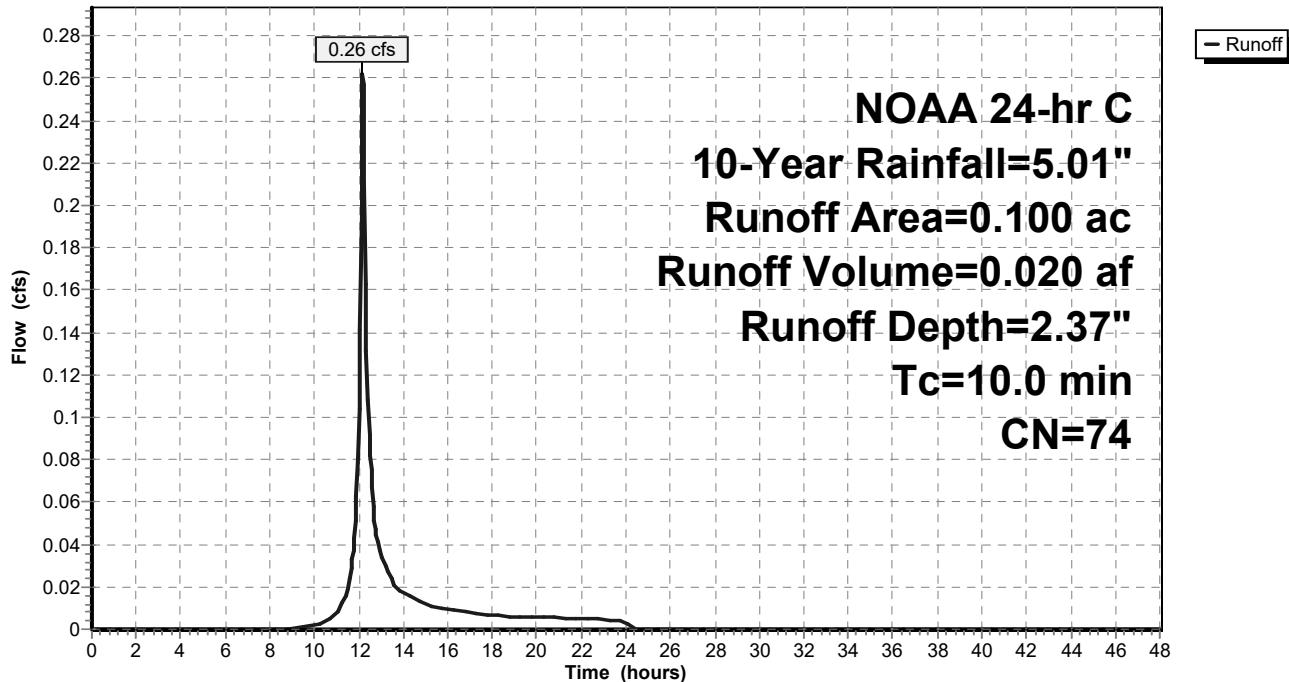
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 10-Year Rainfall=5.01"

Area (ac)	CN	Description
0.100	74	>75% Grass cover, Good, HSG C
0.100		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 16S: PDA-1UD B-Pervious**

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.01"

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**Summary for Pond 8P: WET POND**

Inflow Area = 4.850 ac, 71.13% Impervious, Inflow Depth = 4.06" for 10-Year event  
 Inflow = 18.35 cfs @ 12.17 hrs, Volume= 1.640 af  
 Outflow = 4.12 cfs @ 12.60 hrs, Volume= 1.296 af, Atten= 78%, Lag= 26.1 min  
 Primary = 4.12 cfs @ 12.60 hrs, Volume= 1.296 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
 Peak Elev= 71.60' @ 12.60 hrs Surf.Area= 14,168 sf Storage= 40,025 cf

Plug-Flow detention time= 623.6 min calculated for 1.296 af (79% of inflow)  
 Center-of-Mass det. time= 539.8 min ( 1,307.0 - 767.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	68.50'	60,825 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
68.50	11,408	0	0
69.00	12,104	5,878	5,878
70.00	12,902	12,503	18,381
71.00	13,711	13,307	31,688
72.00	14,475	14,093	45,781
73.00	15,613	15,044	60,825

Device	Routing	Invert	Outlet Devices
#1	Primary	66.50'	<b>15.0" Round Culvert</b> L= 100.0' Ke= 1.000 Inlet / Outlet Invert= 66.50' / 66.00' S= 0.0050 '/' Cc= 0.900 n= 0.015 Concrete sewer w/manholes & inlets, Flow Area= 1.23 sf
#2	Device 1	68.50'	<b>2.5" Vert. Orifice</b> C= 0.600
#3	Device 1	71.15'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)
#4	Device 1	72.90'	<b>48.0" x 42.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=4.12 cfs @ 12.60 hrs HW=71.60' (Free Discharge)

↑ 1=Culvert (Passes 4.12 cfs of 9.09 cfs potential flow)

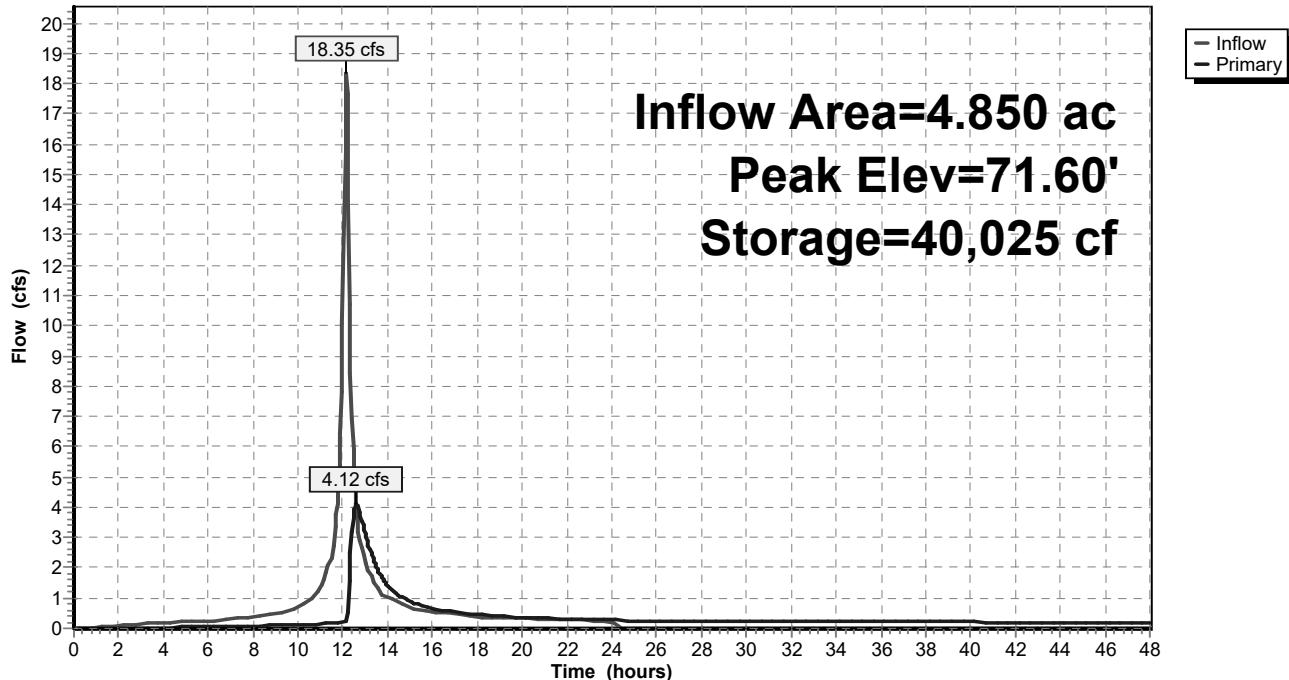
↑ 2=Orifice (Orifice Controls 0.28 cfs @ 8.33 fps)

↑ 3=Sharp-Crested Rectangular Weir (Weir Controls 3.83 cfs @ 2.19 fps)

↑ 4=Grate (Controls 0.00 cfs)

**Pond 8P: WET POND**

Hydrograph



**Summary for Link 10L: PDA - 1**

Inflow Area = 4.170 ac, 82.73% Impervious, Inflow Depth = 4.36" for 10-Year event

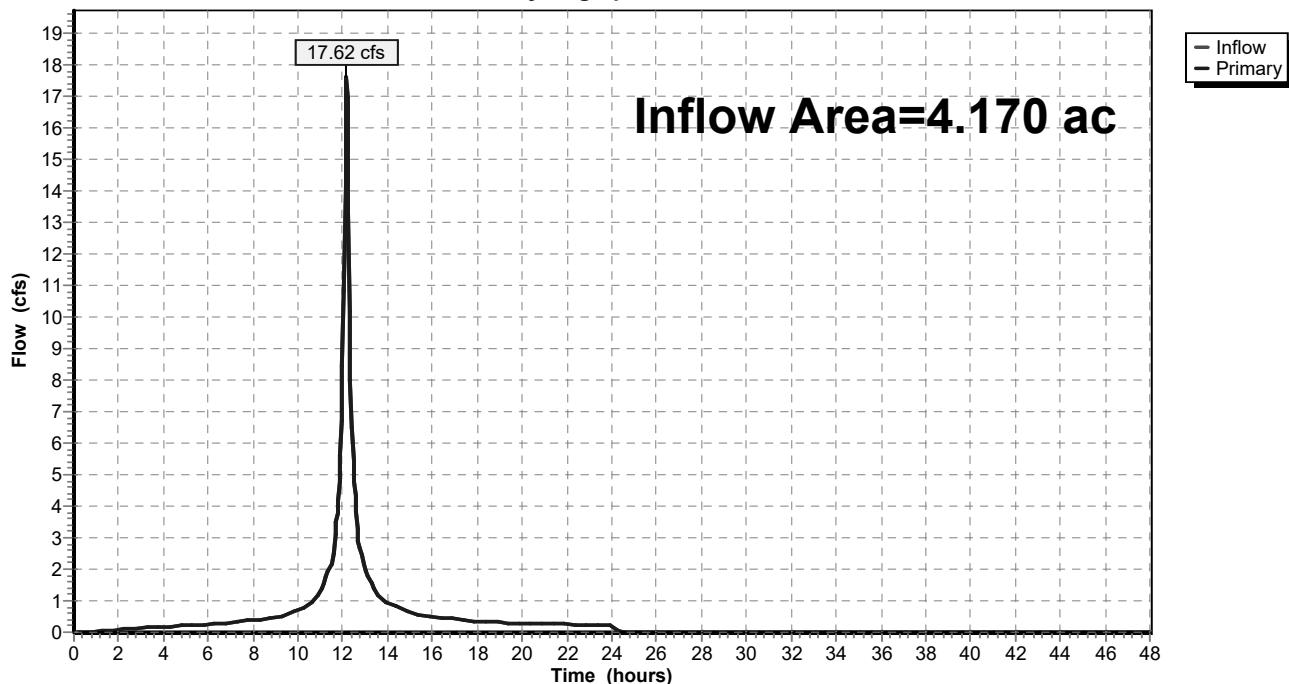
Inflow = 17.62 cfs @ 12.17 hrs, Volume= 1.515 af

Primary = 17.62 cfs @ 12.17 hrs, Volume= 1.515 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 10L: PDA - 1**

Hydrograph



**Summary for Link 13L: PDA-1 UD A**

Inflow Area = 0.540 ac, 40.74% Impervious, Inflow Depth = 3.35" for 10-Year event

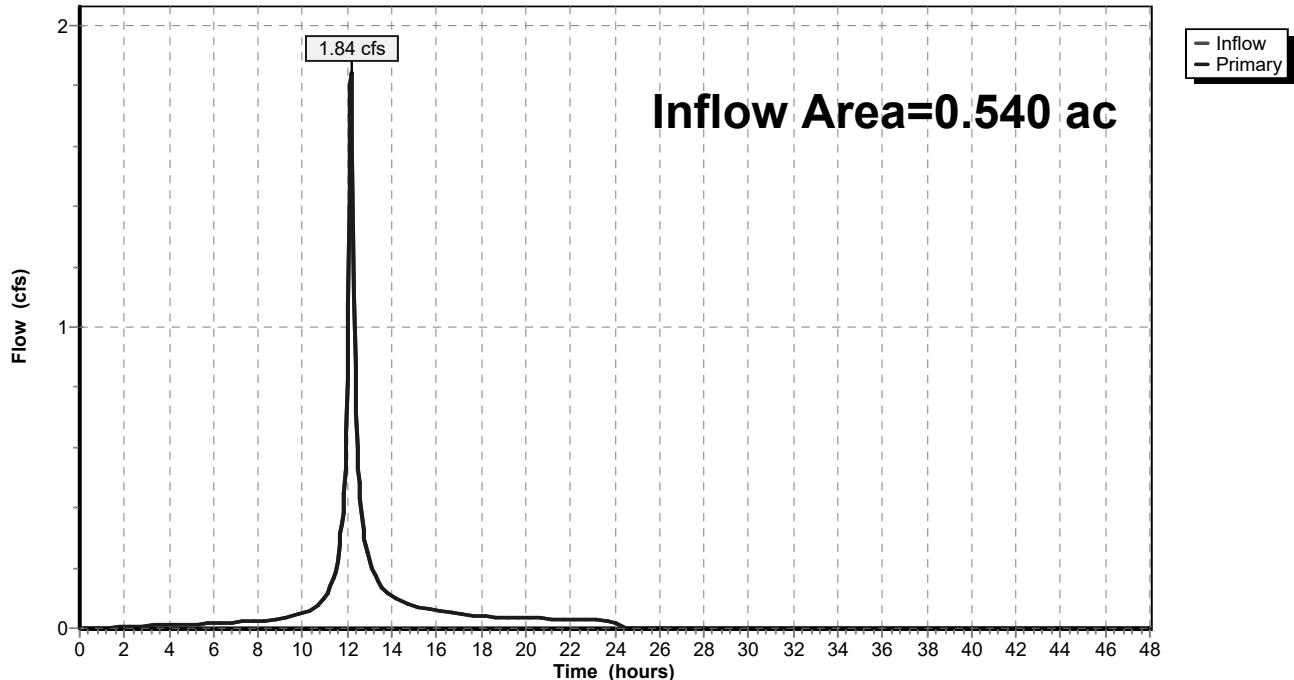
Inflow = 1.84 cfs @ 12.17 hrs, Volume= 0.151 af

Primary = 1.84 cfs @ 12.17 hrs, Volume= 0.151 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 13L: PDA-1 UD A**

Hydrograph



**Summary for Link 14L: OVERALL SITE**

Inflow Area = 5.490 ac, 66.85% Impervious, Inflow Depth > 3.20" for 10-Year event

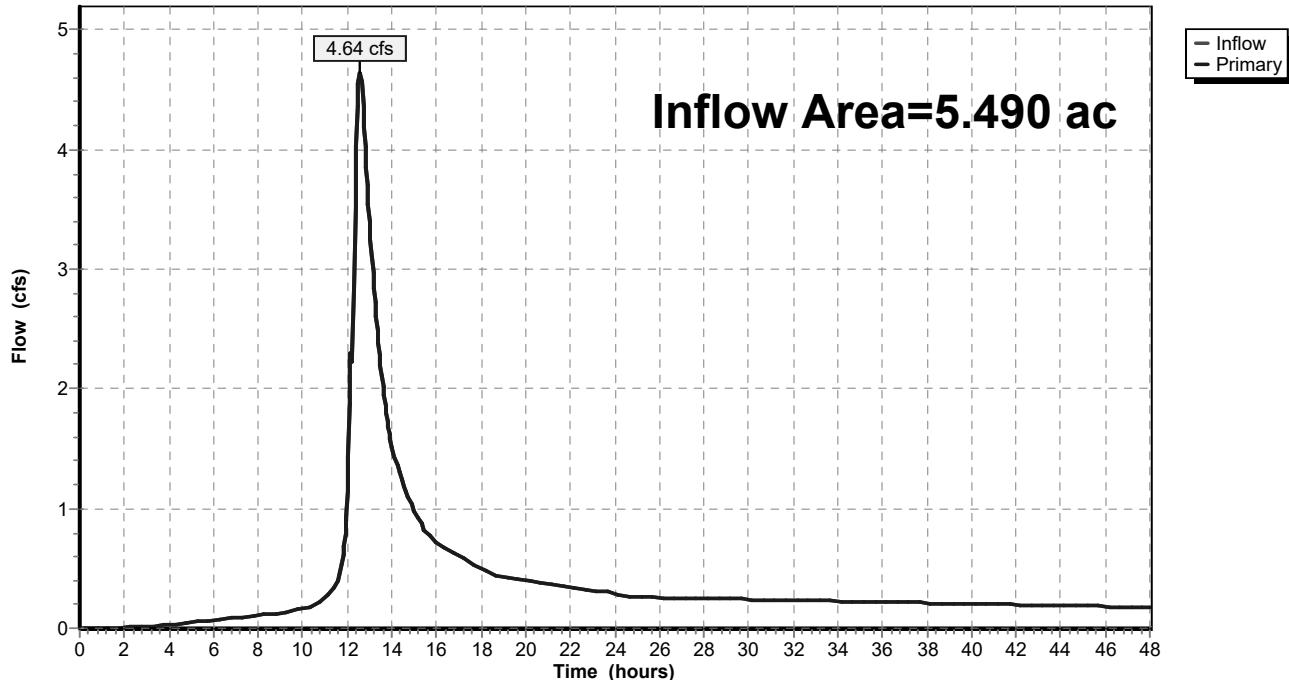
Inflow = 4.64 cfs @ 12.57 hrs, Volume= 1.466 af

Primary = 4.64 cfs @ 12.57 hrs, Volume= 1.466 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 14L: OVERALL SITE**

Hydrograph



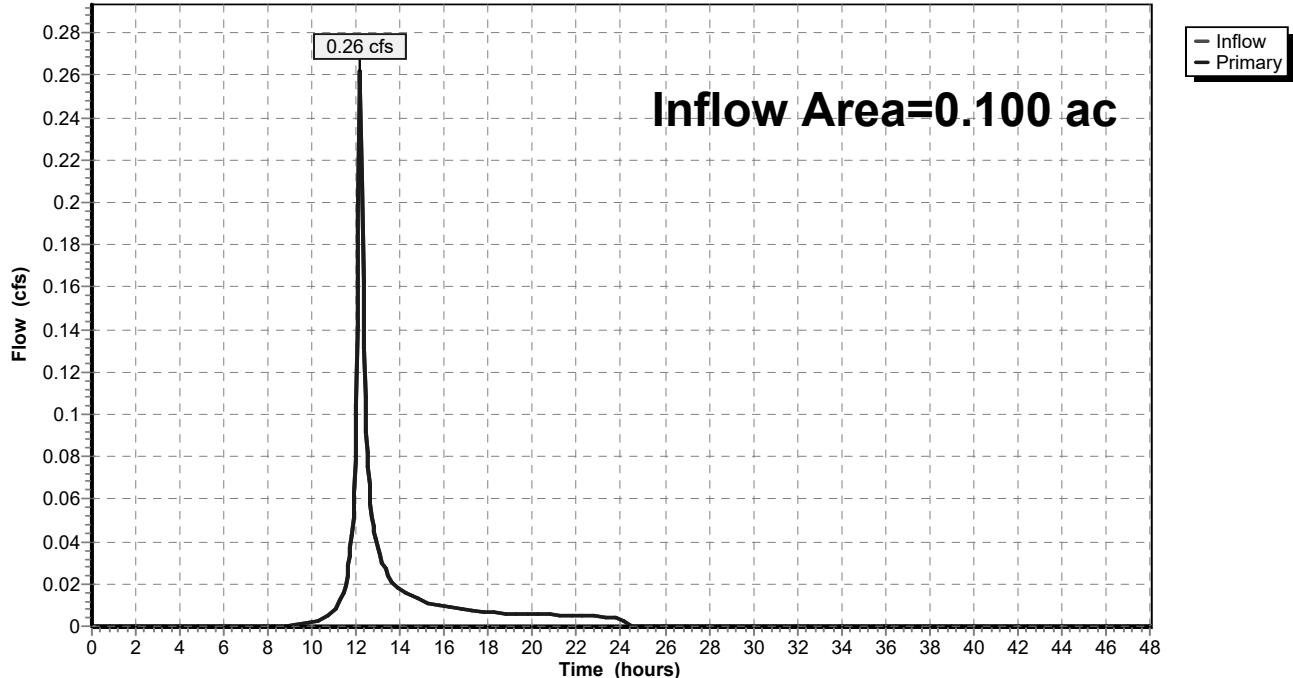
**Summary for Link 17L: PDA-1 UD B**

Inflow Area = 0.100 ac, 0.00% Impervious, Inflow Depth = 2.37" for 10-Year event  
Inflow = 0.26 cfs @ 12.18 hrs, Volume= 0.020 af  
Primary = 0.26 cfs @ 12.18 hrs, Volume= 0.020 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 17L: PDA-1 UD B**

Hydrograph



**Summary for Link 18L: TOTAL PDA-1 UD**

Inflow Area = 0.640 ac, 34.38% Impervious, Inflow Depth = 3.20" for 10-Year event

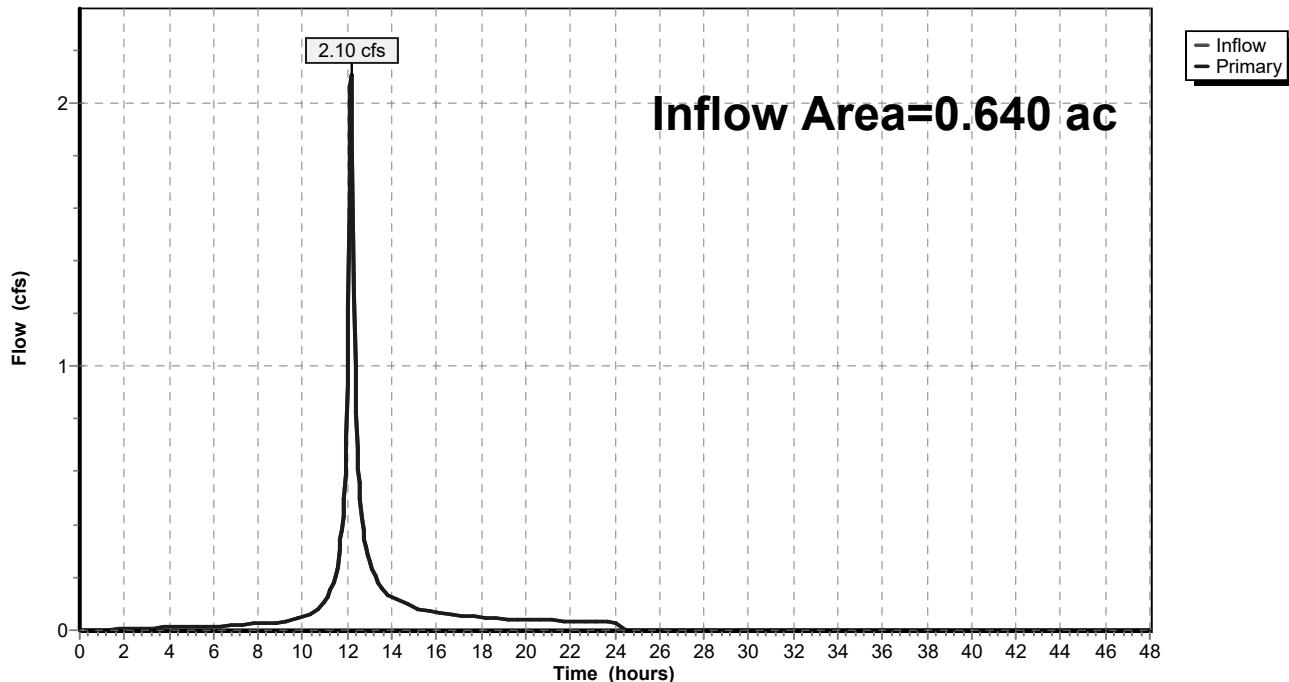
Inflow = 2.10 cfs @ 12.17 hrs, Volume= 0.171 af

Primary = 2.10 cfs @ 12.17 hrs, Volume= 0.171 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 18L: TOTAL PDA-1 UD**

Hydrograph



Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment6S: PDA-1-Impervious</b>	Runoff Area=3.450 ac 100.00% Impervious Runoff Depth=5.95" Tc=10.0 min CN=98 Runoff=19.48 cfs 1.711 af
<b>Subcatchment7S: PDA-1-Pervious</b>	Runoff Area=0.720 ac 0.00% Impervious Runoff Depth=3.35" Tc=10.0 min CN=74 Runoff=2.66 cfs 0.201 af
<b>Subcatchment9S: PDA OFF-SITE PERVIOUS</b>	Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=3.15" Tc=0.0 min CN=72 Runoff=3.14 cfs 0.178 af
<b>Subcatchment11S: PDA-1 UD</b>	Runoff Area=0.220 ac 100.00% Impervious Runoff Depth=5.95" Tc=10.0 min CN=98 Runoff=1.24 cfs 0.109 af
<b>Subcatchment12S: PDA-1UDA-Pervious</b>	Runoff Area=0.320 ac 0.00% Impervious Runoff Depth=3.35" Tc=10.0 min CN=74 Runoff=1.18 cfs 0.089 af
<b>Subcatchment16S: PDA-1UDB-Pervious</b>	Runoff Area=0.100 ac 0.00% Impervious Runoff Depth=3.35" Tc=10.0 min CN=74 Runoff=0.37 cfs 0.028 af
<b>Pond 8P: WET POND</b>	Peak Elev=71.96' Storage=45,216 cf Inflow=23.16 cfs 2.090 af Outflow=9.41 cfs 1.742 af
<b>Link 10L: PDA - 1</b>	Inflow=22.14 cfs 1.912 af Primary=22.14 cfs 1.912 af
<b>Link 13L: PDA-1 UD A</b>	Inflow=2.43 cfs 0.198 af Primary=2.43 cfs 0.198 af
<b>Link 14L: OVERALL SITE</b>	Inflow=10.64 cfs 1.968 af Primary=10.64 cfs 1.968 af
<b>Link 17L: PDA-1 UD B</b>	Inflow=0.37 cfs 0.028 af Primary=0.37 cfs 0.028 af
<b>Link 18L: TOTAL PDA-1 UD</b>	Inflow=2.80 cfs 0.226 af Primary=2.80 cfs 0.226 af

**Total Runoff Area = 5.490 ac Runoff Volume = 2.316 af Average Runoff Depth = 5.06"**  
**33.15% Pervious = 1.820 ac 66.85% Impervious = 3.670 ac**

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NOAA 24-hr C 25-Year Rainfall=6.19"

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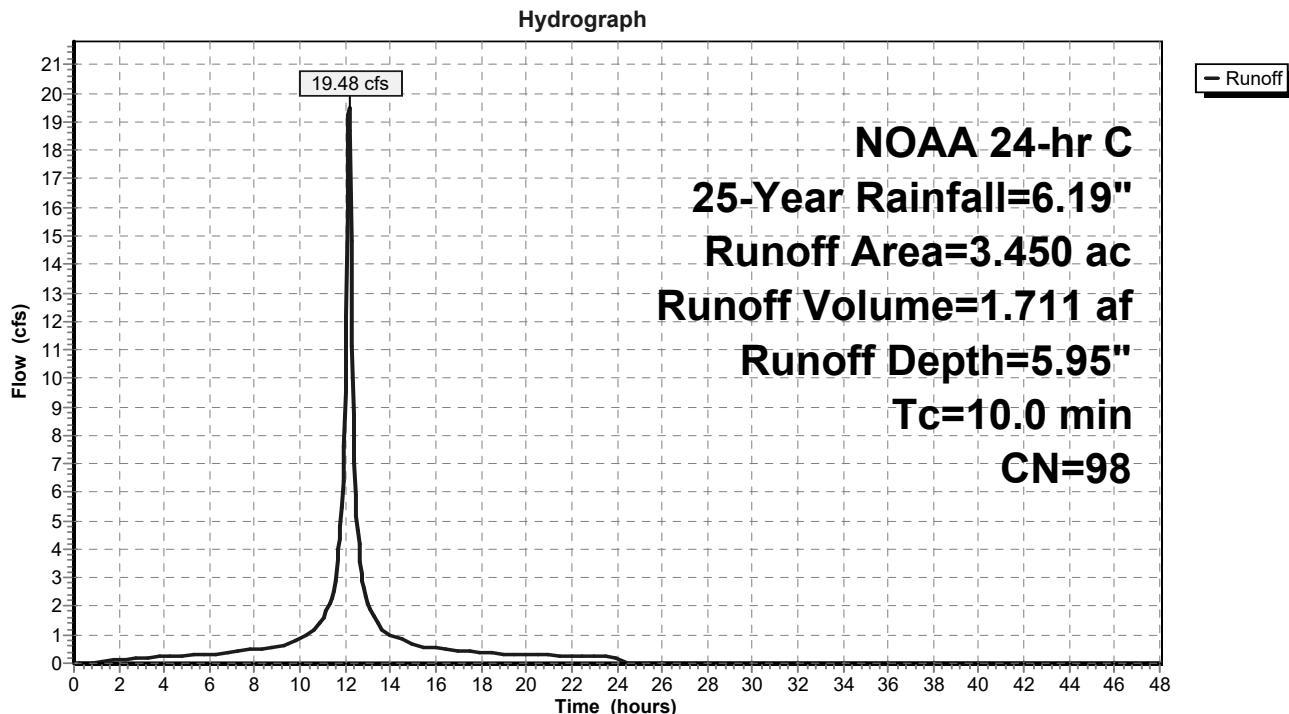
**Summary for Subcatchment 6S: PDA-1-Impervious**

Runoff = 19.48 cfs @ 12.17 hrs, Volume= 1.711 af, Depth= 5.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
3.450	98	Paved parking, HSG C
3.450		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 6S: PDA-1-Impervious**

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NOAA 24-hr C 25-Year Rainfall=6.19"

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**Summary for Subcatchment 7S: PDA-1-Pervious**

Runoff = 2.66 cfs @ 12.18 hrs, Volume= 0.201 af, Depth= 3.35"

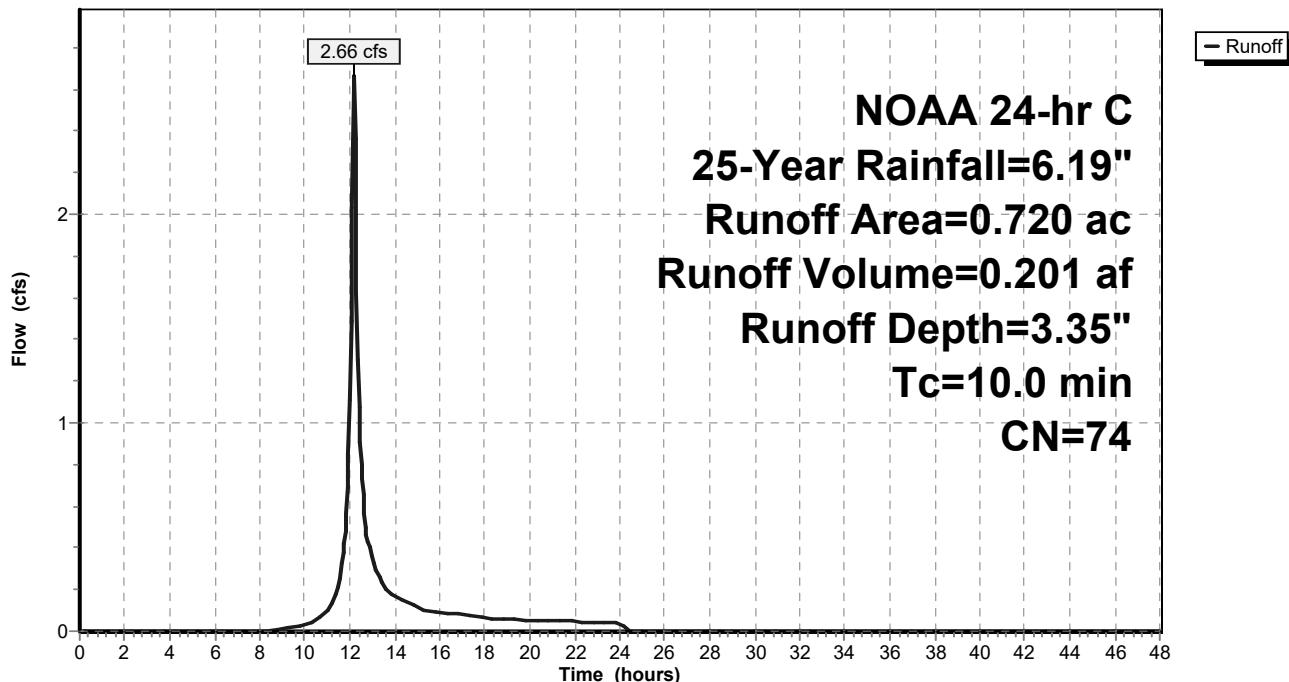
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
0.720	74	>75% Grass cover, Good, HSG C
0.720		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 7S: PDA-1-Pervious**

Hydrograph



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NOAA 24-hr C 25-Year Rainfall=6.19"

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**Summary for Subcatchment 9S: PDA OFF-SITE PERVIOUS**[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 3.14 cfs @ 12.05 hrs, Volume= 0.178 af, Depth= 3.15"

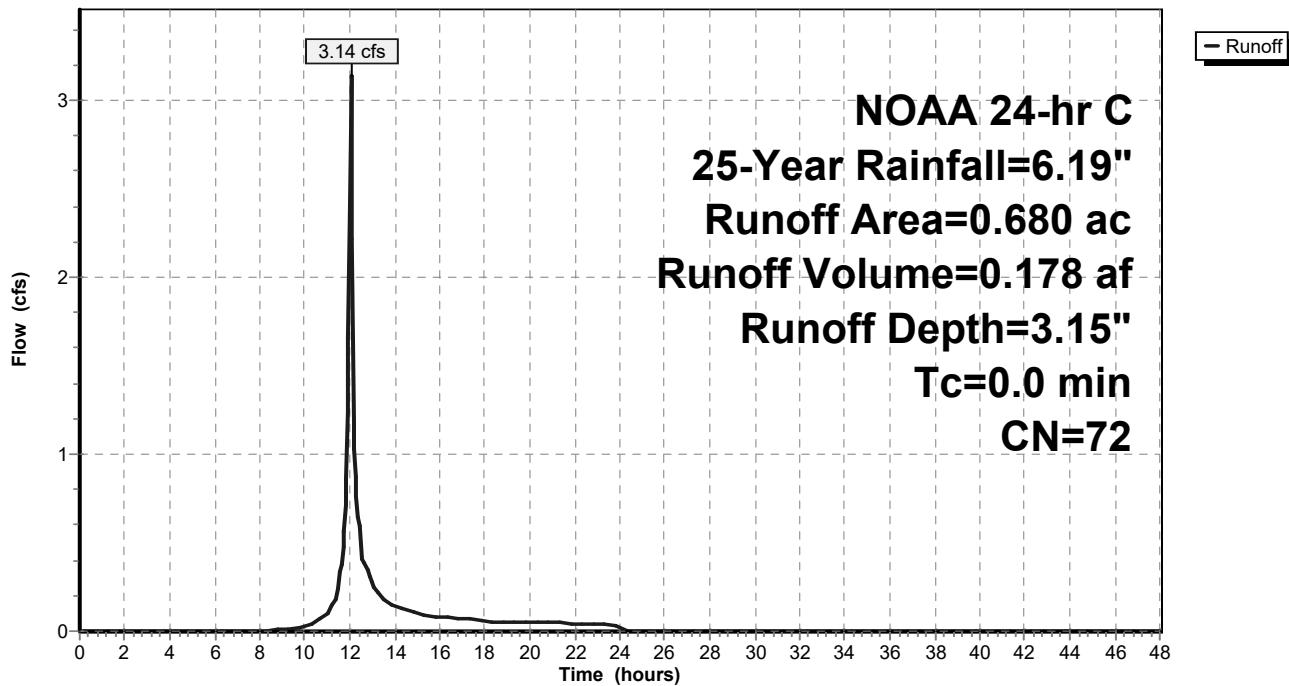
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0				Direct Entry, 10	

**Subcatchment 9S: PDA OFF-SITE PERVIOUS**

Hydrograph



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NOAA 24-hr C 25-Year Rainfall=6.19"

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**Summary for Subcatchment 11S: PDA-1 UD A-Impervious**

Runoff = 1.24 cfs @ 12.17 hrs, Volume= 0.109 af, Depth= 5.95"

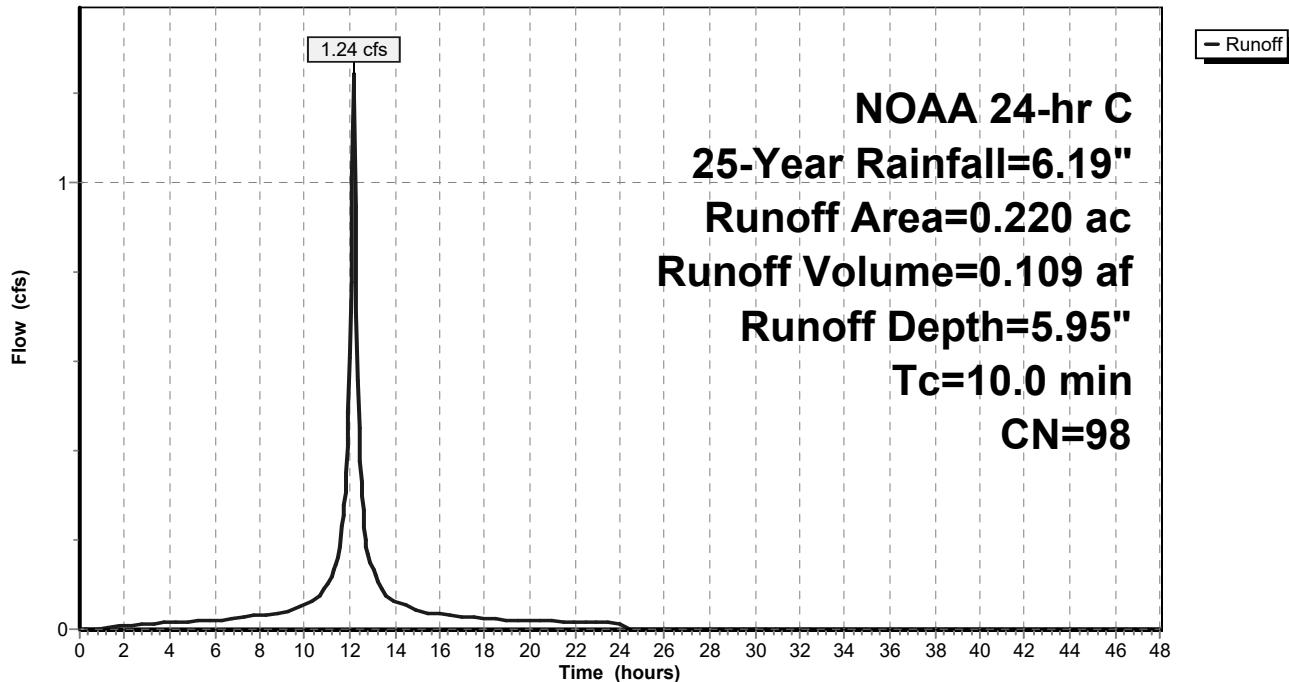
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
0.220	98	Paved parking, HSG C
0.220		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 11S: PDA-1 UD A-Impervious**

Hydrograph



**Summary for Subcatchment 12S: PDA-1UD A-Pervious**

Runoff = 1.18 cfs @ 12.18 hrs, Volume= 0.089 af, Depth= 3.35"

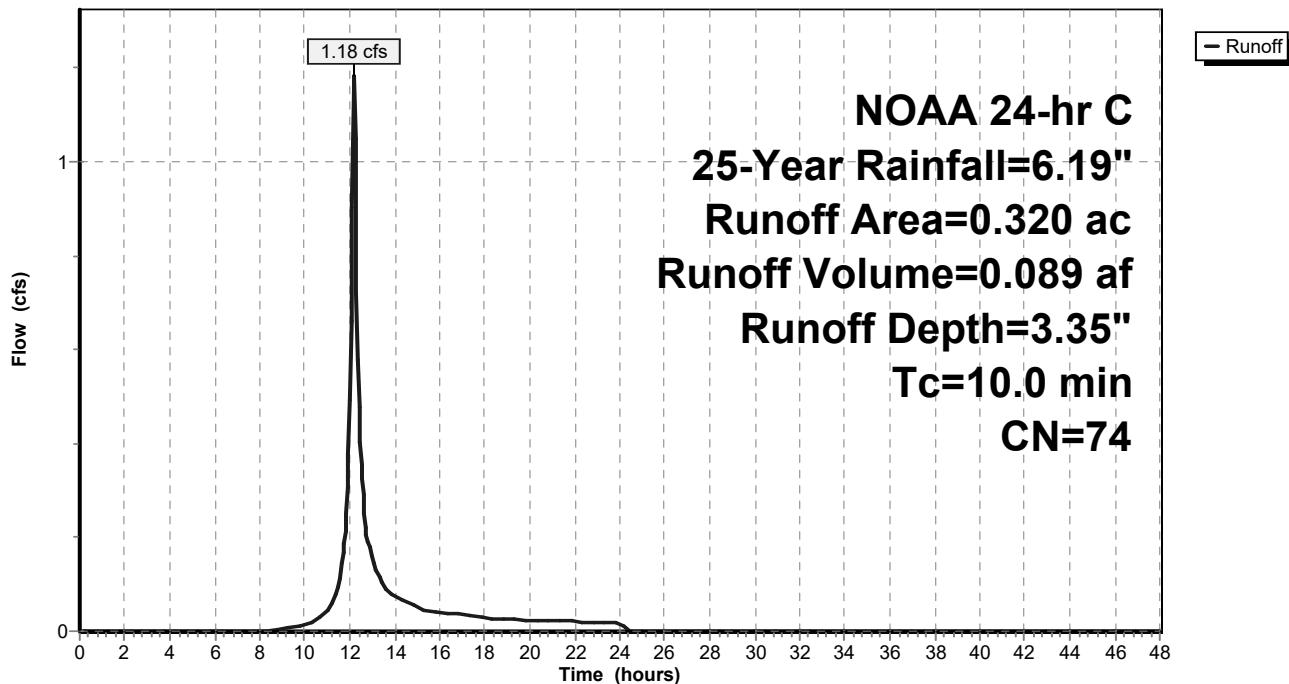
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
0.320	74	>75% Grass cover, Good, HSG C
0.320		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 12S: PDA-1UD A-Pervious**

Hydrograph



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NOAA 24-hr C 25-Year Rainfall=6.19"

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**Summary for Subcatchment 16S: PDA-1UD B-Pervious**

Runoff = 0.37 cfs @ 12.18 hrs, Volume= 0.028 af, Depth= 3.35"

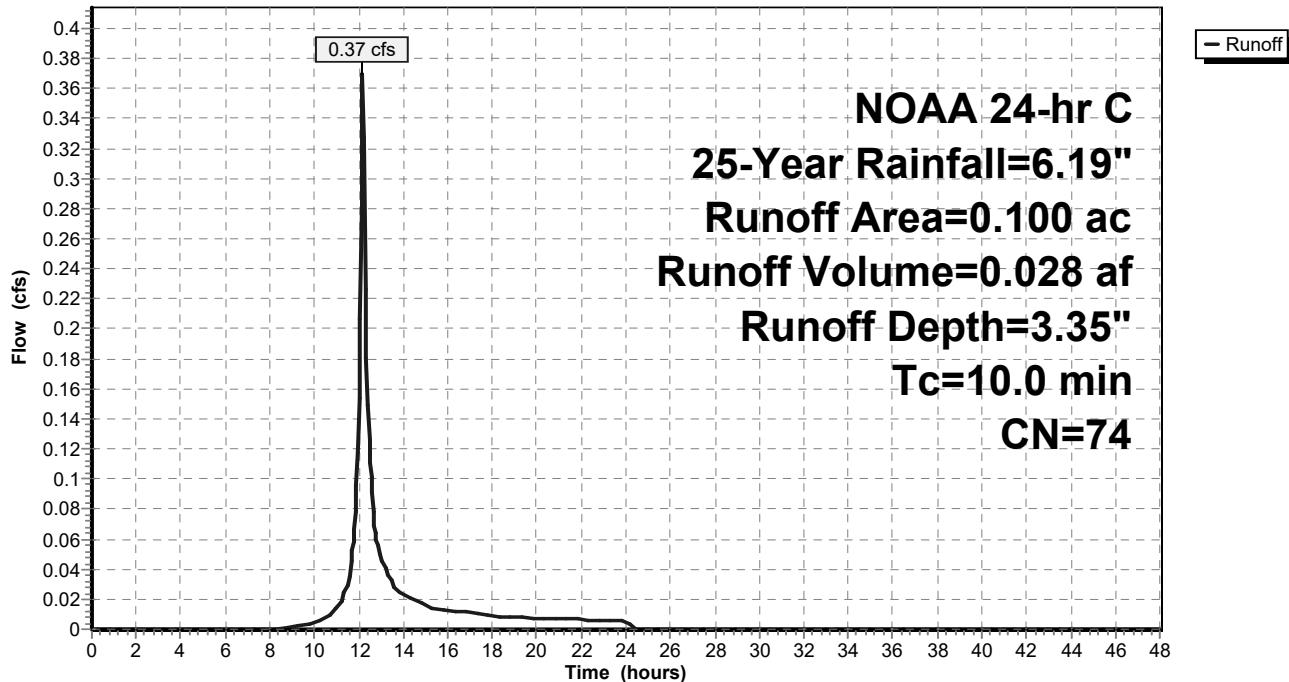
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 25-Year Rainfall=6.19"

Area (ac)	CN	Description
0.100	74	>75% Grass cover, Good, HSG C
0.100		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 16S: PDA-1UD B-Pervious**

Hydrograph



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NOAA 24-hr C 25-Year Rainfall=6.19"

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**Summary for Pond 8P: WET POND**

Inflow Area = 4.850 ac, 71.13% Impervious, Inflow Depth = 5.17" for 25-Year event  
 Inflow = 23.16 cfs @ 12.17 hrs, Volume= 2.090 af  
 Outflow = 9.41 cfs @ 12.39 hrs, Volume= 1.742 af, Atten= 59%, Lag= 13.3 min  
 Primary = 9.41 cfs @ 12.39 hrs, Volume= 1.742 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
 Peak Elev= 71.96' @ 12.39 hrs Surf.Area= 14,445 sf Storage= 45,216 cf

Plug-Flow detention time= 492.4 min calculated for 1.742 af (83% of inflow)  
 Center-of-Mass det. time= 418.8 min ( 1,183.0 - 764.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	68.50'	60,825 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
68.50	11,408	0	0
69.00	12,104	5,878	5,878
70.00	12,902	12,503	18,381
71.00	13,711	13,307	31,688
72.00	14,475	14,093	45,781
73.00	15,613	15,044	60,825

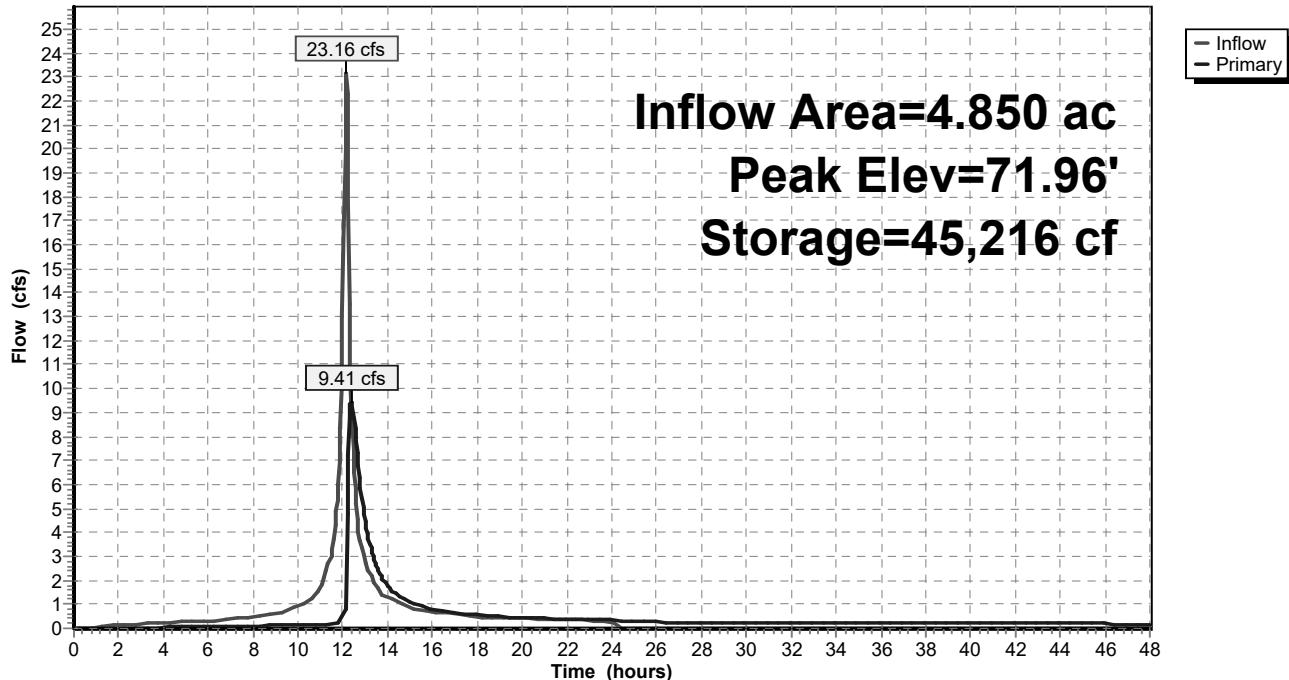
Device	Routing	Invert	Outlet Devices
#1	Primary	66.50'	<b>15.0" Round Culvert</b> L= 100.0' Ke= 1.000 Inlet / Outlet Invert= 66.50' / 66.00' S= 0.0050 '/' Cc= 0.900 n= 0.015 Concrete sewer w/manholes & inlets, Flow Area= 1.23 sf
#2	Device 1	68.50'	<b>2.5" Vert. Orifice</b> C= 0.600
#3	Device 1	71.15'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)
#4	Device 1	72.90'	<b>48.0" x 42.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=9.44 cfs @ 12.39 hrs HW=71.96' (Free Discharge)

- ↑ 1=Culvert (Passes 9.44 cfs of 9.46 cfs potential flow)
- 2=Orifice (Orifice Controls 0.30 cfs @ 8.82 fps)
- 3=Sharp-Crested Rectangular Weir (Weir Controls 9.14 cfs @ 2.94 fps)
- 4=Grate (Controls 0.00 cfs)

**Pond 8P: WET POND**

Hydrograph



**Summary for Link 10L: PDA - 1**

Inflow Area = 4.170 ac, 82.73% Impervious, Inflow Depth = 5.50" for 25-Year event

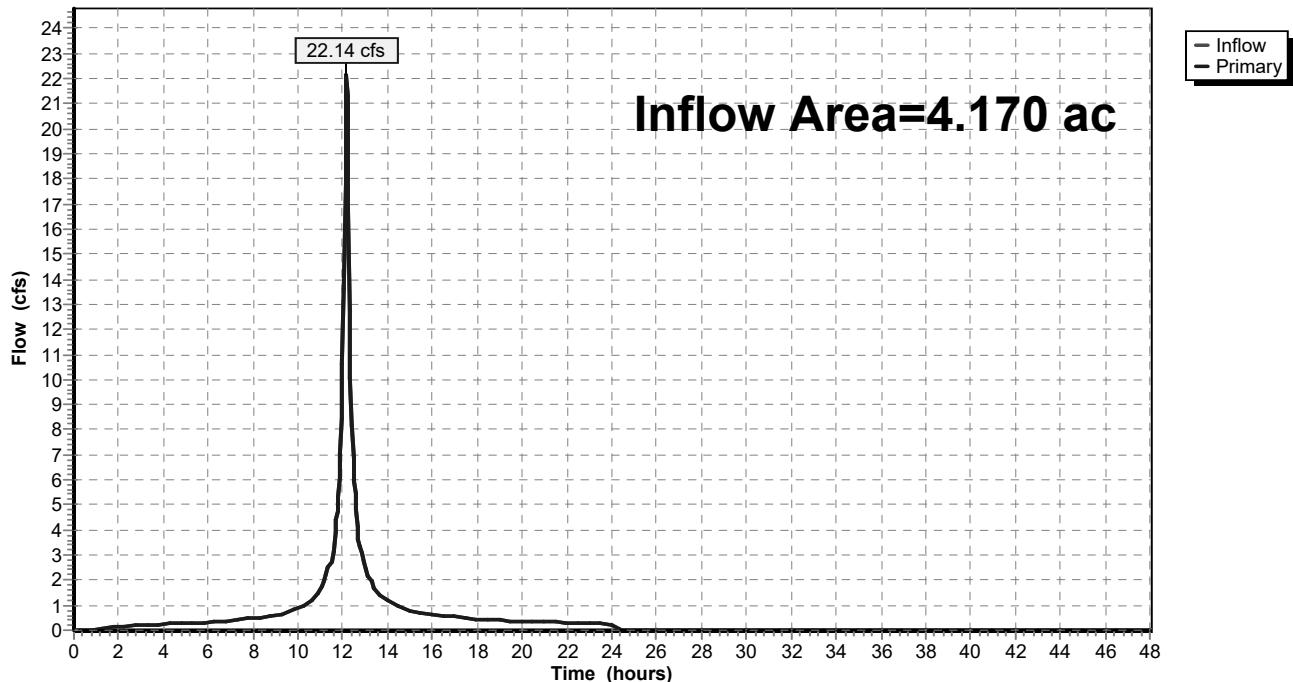
Inflow = 22.14 cfs @ 12.17 hrs, Volume= 1.912 af

Primary = 22.14 cfs @ 12.17 hrs, Volume= 1.912 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 10L: PDA - 1**

Hydrograph



**Summary for Link 13L: PDA-1 UD A**

Inflow Area = 0.540 ac, 40.74% Impervious, Inflow Depth = 4.41" for 25-Year event

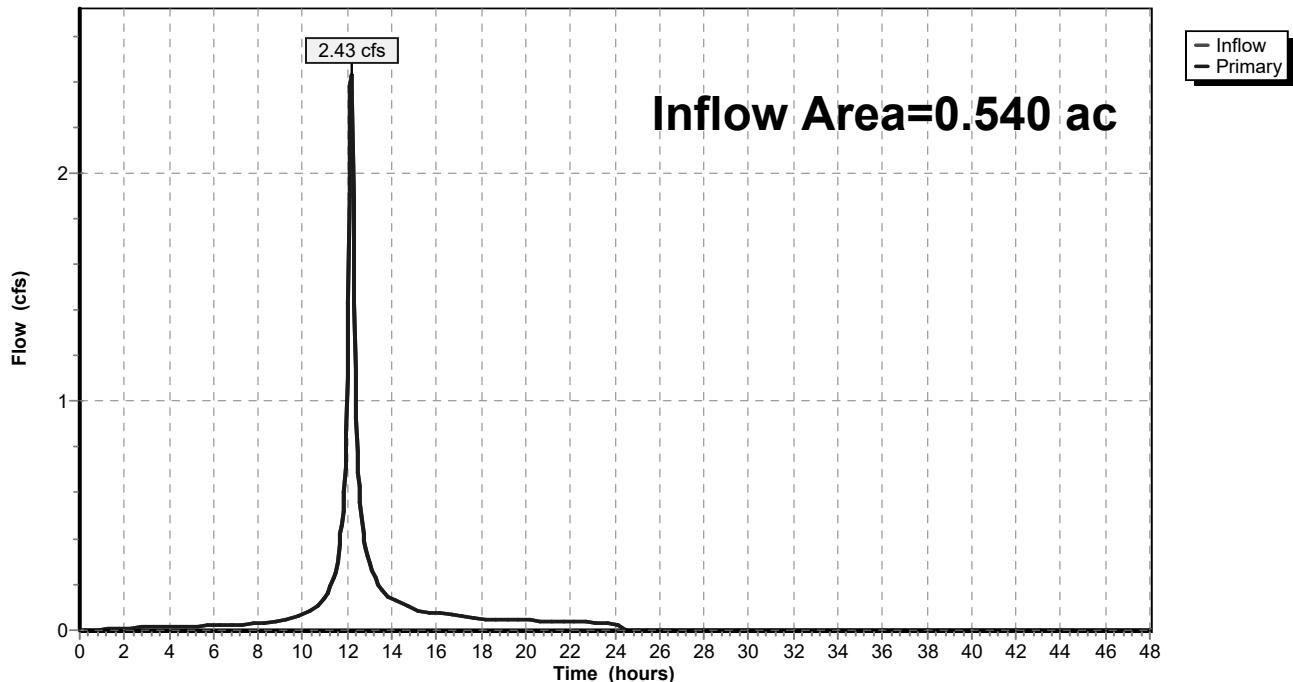
Inflow = 2.43 cfs @ 12.17 hrs, Volume= 0.198 af

Primary = 2.43 cfs @ 12.17 hrs, Volume= 0.198 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 13L: PDA-1 UD A**

Hydrograph



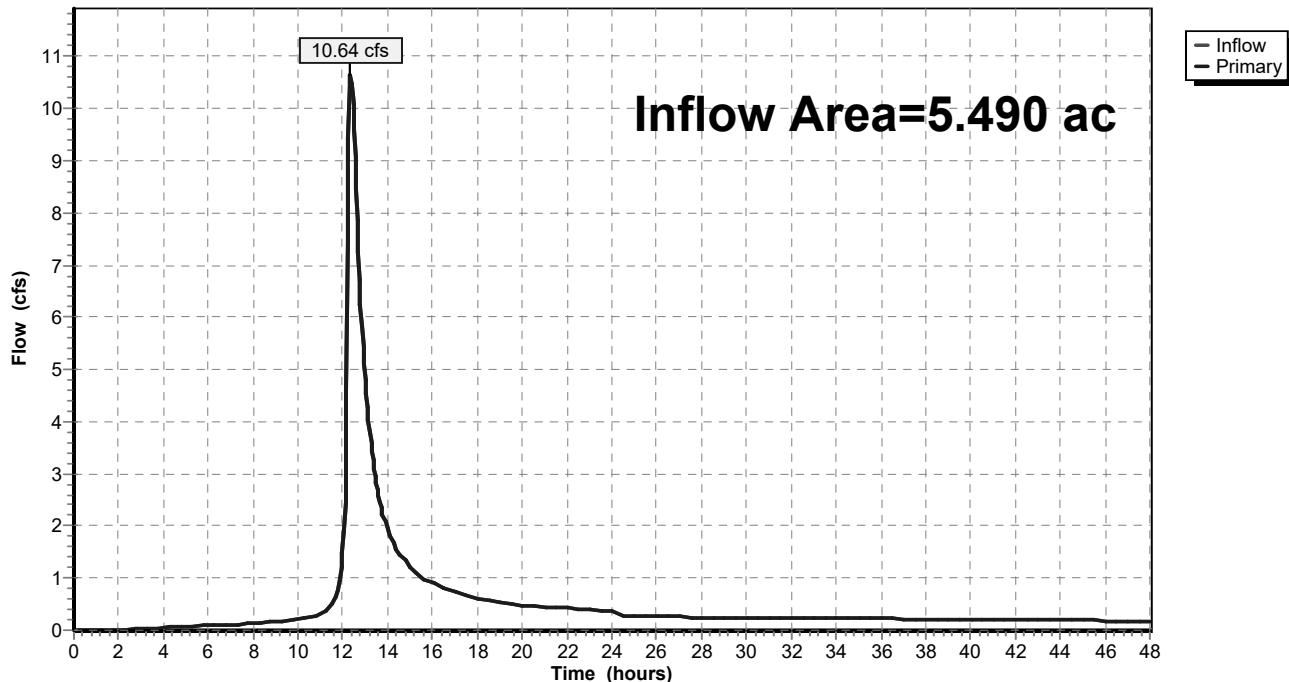
**Summary for Link 14L: OVERALL SITE**

Inflow Area = 5.490 ac, 66.85% Impervious, Inflow Depth > 4.30" for 25-Year event

Inflow = 10.64 cfs @ 12.35 hrs, Volume= 1.968 af

Primary = 10.64 cfs @ 12.35 hrs, Volume= 1.968 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 14L: OVERALL SITE****Hydrograph**

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NOAA 24-hr C 25-Year Rainfall=6.19"

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**Summary for Link 17L: PDA-1 UD B**

Inflow Area = 0.100 ac, 0.00% Impervious, Inflow Depth = 3.35" for 25-Year event

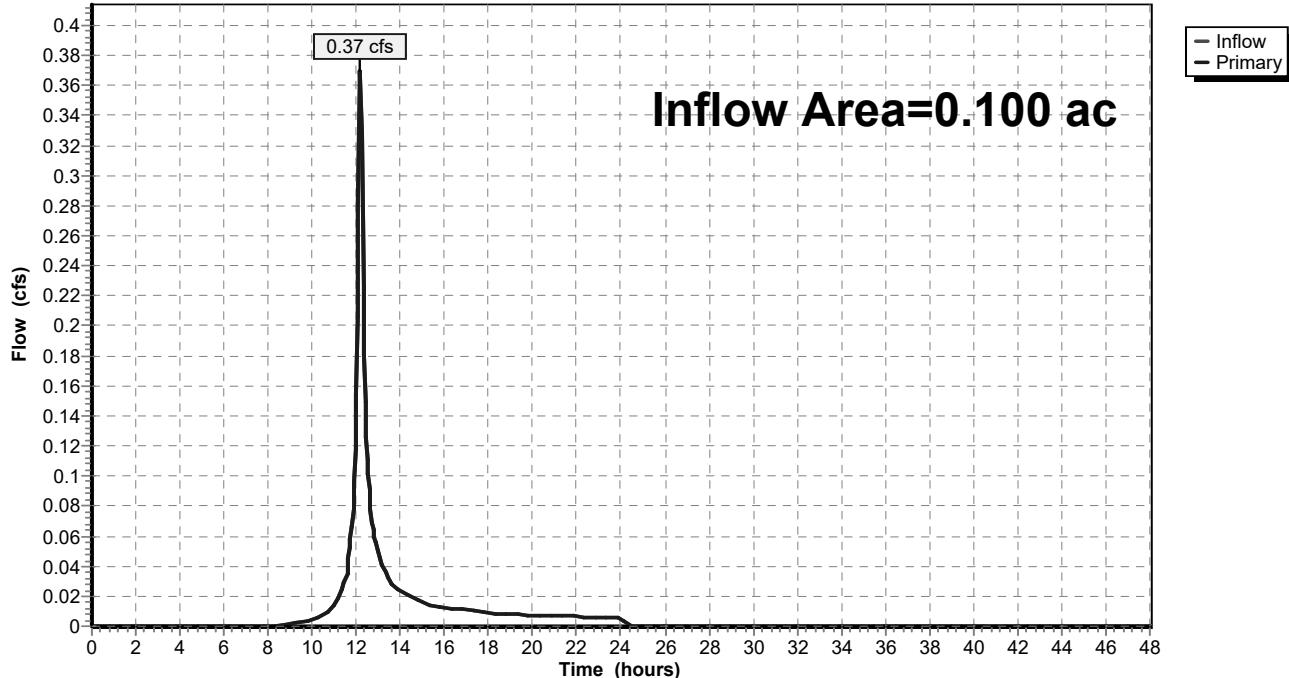
Inflow = 0.37 cfs @ 12.18 hrs, Volume= 0.028 af

Primary = 0.37 cfs @ 12.18 hrs, Volume= 0.028 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 17L: PDA-1 UD B**

Hydrograph



**Summary for Link 18L: TOTAL PDA-1 UD**

Inflow Area = 0.640 ac, 34.38% Impervious, Inflow Depth = 4.24" for 25-Year event

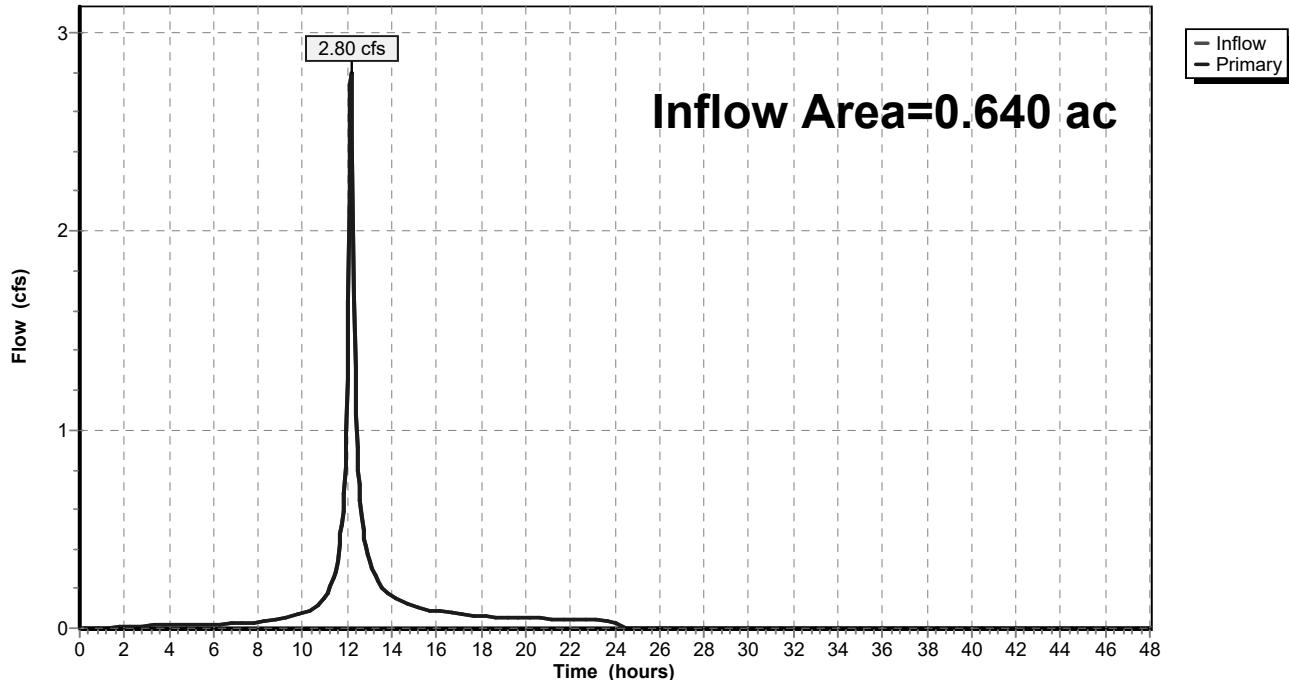
Inflow = 2.80 cfs @ 12.17 hrs, Volume= 0.226 af

Primary = 2.80 cfs @ 12.17 hrs, Volume= 0.226 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 18L: TOTAL PDA-1 UD**

Hydrograph



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NOAA 24-hr C 100-Year Rainfall=8.21"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment6S: PDA-1-Impervious** Runoff Area=3.450 ac 100.00% Impervious Runoff Depth=7.97"  
Tc=10.0 min CN=98 Runoff=25.88 cfs 2.291 af**Subcatchment7S: PDA-1-Pervious** Runoff Area=0.720 ac 0.00% Impervious Runoff Depth=5.11"  
Tc=10.0 min CN=74 Runoff=4.04 cfs 0.307 af**Subcatchment9S: PDA OFF-SITE PERVIOUS** Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=4.88"  
Tc=0.0 min CN=72 Runoff=4.81 cfs 0.276 af**Subcatchment11S: PDA-1 UD** Runoff Area=0.220 ac 100.00% Impervious Runoff Depth=7.97"  
Tc=10.0 min CN=98 Runoff=1.65 cfs 0.146 af**Subcatchment12S: PDA-1UDA-Pervious** Runoff Area=0.320 ac 0.00% Impervious Runoff Depth=5.11"  
Tc=10.0 min CN=74 Runoff=1.80 cfs 0.136 af**Subcatchment16S: PDA-1UDB-Pervious** Runoff Area=0.100 ac 0.00% Impervious Runoff Depth=5.11"  
Tc=10.0 min CN=74 Runoff=0.56 cfs 0.043 af**Pond 8P: WET POND** Peak Elev=72.89' Storage=59,183 cf Inflow=31.45 cfs 2.875 af  
Outflow=10.36 cfs 2.522 af**Link 10L: PDA - 1** Inflow=29.92 cfs 2.598 af  
Primary=29.92 cfs 2.598 af**Link 13L: PDA-1 UD A** Inflow=3.45 cfs 0.282 af  
Primary=3.45 cfs 0.282 af**Link 14L: OVERALL SITE** Inflow=13.84 cfs 2.847 af  
Primary=13.84 cfs 2.847 af**Link 17L: PDA-1 UD B** Inflow=0.56 cfs 0.043 af  
Primary=0.56 cfs 0.043 af**Link 18L: TOTAL PDA-1 UD** Inflow=4.01 cfs 0.325 af  
Primary=4.01 cfs 0.325 af**Total Runoff Area = 5.490 ac Runoff Volume = 3.200 af Average Runoff Depth = 6.99"**  
**33.15% Pervious = 1.820 ac 66.85% Impervious = 3.670 ac**

**Proposed**

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NOAA 24-hr C 100-Year Rainfall=8.21"

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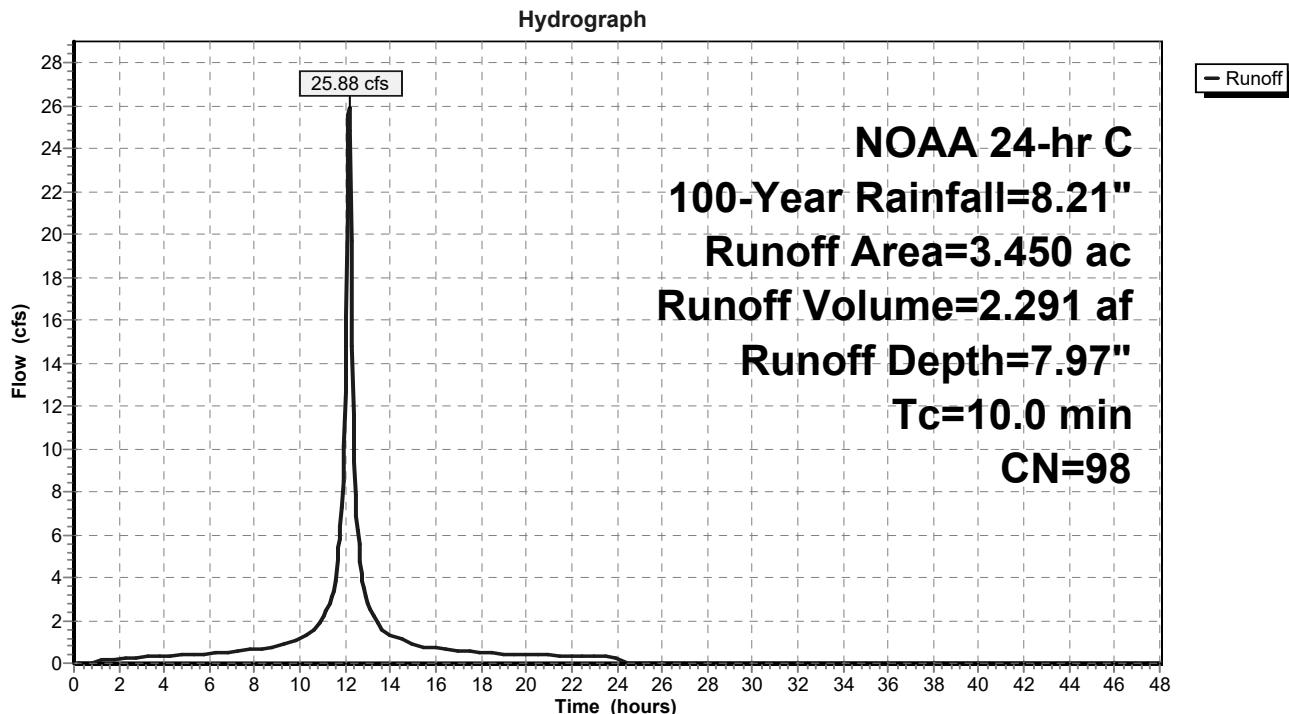
**Summary for Subcatchment 6S: PDA-1-Impervious**

Runoff = 25.88 cfs @ 12.17 hrs, Volume= 2.291 af, Depth= 7.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
3.450	98	Paved parking, HSG C
3.450		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 6S: PDA-1-Impervious**

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NOAA 24-hr C 100-Year Rainfall=8.21"

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**Summary for Subcatchment 7S: PDA-1-Pervious**

Runoff = 4.04 cfs @ 12.17 hrs, Volume= 0.307 af, Depth= 5.11"

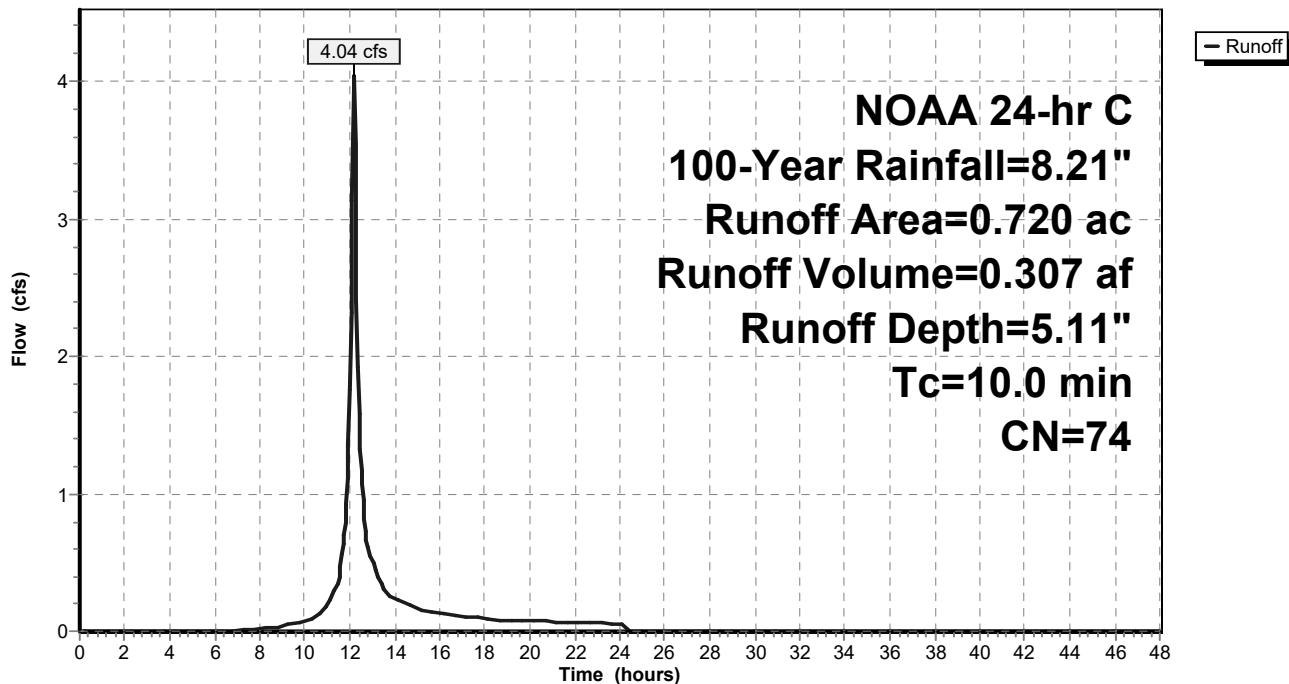
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
0.720	74	>75% Grass cover, Good, HSG C
0.720		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 7S: PDA-1-Pervious**

Hydrograph



**Summary for Subcatchment 9S: PDA OFF-SITE PERVIOUS**

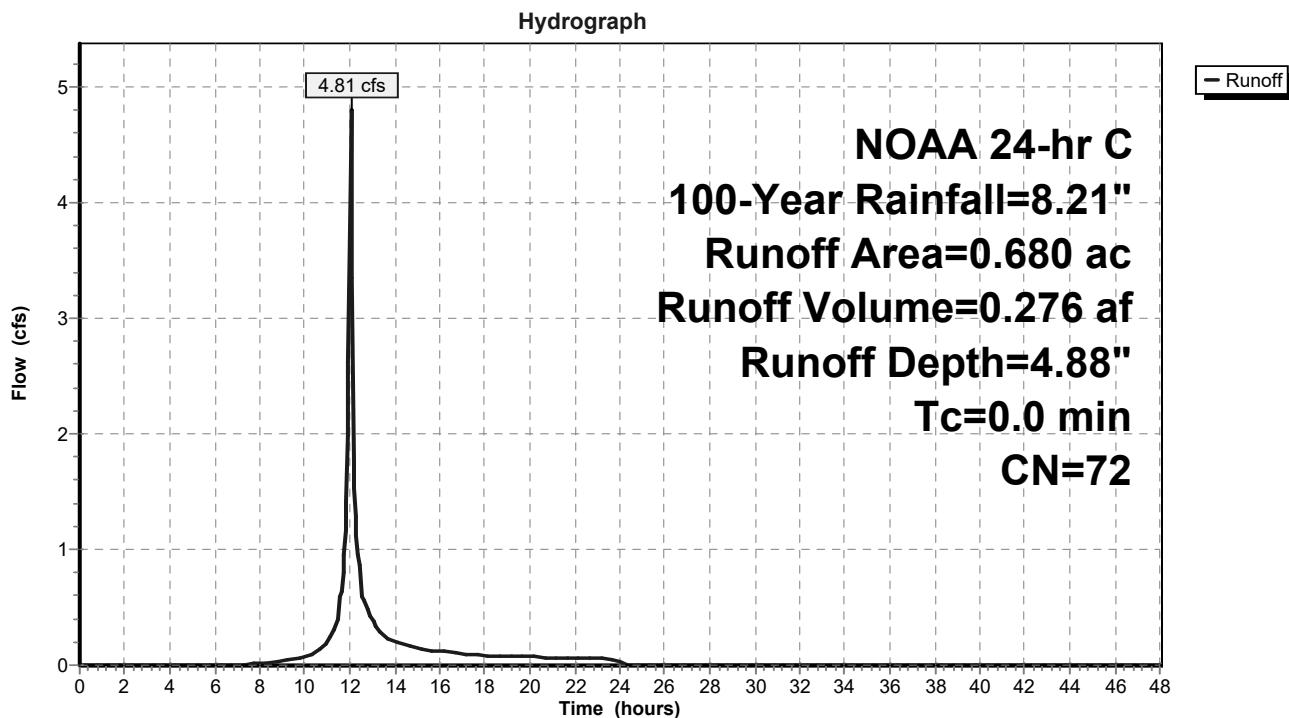
[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 4.81 cfs @ 12.05 hrs, Volume= 0.276 af, Depth= 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0				Direct Entry, 10	

**Subcatchment 9S: PDA OFF-SITE PERVIOUS**

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NOAA 24-hr C 100-Year Rainfall=8.21"

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**Summary for Subcatchment 11S: PDA-1 UD A-Impervious**

Runoff = 1.65 cfs @ 12.17 hrs, Volume= 0.146 af, Depth= 7.97"

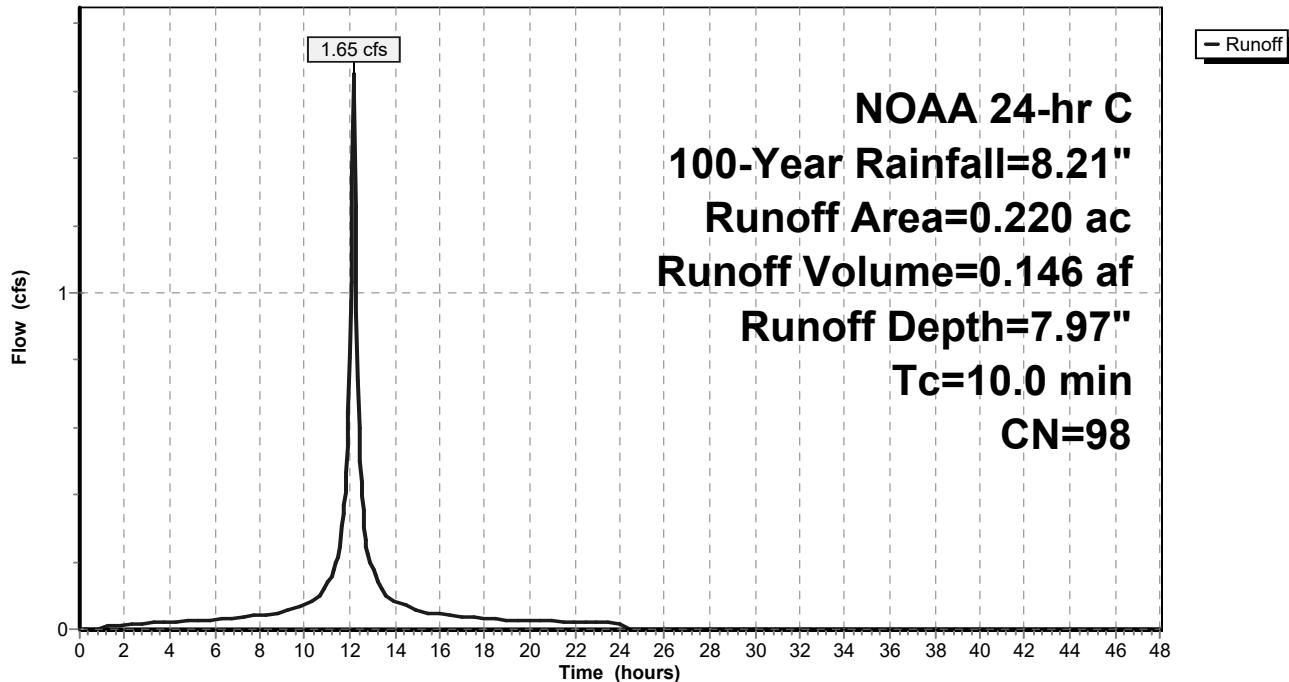
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
0.220	98	Paved parking, HSG C
0.220		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 11S: PDA-1 UD A-Impervious**

Hydrograph



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NOAA 24-hr C 100-Year Rainfall=8.21"

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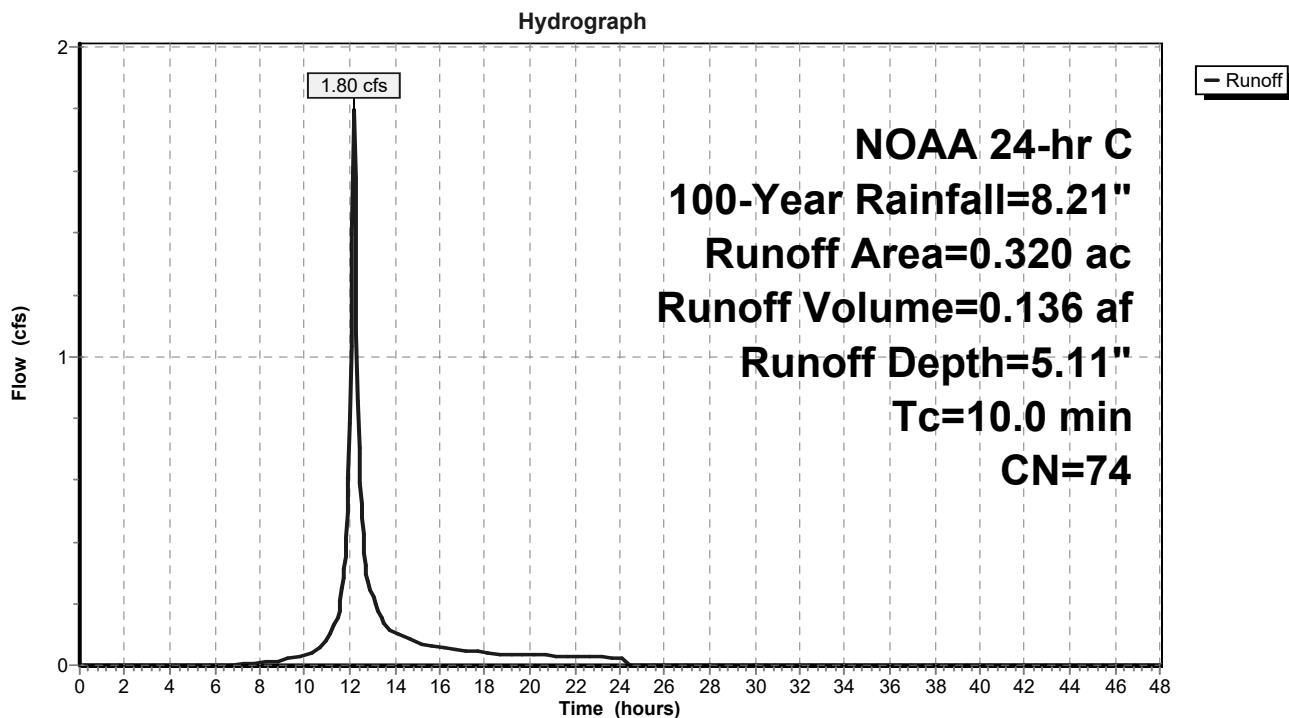
**Summary for Subcatchment 12S: PDA-1UD A-Pervious**

Runoff = 1.80 cfs @ 12.17 hrs, Volume= 0.136 af, Depth= 5.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
0.320	74	>75% Grass cover, Good, HSG C
0.320		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 12S: PDA-1UD A-Pervious**

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NOAA 24-hr C 100-Year Rainfall=8.21"

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**Summary for Subcatchment 16S: PDA-1UD B-Pervious**

Runoff = 0.56 cfs @ 12.17 hrs, Volume= 0.043 af, Depth= 5.11"

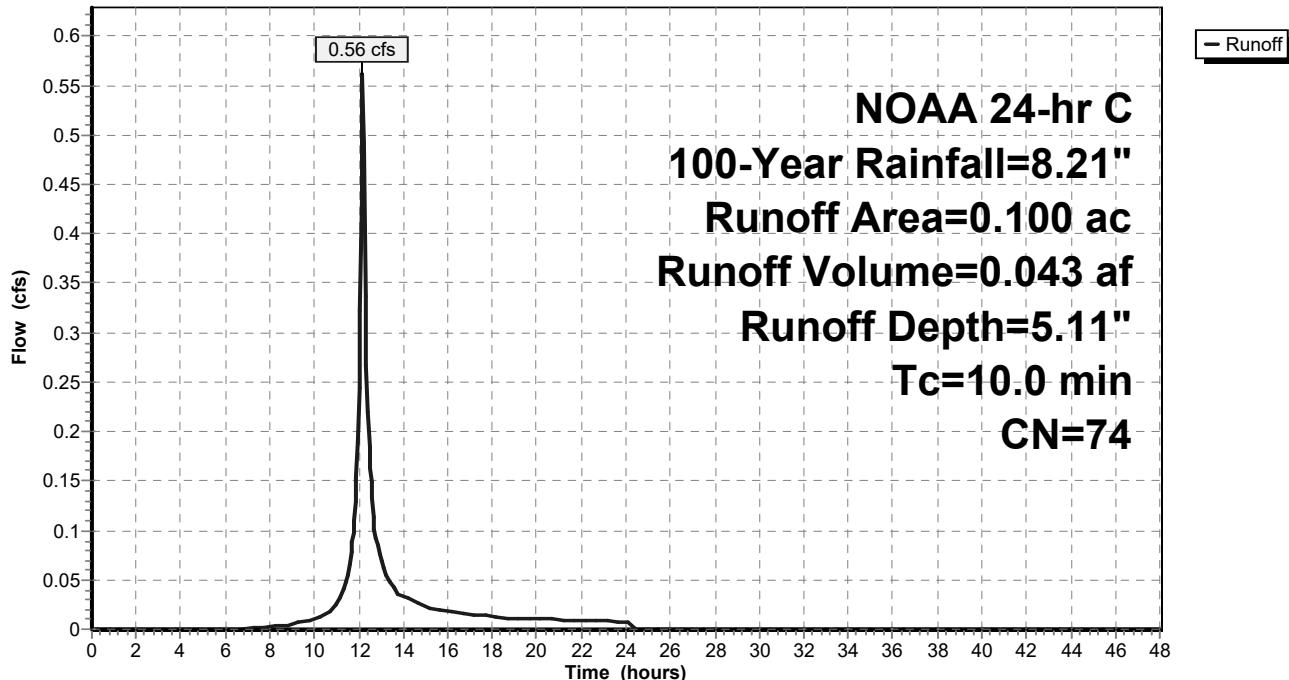
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year Rainfall=8.21"

Area (ac)	CN	Description
0.100	74	>75% Grass cover, Good, HSG C
0.100		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 16S: PDA-1UD B-Pervious**

Hydrograph



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NOAA 24-hr C 100-Year Rainfall=8.21"

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**Summary for Pond 8P: WET POND**

Inflow Area = 4.850 ac, 71.13% Impervious, Inflow Depth = 7.11" for 100-Year event  
 Inflow = 31.45 cfs @ 12.16 hrs, Volume= 2.875 af  
 Outflow = 10.36 cfs @ 12.45 hrs, Volume= 2.522 af, Atten= 67%, Lag= 16.9 min  
 Primary = 10.36 cfs @ 12.45 hrs, Volume= 2.522 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
 Peak Elev= 72.89' @ 12.45 hrs Surf.Area= 15,493 sf Storage= 59,183 cf

Plug-Flow detention time= 373.6 min calculated for 2.520 af (88% of inflow)  
 Center-of-Mass det. time= 314.5 min ( 1,074.8 - 760.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	68.50'	60,825 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
68.50	11,408	0	0
69.00	12,104	5,878	5,878
70.00	12,902	12,503	18,381
71.00	13,711	13,307	31,688
72.00	14,475	14,093	45,781
73.00	15,613	15,044	60,825

Device	Routing	Invert	Outlet Devices
#1	Primary	66.50'	<b>15.0" Round Culvert</b> L= 100.0' Ke= 1.000 Inlet / Outlet Invert= 66.50' / 66.00' S= 0.0050 '/' Cc= 0.900 n= 0.015 Concrete sewer w/manholes & inlets, Flow Area= 1.23 sf
#2	Device 1	68.50'	<b>2.5" Vert. Orifice</b> C= 0.600
#3	Device 1	71.15'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)
#4	Device 1	72.90'	<b>48.0" x 42.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=10.36 cfs @ 12.45 hrs HW=72.89' (Free Discharge)

↑ 1=Culvert (Barrel Controls 10.36 cfs @ 8.44 fps)

↑ 2=Orifice (Passes < 0.34 cfs potential flow)

↑ 3=Sharp-Crested Rectangular Weir(Passes < 27.49 cfs potential flow)

↑ 4=Grate ( Controls 0.00 cfs)

**Proposed**

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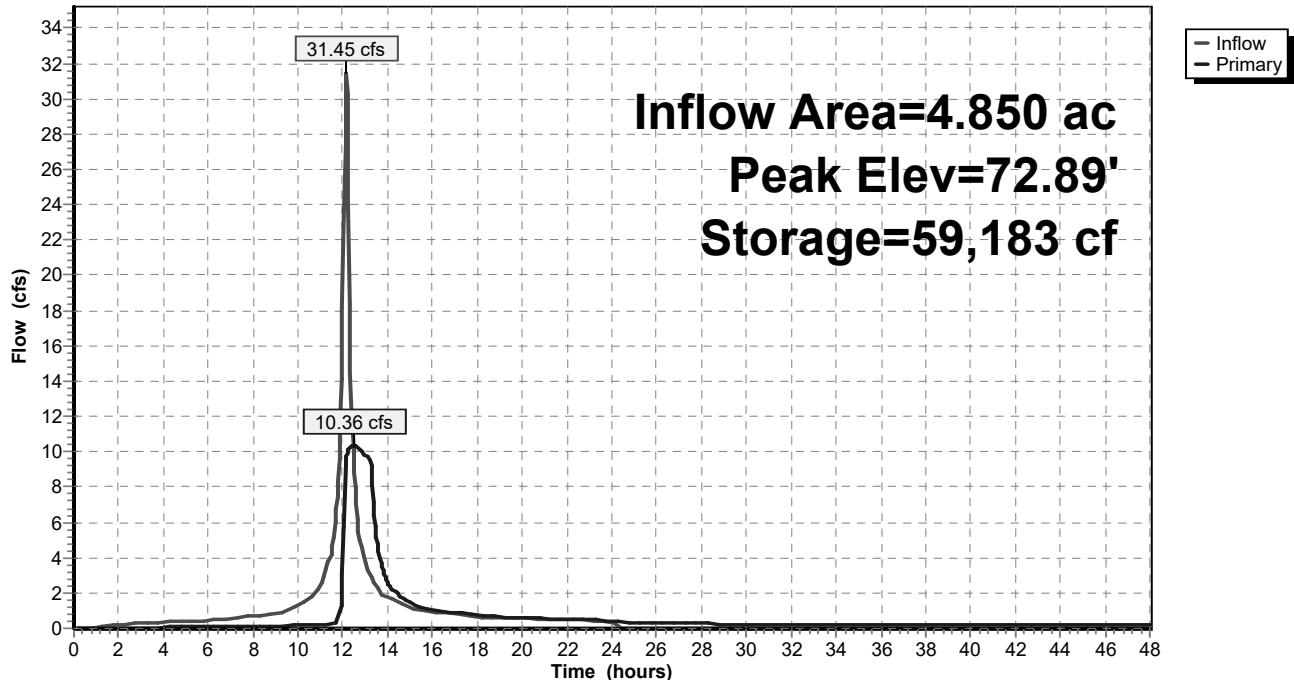
NOAA 24-hr C 100-Year Rainfall=8.21"

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**Pond 8P: WET POND**

Hydrograph



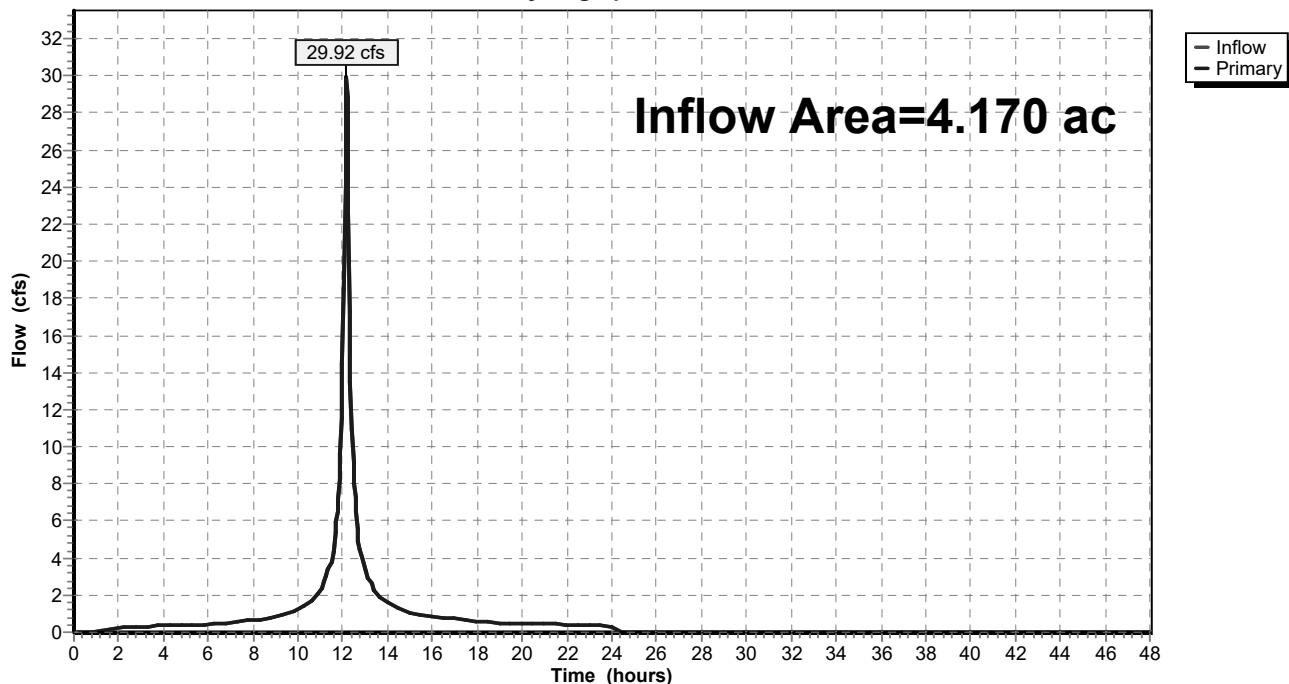
**Summary for Link 10L: PDA - 1**

Inflow Area = 4.170 ac, 82.73% Impervious, Inflow Depth = 7.48" for 100-Year event

Inflow = 29.92 cfs @ 12.17 hrs, Volume= 2.598 af

Primary = 29.92 cfs @ 12.17 hrs, Volume= 2.598 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 10L: PDA - 1****Hydrograph**

**Summary for Link 13L: PDA-1 UD A**

Inflow Area = 0.540 ac, 40.74% Impervious, Inflow Depth = 6.28" for 100-Year event

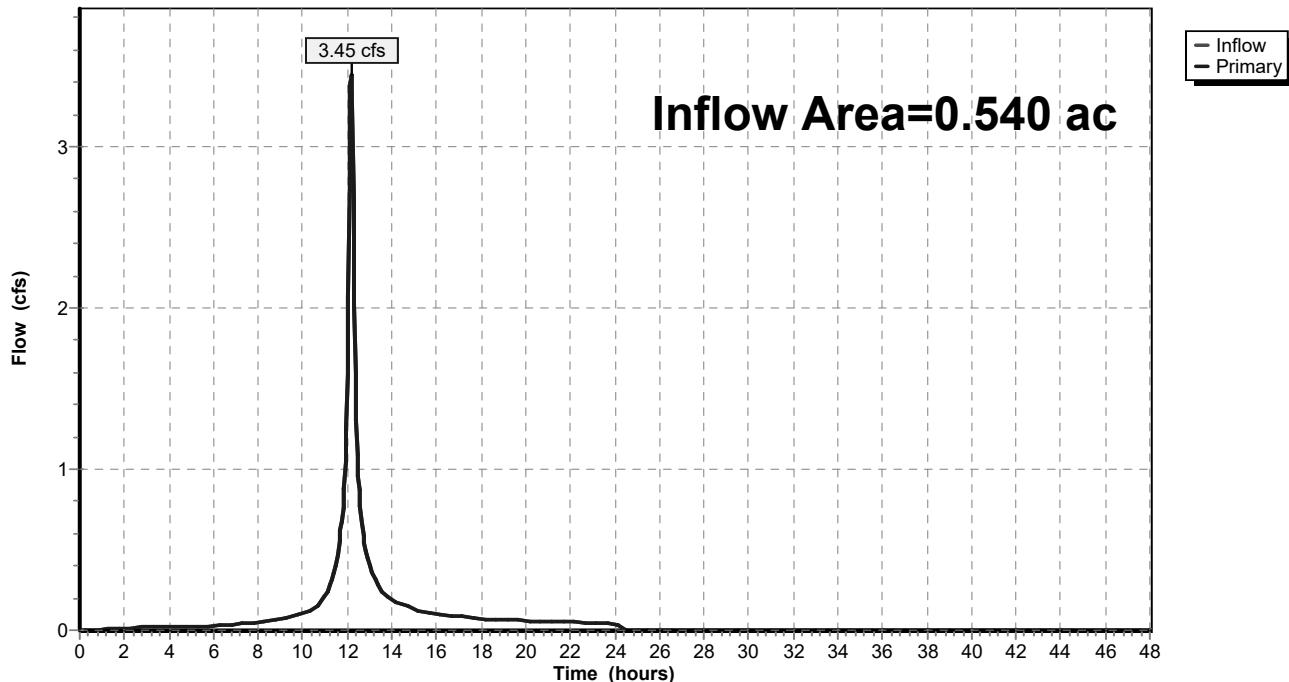
Inflow = 3.45 cfs @ 12.17 hrs, Volume= 0.282 af

Primary = 3.45 cfs @ 12.17 hrs, Volume= 0.282 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 13L: PDA-1 UD A**

Hydrograph



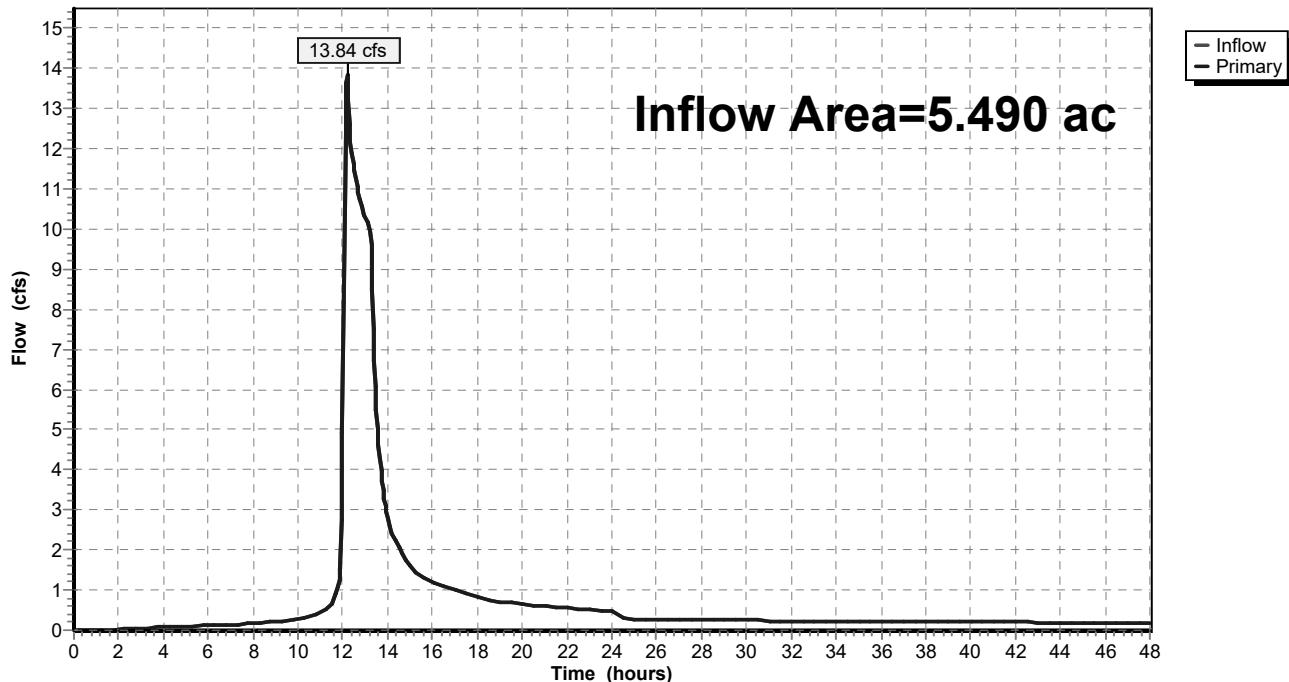
**Summary for Link 14L: OVERALL SITE**

Inflow Area = 5.490 ac, 66.85% Impervious, Inflow Depth > 6.22" for 100-Year event

Inflow = 13.84 cfs @ 12.19 hrs, Volume= 2.847 af

Primary = 13.84 cfs @ 12.19 hrs, Volume= 2.847 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 14L: OVERALL SITE****Hydrograph**

**Summary for Link 17L: PDA-1 UD B**

Inflow Area = 0.100 ac, 0.00% Impervious, Inflow Depth = 5.11" for 100-Year event

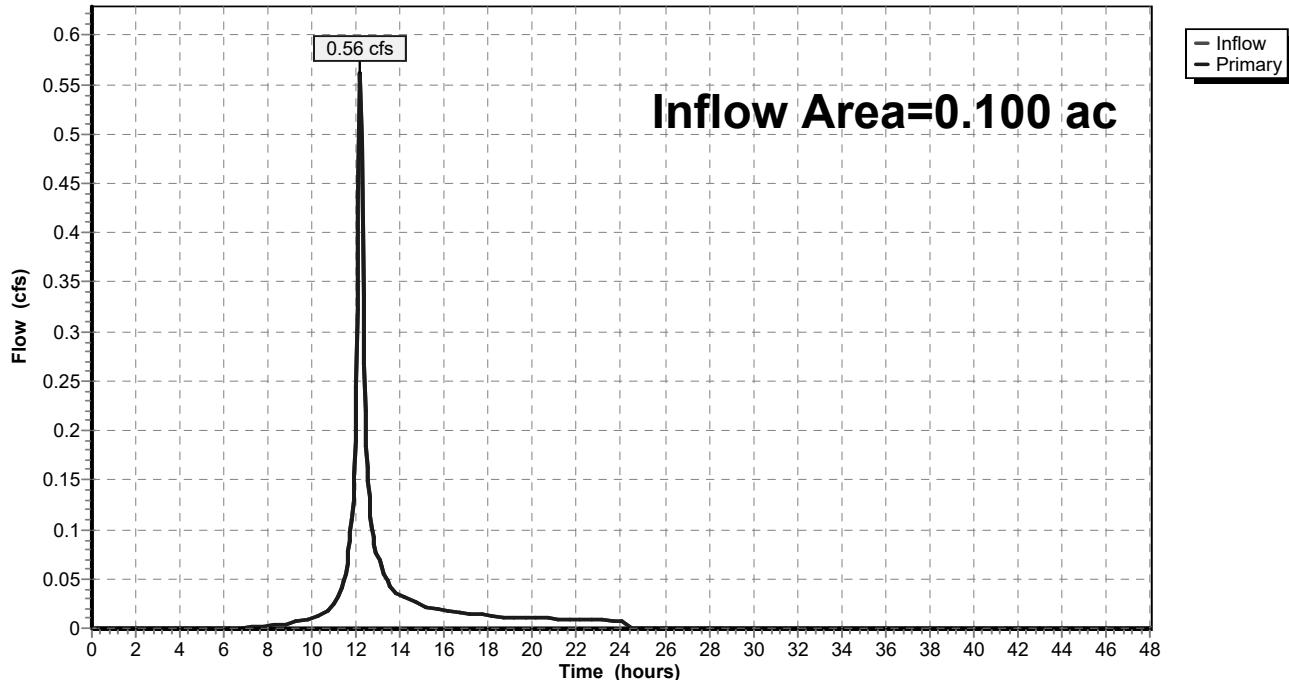
Inflow = 0.56 cfs @ 12.17 hrs, Volume= 0.043 af

Primary = 0.56 cfs @ 12.17 hrs, Volume= 0.043 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 17L: PDA-1 UD B**

Hydrograph



**Summary for Link 18L: TOTAL PDA-1 UD**

Inflow Area = 0.640 ac, 34.38% Impervious, Inflow Depth = 6.10" for 100-Year event

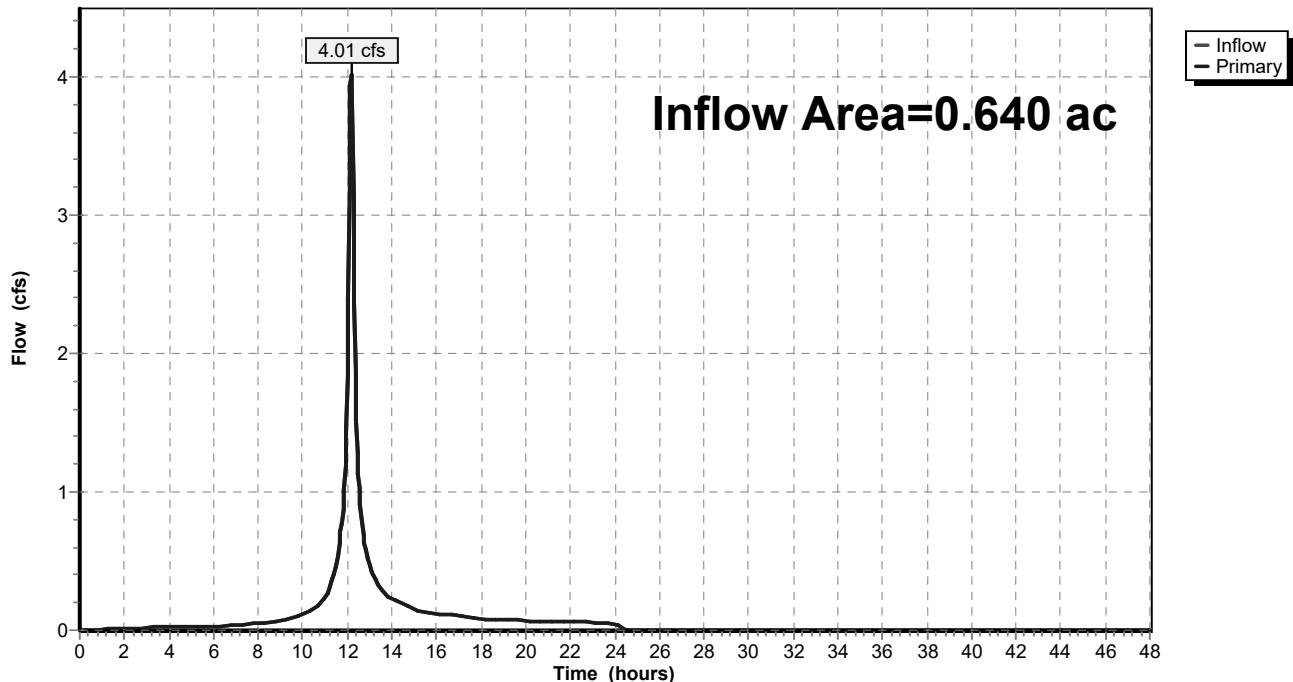
Inflow = 4.01 cfs @ 12.17 hrs, Volume= 0.325 af

Primary = 4.01 cfs @ 12.17 hrs, Volume= 0.325 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 18L: TOTAL PDA-1 UD**

Hydrograph



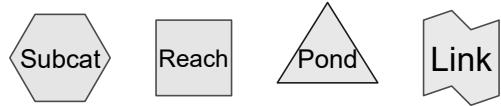
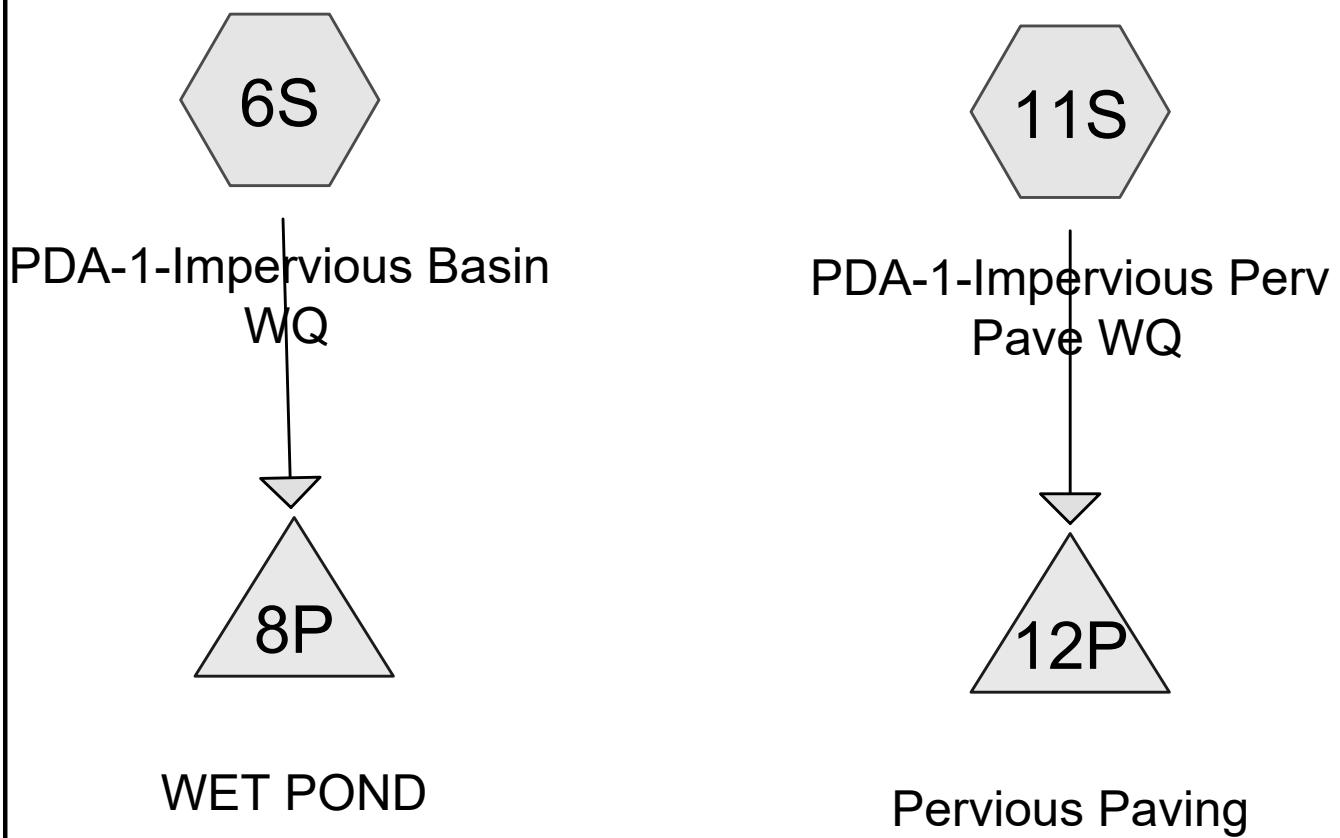




## **APPENDIX C**

NJDEP Water Quality Storm Routing, Calculations, Dewatering &  
Water Budget





**Routing Diagram for WQ Storm**  
Prepared by Maser Consulting PA, Printed 11/2/2020  
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**WQ Storm**

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**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
1.390	98	Paved parking, HSG C (6S, 11S)
<b>1.390</b>	<b>98</b>	<b>TOTAL AREA</b>

**WQ Storm**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
1.390	HSG C	6S, 11S
0.000	HSG D	
0.000	Other	
<b>1.390</b>		<b>TOTAL AREA</b>

**WQ Storm**

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**Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	1.390	0.000	0.000	1.390	Paved parking	6S, 11S
<b>0.000</b>	<b>0.000</b>	<b>1.390</b>	<b>0.000</b>	<b>0.000</b>	<b>1.390</b>	<b>TOTAL AREA</b>	

**WQ Storm**

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**Pipe Listing (all nodes)**

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	8P	66.50	66.00	100.0	0.0050	0.015	15.0	0.0	0.0

Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment6S: PDA-1-Impervious** Runoff Area=1.110 ac 100.00% Impervious Runoff Depth=1.03"  
Tc=10.0 min CN=98 Runoff=2.86 cfs 0.096 af

**Subcatchment11S: PDA-1-Impervious** Runoff Area=0.280 ac 100.00% Impervious Runoff Depth=1.03"  
Tc=10.0 min CN=98 Runoff=0.72 cfs 0.024 af

**Pond 8P: WET POND** Peak Elev=68.83' Storage=3,889 cf Inflow=2.86 cfs 0.096 af  
Outflow=0.08 cfs 0.086 af

**Pond 12P: Pervious Paving** Peak Elev=73.98' Storage=571 cf Inflow=0.72 cfs 0.024 af  
Outflow=0.14 cfs 0.024 af

**Total Runoff Area = 1.390 ac Runoff Volume = 0.120 af Average Runoff Depth = 1.03"**  
**0.00% Pervious = 0.000 ac 100.00% Impervious = 1.390 ac**

**WQ Storm**

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NJ DEP 2-hr W.Q. Rainfall=1.25"

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**Summary for Subcatchment 6S: PDA-1-Impervious Basin WQ**

Runoff = 2.86 cfs @ 1.15 hrs, Volume= 0.096 af, Depth= 1.03"

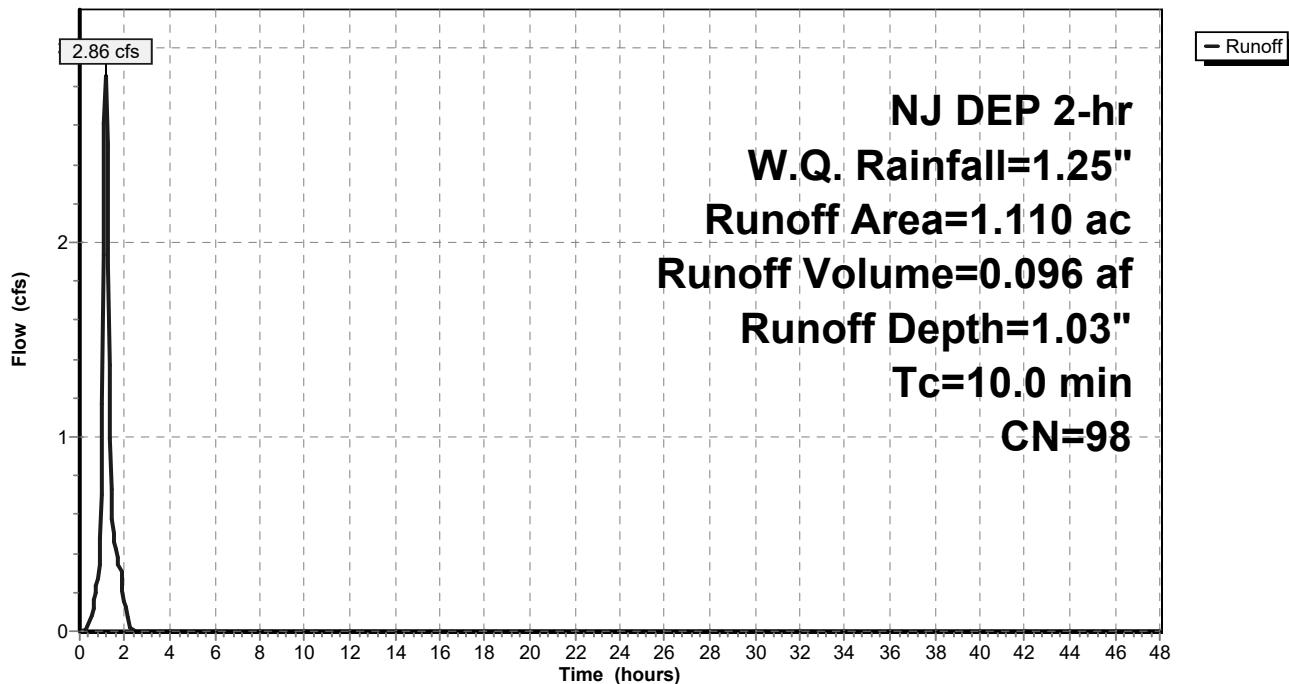
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NJ DEP 2-hr W.Q. Rainfall=1.25"

Area (ac)	CN	Description
1.110	98	Paved parking, HSG C
1.110		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 6S: PDA-1-Impervious Basin WQ**

Hydrograph



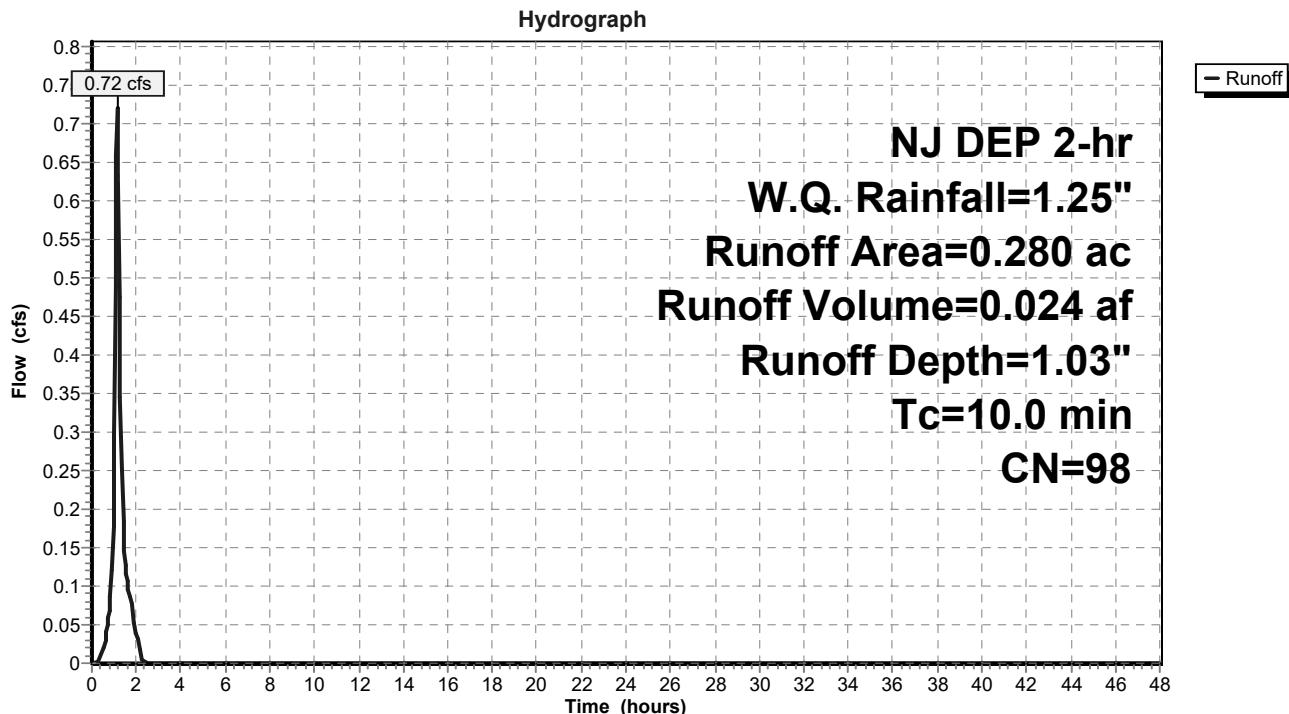
**Summary for Subcatchment 11S: PDA-1-Impervious Perv Pave WQ**

Runoff = 0.72 cfs @ 1.15 hrs, Volume= 0.024 af, Depth= 1.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NJ DEP 2-hr W.Q. Rainfall=1.25"

Area (ac)	CN	Description
0.280	98	Paved parking, HSG C
0.280		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 11S: PDA-1-Impervious Perv Pave WQ**

### Summary for Pond 8P: WET POND

Inflow Area = 1.110 ac, 100.00% Impervious, Inflow Depth = 1.03" for W.Q. event  
 Inflow = 2.86 cfs @ 1.15 hrs, Volume= 0.096 af  
 Outflow = 0.08 cfs @ 2.11 hrs, Volume= 0.086 af, Atten= 97%, Lag= 58.0 min  
 Primary = 0.08 cfs @ 2.11 hrs, Volume= 0.086 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
 Peak Elev= 68.83' @ 2.11 hrs Surf.Area= 11,873 sf Storage= 3,889 cf

Plug-Flow detention time= 663.2 min calculated for 0.086 af (90% of inflow)  
 Center-of-Mass det. time= 659.3 min ( 733.3 - 74.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	68.50'	60,825 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
68.50	11,408	0	0
69.00	12,104	5,878	5,878
70.00	12,902	12,503	18,381
71.00	13,711	13,307	31,688
72.00	14,475	14,093	45,781
73.00	15,613	15,044	60,825

Device	Routing	Invert	Outlet Devices
#1	Primary	66.50'	<b>15.0" Round Culvert</b> L= 100.0' Ke= 1.000 Inlet / Outlet Invert= 66.50' / 66.00' S= 0.0050 '/' Cc= 0.900 n= 0.015 Concrete sewer w/manholes & inlets, Flow Area= 1.23 sf
#2	Device 1	68.50'	<b>2.5" Vert. Orifice</b> C= 0.600
#3	Device 1	71.15'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)
#4	Device 1	72.90'	<b>48.0" x 42.0" Horiz. Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.08 cfs @ 2.11 hrs HW=68.83' (Free Discharge)

↑ 1=Culvert (Passes 0.08 cfs of 5.49 cfs potential flow)

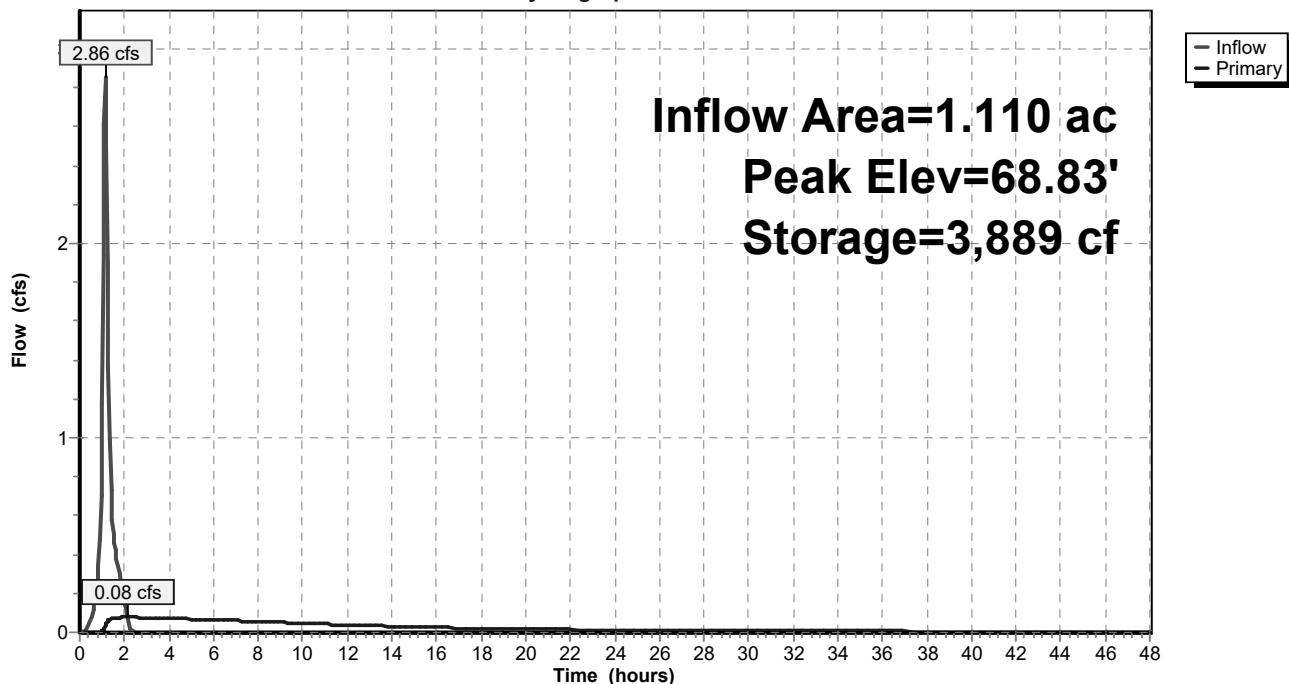
↑ 2=Orifice (Orifice Controls 0.08 cfs @ 2.31 fps)

↑ 3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

↑ 4=Grate (Controls 0.00 cfs)

**Pond 8P: WET POND**

Hydrograph



### Summary for Pond 12P: Pervious Paving

Inflow Area = 0.280 ac, 100.00% Impervious, Inflow Depth = 1.03" for W.Q. event  
 Inflow = 0.72 cfs @ 1.15 hrs, Volume= 0.024 af  
 Outflow = 0.14 cfs @ 1.48 hrs, Volume= 0.024 af, Atten= 81%, Lag= 20.0 min  
 Primary = 0.14 cfs @ 1.48 hrs, Volume= 0.024 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
 Peak Elev= 73.98' @ 1.48 hrs Surf.Area= 10,747 sf Storage= 571 cf

Plug-Flow detention time= 42.1 min calculated for 0.024 af (100% of inflow)  
 Center-of-Mass det. time= 42.1 min ( 116.1 - 74.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	73.85'	5,760 cf	<b>Stone Storage (Prismatic)</b> Listed below (Recalc) 14,401 cf Overall x 40.0% Voids

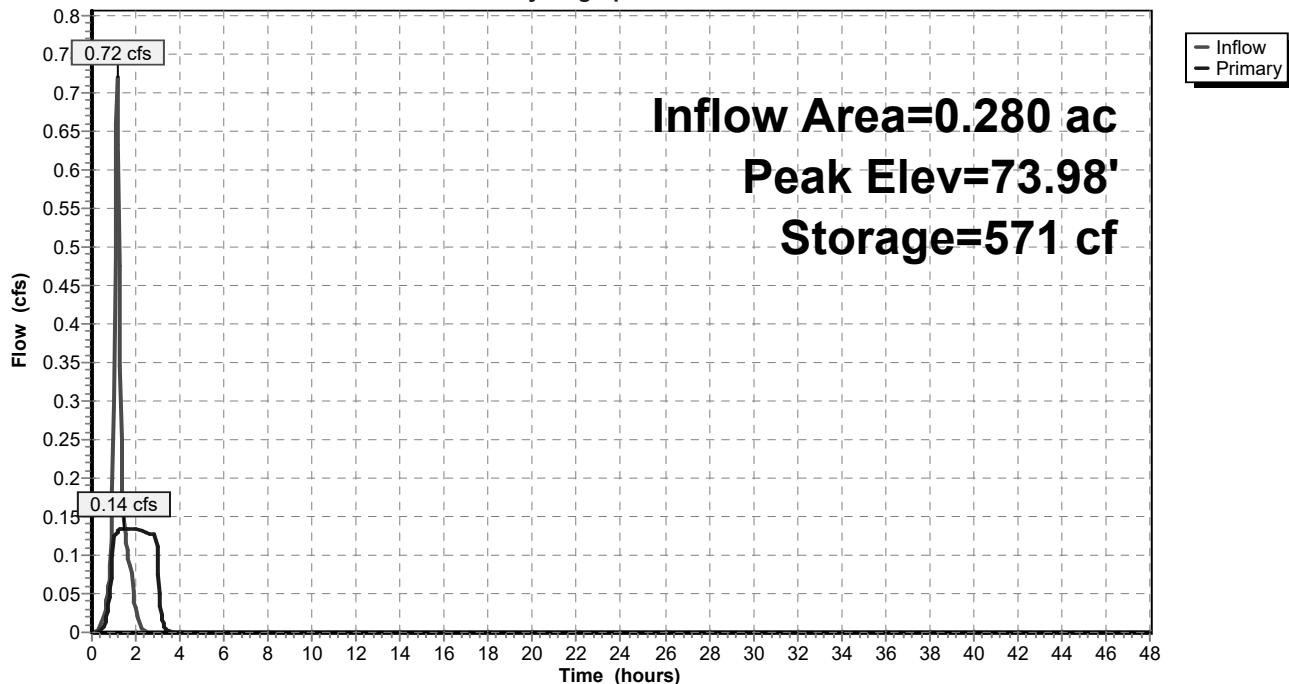
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
73.85	10,747	0	0
75.19	10,747	14,401	14,401

Device	Routing	Invert	Outlet Devices
#1	Primary	73.85'	<b>0.500 in/hr Exfiltration over Surface area</b> Conductivity to Groundwater Elevation = 72.30'

**Primary OutFlow** Max=0.14 cfs @ 1.48 hrs HW=73.98' (Free Discharge)  
 ↑ 1=Exfiltration ( Controls 0.14 cfs )

**Pond 12P: Pervious Paving**

Hydrograph





Project: Elizabeth Ave

Project#:

Sheet#:

of

Scale:

Calculated By: MB

Date:

Checked By:

Date:

Office Submitted By:

Date:

10/7/24

Engineers | Planners | Surveyors | Landscape Architects | Environmental Scientists

## Pervious Paving Capacity

Area of Perv Pave:  $1\phi 27\phi \text{ SF} (.24 \text{ Ac})$

Total Area draining to Perv Pave

$\phi .32 \text{ AC}$

- .24 Pavement
- $\phi 3$  Conc
- $\phi 5$  Grass

WQ Runoff =  $\phi .\phi 24 \text{ acf} = 1\phi 45 \text{ cf}$

$1\phi 45 \text{ cf}$  → Runoff volume

$1\phi 27\phi \text{ SF}$  → Pave(Perv) Area

$$= \phi .1\phi \text{ ft} = \frac{1.22''}{\phi .45\phi \text{ voids}}$$

3.05" stone needed  
for WQ

GW Recharge  
requires  
6.5" of stone



WATER BUDGET  
MC#: 19000694A

JOB DESCRIPTION: Elizabeth Ave Warehouse  
BASIN NAME: Wet Pond 1

Volume = Initial Volume + Rainfall - Evapotranspiration - Infiltration

$$V = V_i + R - PET - I$$

Drainage Area to Basin:

Initial Permanent Pool Volume:

Normal Water Surface Area:

Volume = Initial Volume + Rainfall - Evapotranspiration

- Infiltration

(See Sheet 2)

Monthly Evapotranspiration Rate:

0.02 inches / hour

	Rainfall "R"						Somerset County - ONJSC monthly rainfall data - 1965 (Dry Year)						Infiltration Rate:						Infiltration Rate:					
	January	February	March	April	May	June	July	August	September	October	November	December	January	February	March	April	May	June	July	August	September	October	November	December
Monthly Rainfall (1965)	2.72	2.77	3.2	2.47	1.39	1.27	3.13	2.79	2.94	2.61	1.67	1.88	0.227	0.231	0.206	0.116	0.106	0.261	0.316	0.245	0.218	0.139	0.157	29.84
"R" Total	47887	48767	56338	43486	24472	22359	55105	66725	51760	45950	29401	33098	316	316	316	316	316	316	316	316	316	316	316	316
Monthly PET	0.00	0.01	0.59	1.70	3.33	5.65	5.01	3.51	0.293	0.162	0.067	0.12	0.000	0.001	0.049	0.142	0.278	0.407	0.418	0.293	0.162	0.067	0.101	0.155
"PET" Total	0	9	564	1618	3167	4643	5373	4765	3338	1846	764	115	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92
Infiltration "I"	January	February	March	April	May	June	July	August	September	October	November	December	January	February	March	April	May	June	July	August	September	October	November	December
Infiltration Rate	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017
"I" Total	14145.92	12776.96	14145.92	13689.6	14145.92	13689.6	14145.92	13689.6	14145.92	14145.92	14145.92	14145.92	13689.6	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92	14145.92
Net Gain / (Loss)	January	February	March	April	May	June	July	August	September	October	November	December	January	February	March	April	May	June	July	August	September	October	November	December
Permanent Pool Volume	18978	18978	18978	18978	18978	18978	18978	18978	18978	18978	18978	18978	54960	60606	47156	26137	23005	54564	66792	53711	48936	33925	18978	18978

Note: If permanent pool volume exceeds initial permanent pool volume at the end of the month, then permanent pool volume resets to initial permanent pool volume.  
This accounts for the loss of rainfall volume through the outlet structure.

**RESULT:** There are not any times where there are three consecutive months of drying. Therefore, the basin meets the NJDEP BMP Guidelines of not having a drying period longer than two consecutive months. (Page 9.2-10 of NJDEP BMP Manual)

Formulas:

$$"R" \text{ Total (cubic feet / month)} = \text{Avg. Monthly Rainfall (feet / month) } \times \text{Drainage Area to Basin (square feet)}$$

$$"PET" \text{ Total (cubic feet / month)} = \text{Monthly Evapotranspiration Rate (feet / month) } \times \text{Normal Water Surface Area (square feet)}$$

$$"I" \text{ Total (cubic feet / month)} = \text{Infiltration Rate (feet / month) } \times \text{Normal Water Surface Area (square feet)}$$

DATE: 10/23/2020  
DESIGN BY: LMB

Sheet 1

**WATER BUDGET**  
MC#: 19000694A

**JOB DESCRIPTION:** Elizabeth Ave Warehouse  
**BASIN NAME:** Wet Pond 1

**DATE:** 10/23/2020  
**DESIGN BY:** LMB

**Volume = Initial Volume + Rainfall - Evapotranspiration - Infiltration**  
 $V = V_i + R - PET - I$

**Drainage Area to Basin:**

4.85 acres  
211266 square feet  
18,978 cubic feet  
11,408 square feet

**Initial Permanent Pool Volume:**

**Normal Water Surface Area:**

	"R"	Somerset County - ONJSC monthly rainfall data - 1987 (Median Year)										
	January	February	March	April	May	June	July	August	September	October	November	December
<b>Monthly Rainfall (1987)</b>	4.91	1.13	2.66	5.72	2.05	4.39	7.37	4.86	4.49	4.37	3.42	1.79
<b>"R" Total</b>	0.409	0.094	0.222	0.477	0.171	0.366	0.614	0.405	0.374	0.364	0.285	0.149 feet / month
<b>"R" Total</b>	<b>86443</b>	<b>19894</b>	<b>46831</b>	<b>100703</b>	<b>36091</b>	<b>77288</b>	<b>129753</b>	<b>85563</b>	<b>79049</b>	<b>76936</b>	<b>60211</b>	<b>31514 cubic feet / month</b>

	"PET"											
	January	February	March	April	May	June	July	August	September	October	November	December
<b>Monthly PET</b>	0.00	0.01	0.59	1.70	3.33	4.88	5.65	5.01	3.51	1.94	0.80	0.12 inches / month
<b>"PET" Total</b>	0.000	0.001	0.049	0.142	0.278	0.407	0.471	0.418	0.293	0.162	0.067	0.010 feet / month
<b>"PET" Total</b>	<b>0</b>	<b>9</b>	<b>564</b>	<b>1618</b>	<b>3167</b>	<b>4643</b>	<b>5373</b>	<b>4765</b>	<b>3338</b>	<b>1846</b>	<b>764</b>	<b>115 cubic feet / month</b>

	"I"											
	January	February	March	April	May	June	July	August	September	October	November	December
<b>Infiltration Rate</b>	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02 inches / hour
<b>"I" Total</b>	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017 feet / hour
<b>"I" Total</b>	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04 feet / day
<b>"I" Total</b>	1.24	1.12	1.24	1.20	1.24	1.20	1.24	1.24	1.24	1.24	1.20	1.24 feet / month
<b>"I" Total</b>	<b>14145.92</b>	<b>12776.96</b>	<b>14145.92</b>	<b>13689.6</b>	<b>14145.92</b>	<b>13689.6</b>	<b>14145.92</b>	<b>14145.92</b>	<b>13689.6</b>	<b>14145.92</b>	<b>13689.6</b>	<b>14145.92 cubic feet / month</b>

	"Gain / (Loss)"											
	January	February	March	April	May	June	July	August	September	October	November	December
<b>Net Gain / (Loss)</b>	72297	7109	32121	85396	18778	58956	110233	66652	62022	60944	45757	17253 cubic feet / month
<b>Permanent Pool Volume</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>104374</b>	<b>37756</b>	<b>77934</b>	<b>129211</b>	<b>85630</b>	<b>81000</b>	<b>79922</b>	<b>64735</b>	<b>36231 cubic feet</b>
<b>Permanent Pool Volume</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978</b>	<b>18978 cubic feet</b>

**Note:** If permanent pool volume exceeds initial permanent pool volume at the end of the month, then permanent pool volume resets to initial permanent pool volume.  
This accounts for the loss of rainfall volume through the outlet structure.

**RESULT:** There are not any times where there are three consecutive months of drying. Therefore, the basin meets the NJDEP BMP Guidelines of not having a drying period longer than two consecutive months. (Page 9.2-10 of NJDEP BMP Manual)

**Formulas:**

"R" Total (cubic feet / month) =

Monthly Evapotranspiration Rate (feet / month) × Normal Water Surface Area (square feet)

"PET" Total (cubic feet / month) =

Infiltration Rate (feet / month) × Normal Water Surface Area (square feet)

Avg. Monthly Rainfall (feet / month) × Drainage Area to Basin (square feet)

Monthly Evapotranspiration Rate (feet / month) × Normal Water Surface Area (square feet)

Infiltration Rate (feet / month) × Normal Water Surface Area (square feet)

**WATER BUDGET**  
MC#: 19000694A

**JOB DESCRIPTION:** Elizabeth Ave Warehouse  
**BASIN NAME:** Wet Pond 1

**DATE:** 10/23/2020  
**DESIGN BY:** LMB

**Volume = Initial Volume + Rainfall - Evapotranspiration - Infiltration**

$$V = V_i + R - PET - I$$

**Drainage Area to Basin:**

4.85 acres  
211266 square feet  
18,978 cubic feet  
11,408 square feet

**Initial Permanent Pool Volume:**  
**Normal Water Surface Area:**

	Somerset County - ONJSC monthly rainfall data - 2011 (Wet Year)						Infiltration Rate:	Monthly Evapotranspiration Rate:	(See Sheet 2)
	January	February	March	April	May	June			
Monthly Rainfall (2011)	3.38	2.97	6.4	6.86	4.65	3.5	3.43	16.83	8.77
"R" Total	0.282	0.248	0.533	0.572	0.388	0.292	0.286	1.403	0.731
	598507	52288	112675	120774	81866	61619	60387	296301	154400
								79049	65669
									75704 cubic feet / month
<b>Evapotranspiration</b>	<b>"PET"</b>								
Monthly PET	January	February	March	April	May	June	July	August	September
"PET" Total	0.00	0.01	0.59	1.70	3.33	4.88	5.65	5.01	3.51
	0.000	0.001	0.049	0.142	0.278	0.407	0.471	0.418	0.293
	0	9	564	1618	3167	4643	5373	4765	3338
									1846
									764
									115 cubic feet / month
<b>Infiltration</b>	<b>"I"</b>								
Infiltration Rate	January	February	March	April	May	June	July	August	September
"I" Total	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017	0.0017
	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04
	1.24	1.12	1.24	1.20	1.24	1.20	1.24	1.24	1.24
	14145.92	12776.96	14145.92	13689.6	14145.92	13689.6	14145.92	14145.92	13689.6
									14145.92 cubic feet / month
<b>Net Gain / (Loss)</b>									
Permanent Pool Volume	January	February	March	April	May	June	July	August	September
	18978	18978	18978	18978	18978	18978	18978	18978	18978
									18978 cubic feet
									18978 cubic feet
									18978 cubic feet

**Note:** If permanent pool volume exceeds initial permanent pool volume at the end of the month, then permanent pool volume resets to initial permanent pool volume.  
This accounts for the loss of rainfall volume through the outlet structure.

**RESULT:** There are not any times where there are three consecutive months of drying. Therefore, the basin meets the NJDEP BMP Guidelines of not having a drying period longer than two consecutive months. (Page 9.2-10 of NJDEP BMP Manual)

**Formulas:**

$$"R" \text{ Total (cubic feet / month)} =$$

$$"PET" \text{ Total (cubic feet / month)} =$$

$$"I" \text{ Total (cubic feet / month)} =$$

Avg. Monthly Rainfall (feet / month) x Drainage Area to Basin (square feet)

Monthly Evapotranspiration Rate (feet / month) x Normal Water Surface Area (square feet)

Infiltration Rate (feet / month) x Normal Water Surface Area (square feet)

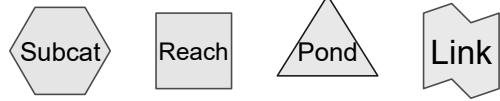
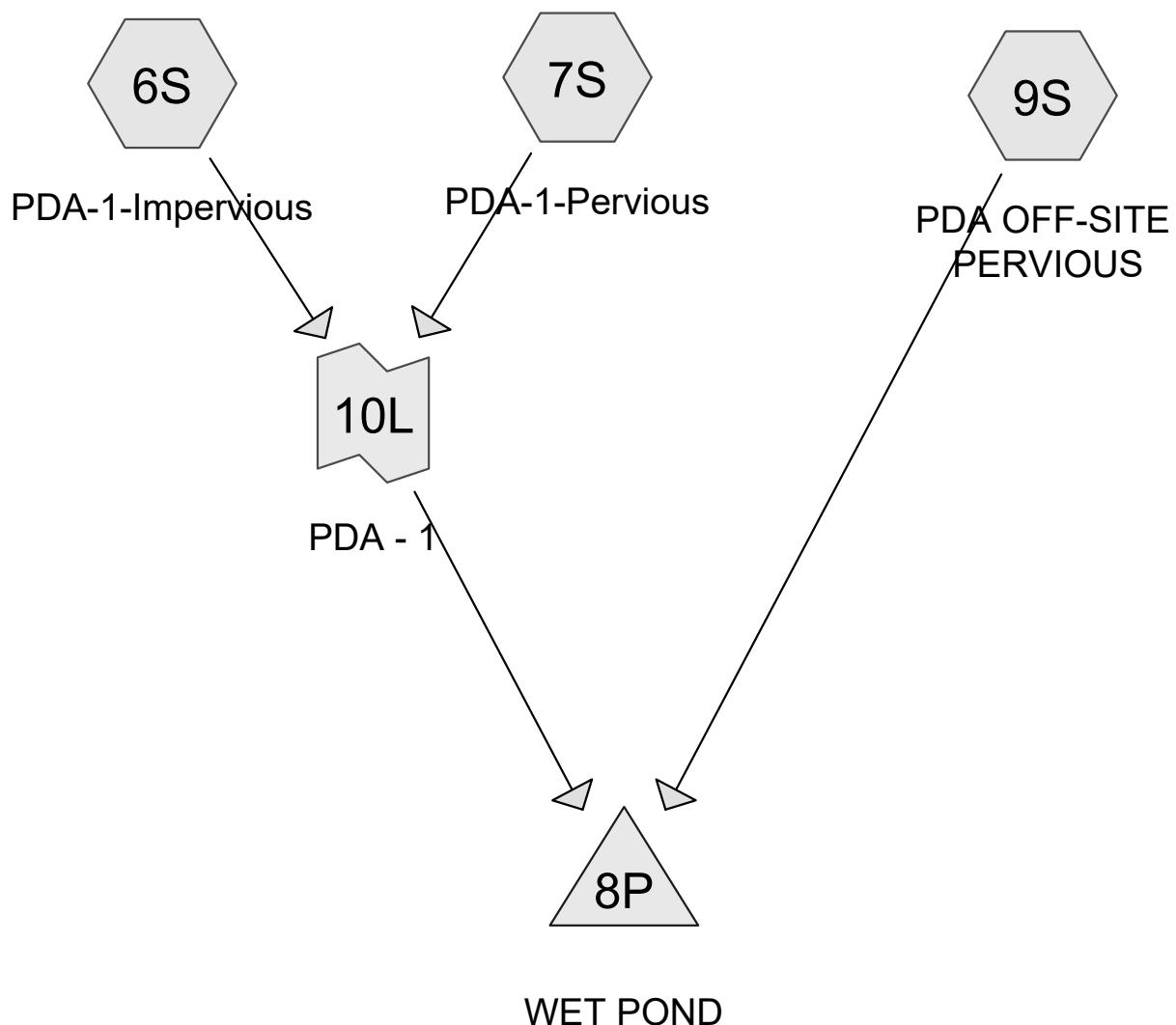




## **APPENDIX D**

Emergency Spillway Calculations (150% of 100 Year Storm Routing)





**Routing Diagram for Emergency Spillway**  
Prepared by Maser Consulting PA, Printed 11/2/2020  
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## **Emergency Spillway**

Prepared by Maser Consulting PA

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Page 2

### **Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
0.720	74	>75% Grass cover, Good, HSG C (7S)
3.450	98	Paved parking, HSG C (6S)
0.680	72	Woods/grass comb., Good, HSG C (9S)
<b>4.850</b>	<b>91</b>	<b>TOTAL AREA</b>

## **Emergency Spillway**

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Page 3

### **Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
4.850	HSG C	6S, 7S, 9S
0.000	HSG D	
0.000	Other	
<b>4.850</b>		<b>TOTAL AREA</b>

## **Emergency Spillway**

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### **Ground Covers (all nodes)**

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	0.720	0.000	0.000	0.720	>75% Grass cover, Good	7S
0.000	0.000	3.450	0.000	0.000	3.450	Paved parking	6S
0.000	0.000	0.680	0.000	0.000	0.680	Woods/grass comb., Good	9S
<b>0.000</b>	<b>0.000</b>	<b>4.850</b>	<b>0.000</b>	<b>0.000</b>	<b>4.850</b>	<b>TOTAL AREA</b>	

**Emergency Spillway**

Prepared by Maser Consulting PA

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NOAA 24-hr C 100-Year+150% Rainfall=12.32"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment6S: PDA-1-Impervious** Runoff Area=3.450 ac 100.00% Impervious Runoff Depth=12.08"  
Tc=10.0 min CN=98 Runoff=38.89 cfs 3.473 af**Subcatchment7S: PDA-1-Pervious** Runoff Area=0.720 ac 0.00% Impervious Runoff Depth=8.92"  
Tc=10.0 min CN=74 Runoff=6.90 cfs 0.535 af**Subcatchment9S: PDA OFF-SITE PERVIOUS** Runoff Area=0.680 ac 0.00% Impervious Runoff Depth=8.63"  
Tc=0.0 min CN=72 Runoff=8.29 cfs 0.489 af**Pond 8P: WET POND** Peak Elev=73.49' Storage=68,687 cf Inflow=48.37 cfs 4.497 af  
Outflow=47.05 cfs 3.101 af**Link 10L: PDA - 1** Inflow=45.79 cfs 4.008 af  
Primary=45.79 cfs 4.008 af**Total Runoff Area = 4.850 ac Runoff Volume = 4.497 af Average Runoff Depth = 11.13"**  
**28.87% Pervious = 1.400 ac 71.13% Impervious = 3.450 ac**

**Emergency Spillway**

Prepared by Maser Consulting PA

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NOAA 24-hr C 100-Year+150% Rainfall=12.32"

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Page 6

**Summary for Subcatchment 6S: PDA-1-Impervious**

Runoff = 38.89 cfs @ 12.17 hrs, Volume= 3.473 af, Depth=12.08"

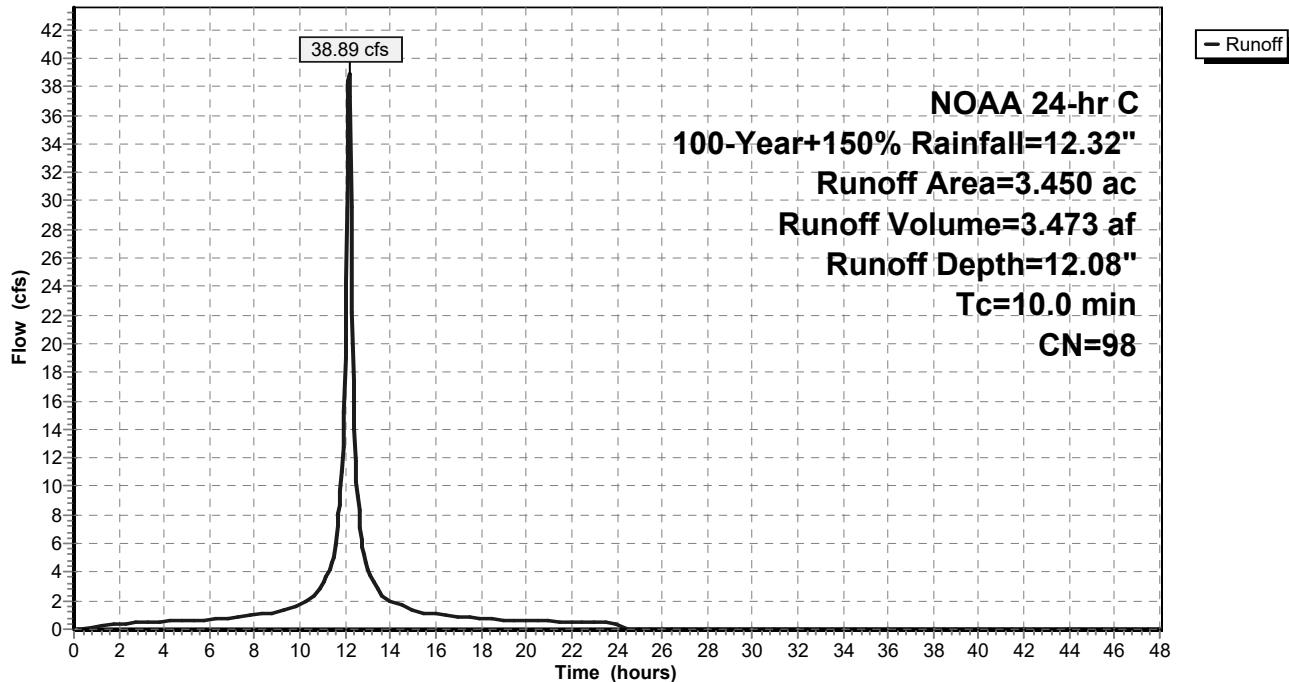
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year+150% Rainfall=12.32"

Area (ac)	CN	Description
3.450	98	Paved parking, HSG C
3.450		100.00% Impervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 6S: PDA-1-Impervious**

Hydrograph



**Emergency Spillway**

Prepared by Maser Consulting PA

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NOAA 24-hr C 100-Year+150% Rainfall=12.32"

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**Summary for Subcatchment 7S: PDA-1-Pervious**

Runoff = 6.90 cfs @ 12.17 hrs, Volume= 0.535 af, Depth= 8.92"

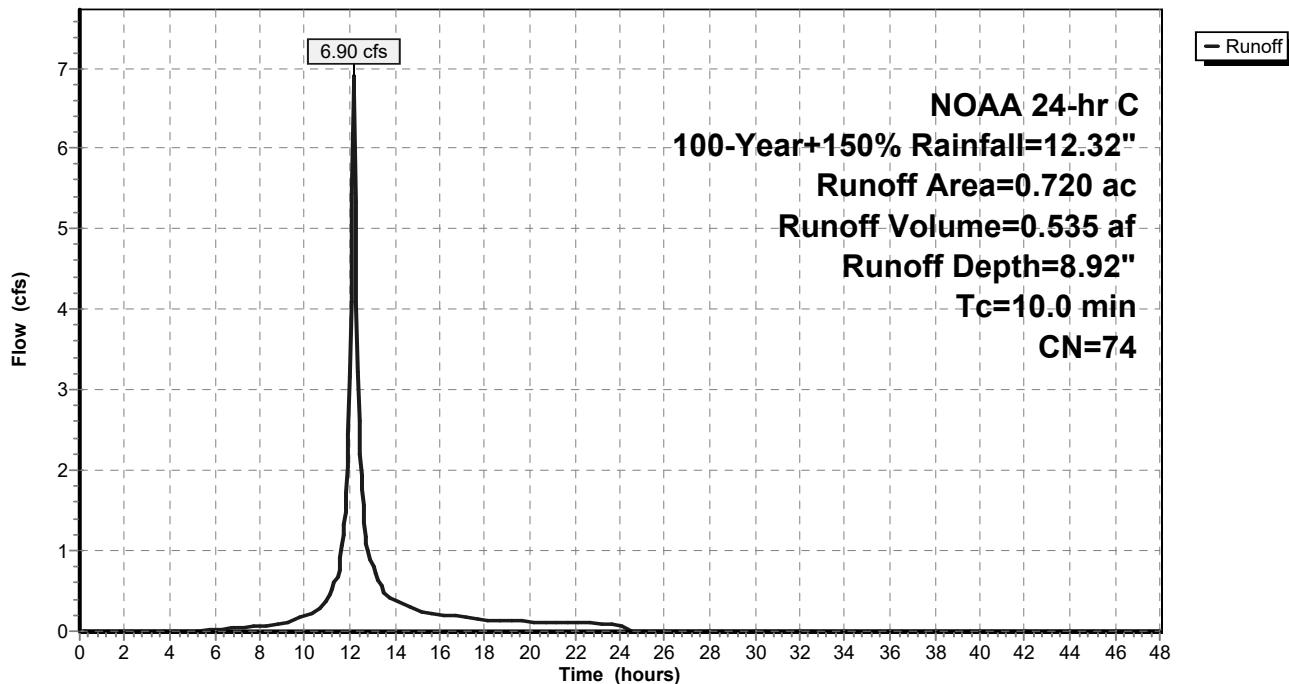
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs  
NOAA 24-hr C 100-Year+150% Rainfall=12.32"

Area (ac)	CN	Description
0.720	74	>75% Grass cover, Good, HSG C
0.720		100.00% Pervious Area

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.0	Direct Entry,				

**Subcatchment 7S: PDA-1-Pervious**

Hydrograph



**Emergency Spillway**

Prepared by Maser Consulting PA

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NOAA 24-hr C 100-Year+150% Rainfall=12.32"

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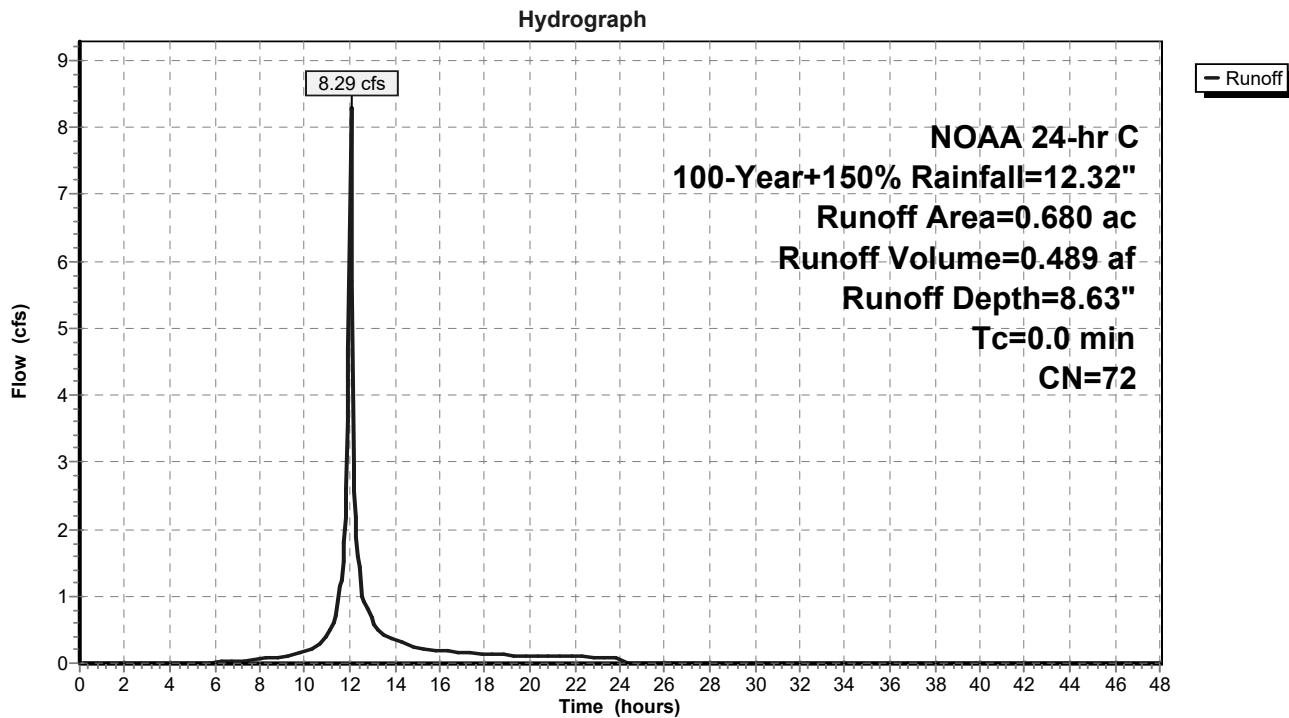
**Summary for Subcatchment 9S: PDA OFF-SITE PERVIOUS**[46] Hint:  $T_c=0$  (Instant runoff peak depends on  $dt$ )

Runoff = 8.29 cfs @ 12.05 hrs, Volume= 0.489 af, Depth= 8.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs,  $dt= 0.05$  hrs  
NOAA 24-hr C 100-Year+150% Rainfall=12.32"

Area (ac)	CN	Description
0.680	72	Woods/grass comb., Good, HSG C
0.680		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.0	Direct Entry, 10				

**Subcatchment 9S: PDA OFF-SITE PERVIOUS**

**Emergency Spillway**

Prepared by Maser Consulting PA

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NOAA 24-hr C 100-Year+150% Rainfall=12.32"

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**Summary for Pond 8P: WET POND**

Inflow Area = 4.850 ac, 71.13% Impervious, Inflow Depth = 11.13" for 100-Year+150% event

Inflow = 48.37 cfs @ 12.16 hrs, Volume= 4.497 af

Outflow = 47.05 cfs @ 12.19 hrs, Volume= 3.101 af, Atten= 3%, Lag= 1.7 min

Primary = 47.05 cfs @ 12.19 hrs, Volume= 3.101 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Peak Elev= 73.49' @ 12.19 hrs Surf.Area= 16,420 sf Storage= 68,687 cf

Plug-Flow detention time= 194.2 min calculated for 3.097 af (69% of inflow)

Center-of-Mass det. time= 94.2 min ( 849.1 - 755.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	68.50'	77,260 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
68.50	11,408	0	0
69.00	12,104	5,878	5,878
70.00	12,902	12,503	18,381
71.00	13,711	13,307	31,688
72.00	14,475	14,093	45,781
73.00	15,613	15,044	60,825
74.00	17,258	16,436	77,260

Device	Routing	Invert	Outlet Devices
#1	Primary	73.00'	<b>50.0' long x 1.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

**Primary OutFlow Max=46.56 cfs @ 12.19 hrs HW=73.49' (Free Discharge)**↑**1=Broad-Crested Rectangular Weir**(Weir Controls 46.56 cfs @ 1.91 fps)

**Emergency Spillway**

Prepared by Maser Consulting PA

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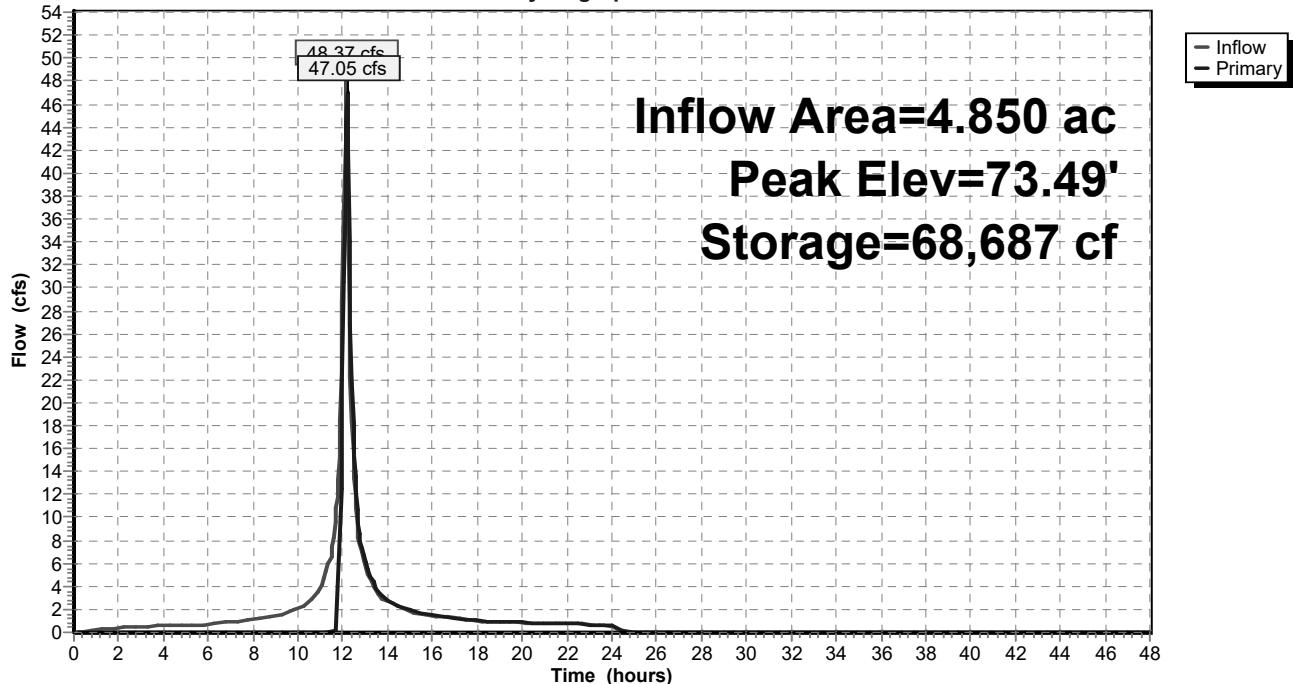
NOAA 24-hr C 100-Year+150% Rainfall=12.32"

Printed 11/2/2020

Page 10

**Pond 8P: WET POND**

Hydrograph



**Emergency Spillway**

Prepared by Maser Consulting PA

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NOAA 24-hr C 100-Year+150% Rainfall=12.32"

Printed 11/2/2020

Page 11

**Summary for Link 10L: PDA - 1**

Inflow Area = 4.170 ac, 82.73% Impervious, Inflow Depth = 11.53" for 100-Year+150% event

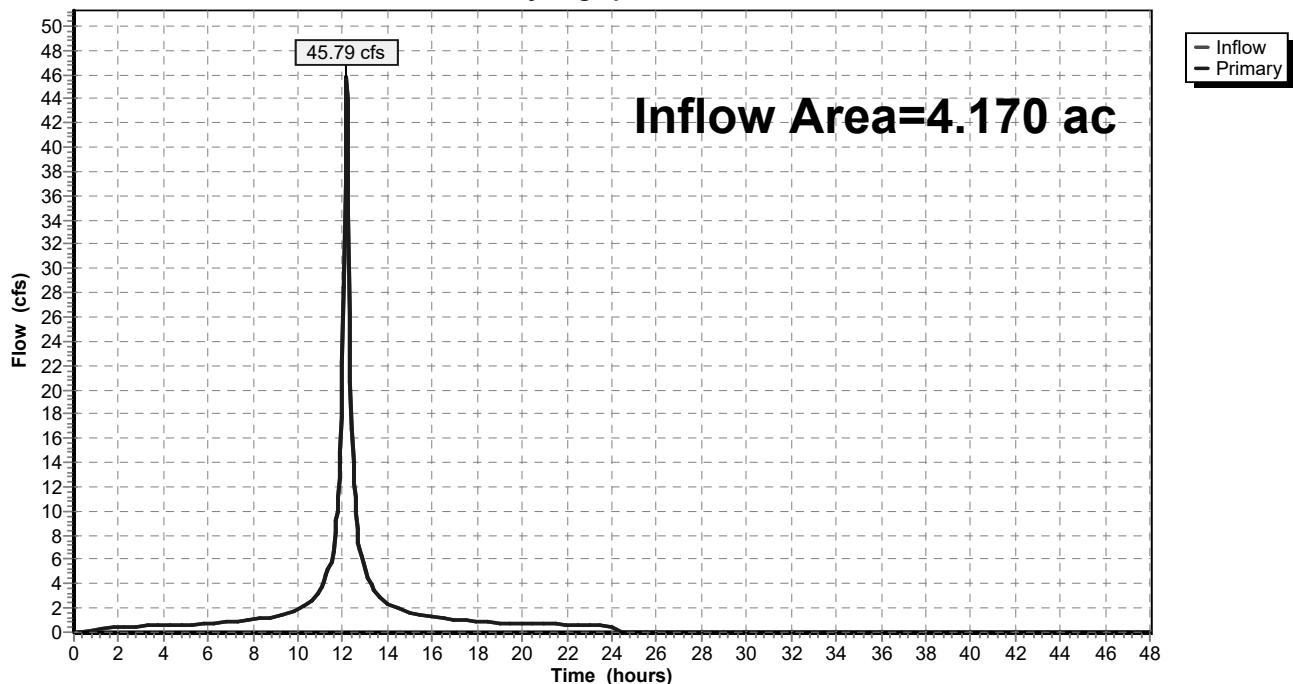
Inflow = 45.79 cfs @ 12.17 hrs, Volume= 4.008 af

Primary = 45.79 cfs @ 12.17 hrs, Volume= 4.008 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

**Link 10L: PDA - 1**

Hydrograph







## **APPENDIX E**

Pipe Calculations for Stormwater Conveyance System & HGL Profiles



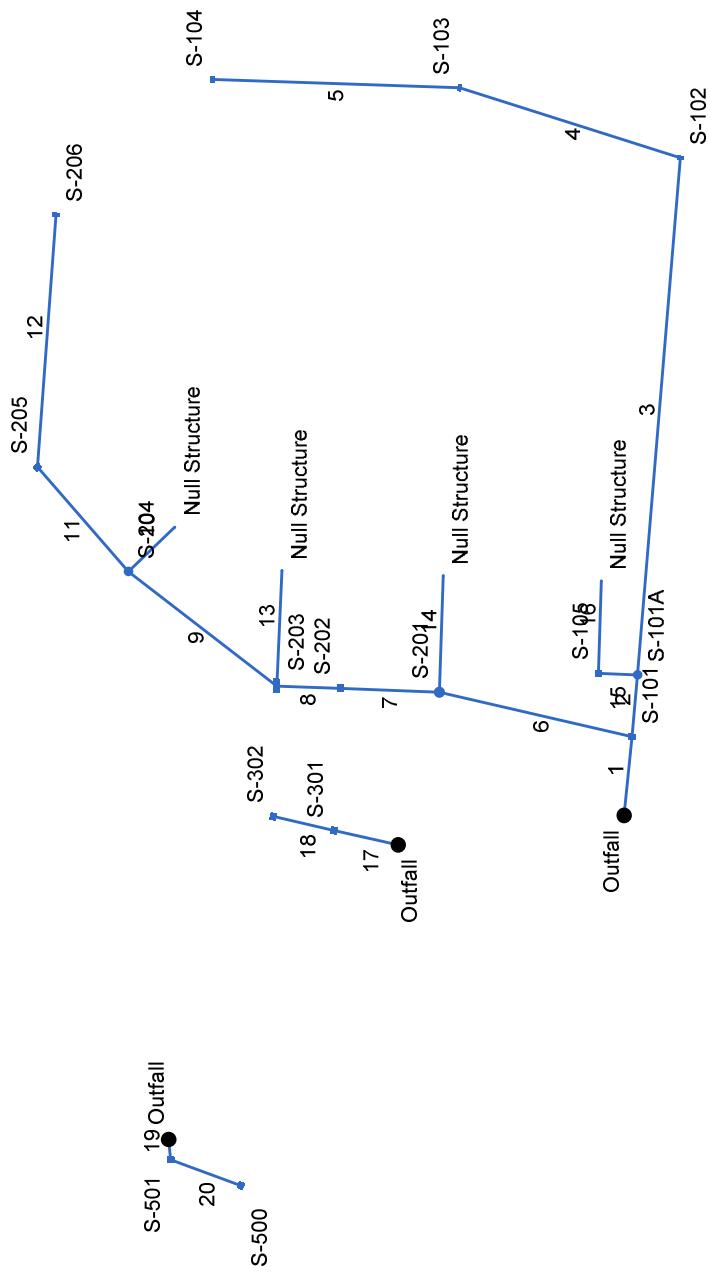
**INLET DRAINAGE AREA  
COMPOSITE "C" CALCULATIONS**

10/26/20

DESCRIPTION (Inlet or Manhole #)	TOTAL AREA (SF)	IMP. AREA (SF) 0.99	HSG C (LAWN) 0.51	HSG C (WOODS) 0.45	COMPOSITE "C"		CHECK SUM	CHECK SUM
					CHECK	CHECK?		
WET POND								
IDA-104	0.48	0.07	0.11	0.30	0.54	0.48	OK	OK
IDA-105	0.60	0.10	0.13	0.37	0.55	0.60	OK	OK
IDA-102	0.20	0.07	0.13	0.13	0.68	0.20	OK	OK
IDA-105	0.21	0.12	0.09	0.09	0.78	0.21	OK	OK
IDA-101	0.03	0.03	0.00	0.00	0.99	0.03	OK	OK
IDA-206	0.12	0.06	0.06	0.06	0.75	0.12	OK	OK
IDA-205	0.22	0.19	0.03	0.03	0.92	0.22	OK	OK
IDA-203	0.16	0.14	0.02	0.02	0.93	0.16	OK	OK
IDA-202	0.02	0.01	0.01	0.01	0.75	0.02	OK	OK
IDA-302	0.05	0.05			0.99	0.05	OK	OK
IDA-301	0.02	0.02			0.99	0.02	OK	OK
IDA-500	0.11	0.10	0.01		0.95	0.11	OK	OK
IDA-501	0.10	0.09	0.01		0.94	0.10	OK	OK
IDA-RR-1	0.30	0.30			0.99	0.30	OK	OK
IDA-RR-2	0.60	0.60			0.99	0.60	OK	OK
IDA-RR-3	0.60	0.60			0.99	0.60	OK	OK
IDA-RR-4	0.26	0.26			0.99	0.26	OK	OK
CC-1	0.21	0.21			0.99	0.21	OK	OK
CC-2	0.36	0.34	0.02		0.96	0.36	OK	OK



# Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan



Project File: 201102\_Proposed Storm.stm

Number of lines: 20

Date: 11/2/2020

# MC RPRT\_A

Line No.	Line ID	Inlet ID	Drgg Area	Runoff Coeff	Tc	i Sys	Q Capt	Total Runoff	Capac Full	Vel Ave	(ft/s)	(ft/s)	(in)	Line Slope (%)	Line Size (in)	Line Length (ft)	Invert Up (ft)	Invert Dn (ft)	Gnd/Rim El Up (ft)	Gnd/Rim El Dn (ft)
			(ac)	(C)	(min)	(in/hr)	(cfs)	(cfs)	(cfs)	(ft/s)	(ft/s)	(ft/s)	(ft/s)	(%)	(ft)	(ft)	(ft)	(ft)		
1	P-101	S-101	0.03	0.99	14.1	5.05	0.17	15.73	22.67	5.01	Cir	0.013	24	1.00	48	68.98	68.50	74.47	71.25	
2	P-101A	S-101A	0.00	0.00	13.1	5.19	....	6.16	10.50	5.40	Cir	0.013	18	1.00	38	71.23	70.85	75.18	74.47	
3	P-102	S-102	0.20	0.68	11.9	5.40	0.78	3.92	4.57	4.19	Cir	0.013	15	0.50	314	73.05	71.48	77.20	75.18	
4	P-103	S-103	0.60	0.55	11.1	5.54	1.90	3.27	4.56	3.00	Cir	0.013	15	0.50	141	73.75	73.05	77.50	77.20	
5	P-104	S-104	0.48	0.54	10.0	5.75	1.49	4.49	4.57	2.28	Cir	0.013	15	0.50	150	74.50	73.75	77.80	77.50	
6	P-201	S-201	0.00	0.00	13.6	5.11	....	9.72	15.99	4.46	Cir	0.013	24	0.50	120	70.96	70.36	74.76	74.47	
7	P-202	S-202	0.02	0.75	13.4	5.14	0.09	6.73	8.13	5.11	Cir	0.013	18	0.60	60	71.82	71.46	75.58	74.76	
8	P-203	S-203	0.16	0.93	13.3	5.17	0.86	6.68	8.08	4.49	Cir	0.013	18	0.59	39	72.05	71.82	76.48	75.58	
9	P-204	S-204	0.00	0.00	12.3	5.33	....	2.93	7.43	1.84	Cir	0.013	18	0.50	114	72.62	72.05	78.48	76.48	
10	P-209	Null Structure	0.26	0.99	10.0	5.75	....	1.48	2.41	4.65	Cir	0.012	10	1.04	39	74.00	73.60	0.00	78.48	
11	P-205	S-205	0.22	0.92	11.6	5.45	1.16	1.59	4.57	2.14	Cir	0.013	15	0.50	84	73.29	72.87	76.99	78.48	
12	P-206	S-206	0.12	0.75	10.0	5.75	0.52	0.52	4.55	1.59	Cir	0.013	15	0.50	153	74.05	73.29	77.32	76.99	
13	P-208	Null Structure	0.60	0.99	10.0	5.75	....	3.42	3.94	5.65	Cir	0.012	12	1.04	70	74.00	73.27	0.00	76.48	
14	P-207A	Null Structure	0.60	0.99	10.0	5.75	....	3.42	3.93	5.63	Cir	0.012	12	1.04	70	74.00	73.27	0.00	74.76	
15	P-105	S-105	0.21	0.78	10.2	5.71	0.94	2.63	4.96	4.10	Cir	0.012	15	0.50	24	71.75	71.63	74.70	75.18	
16	P-106	Null Structure	0.30	0.99	10.0	5.75	....	1.71	2.42	4.80	Cir	0.012	10	1.04	56	72.75	72.17	0.00	74.70	
17	P-301	S-301	0.02	0.99	12.7	5.26	0.11	0.36	4.56	0.30	Cir	0.013	15	0.50	40	68.70	68.50	74.99	70.44	
18	P-302	S-302	0.05	0.99	10.0	5.75	0.28	0.28	4.58	0.23	Cir	0.013	15	0.50	38	68.89	68.70	74.39	74.99	
19	P-501	S-501	0.10	0.94	10.3	5.69	0.54	1.13	7.32	3.00	Cir	0.013	18	0.49	12	62.51	62.45	69.77	64.16	
20	P-500	S-500	0.11	0.95	10.0	5.75	0.60	0.60	7.47	2.52	Cir	0.013	18	0.51	45	66.14	65.91	69.09	69.77	

Project File: New.stm

NOTES: Intensity =  $54.48 / (\text{Inlet time} + 11.00)^{0.74}$  -- Return period = 25 Yrs; \*\* Critical depth

Number of lines: 20

Date: 1/12/2020

# MC-RPRT\_B

Line No.	Line ID	Inlet ID	Total Runoff (cfs)	Capac Full (cfs)	Vel Up (ft/s)	Vel Dn (ft/s)	Line Size (in)	Line Slope (%)	Line Length (ft)	Invert Up (ft)	Invert Dn (ft)	Grd/Rim El Up (ft)	Grd/Rim El Dn (ft)	HGL Up (ft)	HGL Dn (ft)	Cover Up (ft)	Cover Dn (ft)
1	P-101	S-101	15.73	22.67	5.01	24	1.00	48	68.98	68.50	74.47	71.25	71.33	71.10	3.49	0.75	
2	P-101A	S-101A	6.16	10.50	6.18	4.62	18	1.00	38	71.23	70.85	75.18	74.47	72.06 j	71.91	2.45	2.12
3	P-102	S-102	3.92	4.57	4.19	4.18	15	0.50	314	73.05	71.48	77.20	75.18	73.94	72.37	2.90	2.45
4	P-103	S-103	3.27	4.56	3.34	2.66	15	0.50	141	73.75	73.05	77.50	77.20	74.68	74.34	2.50	2.90
5	P-104	S-104	1.49	4.57	3.16	1.40	15	0.50	150	74.50	73.75	77.80	77.50	75.01	74.77	2.05	2.50
6	P-201	S-201	9.72	15.99	5.21	3.72	24	0.50	120	70.96	70.36	74.76	74.47	72.11	71.91	1.80	2.11
7	P-202	S-202	6.73	8.13	5.20	5.03	18	0.60	60	71.82	71.46	75.58	74.76	72.85	72.52	2.26	1.80
8	P-203	S-203	6.68	8.08	4.71	4.27	18	0.59	39	72.05	71.82	76.48	75.58	73.17	73.06	2.93	2.26
9	P-204	S-204	2.93	7.43	2.03	1.66	18	0.50	114	72.62	72.05	78.48	76.48	73.76	73.69	4.36	2.93
10	P-209	Null Structure	1.48	2.41	4.65	4.65	10	1.04	39	74.00	73.60	0.00	78.48	74.47	74.07	n/a	4.04
11	P-205	S-205	1.59	4.57	2.70	1.58	15	0.50	84	73.29	72.87	76.99	78.48	73.90	73.83	2.45	4.36
12	P-206	S-206	0.52	4.55	2.49	0.69	15	0.50	153	74.05	73.29	77.32	76.99	74.33	74.02	2.02	2.45
13	P-208	Null Structure	3.42	3.94	5.65	5.65	12	1.04	70	74.00	73.27	0.00	76.48	74.72	73.99	n/a	2.21
14	P-207A	Null Structure	3.42	3.93	5.63	5.63	12	1.04	70	74.00	73.27	0.00	74.76	74.72	73.99	n/a	0.49
15	P-105	S-105	2.63	4.96	4.10	4.10	15	0.50	24	71.75	71.63	74.70	75.18	72.40	72.28	1.70	2.30
16	P-106	Null Structure	1.71	2.42	4.80	4.80	10	1.04	56	72.75	72.17	0.00	74.70	73.27	72.69	n/a	1.70
17	P-301	S-301	0.36	4.56	0.30	0.30	15	0.50	40	68.70	68.50	74.99	70.44	71.10	71.10	5.04	0.69
18	P-302	S-302	0.28	4.58	0.23	0.23	15	0.50	38	68.89	68.70	74.39	74.99	71.10	71.10	4.25	5.04
19	P-501	S-501	1.13	7.32	2.99	3.02	18	0.49	12	62.51	62.45	69.77	64.16	62.91	62.85	5.76	0.21
20	P-500	S-500	0.60	7.47	2.50	2.53	18	0.51	45	66.14	65.91	69.09	69.77	66.43	66.20	1.45	2.36

Project File: New.stm

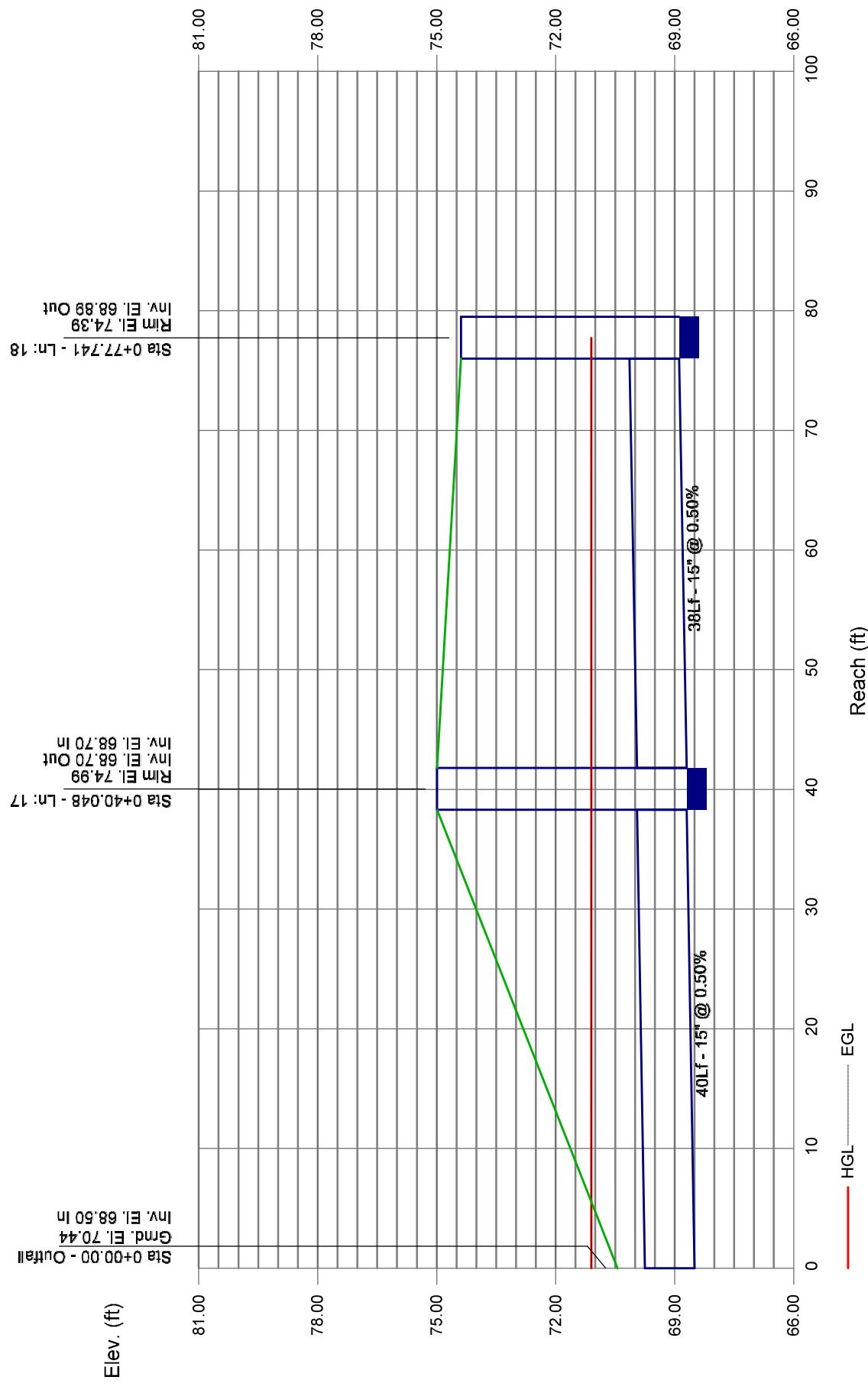
NOTES: \*\* Critical depth

Number of lines: 20

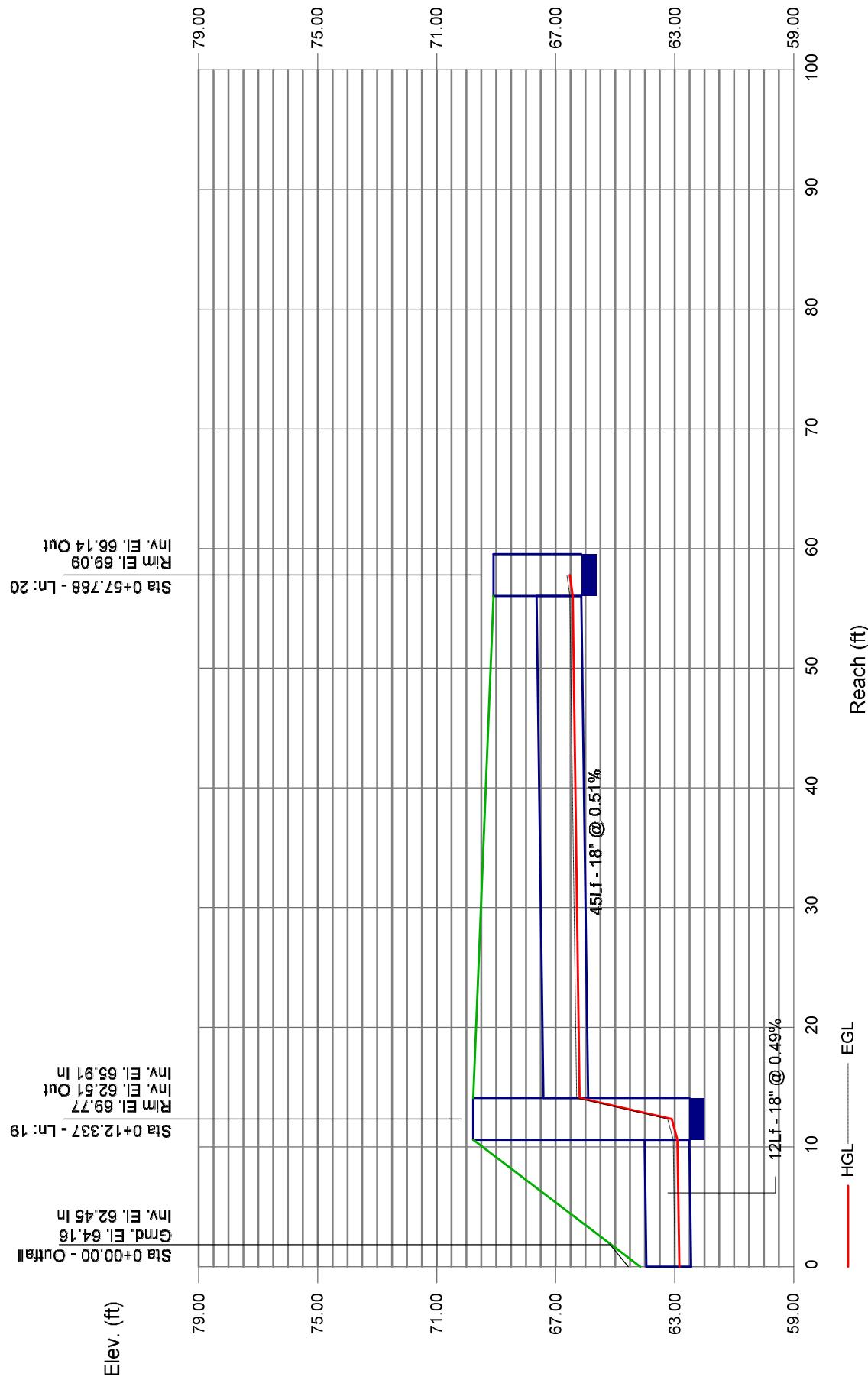
Date: 1/1/2020



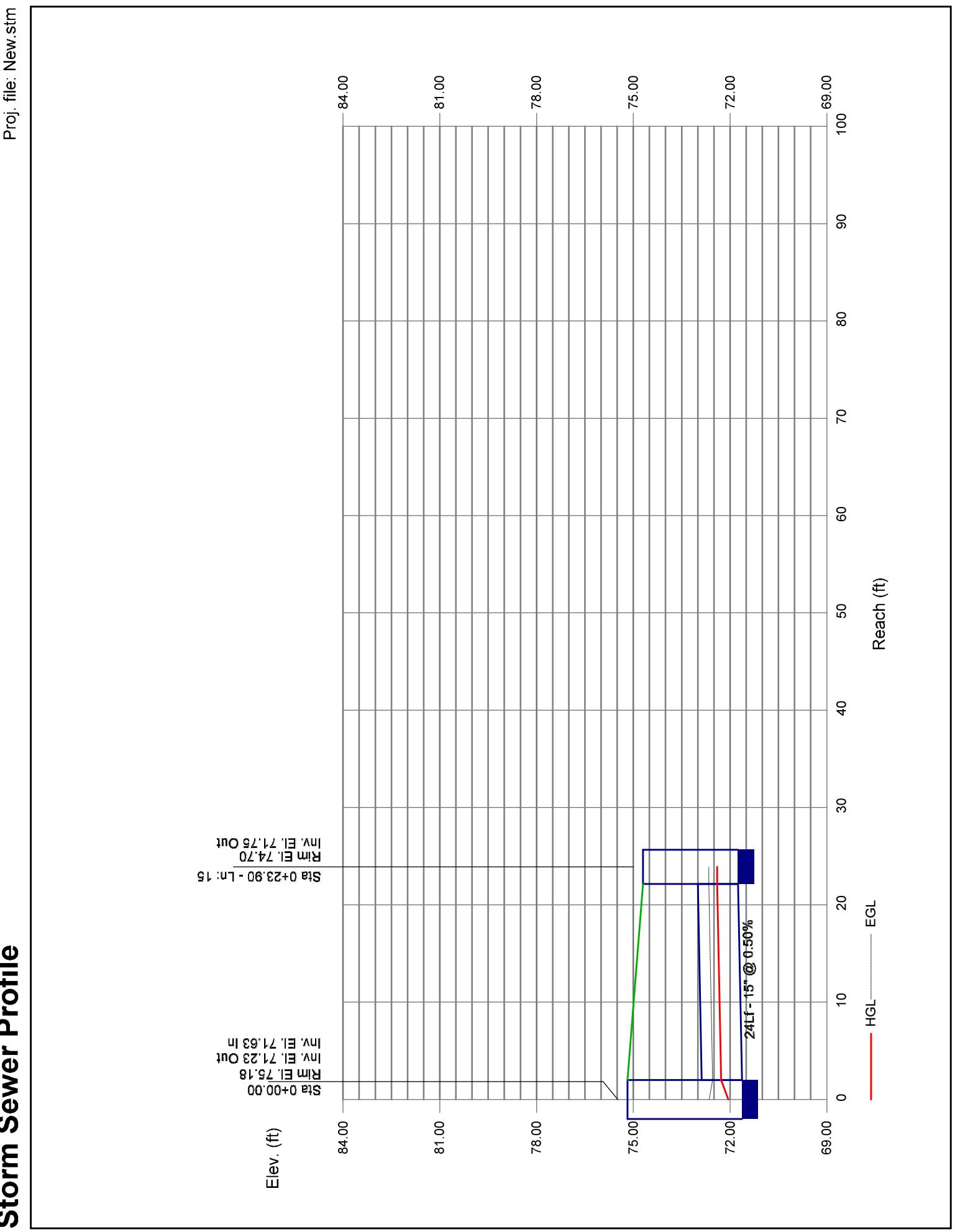
# Storm Sewer Profile



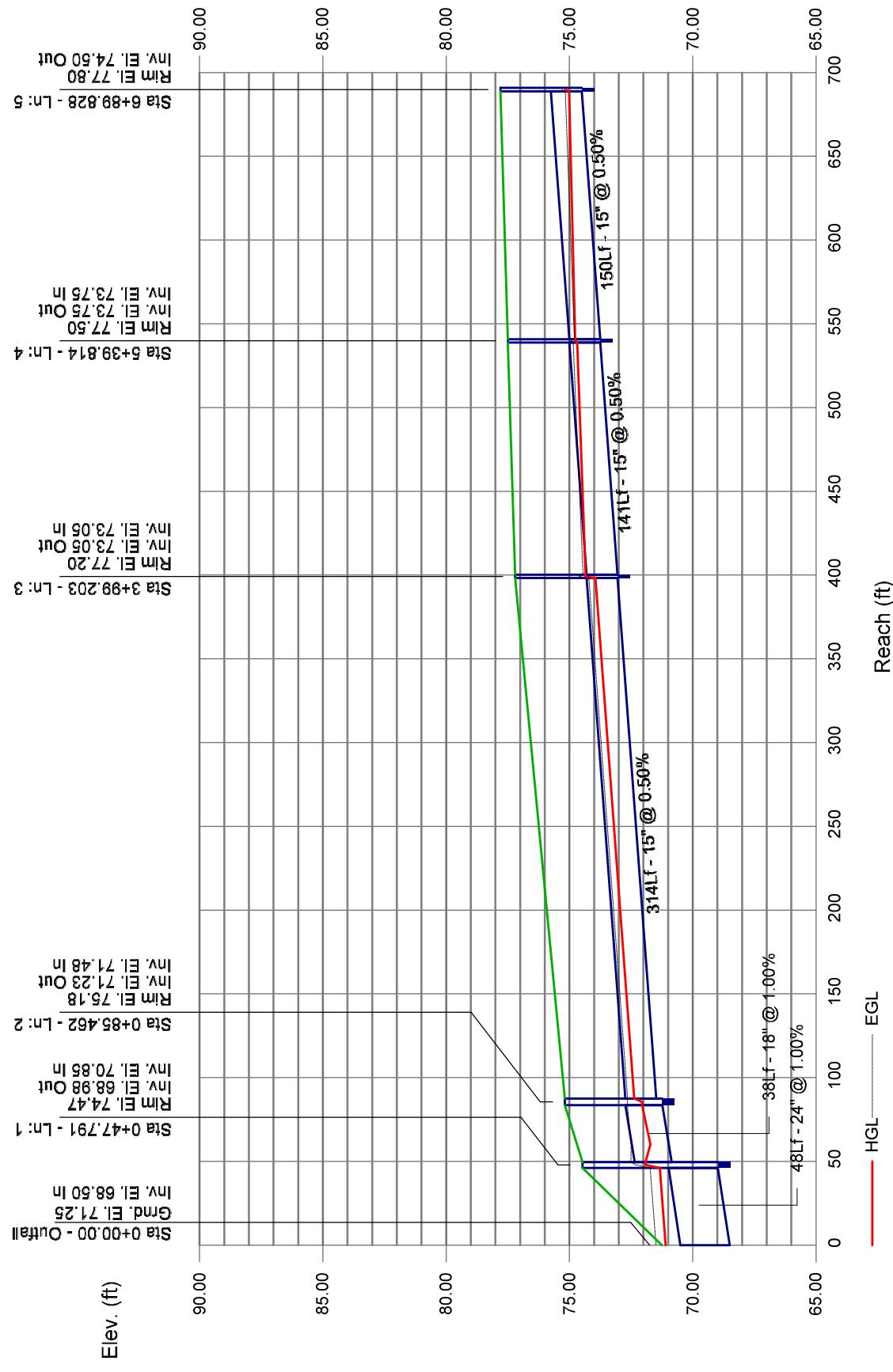
# Storm Sewer Profile



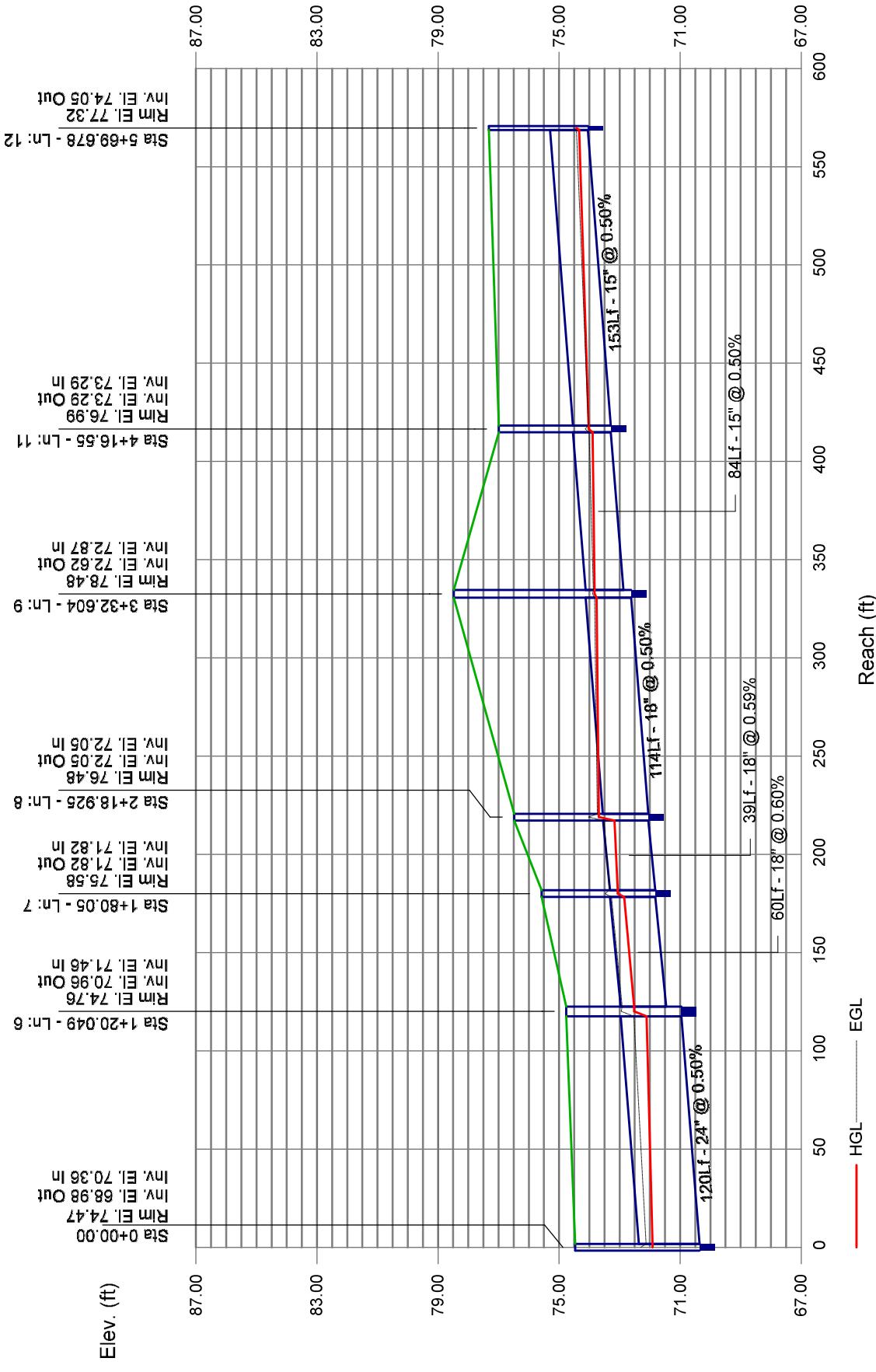
# Storm Sewer Profile



# Storm Sewer Profile



# Storm Sewer Profile







## **APPENDIX F**

Conduit Outlet Protection & Curb Cut Calculaitons



# CONDUIT OUTLET PROTECTION

Project: Elizabeth Realty Partners LLC

Calc. By: MSB Date: 10/26/2020

Location: Franklin Township (Somerset)

Checked By: MSY Date: \_\_\_\_\_

Outlet #	Do, Outlet Dia. (ft)	Q (cfs)	TW (ft)	q=Q/Do	La (ft)	Width at outlet (3xDo) (ft)	W, Width at end (ft)	d50 (in)	COMMENTS
HW - S-100	2	15.73	2.59	7.87	17	6	12.8	3	THICKNESS = 6"
		$q=15.73/2$ $=7.87$		$La=3(7.87)/2^{0.5}$ $=16.69$ use 17'		$W=3(2)+0.4(17)=12.8'$			$D50=0.016(7.77^{1.33})/2.59$ $=.094'=1.13''$ Use 3"
HW - S-300	1.25	0.36	2.59	0.29	4	3.75	5.4	3	THICKNESS = 6"
		$q=0.36/1.25$ $=0.29$		$La=3(0.29)/1.25^{0.5}$ $=0.83$ use 4'		$W=3(1.5)+0.4(4)=5.4$			$D50=0.016(0.29^{1.33})/2.59$ $=0.001'=0.02''$ Use 3"

DESIGN IN ACCORDANCE WITH STANDARD FOR SOIL EROSION AND SEDIMENT CONTROL IN NEW JERSEY.

FOR TW<0.5 Do (FT):

Do-DIAMETER OF OUTLET, FT.

$$La = (1.8 \times q)/(Do^{0.5})+7(Do)$$

Q-DESIGN STORM DISCHARGE, CFS

$$W=3Do+La$$

q=Q/Do

La-LENGTH OF APRON, FT.

FOR TW≥1/2 Do(FT):

W-WIDTH OF APRON, FT.

$$La = (3 \times q)/(Do^{0.5})$$

d50-MEDIAN STONE SIZE, FT.

$$W=3Do+0.4La$$

TW-TAILWATER DEPTH, FT

RIPRAP (FT):

TAILWATER MEASUREMENTS:

$$d50=(0.016/TW)(q)^{1.33}$$

TW=0.2Do FOR DISCHARGE ABOVE FLOOD ELEVATION.

$$TW=(2 \text{ yr FLOOD ELEV.})-(INVERT ELEV.)$$



MADE BY:	MSB	DATE:	10/30/20	DRAINAGE CALCULATIONS								
REV. BY:		DATE:		PROJECT	Elizabeth Ave							
				PROJ. NO.	1900649A							
Scour Hole Conduit Outlet Protection Computation												
	Scour Hole Location	D <sub>o</sub> (ft)	W <sub>o</sub> (ft)	Q (cfs)	TW (ft)	Y (ft)	D <sub>50</sub> (in)	3Do (ft)	2Wo (ft)	L (ft)	W (ft)	Stone Thickness
	HW S-502	1.50	1.50	1.13	0.30	0.75	.3 inch	4.5	3.0	9.0	7.5	.7 inch
	HW S-403	1.50	1.50	9.41	0.30	0.75	5.7 inch	4.5	3.0	9.0	7.5	11.5 inch





PROJECT- ELIZABETH REALTY PARTNERS LLC  
NUMBER- 19000649A  
BY- MSB  
DATE- 10/12/2020  
REVISED-

### Rip Rap Slope Protection Calculations - Rip Rap Slope Protection for Curb Cut #1

#### **1. Peak Runoff Calculations**

Runoff Coefficient, C=	0.99
Rainfall Intensity, i=	5.01 inches/hour
Drainage Area, A=	0.21 Acres
10 Year Runoff, Q <sub>(10)</sub> =	1.04 CFS

#### **2. Riprap Calculations**

Bottom Width, b=	5 ft
Bed Slope, S=	0.33 ft/ft
Unit Discharge, q=	0.21 CFS/ft

$$D_{50} = [q(s)^{0.58} / 3.93(10)^{-2}]^{1/1.89}$$

$$\text{Riprap Size, } D_{50} = 1.7 \text{ inches}$$

$$n = 0.047(D_{50}S)^{0.147}$$

$$\text{Mannings, } n = 0.043$$

$$z = [n(q)/1.486(S)]^{3/5}$$

$$\text{Flow depth, } z = 0.07 \text{ ft}$$

#### **3. Riprap Slope Protection Dimensions**

Bottom Width, W=	5 ft
D <sub>50</sub> =	3 inches
Thickness, T=	6 inches
Channel Depth, Z=	0.5 ft

See Rip Rap Slope Protection Detail on Construction Details sheet.

See Inlet Area Map for contributory drainage area.



PROJECT- ELIZABETH REALTY PARTNERS LLC  
NUMBER- 19000649A  
BY- MSB  
DATE- 10/12/2020  
REVISED-

### **Rip Rap Slope Protection Calculations - Rip Rap Slope Protection for Curb Cut #1**

#### **1. Peak Runoff Calculations**

Runoff Coefficient, C=	0.99
Rainfall Intensity, i=	5.01 inches/hour
Drainage Area, A=	0.36 Acres
10 Year Runoff, Q <sub>(10)</sub> =	1.79 CFS

#### **2. Riprap Calculations**

Bottom Width, b=	5 ft
Bed Slope, S=	0.33 ft/ft

Unit Discharge, q=	0.36 CFS/ft
--------------------	-------------

$$D_{50} = [q(s)^{0.58} / 3.93(10)^{-2}]^{1/1.89}$$

Riprap Size, D <sub>50</sub> =	2.3 inches
--------------------------------	------------

$$n = 0.047(D_{50}S)^{0.147}$$

Mannings, n=	0.045
--------------	-------

$$z = [n(q)/1.486(S)^{0.50}]^{3/5}$$

Flow depth, z=	0.09 ft
----------------	---------

#### **3. Riprap Slope Protection Dimensions**

Bottom Width, W=	5 ft
D <sub>50</sub> =	3 inches
Thickness, T=	6 inches
Channel Depth, Z=	0.5 ft

See Rip Rap Slope Protection Detail on Construction Details sheet.

See Inlet Area Map for contributory drainage area.



## **APPENDIX G**

Soil Test Pit Logs and Permeability Results

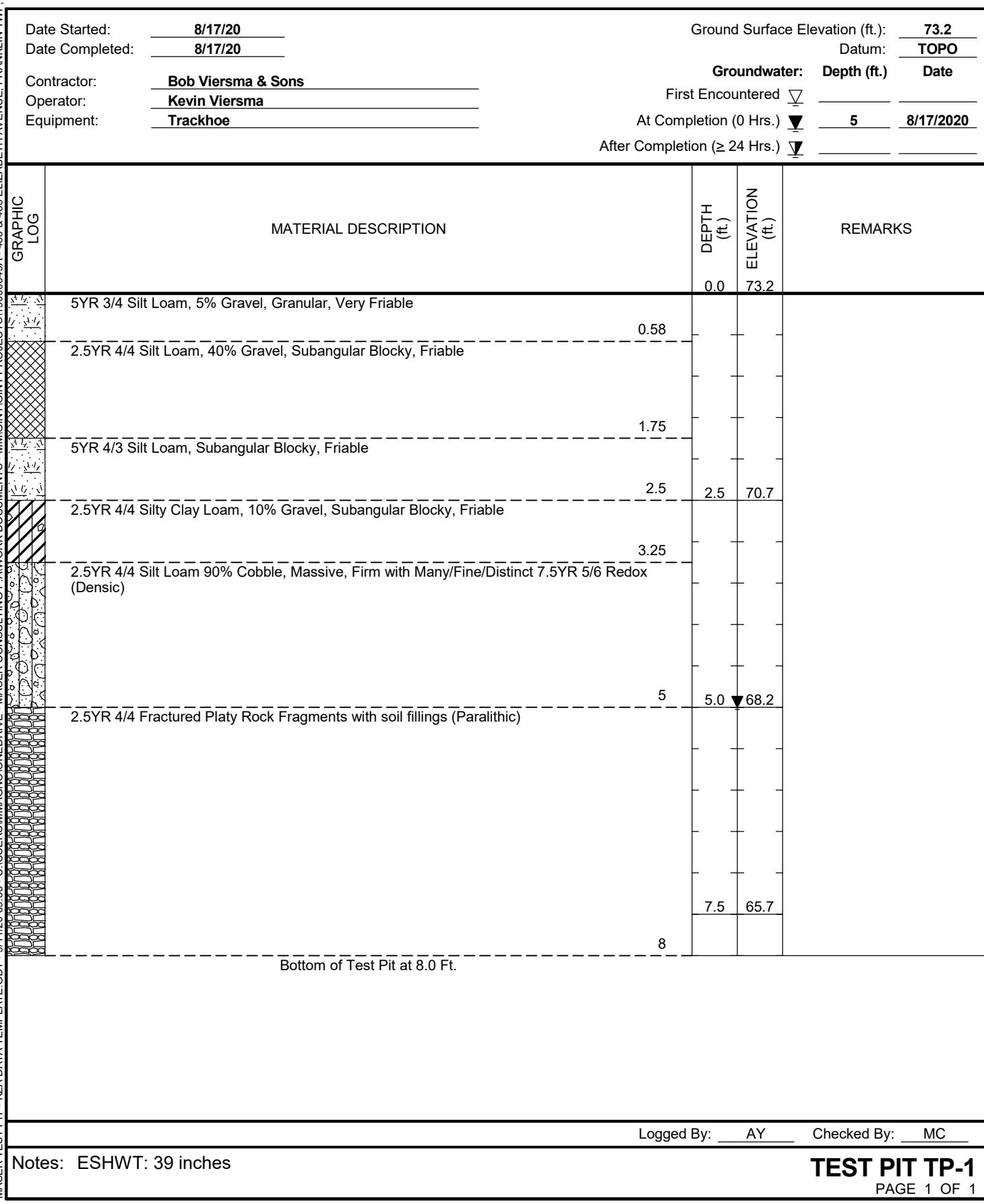




Project: 483 & 485 ELIZABETH AVENUE  
 Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
 Number: 19000649A

# TEST PIT TP-1

PAGE 1 OF 1

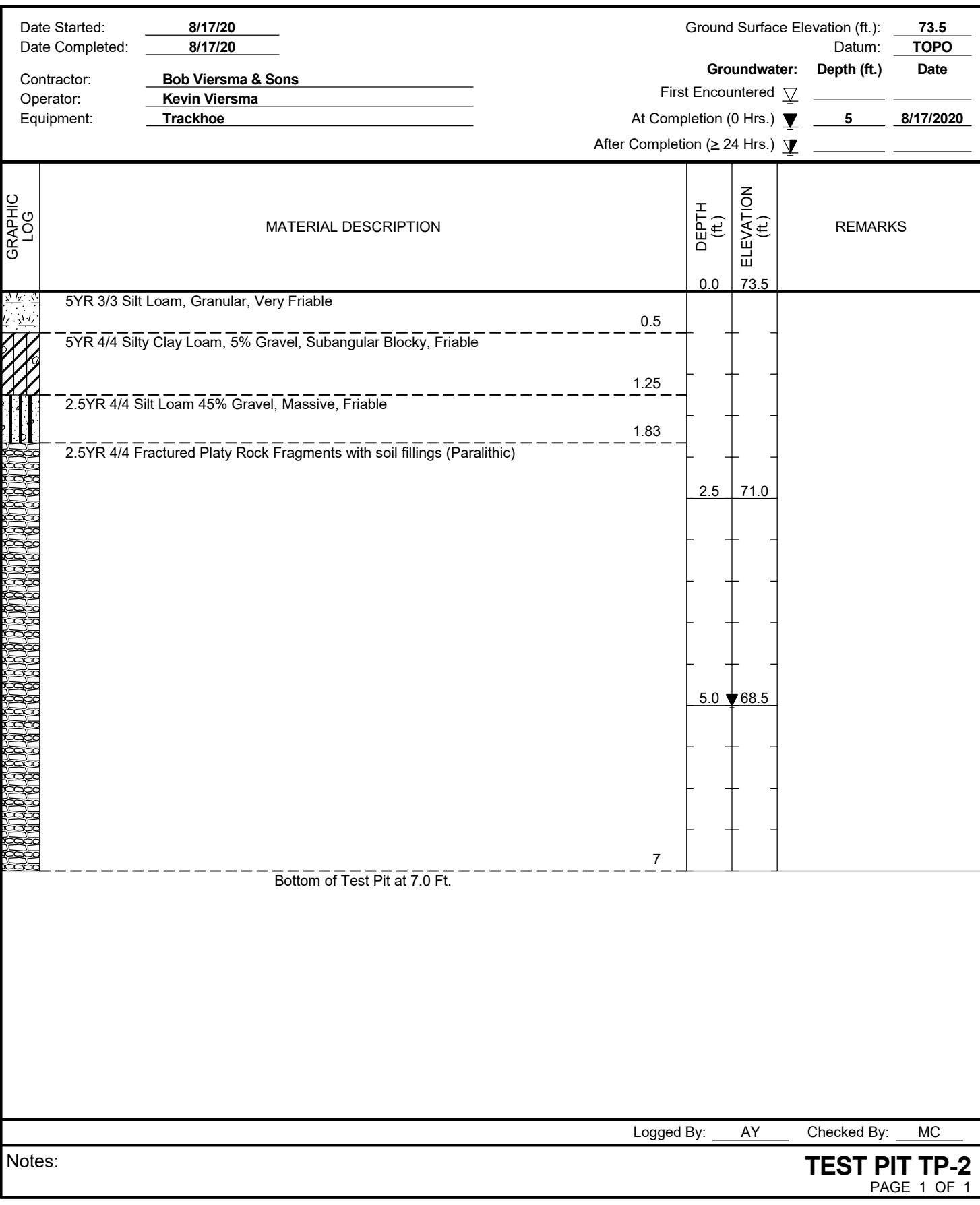




Consulting, Municipal & Environmental Engineers  
Planners • Surveyors • Landscape Architects

Project: 483 & 485 ELIZABETH AVENUE  
Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

TEST PIT TP-2  
PAGE 1 OF 1





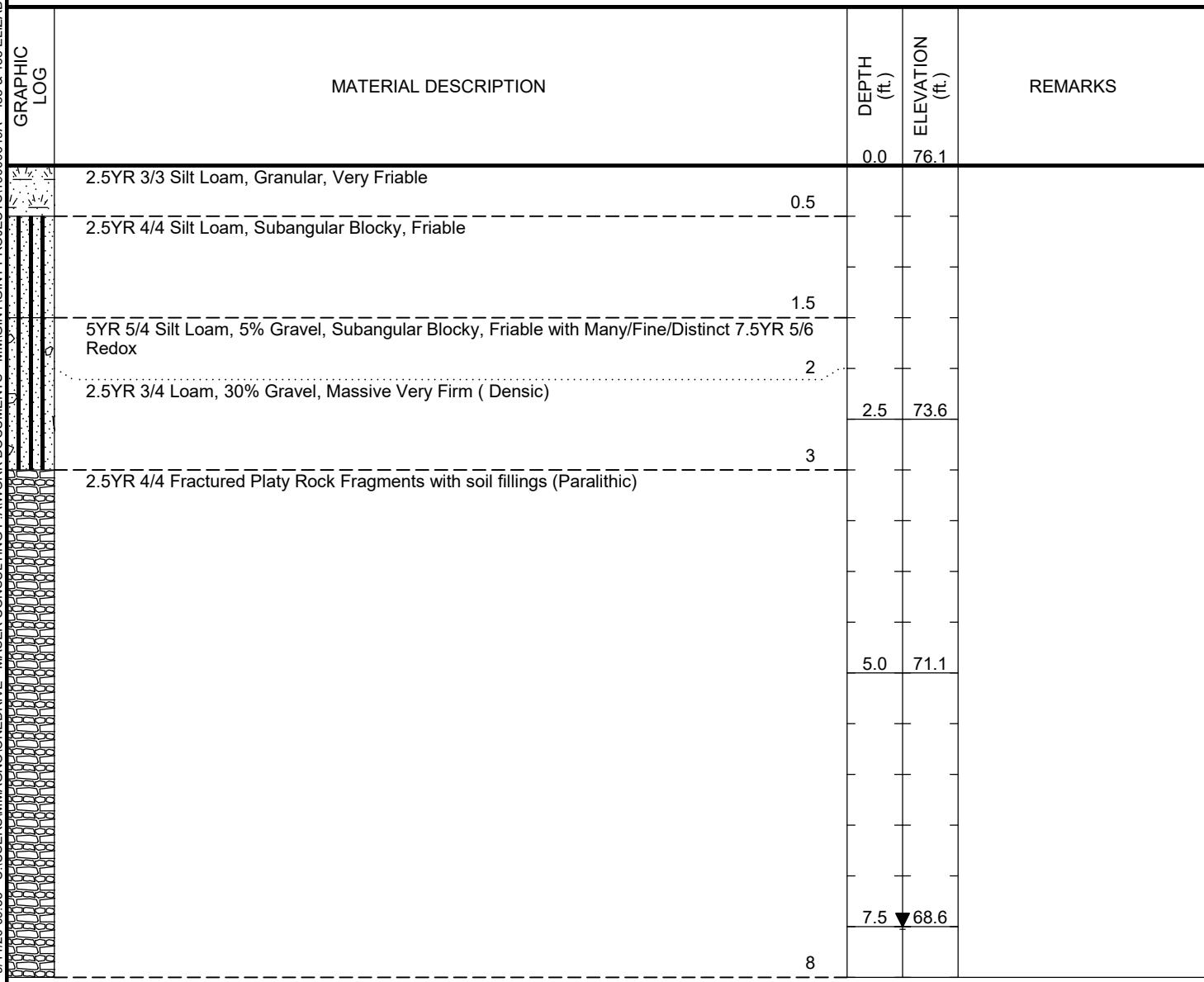
Consulting, Municipal & Environmental Engineers  
Planners • Surveyors • Landscape Architects

Project: 483 & 485 ELIZABETH AVENUE  
Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

# TEST PIT TP-3

PAGE 1 OF 1

Date Started:	8/17/20	Ground Surface Elevation (ft.):	76.1
Date Completed:	8/17/20	Datum:	TOPO
Contractor:	Bob Viersma & Sons	Groundwater:	Depth (ft.)
Operator:	Kevin Viersma	First Encountered	▽
Equipment:	Trackhoe	At Completion (0 Hrs.)	▽ 7.5 8/17/2020
		After Completion ( $\geq$ 24 Hrs.)	▽



Logged By: AY Checked By: MC

Notes: ESHWT: 20 inches

# TEST PIT TP-3

PAGE 1 OF 1



Consulting, Municipal & Environmental Engineers  
Planners • Surveyors • Landscape Architects

Project: 483 & 485 ELIZABETH AVENUE  
Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

TEST PIT TP-4  
PAGE 1 OF 1

Date Started:	8/17/20	Ground Surface Elevation (ft.):	74.3
Date Completed:	8/17/20	Datum:	TOPO
Contractor:	Bob Viersma & Sons	Groundwater:	Depth (ft.) Date
Operator:	Kevin Viersma	First Encountered	▽
Equipment:	Trackhoe	At Completion (0 Hrs.)	▽ 4.1 8/17/2020
		After Completion ( $\geq$ 24 Hrs.)	▽
GRAPHIC LOG	MATERIAL DESCRIPTION	DEPTH (ft.)	ELEVATION (ft.)
		0.0	74.3
	2.5YR 4/4 Silt Loam, 10% Gravel, Granular, Very Friable	0.5	
	2.5YR 3/4 Silt Loam, 40% Gravel, Subangular Blocky, Friable	1.5	
	5YR 4/3 Silt Loam, 5% Gravel, Subangular Blocky, Friable	2	
	5YR 4/4 Silty Clay Loam 5% Gravel, Subangular Blocky, Friable with Many/Fine/Faint 7.5YR 5/6 Redox	2.5	71.8
	2.5YR 4/4 Fractured Platy Rock Fragments with soil fillings (Paralithic)	3	
		5.0	69.3
		7.5	66.8
	Bottom of Test Pit at 8.0 Ft.	8	
Notes: ESHWT: 24 inches		Logged By: AY	Checked By: MC
		TEST PIT TP-4 PAGE 1 OF 1	



Consulting • Municipal & Environmental Engineers  
Planners • Surveyors • Landscape Architects

Project: 483 & 485 ELIZABETH AVENUE  
Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

TEST PIT TP-5  
PAGE 1 OF 1

Date Started:	8/17/20	Ground Surface Elevation (ft.):	81	
Date Completed:	8/17/20	Datum:	TOPO	
Contractor:	Bob Viersma & Sons	Groundwater:	Depth (ft.) Date	
Operator:	Kevin Viersma	First Encountered	▽ _____	
Equipment:	Trackhoe	At Completion (0 Hrs.)	▽ 7.7 8/17/2020	
After Completion ( $\geq$ 24 Hrs.)	▽ _____			
GRAPHIC LOG	MATERIAL DESCRIPTION	DEPTH (ft.)	ELEVATION (ft.)	REMARKS
	5YR 2.5/1 Silt Loam, Granular, Very Friable 7.5YR 5/4 Silt Loam 5% Gravel, Subangular Blocky, Friable 5YR 5/4 Fractured Platy Shale with 2% Soil Fillings	0.0 0.5 1.58 2.5 5.0 7.5 10	81.0 78.5 76.0 73.5 71.0 AY MC	
	Bottom of Test Pit at 10.0 Ft.	Logged By:	AY	Checked By: MC
Notes:				
				TEST PIT TP-5 PAGE 1 OF 1



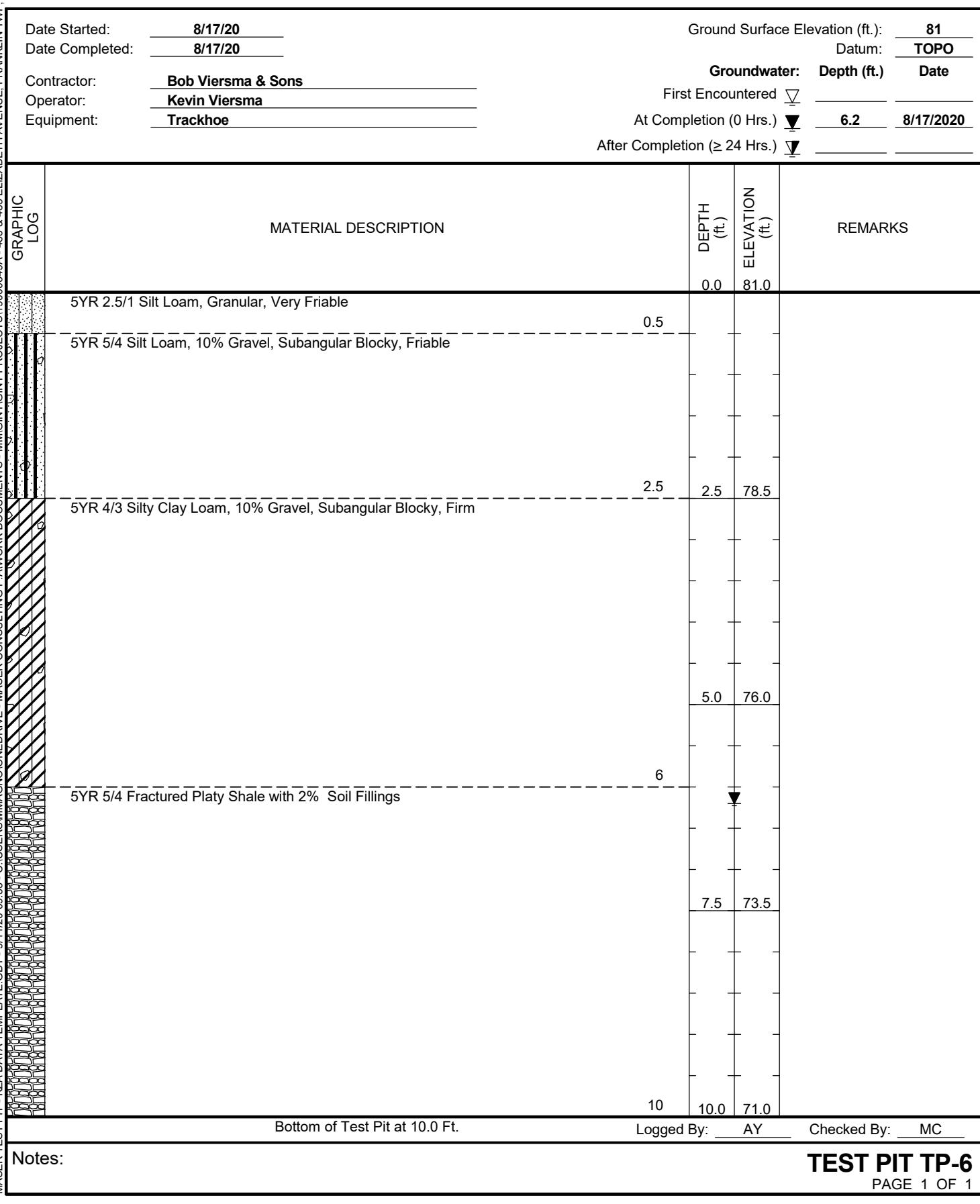
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Project: 483 & 485 ELIZABETH AVENUE  
Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

# TEST PIT TP-6

PAGE 1 OF 1

MASER TEST PIT - KZA DATA TEMPLATE.GDT - 9/11/20 09:55 - C:\USERS\MMAGNO\ONEDRIVE - MASER CONSULTING PA\WORK DOCUMENTS - MMGINTGINT PROJECTS\19000649A - 483 & 485 ELIZABETH AVENUE, FRANKLIN TWP, NJ.GPJ





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Project: 483 & 485 ELIZABETH AVENUE  
Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

# TEST PIT TP-7

PAGE 1 OF 1

MASER TEST PIT - KZA DATA TEMPLATE.GDT - 9/11/20 09:55 - C:\USERS\MMAGNO\ONEDRIVE - MASER CONSULTING PA\WORK DOCUMENTS - MMGINTGINT PROJECTS\19000649A - 483 & 485 ELIZABETH AVENUE, FRANKLIN TWP, NJ.GPJ

Date Started:	8/17/20	Ground Surface Elevation (ft.):	78.3	
Date Completed:	8/17/20	Datum:	TOPO	
Contractor:	Bob Viersma & Sons	Groundwater:	Depth (ft.)	
Operator:	Kevin Viersma	First Encountered	▽	
Equipment:	Trackhoe	At Completion (0 Hrs.)	▽ NE 8/17/2020	
		After Completion ( $\geq$ 24 Hrs.)	▽	
GRAPHIC LOG	MATERIAL DESCRIPTION	DEPTH (ft.)	ELEVATION (ft.)	REMARKS
		0.0	78.3	
	5YR 3/4 Silt Loam, Granular, Very Friable	0.5		
	5YR 4/4 Silty Clay Loam, 20% Gravel, 5% Cobble, Subangular Blocky, Friable	2		
	5YR 4/3 Loam, 20% Gravel, Subangular Blocky, Very Friable	2.5	75.8	
	2.5YR 4/4 Fractured Platy Rock Fragments with soil fillings (Paralithic)	5	5.0	73.3
	Bottom of Test Pit at 6.0 Ft.	6		
Notes:	Logged By: AY			Checked By: MC
				TEST PIT TP-7
				PAGE 1 OF 1



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Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

# TEST PIT TP-8

PAGE 1 OF 1

Date Started:	8/17/20	Ground Surface Elevation (ft.):	75.4		
Date Completed:	8/17/20	Datum:	TOPO		
Contractor:	Bob Viersma & Sons	Groundwater:	Depth (ft.)		
Operator:	Kevin Viersma	First Encountered	▽		
Equipment:	Trackhoe	At Completion (0 Hrs.)	▽ NE 8/17/2020		
		After Completion ( $\geq$ 24 Hrs.)	▽		
GRAPHIC LOG	MATERIAL DESCRIPTION	DEPTH (ft.)	ELEVATION (ft.)	REMARKS	
		0.0	75.4		
	5YR 4/4 Silt Loam, Granular, Very Friable	0.5			
	5YR 5/4 Silty Clay Loam, 10% Gravel, Subangular Blocky, Firm				
	2.5YR 4/4 Silt Loam, 50% Gravel, Massive, Friable	2	72.9		
	2.5YR 4/4 Fractured Platy Rock Fragments with soil fillings (Paralithic)	3			
		5.0	70.4		
		7.5	67.9		
	Bottom of Test Pit at 8.0 Ft.	8			
Notes:		Logged By:	AY	Checked By:	MC
<b>TEST PIT TP-8</b> PAGE 1 OF 1					



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Project: 483 & 485 ELIZABETH AVENUE  
Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

# TEST PIT TP-9

PAGE 1 OF 1

MASER TEST PIT - KZA DATA TEMPLATE.GDT - 9/11/20 09:55 - C:\USERS\MMAGNO\ONEDRIVE - MASER CONSULTING PA\WORK DOCUMENTS - MMGINTGNT PROJECTS\19000649A - 483 & 485 ELIZABETH AVENUE, FRANKLIN TWP, NJ.GPJ

Date Started: 8/17/20  
Date Completed: 8/17/20

Ground Surface Elevation (ft.): 78.3  
Datum: TOPO

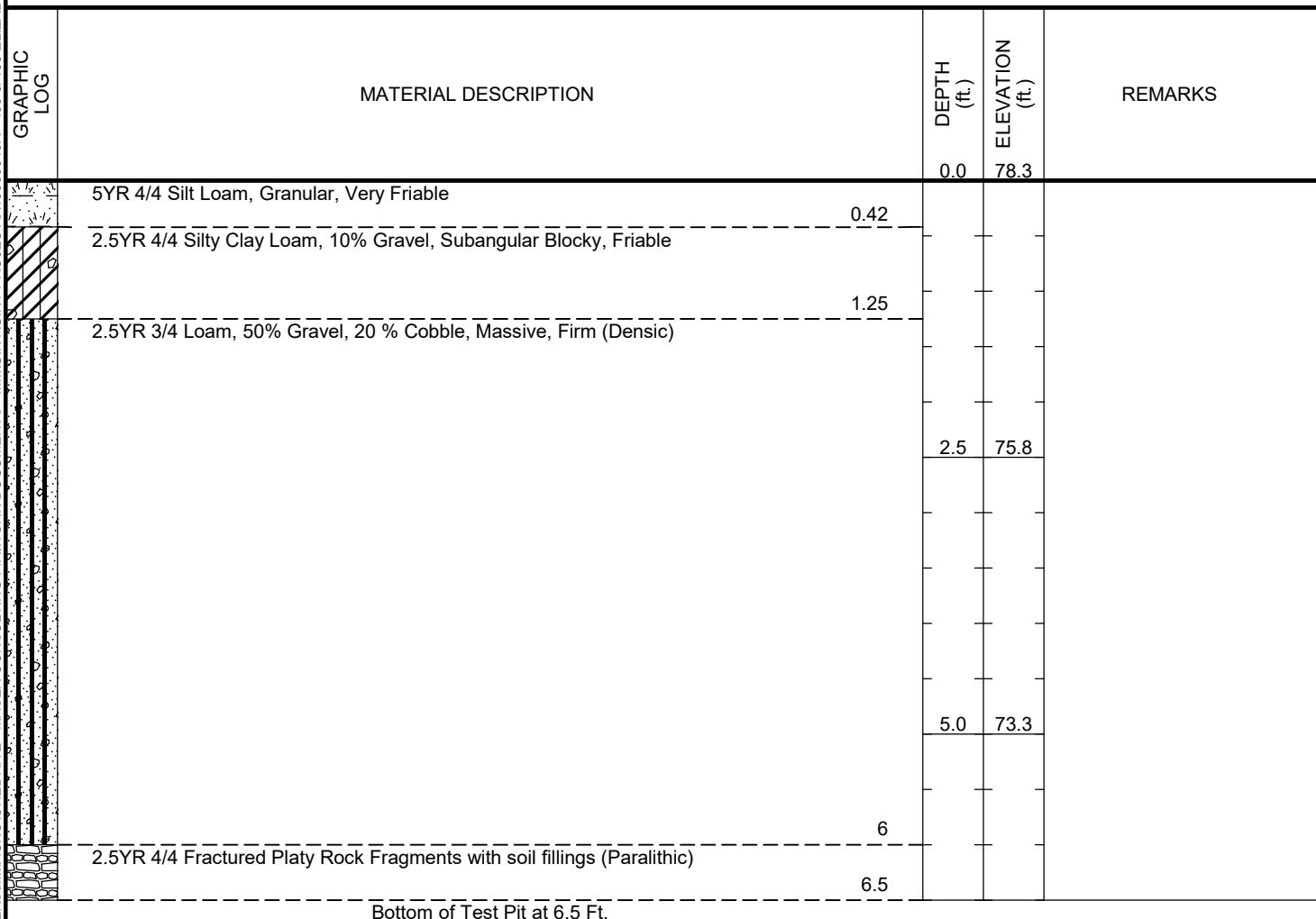
Contractor: Bob Viersma & Sons  
Operator: Kevin Viersma  
Equipment: Trackhoe

Groundwater: Depth (ft.) Date

First Encountered ▽ \_\_\_\_\_

At Completion (0 Hrs.) ▽ NE 8/17/2020

After Completion (≥ 24 Hrs.) ▽ \_\_\_\_\_



Logged By: AY Checked By: MC

Notes:

# TEST PIT TP-9

PAGE 1 OF 1



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Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ  
Number: 19000649A

# TEST PIT TP-10

PAGE 1 OF 1

MASER TEST PIT - KZA DATA TEMPLATE.GDT - 9/11/20 09:55 - C:\USERS\MMAGNO\ONEDRIVE - MASER CONSULTING PA\WORK DOCUMENTS - MMGINTGINT PROJECTS\19000649A - 483 & 485 ELIZABETH AVENUE, FRANKLIN TWP, NJ.GPJ

Date Started:	8/17/20	Ground Surface Elevation (ft.):	79.8	
Date Completed:	8/17/20	Datum:	TOPO	
Contractor:	Bob Viersma & Sons	Groundwater:	Depth (ft.) Date	
Operator:	Kevin Viersma	First Encountered	<input type="button" value="▼"/>	
Equipment:	Trackhoe	At Completion (0 Hrs.)	<input type="button" value="▼"/> NE 8/17/2020	
		After Completion ( $\geq$ 24 Hrs.)	<input type="button" value="▼"/>	
GRAPHIC LOG	MATERIAL DESCRIPTION	DEPTH (ft.)	ELEVATION (ft.)	REMARKS
		0.0	79.8	
	5YR 3/3 Silt Loam, 5% Gravel, Granular, Very Friable	0.42		
	5YR 5/4 Silt Loam, 5% Gravel, Platy, Friable	1		
	2.5YR 4/4 Silty Clay Loam, 20% Gravel, 5% Cobble, Subangular Blocky, Friable	1.67		
	2.5YR 3/4 Silt Loam, 90% Cobble, Massive, Very Firm (Densic)	2.5	77.3	
		5.0	74.8	
		6		
	Bottom of Test Pit at 6.0 Ft.			
Notes:	Logged By:	AY	Checked By:	MC
<b>TEST PIT TP-10</b>				PAGE 1 OF 1



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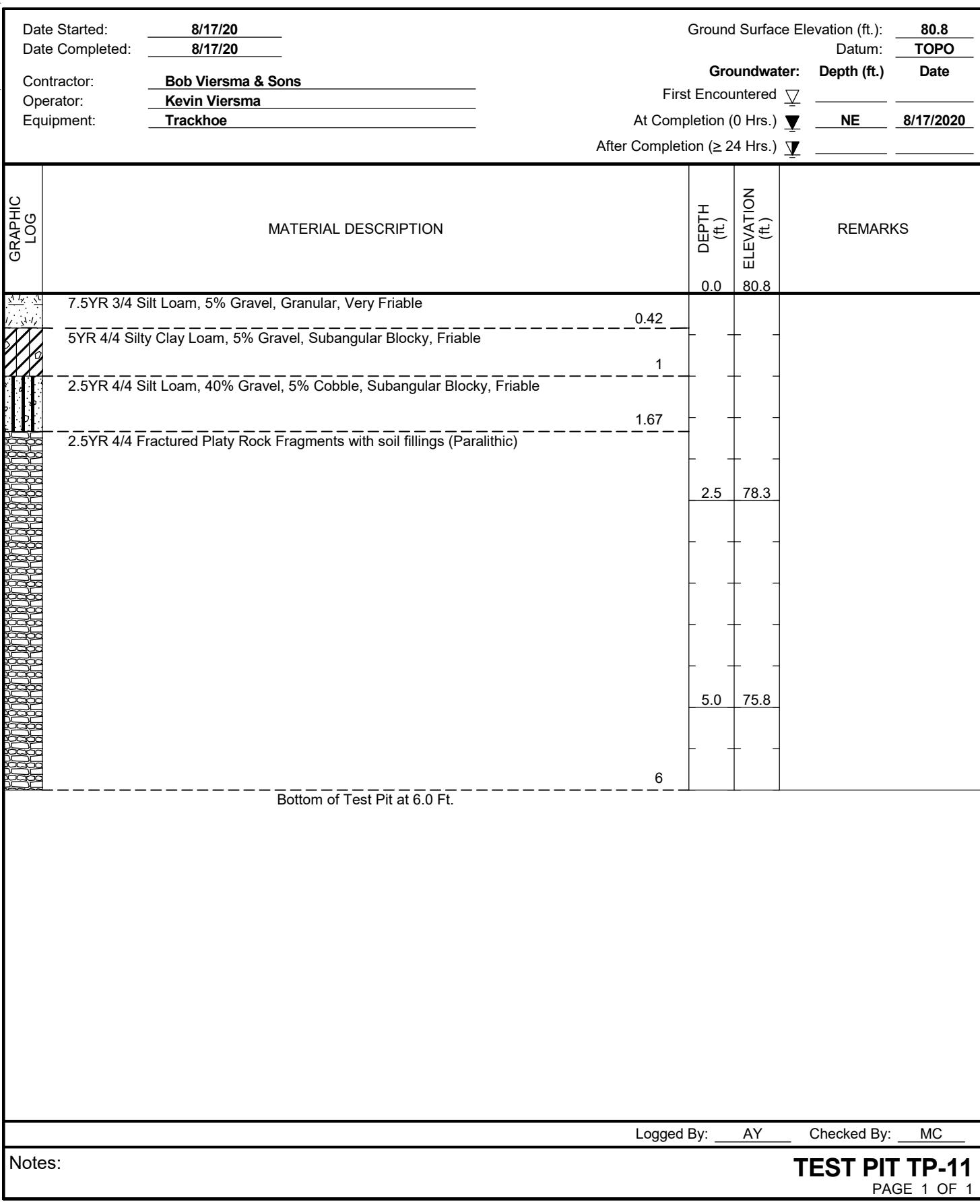
Project: 483 & 485 ELIZABETH AVENUE

Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ

Number: 19000649A

# TEST PIT TP-11

PAGE 1 OF 1





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Location: FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ

Number: 19000649A

# TEST PIT TP-12

PAGE 1 OF 1

Date Started:	8/17/20	Ground Surface Elevation (ft.):	85.3		
Date Completed:	8/17/20	Datum:	TOPO		
Contractor:	Bob Viersma & Sons	Groundwater:	Depth (ft.) Date		
Operator:	Kevin Viersma	First Encountered	▽ _____		
Equipment:	Trackhoe	At Completion (0 Hrs.)	▽ NE 8/17/2020		
After Completion ( $\geq$ 24 Hrs.)	▽ _____				
GRAPHIC LOG	MATERIAL DESCRIPTION	DEPTH (ft.)	ELEVATION (ft.)	REMARKS	
	7.5YR 3/3 Silt Loam, 5% Gravel, Granular, Very Friable 5YR 5/6 Silt Loam, 20% Gravel, Subangular Blocky, Friable 2.5YR 4/4 Fractured Platy Rock Fragments with soil fillings (Paralithic)	0.0 0.5 1.67 2.5 5	85.3 82.8 80.3 5.0		
Bottom of Test Pit at 5.0 Ft.					
Notes:		Logged By:	AY	Checked By:	MC
<b>TEST PIT TP-12</b>					
PAGE 1 OF 1					



**483 & 485 ELIZABETH AVENUE  
MC PROJECT NO. 19000649A**

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## **APPENDIX B**

### **TUBE PERMEAMETER TEST RESULTS**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-1A **Depth:** 7"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	14.7	4.96	2.875	121.7	106.1
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	128.5	2.142	19.0	0.78	1.025	0.80
2	90.0	80.0	10.0	125.1	2.086	19.0	0.80	1.025	0.82
3	90.0	80.0	10.0	129.8	2.163	19.0	0.77	1.025	0.79
4	80.0	70.0	10.0	191.6	3.194	19.0	0.59	1.025	0.61
5	80.0	70.0	10.0	194.6	3.243	19.0	0.58	1.025	0.60
6	80.0	70.0	10.0	192.7	3.212	19.0	0.59	1.025	0.61
7	70.0	60.0	10.0	293.8	4.897	18.4	0.45	1.041	0.47
8	70.0	60.0	10.0	295.7	4.928	18.4	0.44	1.041	0.46
9	70.0	60.0	10.0	299.7	4.995	18.4	0.44	1.041	0.46
10	60.0	50.0	10.0	383.5	6.391	18.0	0.40	1.051	0.43
11	60.0	50.0	10.0	388.9	6.481	18.0	0.40	1.051	0.42
12	60.0	50.0	10.0	383.9	6.398	18.0	0.40	1.051	0.43
13	50.0	40.0	10.0	553.6	9.226	18.0	0.34	1.051	0.36
14	50.0	40.0	10.0	558.4	9.306	18.0	0.34	1.051	0.36
15	50.0	40.0	10.0	557.5	9.291	18.0	0.34	1.051	0.36

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr): 0.53**

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS: K1**

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Some localized gaps in soil due to gravel pieces and organic matter



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-1B **Depth:** 7"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	14.7	4.48	2.875	118.2	103.1
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	21.7	0.362	19.0	4.18	1.025	4.29
2	90.0	80.0	10.0	21.6	0.361	19.0	4.19	1.025	4.30
3	90.0	80.0	10.0	21.6	0.360	19.0	4.20	1.025	4.31
4	80.0	70.0	10.0	35.9	0.598	19.0	2.87	1.025	2.94
5	80.0	70.0	10.0	35.6	0.593	19.0	2.89	1.025	2.96
6	80.0	70.0	10.0	35.7	0.595	19.0	2.88	1.025	2.95
7	70.0	60.0	10.0	45.5	0.758	19.0	2.61	1.025	2.68
8	70.0	60.0	10.0	45.5	0.758	19.0	2.61	1.025	2.68
9	70.0	60.0	10.0	45.6	0.759	19.0	2.61	1.025	2.67
10	60.0	50.0	10.0	52.8	0.879	19.0	2.66	1.025	2.73
11	60.0	50.0	10.0	52.9	0.882	19.0	2.66	1.025	2.72
12	60.0	50.0	10.0	52.8	0.879	19.0	2.66	1.025	2.73
13	50.0	40.0	10.0	64.1	1.068	19.0	2.68	1.025	2.75
14	50.0	40.0	10.0	64.2	1.070	19.0	2.68	1.025	2.75
15	50.0	40.0	10.0	64.2	1.070	19.0	2.68	1.025	2.75

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 3.08

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K3

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Some localized gaps in soil due to gravel pieces and organic matter



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-1A **Depth:** 30"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	22.7	4.83	2.875	123.5	100.6
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	4.2	0.069	19.7	23.52	1.008	23.70
2	90.0	80.0	10.0	4.3	0.071	19.7	23.03	1.008	23.20
3	90.0	80.0	10.0	4.3	0.071	19.7	22.92	1.008	23.09
4	80.0	70.0	10.0	5.8	0.096	19.7	19.30	1.008	19.44
5	80.0	70.0	10.0	5.9	0.098	19.7	18.93	1.008	19.08
6	80.0	70.0	10.0	5.8	0.097	19.7	19.16	1.008	19.31
7	70.0	60.0	10.0	7.8	0.130	19.7	16.46	1.008	16.59
8	70.0	60.0	10.0	8.0	0.133	19.7	16.01	1.008	16.13
9	70.0	60.0	10.0	8.2	0.136	19.7	15.66	1.008	15.78
10	60.0	50.0	10.0	10.0	0.167	19.7	15.15	1.008	15.26
11	60.0	50.0	10.0	10.3	0.172	19.7	14.65	1.008	14.76
12	60.0	50.0	10.0	10.2	0.171	19.7	14.81	1.008	14.92
13	50.0	40.0	10.0	14.3	0.239	19.7	12.96	1.008	13.05
14	50.0	40.0	10.0	14.1	0.235	19.7	13.16	1.008	13.26
15	50.0	40.0	10.0	14.7	0.245	19.7	12.60	1.008	12.69

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 17.35

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Localized void along sample wall but did not extend full length of sample.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-1B **Depth:** 30"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	25.5	5.04	2.875	125.0	99.6
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	16.1	0.268	19.6	6.34	1.010	6.40
2	90.0	80.0	10.0	16.2	0.271	19.6	6.28	1.010	6.34
3	90.0	80.0	10.0	16.3	0.271	19.6	6.26	1.010	6.32
4	80.0	70.0	10.0	21.4	0.357	19.4	5.39	1.015	5.47
5	80.0	70.0	10.0	21.4	0.356	19.4	5.41	1.015	5.49
6	80.0	70.0	10.0	21.4	0.357	19.4	5.39	1.015	5.47
7	70.0	60.0	10.0	26.4	0.441	19.4	5.05	1.015	5.12
8	70.0	60.0	10.0	26.5	0.441	19.4	5.04	1.015	5.12
9	70.0	60.0	10.0	26.5	0.442	19.4	5.03	1.015	5.11
10	60.0	50.0	10.0	31.4	0.523	19.3	5.03	1.018	5.12
11	60.0	50.0	10.0	31.2	0.520	19.3	5.05	1.018	5.14
12	60.0	50.0	10.0	31.3	0.521	19.3	5.05	1.018	5.13
13	50.0	40.0	10.0	39.4	0.656	19.2	4.91	1.020	5.00
14	50.0	40.0	10.0	39.2	0.654	19.2	4.92	1.020	5.02
15	50.0	40.0	10.0	39.4	0.656	19.2	4.91	1.020	5.00

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 5.42

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K3

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Localized void along sample wall but did not extend full length of sample.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-2A **Depth:** 6"

**Visual Description of Soil (USCS):** Brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type: Undisturbed <input checked="" type="checkbox"/>	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Re-Compacted <input type="checkbox"/>	27.5	5.02	2.875	110.6	86.8

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	12.8	0.213	18.7	7.97	1.033	8.23
2	90.0	80.0	10.0	12.8	0.213	18.7	7.97	1.033	8.23
3	90.0	80.0	10.0	12.8	0.214	18.7	7.93	1.033	8.19
4	80.0	70.0	10.0	16.1	0.268	18.7	7.18	1.033	7.41
5	80.0	70.0	10.0	16.2	0.269	18.7	7.13	1.033	7.37
6	80.0	70.0	10.0	16.2	0.269	18.7	7.14	1.033	7.37
7	70.0	60.0	10.0	19.4	0.323	18.9	6.87	1.028	7.06
8	70.0	60.0	10.0	19.4	0.323	18.9	6.87	1.028	7.06
9	70.0	60.0	10.0	19.4	0.324	18.9	6.85	1.028	7.04
10	60.0	50.0	10.0	23.2	0.387	18.9	6.78	1.028	6.96
11	60.0	50.0	10.0	23.3	0.388	18.9	6.76	1.028	6.95
12	60.0	50.0	10.0	23.3	0.389	18.9	6.75	1.028	6.94
13	50.0	40.0	10.0	30.6	0.510	19.0	6.30	1.025	6.45
14	50.0	40.0	10.0	30.6	0.509	19.0	6.30	1.025	6.46
15	50.0	40.0	10.0	30.6	0.510	19.0	6.30	1.025	6.46

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 7.21

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-2B **Depth:** 6"

**Visual Description of Soil (USCS):** Brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	30.9	4.90	2.875	111.6	85.3
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	29.0	0.484	18.7	3.41	1.033	3.52
2	90.0	80.0	10.0	29.9	0.498	18.7	3.32	1.033	3.43
3	90.0	80.0	10.0	29.8	0.497	18.7	3.32	1.033	3.43
4	80.0	70.0	10.0	37.2	0.620	18.9	3.02	1.028	3.10
5	80.0	70.0	10.0	37.2	0.621	18.9	3.02	1.028	3.10
6	80.0	70.0	10.0	37.3	0.622	18.9	3.01	1.028	3.10
7	70.0	60.0	10.0	54.6	0.909	18.6	2.38	1.036	2.46
8	70.0	60.0	10.0	54.6	0.910	18.6	2.38	1.036	2.46
9	70.0	60.0	10.0	54.6	0.909	18.6	2.38	1.036	2.46
10	60.0	50.0	10.0	64.4	1.074	18.5	2.38	1.038	2.47
11	60.0	50.0	10.0	64.5	1.075	18.5	2.38	1.038	2.47
12	60.0	50.0	10.0	64.5	1.076	18.5	2.38	1.038	2.47
13	50.0	40.0	10.0	93.9	1.565	18.4	2.00	1.041	2.08
14	50.0	40.0	10.0	93.9	1.565	18.4	2.00	1.041	2.08
15	50.0	40.0	10.0	94.0	1.566	18.4	2.00	1.041	2.08

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 2.71

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K3

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-3A **Depth:** 5"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type: Undisturbed <input checked="" type="checkbox"/>	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Re-Compacted <input type="checkbox"/>	17.9	4.81	2.875	107.1	90.9

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	62.7	1.045	19.0	1.55	1.025	1.59
2	90.0	80.0	10.0	61.8	1.029	19.0	1.58	1.025	1.62
3	90.0	80.0	10.0	62.8	1.046	19.0	1.55	1.025	1.59
4	80.0	70.0	10.0	84.3	1.404	18.9	1.31	1.028	1.35
5	80.0	70.0	10.0	82.1	1.369	18.9	1.34	1.028	1.38
6	80.0	70.0	10.0	83.4	1.390	18.9	1.32	1.028	1.36
7	70.0	60.0	10.0	88.7	1.478	18.8	1.44	1.030	1.48
8	70.0	60.0	10.0	79.2	1.320	18.8	1.61	1.030	1.66
9	70.0	60.0	10.0	79.4	1.324	18.8	1.60	1.030	1.65
10	60.0	50.0	10.0	93.9	1.565	18.7	1.61	1.033	1.66
11	60.0	50.0	10.0	93.3	1.555	18.7	1.62	1.033	1.67
12	60.0	50.0	10.0	92.5	1.541	18.7	1.63	1.033	1.68
13	50.0	40.0	10.0	118.6	1.977	18.6	1.56	1.036	1.61
14	50.0	40.0	10.0	116.1	1.935	18.6	1.59	1.036	1.65
15	50.0	40.0	10.0	117.5	1.959	18.6	1.57	1.036	1.63

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 1.57

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K2

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-3B **Depth:** 5"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type: Undisturbed <input checked="" type="checkbox"/>	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Re-Compacted <input type="checkbox"/>	18.7	4.85	2.875	108.4	91.3

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	2.2	0.037	19.6	44.86	1.010	45.31
2	90.0	80.0	10.0	2.2	0.036	19.6	45.48	1.010	45.94
3	90.0	80.0	10.0	2.2	0.037	19.6	44.26	1.010	44.70
4	80.0	70.0	10.0	2.5	0.041	19.5	45.09	1.013	45.66
5	80.0	70.0	10.0	2.4	0.039	19.5	47.40	1.013	47.99
6	80.0	70.0	10.0	2.4	0.040	19.5	46.22	1.013	46.80
7	70.0	60.0	10.0	2.9	0.049	19.4	44.19	1.015	44.85
8	70.0	60.0	10.0	2.8	0.047	19.4	45.28	1.015	45.96
9	70.0	60.0	10.0	2.9	0.048	19.4	44.80	1.015	45.48
10	60.0	50.0	10.0	3.2	0.053	19.0	48.28	1.025	49.50
11	60.0	50.0	10.0	3.1	0.052	19.0	48.59	1.025	49.81
12	60.0	50.0	10.0	3.2	0.053	19.0	47.67	1.025	48.88
13	50.0	40.0	10.0	3.7	0.062	19.0	50.04	1.025	51.30
14	50.0	40.0	10.0	3.7	0.062	19.0	50.31	1.025	51.57
15	50.0	40.0	10.0	3.7	0.061	19.0	50.58	1.025	51.85

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 47.7

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K5

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Localized void along sample wall but did not extend full length of sample.
- Sample was very loose inside of the tube. Sample able to slide up and down within the tube during preparation.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-4A **Depth:** 6"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	17.0	4.37	2.875	127.2	108.7
Re-Compacted <input type="checkbox"/>					

Radius of Burette, r: 0.3141 in

Radius of Soil Specimen, R: 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	4.6	0.076	19.0	19.38	1.025	19.86
2	90.0	80.0	10.0	4.7	0.078	19.0	19.00	1.025	19.48
3	90.0	80.0	10.0	4.7	0.079	19.0	18.76	1.025	19.23
4	80.0	70.0	10.0	8.2	0.137	19.0	12.23	1.025	12.54
5	80.0	70.0	10.0	8.2	0.137	19.0	12.26	1.025	12.57
6	80.0	70.0	10.0	8.3	0.138	19.0	12.17	1.025	12.48
7	70.0	60.0	10.0	9.2	0.153	18.9	12.67	1.028	13.02
8	70.0	60.0	10.0	9.2	0.154	18.9	12.56	1.028	12.90
9	70.0	60.0	10.0	9.2	0.153	18.9	12.62	1.028	12.97
10	60.0	50.0	10.0	10.2	0.169	18.9	13.50	1.028	13.88
11	60.0	50.0	10.0	10.2	0.170	18.9	13.48	1.028	13.85
12	60.0	50.0	10.0	10.1	0.168	18.9	13.57	1.028	13.95
13	50.0	40.0	10.0	12.9	0.216	18.9	12.97	1.028	13.33
14	50.0	40.0	10.0	13.0	0.216	18.9	12.92	1.028	13.28
15	50.0	40.0	10.0	12.9	0.215	18.9	12.98	1.028	13.34

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

AVERAGE k<sub>20</sub> (in/hr): 14.45

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

SOIL PERMEABILITY CLASS: K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Large stone at top of sample.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-4A **Depth:** 24"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	21.7	4.50	2.875	117.2	96.3
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	7.8	0.129	19.6	11.75	1.010	11.87
2	90.0	80.0	10.0	7.7	0.128	19.6	11.86	1.010	11.98
3	90.0	80.0	10.0	7.7	0.129	19.6	11.80	1.010	11.92
4	80.0	70.0	10.0	8.6	0.144	19.5	11.97	1.013	12.12
5	80.0	70.0	10.0	8.6	0.144	19.5	12.00	1.013	12.15
6	80.0	70.0	10.0	8.6	0.144	19.5	11.97	1.013	12.12
7	70.0	60.0	10.0	9.9	0.165	19.3	12.08	1.018	12.29
8	70.0	60.0	10.0	9.8	0.164	19.3	12.15	1.018	12.37
9	70.0	60.0	10.0	9.9	0.165	19.3	12.06	1.018	12.27
10	60.0	50.0	10.0	11.2	0.186	19.2	12.64	1.020	12.89
11	60.0	50.0	10.0	11.2	0.187	19.2	12.60	1.020	12.86
12	60.0	50.0	10.0	11.1	0.186	19.2	12.67	1.020	12.93
13	50.0	40.0	10.0	13.3	0.222	19.1	12.94	1.023	13.23
14	50.0	40.0	10.0	13.4	0.224	19.1	12.84	1.023	13.13
15	50.0	40.0	10.0	13.4	0.223	19.1	12.89	1.023	13.18

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h1/h2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 12.49

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-7A **Depth:** 6"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	20.1	5.01	2.875	106.7	88.8
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	9.5	0.159	19.0	10.65	1.025	10.92
2	90.0	80.0	10.0	9.6	0.160	19.0	10.60	1.025	10.86
3	90.0	80.0	10.0	9.6	0.159	19.0	10.61	1.025	10.87
4	80.0	70.0	10.0	12.7	0.212	19.0	9.04	1.025	9.27
5	80.0	70.0	10.0	12.8	0.213	19.0	9.02	1.025	9.24
6	80.0	70.0	10.0	12.8	0.214	19.0	8.97	1.025	9.20
7	70.0	60.0	10.0	16.6	0.277	19.0	7.99	1.025	8.20
8	70.0	60.0	10.0	16.8	0.280	19.0	7.89	1.025	8.09
9	70.0	60.0	10.0	16.8	0.281	19.0	7.88	1.025	8.08
10	60.0	50.0	10.0	18.3	0.305	18.9	8.57	1.028	8.81
11	60.0	50.0	10.0	18.3	0.306	18.9	8.56	1.028	8.80
12	60.0	50.0	10.0	18.4	0.307	18.9	8.54	1.028	8.77
13	50.0	40.0	10.0	21.2	0.353	18.9	9.07	1.028	9.32
14	50.0	40.0	10.0	21.2	0.354	18.9	9.06	1.028	9.31
15	50.0	40.0	10.0	21.2	0.353	18.9	9.08	1.028	9.33

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 9.27

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-7B **Depth:** 6"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	20.9	4.87	2.875	114.7	94.9
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	10.6	0.177	18.6	9.29	1.036	9.62
2	90.0	80.0	10.0	10.6	0.177	18.6	9.30	1.036	9.64
3	90.0	80.0	10.0	10.8	0.179	18.6	9.17	1.036	9.50
4	80.0	70.0	10.0	13.2	0.219	18.5	8.50	1.038	8.82
5	80.0	70.0	10.0	13.2	0.219	18.5	8.50	1.038	8.83
6	80.0	70.0	10.0	13.2	0.220	18.5	8.49	1.038	8.81
7	70.0	60.0	10.0	15.3	0.254	18.4	8.46	1.041	8.81
8	70.0	60.0	10.0	15.2	0.253	18.4	8.51	1.041	8.86
9	70.0	60.0	10.0	15.3	0.255	18.4	8.43	1.041	8.77
10	60.0	50.0	10.0	18.8	0.314	18.4	8.12	1.041	8.45
11	60.0	50.0	10.0	18.8	0.314	18.4	8.11	1.041	8.44
12	60.0	50.0	10.0	18.9	0.314	18.4	8.10	1.041	8.43
13	50.0	40.0	10.0	20.0	0.333	18.4	9.36	1.041	9.74
14	50.0	40.0	10.0	20.0	0.333	18.4	9.37	1.041	9.75
15	50.0	40.0	10.0	20.0	0.333	18.4	9.35	1.041	9.73

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 9.08

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-9A **Depth:** 5"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type: Undisturbed <input checked="" type="checkbox"/>	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Re-Compacted <input type="checkbox"/>	23.6	4.88	2.875	118.3	95.7

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	15.9	0.265	19.0	6.22	1.025	6.38
2	90.0	80.0	10.0	15.7	0.262	19.0	6.28	1.025	6.44
3	90.0	80.0	10.0	15.9	0.265	19.0	6.22	1.025	6.38
4	80.0	70.0	10.0	18.8	0.313	19.0	5.97	1.025	6.12
5	80.0	70.0	10.0	18.8	0.313	19.0	5.95	1.025	6.10
6	80.0	70.0	10.0	18.8	0.314	19.0	5.95	1.025	6.10
7	70.0	60.0	10.0	21.2	0.353	18.9	6.11	1.028	6.28
8	70.0	60.0	10.0	21.4	0.357	18.9	6.04	1.028	6.21
9	70.0	60.0	10.0	21.3	0.355	18.9	6.06	1.028	6.23
10	60.0	50.0	10.0	28.6	0.477	18.8	5.34	1.030	5.51
11	60.0	50.0	10.0	28.6	0.476	18.8	5.35	1.030	5.51
12	60.0	50.0	10.0	28.5	0.475	18.8	5.36	1.030	5.52
13	50.0	40.0	10.0	31.5	0.525	18.7	5.94	1.033	6.13
14	50.0	40.0	10.0	31.4	0.524	18.7	5.95	1.033	6.15
15	50.0	40.0	10.0	31.6	0.526	18.7	5.92	1.033	6.12

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 6.08

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Large stone at bottom of sample.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-9B **Depth:** 5"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type: Undisturbed <input checked="" type="checkbox"/>	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Re-Compacted <input type="checkbox"/>	23.0	4.87	2.875	114.4	93.0

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	84.9	1.415	19.2	1.16	1.020	1.18
2	90.0	80.0	10.0	84.8	1.413	19.2	1.16	1.020	1.19
3	90.0	80.0	10.0	84.9	1.415	19.2	1.16	1.020	1.19
4	80.0	70.0	10.0	139.0	2.317	19.1	0.80	1.023	0.82
5	80.0	70.0	10.0	138.9	2.315	19.1	0.80	1.023	0.82
6	80.0	70.0	10.0	139.2	2.321	19.1	0.80	1.023	0.82
7	70.0	60.0	10.0	167.5	2.792	19.0	0.77	1.025	0.79
8	70.0	60.0	10.0	167.6	2.793	19.0	0.77	1.025	0.79
9	70.0	60.0	10.0	167.6	2.793	19.0	0.77	1.025	0.79
10	60.0	50.0	10.0	232.2	3.870	18.7	0.66	1.033	0.68
11	60.0	50.0	10.0	232.3	3.871	18.7	0.66	1.033	0.68
12	60.0	50.0	10.0	232.3	3.871	18.7	0.66	1.033	0.68
13	50.0	40.0	10.0	310.3	5.172	18.7	0.60	1.033	0.62
14	50.0	40.0	10.0	310.5	5.174	18.7	0.60	1.033	0.62
15	50.0	40.0	10.0	310.4	5.174	18.7	0.60	1.033	0.62

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr): 0.82**

**Head, h (4) = (2) - (3); Perm, k<sub>20</sub> (9) = (7)\*(8)**

**SOIL PERMEABILITY CLASS: K2**

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-10A **Depth:** 15"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	Proctor Data:	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:

Undisturbed

Re-Compacted

Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
22.7	4.97	2.875	108.8	88.7

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5	6	7	8	9	
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	771.7	12.861	20.1	0.13	0.998	0.13
2	90.0	80.0	10.0	773.8	12.896	20.1	0.13	0.998	0.13
3	90.0	80.0	10.0	772.5	12.875	20.1	0.13	0.998	0.13
4	80.0	71.0	9.0	900.0	15.000	20.0	0.11	1.000	0.11
5	70.0	62.5	7.5	900.0	15.000	19.8	0.11	1.005	0.11
6	60.0	55.0	5.0	900.0	15.000	19.7	0.08	1.008	0.08
7	50.0	46.3	3.7	900.0	15.000	19.5	0.07	1.013	0.07

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

AVERAGE k<sub>20</sub> (in/hr): 0.11

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

SOIL PERMEABILITY CLASS: K0

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-10B **Depth:** 15"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	18.2	5.07	2.875	111.6	94.4
Re-Compacted <input type="checkbox"/>					

Radius of Burette, r: 0.3141 in

Radius of Soil Specimen, R: 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	21.6	0.360	19.0	4.76	1.025	4.88
2	90.0	80.0	10.0	21.4	0.357	19.0	4.80	1.025	4.92
3	90.0	80.0	10.0	21.5	0.358	19.0	4.78	1.025	4.90
4	80.0	70.0	10.0	25.9	0.432	18.7	4.50	1.033	4.64
5	80.0	70.0	10.0	25.9	0.432	18.7	4.49	1.033	4.64
6	80.0	70.0	10.0	25.7	0.428	18.7	4.53	1.033	4.68
7	70.0	60.0	10.0	30.7	0.512	18.6	4.37	1.036	4.53
8	70.0	60.0	10.0	30.9	0.515	18.6	4.35	1.036	4.51
9	70.0	60.0	10.0	30.8	0.514	18.6	4.36	1.036	4.51
10	60.0	50.0	10.0	41.5	0.692	18.6	3.83	1.036	3.97
11	60.0	50.0	10.0	41.6	0.693	18.6	3.82	1.036	3.96
12	60.0	50.0	10.0	41.5	0.691	18.6	3.83	1.036	3.97
13	50.0	40.0	10.0	58.7	0.978	18.4	3.32	1.041	3.45
14	50.0	40.0	10.0	58.7	0.978	18.4	3.31	1.041	3.45
15	50.0	40.0	10.0	58.7	0.979	18.4	3.31	1.041	3.45

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

AVERAGE k<sub>20</sub> (in/hr): 4.30

Head, h (4) = (2) - (3); Perm, k<sub>20</sub> (9) = (7)\*(8)

SOIL PERMEABILITY CLASS: K3

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Large localized voids along inner tube wall but did not extend full length of sample.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-11A **Depth:** 8"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	21.0	4.71	2.875	115.9	95.8
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	4.9	0.082	19.2	19.47	1.020	19.86
2	90.0	80.0	10.0	4.9	0.082	19.2	19.39	1.020	19.78
3	90.0	80.0	10.0	5.0	0.083	19.2	19.20	1.020	19.58
4	80.0	70.0	10.0	5.2	0.086	19.1	20.96	1.023	21.44
5	80.0	70.0	10.0	5.2	0.087	19.1	20.80	1.023	21.27
6	80.0	70.0	10.0	5.1	0.086	19.1	21.09	1.023	21.56
7	70.0	60.0	10.0	6.1	0.102	19.1	20.37	1.023	20.83
8	70.0	60.0	10.0	6.6	0.109	19.1	19.06	1.023	19.50
9	70.0	60.0	10.0	6.6	0.110	19.1	18.95	1.023	19.38
10	60.0	50.0	10.0	6.9	0.115	19.0	21.40	1.025	21.94
11	60.0	50.0	10.0	6.9	0.116	19.0	21.31	1.025	21.85
12	60.0	50.0	10.0	7.0	0.116	19.0	21.19	1.025	21.72
13	50.0	40.0	10.0	8.2	0.136	19.0	22.15	1.025	22.71
14	50.0	40.0	10.0	8.3	0.138	19.0	21.86	1.025	22.41
15	50.0	40.0	10.0	8.2	0.137	19.0	21.96	1.025	22.52

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 21.09

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K5

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Localized void along sample wall but did not extend full length of sample.
- Sample was very loose inside of the tube. Sample able to slide up and down within the tube during preparation.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-11B **Depth:** 8"

**Visual Description of Soil (USCS):** Red brown silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	22.5	4.72	2.875	109.9	89.7
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	8.6	0.144	19.6	11.06	1.010	11.17
2	90.0	80.0	10.0	8.6	0.143	19.6	11.10	1.010	11.21
3	90.0	80.0	10.0	8.7	0.146	19.6	10.94	1.010	11.05
4	80.0	70.0	10.0	9.7	0.161	19.4	11.22	1.015	11.39
5	80.0	70.0	10.0	9.7	0.161	19.4	11.22	1.015	11.39
6	80.0	70.0	10.0	9.6	0.160	19.4	11.25	1.015	11.42
7	70.0	60.0	10.0	11.2	0.187	19.3	11.14	1.018	11.33
8	70.0	60.0	10.0	11.4	0.189	19.3	11.00	1.018	11.19
9	70.0	60.0	10.0	11.3	0.188	19.3	11.09	1.018	11.28
10	60.0	50.0	10.0	12.9	0.216	19.2	11.43	1.020	11.66
11	60.0	50.0	10.0	13.0	0.216	19.2	11.39	1.020	11.61
12	60.0	50.0	10.0	13.0	0.216	19.2	11.39	1.020	11.62
13	50.0	40.0	10.0	13.3	0.222	19.2	13.56	1.020	13.83
14	50.0	40.0	10.0	13.2	0.221	19.2	13.67	1.020	13.95
15	50.0	40.0	10.0	13.3	0.221	19.2	13.65	1.020	13.93

**Perm, k<sub>T</sub> (7) = 60 \* L/t \* r<sup>2</sup>/R<sup>2</sup> \* ln(h1/h2) = 60\* L/(5) \* r<sup>2</sup>/R<sup>2</sup> \* ln((2)/(3))**

**AVERAGE k<sub>20</sub> (in/hr): 11.87**

**Head, h (4) = (2) - (3); Perm, k<sub>20</sub> (9) = (7)\*(8)**

**SOIL PERMEABILITY CLASS: K4**

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-12A **Depth:** 12"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>	12.0	4.66	2.875	75.4	67.3
Re-Compacted <input type="checkbox"/>					

**Radius of Burette, r:** 0.3141 in

**Radius of Soil Specimen, R:** 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	5.2	0.087	19.1	18.06	1.023	18.47
2	90.0	80.0	10.0	5.3	0.088	19.1	17.96	1.023	18.37
3	90.0	80.0	10.0	5.3	0.088	19.1	17.89	1.023	18.30
4	80.0	70.0	10.0	6.7	0.112	19.0	15.98	1.025	16.38
5	80.0	70.0	10.0	6.7	0.112	19.0	15.91	1.025	16.31
6	80.0	70.0	10.0	6.8	0.113	19.0	15.74	1.025	16.14
7	70.0	60.0	10.0	8.4	0.140	19.0	14.71	1.025	15.08
8	70.0	60.0	10.0	8.4	0.139	19.0	14.78	1.025	15.15
9	70.0	60.0	10.0	8.4	0.141	19.0	14.62	1.025	14.99
10	60.0	50.0	10.0	9.5	0.158	18.9	15.40	1.028	15.83
11	60.0	50.0	10.0	9.4	0.157	18.9	15.48	1.028	15.91
12	60.0	50.0	10.0	9.5	0.158	18.9	15.41	1.028	15.84
13	50.0	40.0	10.0	12.9	0.215	18.9	13.88	1.028	14.27
14	50.0	40.0	10.0	12.9	0.215	18.9	13.86	1.028	14.24
15	50.0	40.0	10.0	12.8	0.213	18.9	13.98	1.028	14.37

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

**AVERAGE k<sub>20</sub> (in/hr):** 15.98

$$\text{Head, } h (4) = (2) - (3); \text{ Perm, } k_{20} (9) = (7)*(8)$$

**SOIL PERMEABILITY CLASS:** K4

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Sample was very loose inside of the tube. Sample able to slide up and down within the tube during preparation.



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## TUBE PERMEAMETER TEST

(N.J.A.C. 7:9A - Standards for Individual Subsurface Sewage Disposal Systems; Subchapter 6, Section 6.2, page 39, Modified)

**Client:** John Kainer **MC #:** 19000649A  
**Project:** 483 and 485 Elizabeth Avenue, Franklin Township, NJ **Date:** September 11, 2020  
**Boring/Sample # or Descrip./Location:** TP-12B **Depth:** 12"

**Visual Description of Soil (USCS):** Brown red silty/clayey SAND with gravel and trace organics

Technician: K. Perry	<b>Proctor Data:</b>	Max Dry Density (pcf)	% of Max Dry Density	Opt. Moisture (%)
		-	-	-

**Initial Specimen Data:**

Sample Type:	Water Content (%)	Length, L (in)	Diameter (in)	Wet Density (pcf)	Dry Density (pcf)
Undisturbed <input checked="" type="checkbox"/>					
Re-Compacted <input type="checkbox"/>	11.1	5.02	2.875	84.0	75.6

Radius of Burette, r: 0.3141 in

Radius of Soil Specimen, R: 1.4375 in

### TEST DATA

1	2	3	4	5		6	7	8	9
Trial No.	Burette Readings		Head, h (cm)	Time, t		Temp, T (°C)	Permeability at T°C, k <sub>T</sub>	Temp Correc.	Permeability at 20°C, k <sub>20</sub>
	h <sub>1</sub> (cm)	h <sub>2</sub> (cm)		Sec	Min				
1	90.0	80.0	10.0	33.0	0.550	19.1	3.08	1.023	3.15
2	90.0	80.0	10.0	35.3	0.589	19.1	2.88	1.023	2.94
3	90.0	80.0	10.0	34.2	0.570	19.1	2.97	1.023	3.04
4	80.0	70.0	10.0	43.8	0.731	19.0	2.63	1.025	2.69
5	80.0	70.0	10.0	43.5	0.724	19.0	2.65	1.025	2.72
6	80.0	70.0	10.0	43.8	0.730	19.0	2.63	1.025	2.70
7	70.0	60.0	10.0	57.6	0.959	19.0	2.31	1.025	2.37
8	70.0	60.0	10.0	56.8	0.947	19.0	2.34	1.025	2.40
9	70.0	60.0	10.0	58.2	0.969	19.0	2.29	1.025	2.34
10	60.0	50.0	10.0	69.3	1.155	18.8	2.27	1.030	2.34
11	60.0	50.0	10.0	69.7	1.162	18.8	2.26	1.030	2.33
12	60.0	50.0	10.0	69.7	1.162	18.8	2.26	1.030	2.33
13	50.0	40.0	10.0	87.3	1.455	18.7	2.20	1.033	2.28
14	50.0	40.0	10.0	89.1	1.485	18.7	2.16	1.033	2.23
15	50.0	40.0	10.0	89.3	1.488	18.7	2.16	1.033	2.23

$$\text{Perm, } k_T (7) = 60 * L/t * r^2/R^2 * \ln(h_1/h_2) = 60 * L/(5) * r^2/R^2 * \ln((2)/(3))$$

AVERAGE k<sub>20</sub> (in/hr): 2.54

Head, h (4) = (2) - (3); Perm, k<sub>20</sub> (9) = (7)\*(8)

SOIL PERMEABILITY CLASS: K3

**Soil Permeability Classes**

> 20 inches per hour (in/hr)	K5
6 - 20 in/hr	K4
2 - 6 in/hr	K3
0.6 - 2 in/hr	K2
0.2 - 0.6 in/hr	K1
< 0.2 in/hr	K0

**Remarks**

- Sample was very loose inside of the tube. Sample able to slide up and down within the tube during preparation.





## **APPENDIX H**

### Groundwater Recharge Worksheet



### Annual Groundwater Recharge Analysis (based on GSR-32)

				Project Name: 483 & 485 Elizabeth Avenue			
				Description: 19000649A			
				Analysis Date: 10/7/2020			
Pre-Developed Conditions							
Land Segment	Area (acres)	TR-55 Land Cover	Soil	Annual Recharge (in)	Annual Recharge (cu.ft)	Land Segment	Area (acres)
1	0.33	Impervious areas	Norton	0.0	-	1	3.6
2	3.69	Woods	Norton	12.5	166,898	2	1.05
3	2.73	Meadow, Pasture, Grassland or range	Norton	12.5	123,874	3	2.1
4	0.43	Woods	Reaville	12.9	20,079	4	0.41
5	0.04	Impervious areas	Reaville	0.0	-	5	0.18
6	1.04	Meadow, Pasture, Grassland or range	Reaville	12.6	47,524	6	0.92
7	0.03	Woods	Penn	12.9	1,400	7	0.03
8	0.03	Impervious areas	Penn	0.0	-	8	0.03
9	0.08	Meadow, Pasture, Grassland or range	Penn	12.6	3,654	9	0.08
10						10	
11						11	
12						12	
13						13	
14						14	
15						15	
Total =	8.4			Total Annual Recharge (in)	Total = 8.4	Total Annual Recharge (in)	Total Annual Recharge (cu.ft)
				11.9	363,429	6.8	208,229
Annual Recharge Requirements Calculation ↓				% of Pre-Developed Annual Recharge to Preserve = 100%			
<b>Post-Development Annual Recharge Deficit= 155,200</b>				<b>(cubic feet)</b>			
<b>Recharge Efficiency Parameters Calculations (area averages)</b>				Total Impenetrable Area (sq.ft)			
RWc= #N/A	(in)			DRWC= #N/A	(in)		
ERWC = #N/A	(in)			EDRWC= #N/A	(in)		

Procedure to fill the Pre-Development and Post-Development Conditions Tables

For each land segment, first enter the area, then select TR-55 Land Cover, then select Soil. Start from the top of the table and proceed downward. Don't leave blank rows (with A=0) in between your segment entries. Rows with A=0 will not be displayed or used in calculations. For impervious areas outside of standard lots select "Impervious Areas" as the Land Cover. Soil type for impervious areas are only required if an infiltration facility will be built within these areas.

Post-Developed Conditions		Land Segment	Area (acres)	TR-55 Land Cover	Soil	Annual Recharge (in)	Annual Recharge (cu.ft)
		1	3.6	Impervious Areas	Norton	0.0	-
		2	1.05	Woods	Norton	12.5	47,491
		3	2.1	Open space	Norton	12.5	95,498
		4	0.41	Woods	Reaville	12.9	19,145
		5	0.18	Impervious Areas	Reaville	0.0	-
		6	0.92	Open space	Reaville	12.3	41,120
		7	0.03	Woods	Penn	12.9	1,400
		8	0.03	Impervious Areas	Penn	0.0	-
		9	0.08	Open space	Penn	12.3	3,574
		10					
		11					
		12					
		13					
		14					
		15					
Total =	8.4			Total Annual Recharge (in)	Total = 8.4	Total Annual Recharge (in)	Total Annual Recharge (cu.ft)
		11.9	363,429			6.8	208,229
% of Pre-Developed Annual Recharge to Preserve = 100%		Total Impenetrable Area (sq.ft)		165,964			

<u>Project Name</u>	<u>Description</u>	<u>Analysis Date</u>	<u>BMP or LID Type</u>
<b>483 &amp; 485 Elizabeth Avenue</b>	<b>19000649A</b>	<b>10/07/20</b>	Pervious Paving
<b>Recharge BMP Input Parameters</b>			
<u>Parameter</u>	<u>Symbol</u>	<u>Value</u>	<u>Unit</u>
BMP Area	ABMP	10270.0	sq.ft
BMP Effective Depth, this is the design variable	dBMP	2.7	in
Upper level of the BMP surface (negative if above ground)	dBMpU	7.0	in
Depth of lower surface of BMP, must be>=dBMPu	dEXC	23.0	in
Post-development Land Segment Location of BMP, Input zero if Location is distributed or undetermined	SegBMP	1	unitless
<b>Root Zone Water capacity Calculated Parameters</b>			
<u>Parameter</u>	<u>Symbol</u>	<u>Value</u>	<u>Unit</u>
Empty Portion of RWC under Post-D Natural Recharge	ERWC	0.73	in
ERWC Modified to consider dEXC	EDRWC	0.00	in
Empty Portion of RWC under Infiltr. BMP	RERWC	0.00	in
<b>Recharge Design Parameters</b>			
<u>Parameter</u>	<u>Symbol</u>	<u>Value</u>	<u>Unit</u>
Inches of Runoff to capture	Qdesign	0.17	in
Inches of Rainfall to capture	Pdesign	0.23	in
Recharge Provided Avg. over Imp. Area		11.2	in
Runoff Captured Avg. over Imp. Area		11.2	in
<b>CALCULATION CHECK MESSAGES</b>			
Volume Balance->	OK		
dBMP Check->	OK		
dEXC Check-->	OK		
BMP Location-->	OK		
<b>Parameters from Annual Recharge Worksheet</b>			
<u>System Performance Calculated Parameters</u>			
Post-D Deficit Recharge (or desired recharge volume)	Vdef	<b>155,200</b>	cu.ft
Post-D Impervious Area (or target Impervious Area)	Aimp	<b>165,964</b>	sq.ft
Root Zone Water Capacity	RWC	<b>2.82</b>	in
RWC Modified to consider dEXC	DRWC	<b>0.00</b>	in
Climatic Factor	C-factor	<b>1.48</b>	no units
Average Annual P	Pavg	<b>45.7</b>	in
Recharge Requirement over Imp. Area	dr	<b>11.2</b>	in
<b>OTHER NOTES</b>			
PostD is accurate only after BMP dimensions are updated to make rech volume= deficit volume. The portion of BMP infiltration prior to filling and the area occupied by BMP are ignored in these calculations. Results are sensitive to dBMP, make sure dBMP selected is small enough for BMP to empty in less than 3 days. For land Segment Location of BMP if you select "impervious areas" RWC will be minimal but not zero as determined by the soil type and a shallow root zone for this Land Cover allowing consideration of lateral flow and other losses.			
<b>How to solve for different recharge volumes:</b> By default the spreadsheet assigns the values of total deficit recharge volume "Vdef" and "Aimp" on this page. This allows solution for a single BMP to handle the entire recharge requirement assuming the runoff from entire impervious area is available to the BMP. To solve for a smaller BMP or a LID/IMP to recharge only part of the recharge requirement, set Vdef to your target value and Aimp the "Default Vdef & Aimp" button.			



## **APPENDIX I**

### References



This simplification is based on the following assumptions:

- shallow steady uniform flow
- constant rainfall excess intensity (that part of a rain available for runoff) both temporally and spatially
- 2-year, 24-hour rainfall assuming standard NRCS rainfall intensity-duration relations apply (Types I, II, and III)
- minor effect of infiltration on travel time

For sheet flow, the roughness coefficient includes the effects of roughness and the effects of raindrop impact including drag over the surface; obstacles such as litter, crop ridges, and rocks; and erosion and transport of sediment. These  $n$  values are only applicable for flow depths of approximately 0.1 foot or less, where sheet flow occurs. Table 15–1 gives roughness coefficient values for sheet flow for various surface conditions.

Kibler and Aron (1982) and others indicated the maximum sheet flow length is less than 100 feet. To support the sheet flow limit of 100 feet, Merkel (2001) reviewed a number of technical papers on sheet flow. McCuen and Spiess (1995) indicated that use of flow length as the limiting variable in the equation 15–8 could lead to less accurate designs, and proposed that the limitation should instead be based on:

$$\ell = \frac{100\sqrt{S}}{n} \quad (\text{eq. 15-9})$$

**Table 15–2** Maximum sheet flow lengths using the McCuen-Spiess limitation criterion

Cover type	$n$ values	Slope (ft/ft)	Length (ft)
Range	0.13	0.01	77
Grass	0.41	0.01	24
Woods	0.80	0.01	12.5
Range	0.13	0.05	172
Grass	0.41	0.05	55
Woods	0.80	0.05	28

where:

- $n$  = Manning's roughness coefficient  
 $\ell$  = limiting length of flow, ft  
 $S$  = slope, ft/ft

Table 15–2 provides maximum sheet flow lengths based on the McCuen-Spiess limiting criteria for various cover type— $n$  value—slope combinations.

**Shallow concentrated flow**—After approximately 100 feet, sheet flow usually becomes shallow concentrated flow collecting in swales, small rills, and gullies. Shallow concentrated flow is assumed not to have a well-defined channel and has flow depths of 0.1 to 0.5 feet. It is assumed that shallow concentrated flow can be represented by one of seven flow types. The curves in figure 15–4 were used to develop the information in table 15–3.

To estimate shallow concentrated flow travel time, velocities are developed using figure 15–4, in which average velocity is a function of watercourse slope and type of channel (Kent 1964). For slopes less than 0.005 foot per foot, the equations in table 15–3 may be used.

After estimating average velocity using figure 15–4, use equation 15–1 to estimate travel time for the shallow concentrated flow segment.

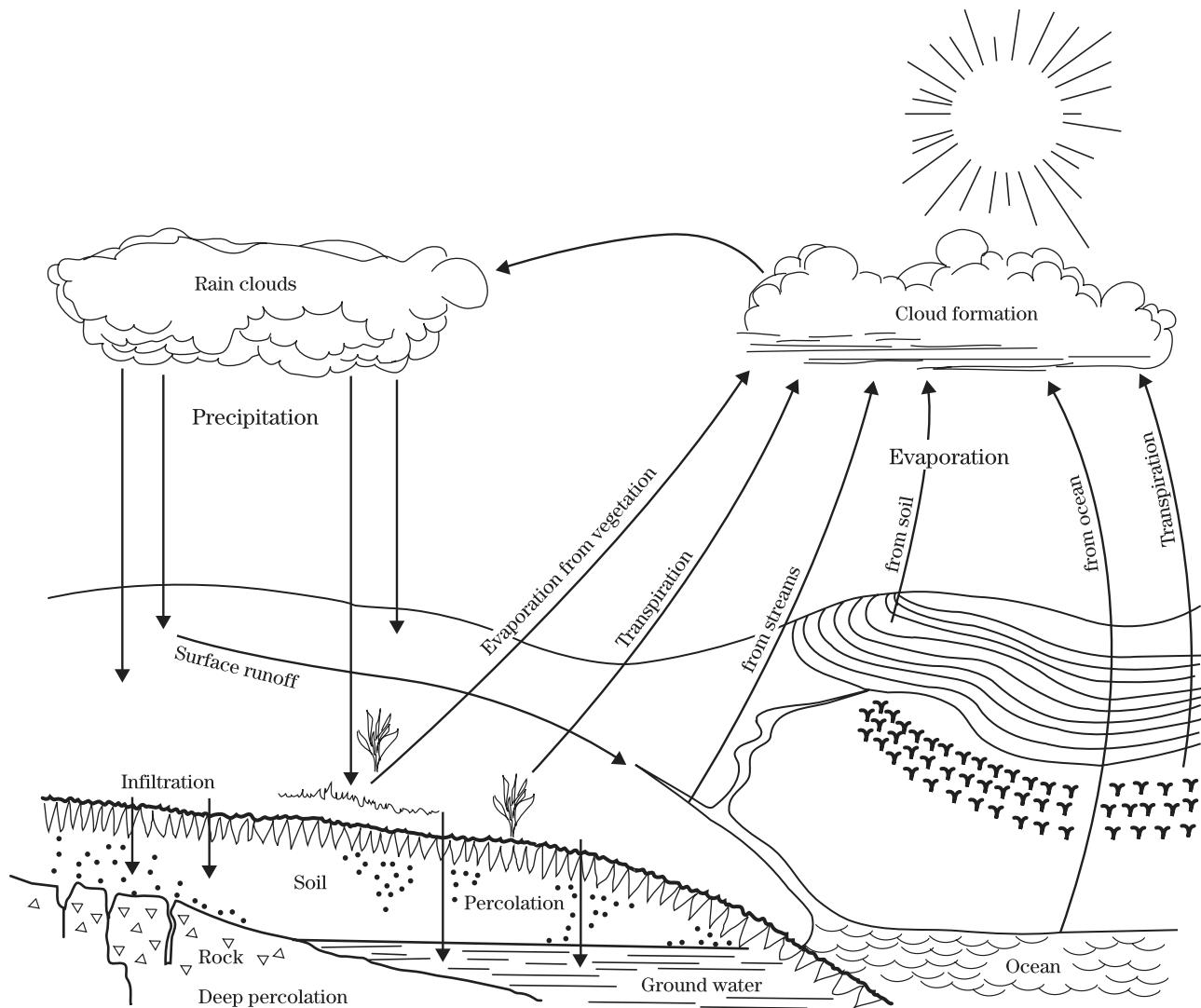
**Open channel flow**—Shallow concentrated flow is assumed to occur after sheet flow ends at shallow depths of 0.1 to 0.5 feet. Beyond that channel flow is assumed to occur. Open channels are assumed to begin where surveyed cross-sectional information has been obtained, where channels are visible on aerial photographs, or where bluelines (indicating streams) appear on U.S. Geological Survey (USGS) quadrangle sheets.

Manning's equation or water surface profile information can be used to estimate average flow velocity. Average flow velocity is usually determined for the bankfull elevation.

Manning's equation is:

$$V = \frac{1.49 r^{\frac{2}{3}} S^{\frac{1}{2}}}{n} \quad (\text{eq. 15-10})$$

## **Chapter 15 Time of Concentration**





**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: Somerset, New Jersey, USA\***  
**Latitude: 40.5257°, Longitude: -74.5433°**  
**Elevation: 79.56 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



### POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

#### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>3.98</b> (3.61-4.40)	<b>4.74</b> (4.30-5.24)	<b>5.63</b> (5.08-6.22)	<b>6.26</b> (5.65-6.91)	<b>7.04</b> (6.32-7.76)	<b>7.60</b> (6.78-8.35)	<b>8.14</b> (7.24-8.96)	<b>8.62</b> (7.63-9.52)	<b>9.23</b> (8.09-10.2)	<b>9.67</b> (8.44-10.7)
10-min	<b>3.18</b> (2.88-3.52)	<b>3.80</b> (3.43-4.19)	<b>4.50</b> (4.07-4.97)	<b>5.01</b> (4.52-5.53)	<b>5.61</b> (5.03-6.19)	<b>6.04</b> (5.40-6.65)	<b>6.46</b> (5.75-7.12)	<b>6.83</b> (6.05-7.54)	<b>7.30</b> (6.40-8.07)	<b>7.62</b> (6.64-8.45)
15-min	<b>2.65</b> (2.40-2.93)	<b>3.18</b> (2.88-3.52)	<b>3.80</b> (3.43-4.20)	<b>4.22</b> (3.81-4.66)	<b>4.74</b> (4.26-5.23)	<b>5.10</b> (4.56-5.62)	<b>5.44</b> (4.84-6.00)	<b>5.75</b> (5.08-6.34)	<b>6.12</b> (5.37-6.77)	<b>6.38</b> (5.56-7.07)
30-min	<b>1.82</b> (1.65-2.01)	<b>2.20</b> (1.99-2.43)	<b>2.70</b> (2.44-2.98)	<b>3.06</b> (2.76-3.38)	<b>3.51</b> (3.15-3.87)	<b>3.84</b> (3.43-4.23)	<b>4.17</b> (3.71-4.60)	<b>4.47</b> (3.96-4.94)	<b>4.87</b> (4.27-5.39)	<b>5.16</b> (4.50-5.72)
60-min	<b>1.13</b> (1.03-1.25)	<b>1.38</b> (1.25-1.52)	<b>1.73</b> (1.56-1.91)	<b>1.99</b> (1.80-2.20)	<b>2.34</b> (2.10-2.58)	<b>2.60</b> (2.33-2.87)	<b>2.87</b> (2.55-3.17)	<b>3.14</b> (2.78-3.46)	<b>3.50</b> (3.07-3.87)	<b>3.77</b> (3.28-4.18)
2-hr	<b>0.692</b> (0.622-0.770)	<b>0.843</b> (0.759-0.936)	<b>1.07</b> (0.962-1.19)	<b>1.25</b> (1.12-1.38)	<b>1.49</b> (1.33-1.65)	<b>1.69</b> (1.50-1.87)	<b>1.89</b> (1.67-2.10)	<b>2.11</b> (1.85-2.33)	<b>2.40</b> (2.08-2.67)	<b>2.64</b> (2.26-2.94)
3-hr	<b>0.513</b> (0.462-0.572)	<b>0.624</b> (0.563-0.697)	<b>0.794</b> (0.715-0.885)	<b>0.925</b> (0.831-1.03)	<b>1.11</b> (0.989-1.23)	<b>1.26</b> (1.12-1.40)	<b>1.41</b> (1.24-1.57)	<b>1.57</b> (1.38-1.75)	<b>1.80</b> (1.55-2.00)	<b>1.97</b> (1.69-2.20)
6-hr	<b>0.329</b> (0.296-0.368)	<b>0.399</b> (0.360-0.446)	<b>0.507</b> (0.455-0.563)	<b>0.594</b> (0.531-0.659)	<b>0.719</b> (0.637-0.796)	<b>0.824</b> (0.726-0.910)	<b>0.936</b> (0.817-1.03)	<b>1.06</b> (0.913-1.17)	<b>1.23</b> (1.05-1.36)	<b>1.38</b> (1.16-1.52)
12-hr	<b>0.199</b> (0.178-0.223)	<b>0.241</b> (0.216-0.270)	<b>0.307</b> (0.274-0.344)	<b>0.363</b> (0.323-0.405)	<b>0.446</b> (0.394-0.496)	<b>0.518</b> (0.454-0.575)	<b>0.596</b> (0.517-0.661)	<b>0.683</b> (0.584-0.758)	<b>0.811</b> (0.682-0.901)	<b>0.921</b> (0.762-1.02)
24-hr	<b>0.113</b> (0.105-0.123)	<b>0.137</b> (0.127-0.149)	<b>0.175</b> (0.162-0.191)	<b>0.208</b> (0.192-0.226)	<b>0.257</b> (0.236-0.279)	<b>0.300</b> (0.272-0.325)	<b>0.347</b> (0.313-0.376)	<b>0.399</b> (0.356-0.434)	<b>0.477</b> (0.419-0.520)	<b>0.545</b> (0.470-0.595)
2-day	<b>0.066</b> (0.060-0.072)	<b>0.079</b> (0.073-0.087)	<b>0.101</b> (0.093-0.112)	<b>0.120</b> (0.109-0.131)	<b>0.146</b> (0.132-0.161)	<b>0.169</b> (0.152-0.185)	<b>0.194</b> (0.173-0.213)	<b>0.221</b> (0.195-0.243)	<b>0.260</b> (0.226-0.287)	<b>0.293</b> (0.252-0.325)
3-day	<b>0.046</b> (0.043-0.051)	<b>0.056</b> (0.052-0.062)	<b>0.071</b> (0.065-0.078)	<b>0.084</b> (0.076-0.092)	<b>0.102</b> (0.093-0.112)	<b>0.118</b> (0.106-0.129)	<b>0.134</b> (0.120-0.147)	<b>0.152</b> (0.135-0.167)	<b>0.178</b> (0.155-0.196)	<b>0.200</b> (0.172-0.221)
4-day	<b>0.037</b> (0.034-0.040)	<b>0.045</b> (0.041-0.049)	<b>0.056</b> (0.052-0.062)	<b>0.066</b> (0.060-0.072)	<b>0.080</b> (0.073-0.088)	<b>0.092</b> (0.083-0.100)	<b>0.104</b> (0.093-0.114)	<b>0.118</b> (0.105-0.129)	<b>0.137</b> (0.120-0.151)	<b>0.153</b> (0.132-0.169)
7-day	<b>0.025</b> (0.023-0.027)	<b>0.030</b> (0.027-0.032)	<b>0.037</b> (0.034-0.040)	<b>0.043</b> (0.039-0.046)	<b>0.051</b> (0.047-0.056)	<b>0.058</b> (0.053-0.063)	<b>0.066</b> (0.059-0.071)	<b>0.074</b> (0.066-0.080)	<b>0.085</b> (0.075-0.093)	<b>0.094</b> (0.082-0.104)
10-day	<b>0.020</b> (0.018-0.021)	<b>0.023</b> (0.022-0.025)	<b>0.029</b> (0.027-0.031)	<b>0.033</b> (0.031-0.036)	<b>0.039</b> (0.036-0.042)	<b>0.044</b> (0.040-0.048)	<b>0.049</b> (0.045-0.053)	<b>0.055</b> (0.049-0.059)	<b>0.062</b> (0.056-0.068)	<b>0.068</b> (0.060-0.075)
20-day	<b>0.013</b> (0.012-0.014)	<b>0.016</b> (0.015-0.017)	<b>0.019</b> (0.018-0.020)	<b>0.021</b> (0.020-0.023)	<b>0.024</b> (0.023-0.026)	<b>0.027</b> (0.025-0.029)	<b>0.029</b> (0.027-0.031)	<b>0.032</b> (0.030-0.034)	<b>0.035</b> (0.032-0.038)	<b>0.038</b> (0.035-0.041)
30-day	<b>0.011</b> (0.010-0.012)	<b>0.013</b> (0.012-0.014)	<b>0.015</b> (0.014-0.016)	<b>0.017</b> (0.016-0.018)	<b>0.019</b> (0.018-0.020)	<b>0.021</b> (0.019-0.022)	<b>0.022</b> (0.021-0.024)	<b>0.024</b> (0.022-0.025)	<b>0.026</b> (0.024-0.028)	<b>0.027</b> (0.025-0.029)
45-day	<b>0.009</b> (0.009-0.010)	<b>0.011</b> (0.010-0.012)	<b>0.013</b> (0.012-0.013)	<b>0.014</b> (0.013-0.015)	<b>0.016</b> (0.015-0.016)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.019)	<b>0.019</b> (0.018-0.020)	<b>0.020</b> (0.019-0.022)	<b>0.021</b> (0.020-0.023)
60-day	<b>0.008</b> (0.008-0.009)	<b>0.010</b> (0.009-0.010)	<b>0.011</b> (0.011-0.012)	<b>0.012</b> (0.012-0.013)	<b>0.014</b> (0.013-0.014)	<b>0.015</b> (0.014-0.015)	<b>0.015</b> (0.015-0.016)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.019)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

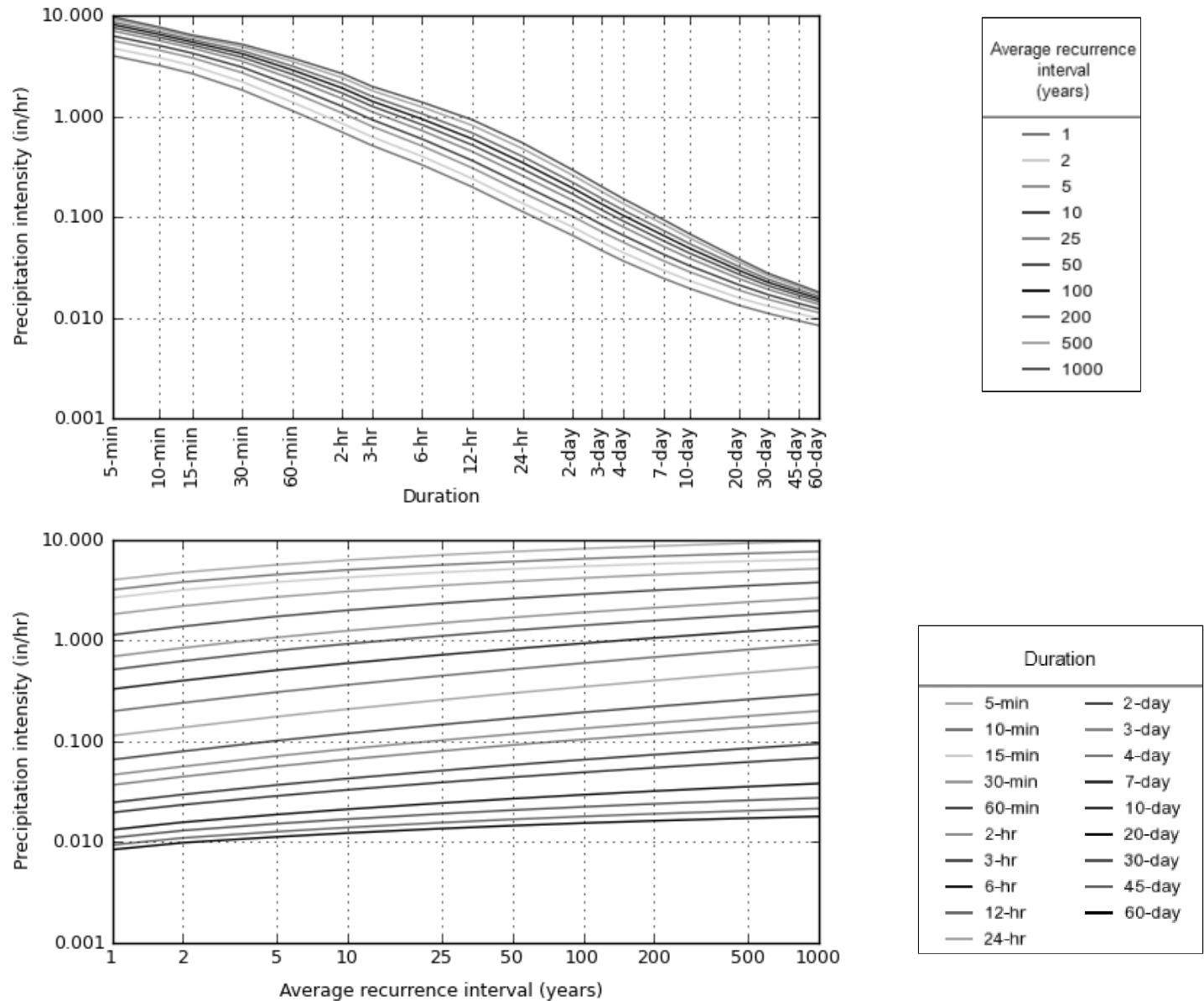
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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#### PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
Latitude: 40.5257°, Longitude: -74.5433°



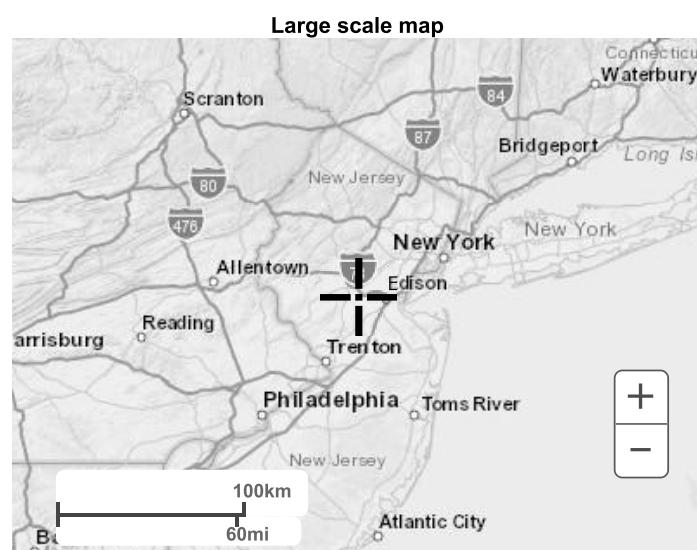
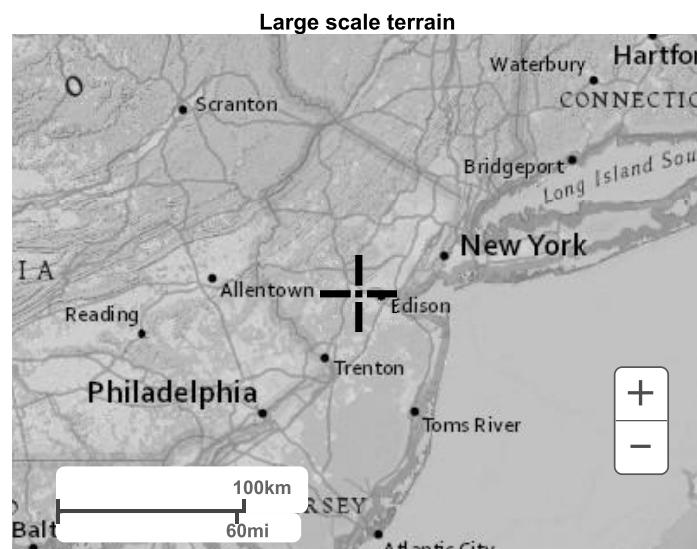
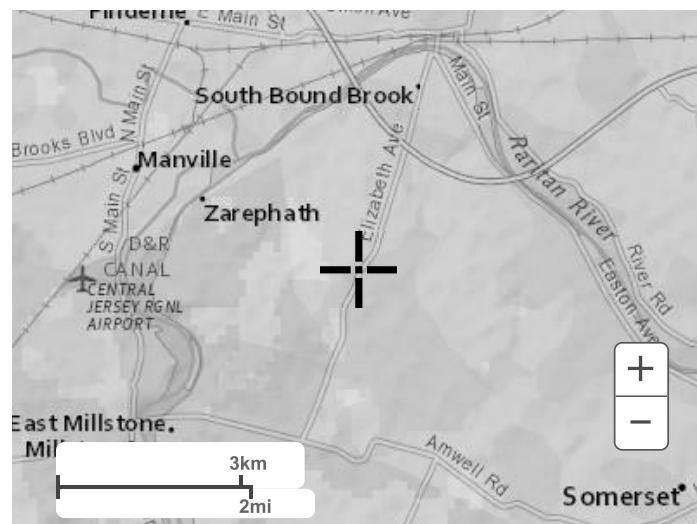
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Created (GMT): Thu Oct 8 23:50:29 2020

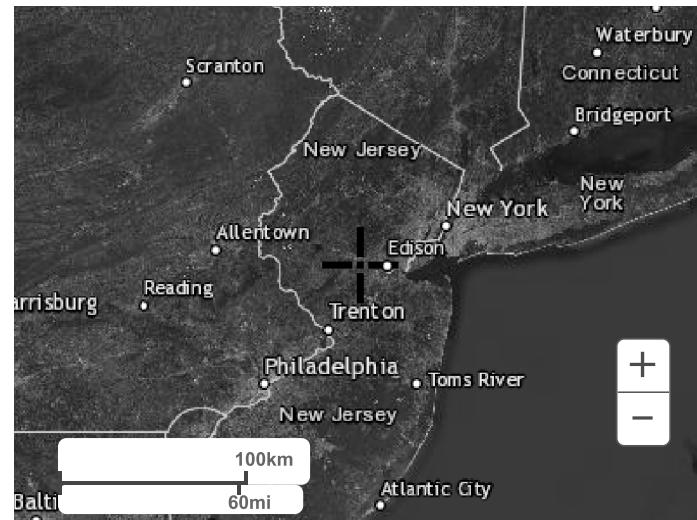
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## Maps & aerials

[Small scale terrain](#)



**Large scale aerial**



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## MAPS





Aerial Map  
Source: NJ 2015 OrthophOTOGRAPHy  
Elizabeth Realty Partners, LLC  
Block 507.14, Lots 61 & 62  
Franklin Township, Somerset County, New Jersey  
MC Project No. 19000649A

0 45 90 180 Feet



— Approximate Site Boundary



Consulting, Municipal & Environmental Engineers  
Planners ■ Surveyors ■ Landscape Architects

Hamilton Office  
1000 Waterview Drive  
Hamilton, NJ 08691  
Phone: 609-587-8200  
Fax: 609-587-8260





Hamilton Office  
1000 Waterview Drive  
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Phone: 609-587-8200  
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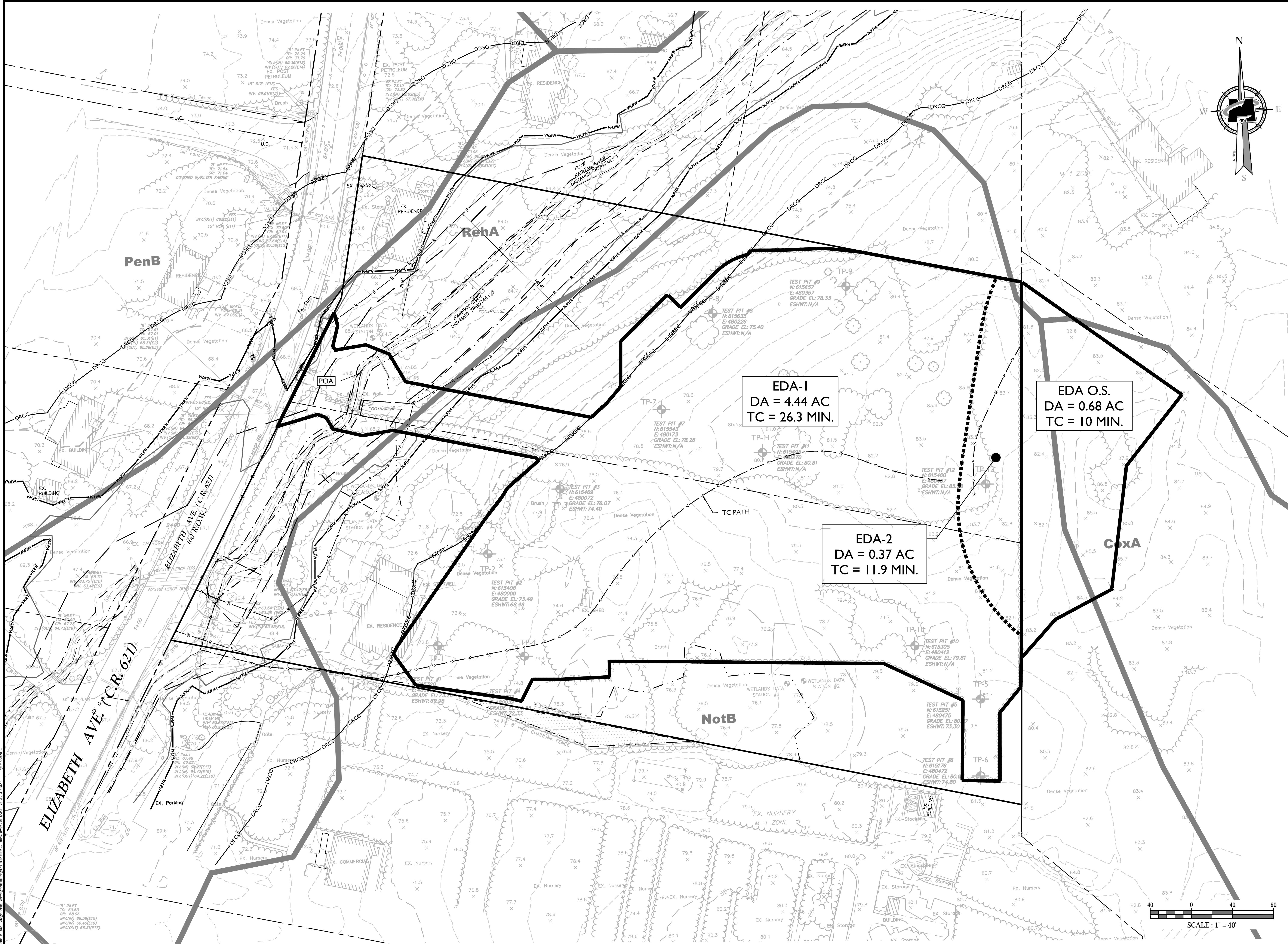
Soils Map  
Source: NJDEP Geographical Information Systems  
Elizabeth Realty Partners, LLC  
Block 507.14, Lots 61 & 62  
Franklin Township, Somerset County, New Jersey  
MC Project No. 19000649A

0 45 90 180 Feet



— Approximate Site Boundary  
— Soil Boundary





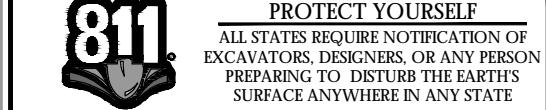
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## MAJOR SITE PLAN

FOR  
**IZABETH REALTY  
PARTNERS LLC**

83 & 485 ELIZABETH  
AVENUE

BLOCK 507.14  
LOTS 61 & 62

**FANKLIN TOWNSHIP  
OMERSET COUNTY, NJ**

**HAMILTON OFFICE**  
1000 Waterview Drive  
Suite 201  
Hamilton, NJ 08691

Phone: 609.587.8200  
Fax: 609.587.8260

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NUMBER.	DRAWING NAME.	

NUMBER:	DRAWING NAME:
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**EXISTING LG**

# EXISTING DRAINAGE MAP

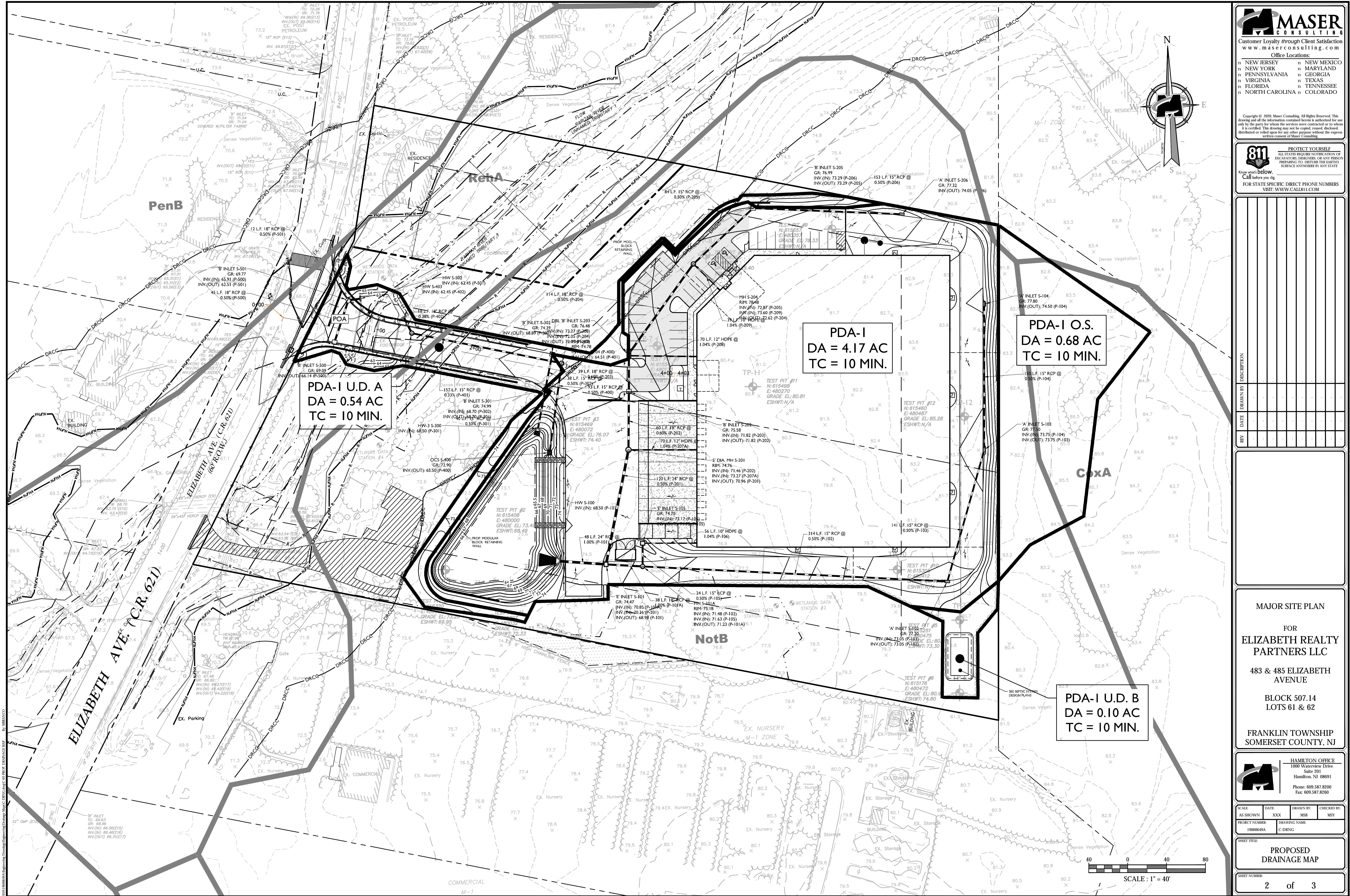
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1 of 3

1 OF 3

## **THE DRAWINGS FOR CONSTRUCTION**







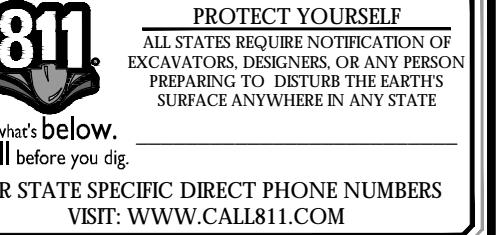
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MAJOR SITE PLAN

FOR  
**LIZABETH REALTY  
PARTNERS LLC**

483 & 485 ELIZABETH  
AVENUE

BLOCK 507.14  
LOTS 61 & 62

# FRANKLIN TOWNSHIP OMERSET COUNTY, NJ

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OWN	XXX	MSB	MSY
T. NUMBER:	DRAWING NAME:		

9000649A C-DRNG  
TITLE: PROPOSED

## DRAINAGE MAP



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