

STORMWATER MANAGEMENT REPORT

Prepared for:

SAFSTOR REAL ESTATE CO, LLC

Block 507.14, Lot 65.01
471 Elizabeth Avenue

Franklin Township
Somerset County, New Jersey

Prepared by:

BOHLER //

N.J. Certificate of Authorization 24GA28161700

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BENJ File No. J200933

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1. Introduction

The subject property is located at 471 Elizabeth Avenue in Franklin Township, Somerset County, New Jersey. The property is identified as Block 507.14, Lot 65.01 on the Franklin Township tax maps and is a total of 4.816 acres in size and will hereafter be referred to as “the site”. The site is bordered to the northeast by an active adult community and New Brunswick Road beyond; to the northwest by Elizabeth Avenue and vacant wooded area beyond; to the southwest by a wooded area and residential uses beyond; and to the southeast by a wooded area and residential uses beyond. A tax map and aerial map is included at the beginning of Appendix C for reference.

The site is currently partially developed within the B-I (Business District) Zone. One 1,060 square foot residential house currently exists on the property along Elizabeth Avenue with a 959 square foot detached garage and asphalt driveway. Beyond the detached garage is a 2,666 square foot industrial building with a gravel parking area. A gravel driveway also exists along Elizabeth Avenue which leads to multiple man-made material piles. The undeveloped portions of the lot are wooded or grassed areas. An existing underground septic field is located on the site to handle sewage from the residential house. A proposed stormwater management system will convey the runoff from the proposed development and impervious areas.

This report summarizes the design objectives, methodology, and calculations for the conveyance, detention, treatment and discharge of stormwater runoff leaving the site and is meant to accompany the Site Plan documents prepared by Bohler Engineering. Pre-development and post-development conditions are examined for stormwater quantity analysis, water quality analysis, groundwater recharge, soil erosion and sediment control, and low impact development based on the *NJDEP Stormwater Management Regulations* of March 2020.

2. Pre-Development Site Conditions

The site contains a total area of 4.816 acres. The studied watershed area is a total of 4.816 acres in size and consists of two unique drainage areas: Existing Drainage Area #1 and Existing Drainage Area #2, which are described in more detail below. In the pre-development condition, the site is partially developed with a few buildings, asphalt and gravel driveways and gravel parking area. Undeveloped land consists of grass and wooded areas. Currently, the runoff generated on site outfalls to Block 507.17, Lot 236 along the southeast property line via overland flow and ultimately flows southeast to a tributary of the Raritan River. The Existing Drainage Area Map in Appendix C illustrates the limits of each existing drainage area and how they relate to the existing site conditions.

2.1 Point of Analysis 1

Existing Drainage Area #1 flows to point of analysis #1 located near the south property corner. The Existing Drainage Area Map in Appendix C illustrates the identified point of analysis and how it relates to the existing topography on the site.

2.1.1 Existing Drainage Area #1

Located on the southwest area of the site, Existing Drainage Area #1 contains 4.088 acres of land, of which 0.238 acres are impervious surface, and includes a residential house, detached garage, asphalt driveway and a portion of the gravel parking area. The topography of the area slopes from north to south from a maximum elevation of approximately 87.30 to a minimum elevation of approximately 70.60 with slopes ranging from 1% to 45%, including the man-made material piles currently on site. A CN value of 98 and 74 were used for

impervious and pervious areas, respectively, with a calculated time of concentration of 12.4 minutes. The runoff from Existing Drainage Area #1 flows through the site to Block 507.17, lot 236 in both the existing and proposed conditions and will be accounted for in the proposed stormwater management design. Existing Drainage Area #1 discharges to Point of Analysis 1.

2.2 Point of Analysis 2

Existing Drainage Area #2 flows to point of analysis #2 located near the east property corner. The Existing Drainage Area Map in Appendix C illustrates the identified point of analysis and how it relates to the existing topography on the site.

2.2.1 Existing Drainage Area #2

The remainder of the area of study in the pre-development condition is contained within Existing Drainage Area #2, which contains 0.728 acres of land, of which 0.129 acres are impervious surface, and includes most of the industrial building and a portion of the asphalt driveway and a portion of the gravel parking area. The topography of the area slopes from north to south from a maximum elevation of approximately 84.30 to a minimum elevation of approximately 74.20 with slopes ranging from 1% to 45%, including the man-made material piles currently on site. A CN value of 98 and 74 were used for impervious and pervious areas, respectively, with a calculated time of concentration of 3.0 minutes. The runoff from Existing Drainage Area #2 flows from north to south and ultimately discharges to Point of Analysis 1.

2.3 Pre-Development Flow Summary

TABLE 2.1

| DATA | EXISTING DRAINAGE AREA #1 | EXISTING DRAINAGE AREA #2 |
|--------------------|---------------------------|---------------------------|
| Area (acres) | 4.088 | 0.728 |
| Impervious (acres) | 0.238 | 0.129 |
| Tc (min) | 12.4 | 3.0 |
| 2 Yr. Flow (CFS) | 5.61 | 2.00 |
| 10 Yr. Flow (CFS) | 11.74 | 3.44 |
| 100 Yr. Flow (CFS) | 24.93 | 6.29 |

3. Post-Development Site Conditions

The post-development condition for the site includes the construction of one, three story self-storage building with associated parking, driveways, sidewalks, utility infrastructure, stormwater conveyance, aboveground and underground detention facilities, and other site improvements. The proposed site is designed in a manner that generally maintains the existing drainage patterns. The studied watershed area in the post-development condition contains the same 4.816 acre area that was studied in the pre-development condition and consists of four unique drainage areas: Proposed Drainage Area #1A, #1B, #1c and #2, which are described in more detail below.

A proposed stormwater conveyance system will collect the runoff from the proposed buildings and impervious areas via inlets, manholes, and stormwater piping and redirect it to the proposed bioretention basins on the site. The construction of the proposed improvements will occupy approximately 3.73 acres of land and will create approximately 1.47 acres of impervious coverage on the site in the post-development condition. The Proposed Drainage Area Map in Appendix C illustrates the limits of each proposed drainage area and how they relate to the proposed site conditions

3.1 Point of Analysis 1

The Proposed Drainage Area #1A, #1B and #1C in the post development condition flows to the same point of analysis identified in the existing condition, located near the south property corner. As noted above, the Proposed Drainage Area Map in Appendix C illustrates the identified point of analysis and how it relates to the proposed topography on the site.

3.1.1 Proposed Drainage Area #1A

Proposed Drainage Area #1A consists of approximately 2.245 acres of land, of which 1.357 acres are impervious surface, and includes the proposed self-storage building, parking areas, sidewalks, stormwater and utility infrastructure. The drainage area also contains grass, landscape and wooded areas. A CN value of 98 and 74 were used for impervious and pervious areas, respectively, with a calculated time of concentration of 10.7 minutes for pervious surfaces. The runoff from Proposed Drainage Area #1A is routed to bioretention basins #1 and #2 and ultimately flows to Block 507.17, Lot 236 and Point of Analysis 1. The routing of the runoff from Proposed Drainage Area #1A is depicted on the Inlet Area Map in Appendix C.

The proposed peak runoff rates for Proposed Drainage Area #1A are analyzed at Point of Analysis 1. The flows tributary to Point of Analysis 1 from Proposed Drainage Area #1 meets the stormwater management criteria set forth in NJAC § 7:8-5.4(a)3.iii. Post-development peak runoff rates for the 2-, 10-, and 100-year storm events for flows tributary to Point of Analysis 1 meet or exceed the

50, 75 and 80 percent reductions, respectively, of the pre-development peak runoff rates. Refer to Section 3.3 for a comparison of pre-development flows to the post-development flows routed through proposed bioretention. Refer to Sections 2.2 and 3.3 for pre-development and post-development flows, respectively.

3.1.2 Proposed Drainage Area #1B

Proposed Drainage Area #1B consists of approximately 0.342 acres of land, of which 0.147 acres are impervious surface, and includes a loading area, driveway, sidewalk and the bioretention basin #3. The drainage area also contains grass, landscape and wooded areas. A CN value of 98 and 74 were used for impervious and pervious areas, respectively, with a calculated time of concentration of 20.8 minutes for pervious surfaces. The runoff from Proposed Drainage Area #1B is routed to bioretention basins #3 and ultimately flows to Block 507.17, Lot 236 and Point of Analysis 1. The routing of the runoff from Proposed Drainage Area #1B is depicted on the Inlet Area Map in Appendix C.

The proposed peak runoff rates for Proposed Drainage Area #1B are analyzed at Point of Analysis 1. The flows tributary to Point of Analysis 1 from Proposed Drainage Area #1 meets the stormwater management criteria set forth in NJAC § 7:8-5.4(a)3.iii. Post-development peak runoff rates for the 2-, 10-, and 100-year storm events for flows tributary to Point of Analysis 1 meet or exceed the 50, 75 and 80 percent reductions, respectively, of the pre-development peak runoff rates. Refer to Section 3.3 for a comparison of pre-development flows to the post-development flows routed through proposed bioretention. Refer to Sections 2.2 and 3.3 for pre-development and post-development flows, respectively.

3.1.3 Proposed Drainage Area #1C

Proposed Drainage Area #1C consists of approximately 1.404 acres of land, of which 0.053 acres are impervious surface which includes the grass paver fire access lane. The drainage area also contains grass, landscape and wooded areas. A CN value of 98 and 74 were used for impervious and pervious areas, respectively, with a calculated time of concentration of 13.9 minutes for pervious surfaces. The runoff from Proposed Drainage Area #1C is routed to the existing wetlands and ultimately flows to Block 507.17, Lot 236 and Point of Analysis 1. The routing of the runoff from Proposed Drainage Area #1C is depicted on the Inlet Area Map in Appendix C.

The proposed peak runoff rates for Proposed Drainage Area #1C are analyzed at Point of Analysis 1. The flows tributary to Point of Analysis 1 from Proposed Drainage Area #1 meets the stormwater management criteria set forth in NJAC

§ 7:8-5.4(a)3.iii. Post-development peak runoff rates for the 2-, 10-, and 100-year storm events for flows tributary to Point of Analysis 1 meet or exceed the 50, 75 and 80 percent reductions, respectively, of the pre-development peak runoff rates. Refer to Section 3.3 for a comparison of pre-development flows to the post-development flows routed through proposed bioretention. Refer to Sections 2.2 and 3.3 for pre-development and post-development flows, respectively.

3.2 Point of Analysis 2

The Proposed Drainage Area #2 in the post development condition flows to the same point of analysis identified in the existing condition, located near the east property corner. As noted above, the Proposed Drainage Area Map in Appendix C illustrates the identified point of analysis and how it relates to the proposed topography on the site.

3.2.1 Proposed Drainage Area #2

Proposed Drainage Area #2 consists of approximately 0.826 acres of land, with no impervious surface, and includes grass, landscape and wooded areas as well as the proposed septic field. A CN value of 98 and 74 were used for impervious and pervious areas, respectively, with a calculated time of concentration of 12.2 minutes for pervious surfaces. The runoff from Proposed Drainage Area #2 is routed to the existing wetlands area which ultimately flows to Block 507.17, Lot 236 and Point of Analysis 2. The routing of the runoff from Proposed Drainage Area #2 is depicted on the Proposed Drainage Area Map in Appendix C.

The proposed peak runoff rates for Proposed Drainage Area #2 are analyzed at Point of Analysis 2. The flows tributary to Point of Analysis 2 from Proposed Drainage Area #2 meets the stormwater management criteria set forth in NJAC § 7:8-5.4(a)3.iii. Post-development peak runoff rates for the 2-, 10-, and 100-year storm events for flows tributary to Point of Analysis 1 meet or exceed the 50, 75 and 80 percent reductions, respectively, of the pre-development peak runoff rates. Refer to Section 3.3 for a comparison of pre-development flows to the post-development flows. Refer to Sections 2.2 and 3.3 for pre-development and post-development flows, respectively.

3.3 Proposed Structural Stormwater Management Strategies

The four drainage areas in the post development condition flow to the same points of analysis identified in the existing condition. Two of the drainage areas, Proposed

Drainage Areas #1A and #1B, flows through the proposed on-site stormwater management system, which is described in more detail below.

3.3.1 Bio-Retention Systems

As part of the stormwater management design of the proposed site, two bio-retention systems are proposed to capture water from impervious areas. The bio-retention systems meet the minimum requirements outlined in the *New Jersey Stormwater Best Management Practices Manual* by providing 24 inches of soil bed depth, an underdrain system, containment and treatment of the entire Water Quality Design Storm volume, a storage depth of 12 inches maximum in a flat-bottom system and 1 foot minimum of separation between the bottom of the bio-retention basin and the seasonal high ground water table for underdrain systems. The proposed bio-retention systems achieve 80% TSS removal.

TABLE 3.2.1

| DESIGN PARAMETERS | | |
|---|---|--------------------------------|
| TSS Removal Rate | Depth of Soil Bed | Vegetation |
| 80% | 18 inches | Terrestrial Forested Community |
| 80% | 24 inches | Site-Tolerant Grasses |
| 90% | 24 inches | Terrestrial Forested Community |
| Storage Volume | Entire Water Quality Design Storm Volume | |
| Minimum Density of Vegetation | 85% | |
| Appropriate Species Selection | See Chapter 7 of the <i>NJ Stormwater Best Management Practices Manual</i> | |
| Maximum Design Storm Drain Time | 72 Hours, Using Slowest Design Permeability Rate | |
| Permeability Rate Factor of Safety | 2 | |
| Minimum Subsoil Design Permeability Rate | 0.5 inches/hour (Under-drain proposed) | |
| Soil Testing Requirements | Must be consistent with Appendix E of the <i>NJ Stormwater Best Management Practices Manual</i> | |

3.3.2 Emergency Spillways

The emergency spillways associated with the proposed basins have been designed to pass a design storm that is equivalent to the 100-year storm plus 50%. At least one foot of freeboard is provided above the peak water elevation while the emergency spillway is operating.

3.4 Post-Development Flow Summary

TABLE 3.3

PROPOSED FLOW SUMMARY

| | Proposed Drainage Area #1 | Proposed Drainage Area #2 |
|--------------------|---------------------------|---------------------------|
| Area (acres) | 3.980 | 0.836 |
| Impervious (acres) | 1.527 | 0.000 |
| Tc (min) | 10.7, 20.8 & 13.9 | 12.2 |
| 2 yr. Flow (cfs) | 2.43 | 0.91 |
| 10 yr. Flow (cfs) | 6.30 | 2.10 |
| 100 yr. Flow (cfs) | 19.24 | 4.76 |

EXISTING/PROPOSED FLOW SUMMARY (DRAINAGE AREA 1)

| | Existing Drainage Area 1 | Total Flows Requiring Reductions (cfs) | Required Reductions | Maximum Allowable Flow to Point of Analysis 1 | Total Proposed Flows to Point of Analysis 1 |
|--------------------|--------------------------|--|---------------------|---|---|
| 2 yr. Flow (cfs) | 5.61 | 5.61 | 50% | 2.81 | 2.43 |
| 10 yr. Flow (cfs) | 11.74 | 11.74 | 25% | 8.81 | 6.30 |
| 100 yr. Flow (cfs) | 24.93 | 24.93 | 20% | 19.94 | 19.24 |

EXISTING/PROPOSED FLOW SUMMARY (DRAINAGE AREA 2)

| | Existing Drainage Area 2 | Total Flows Requiring Reductions (cfs) | Required Reductions | Maximum Allowable Flow to Point of Analysis 2 | Total Proposed Flows to Point of Analysis 2 |
|-----------------------|-----------------------------|---|------------------------|--|--|
| 2 yr. Flow (cfs) | 2.00 | 2.00 | 50% | 1.00 | 0.91 |
| 10 yr. Flow (cfs) | 3.44 | 3.44 | 25% | 2.58 | 2.10 |
| 100 yr. Flow (cfs) | 6.29 | 6.29 | 20% | 5.03 | 4.76 |

4. Stormwater Management Design Methodology

In accordance with the NJDEP Stormwater Management Regulations, the proposed development must meet the requirements, if appropriate, for stormwater quantity reductions, water quality, groundwater recharge, soil erosion and sediment control, and low impact development. The following sections describe how each of the above items are addressed on site in the post-development condition.

4.1 Stormwater Quantity Controls

The Assessment of stormwater quantity has been based upon the Soil Conservation Service Method (SCS) Unit Hydrograph as described in Technical Release Number 55 (TR55), "Urban Hydrology for Small Watersheds". Theoretical storms are modeled with the 24-Hour SCS Unit Dimensionless Hydrograph using the NOAA Atlas 14 Type C rainfall distribution and recurrence intervals of 2, 10, and 100 years. Hydrograph creation and routings are accomplished using the *HydroCAD* Version 10.00 program by HydroCAD Software Solutions, LLC. The following techniques from the *NJDEP Stormwater Management Regulations* is being applied to each drainage area as noted in section 3.3:

1. NJAC § 7:8-5.4(a)3.i states for stormwater runoff leaving the site, post-development runoff hydrographs for the 2-, 10-, and 100-year storms do not exceed, at any point in time, the pre-development runoff hydrographs for the same storm events. The above section of the NJAC will be applied to drainage areas that, under proposed conditions, will remain unchanged or have a net decrease in impervious coverage.
2. NJAC § 7:8-5.4(a)3.iii states the post-development peak runoff rates for the 2-, 10-, and 100-year storm events are 50, 75, and 80 percent, respectively, of the pre-development peak runoff rates. The above section of the NJAC will be applied to drainage areas that are impacted by the proposed development and flow to a detention or retention system.

The project's proposed stormwater management facilities for stormwater peak flow attenuation will consist of three bioretention basins (bioretention basin #1, #2 and #3) addressing the drainage areas outlined in Section 3 of this report. The study requires the establishment of a point of analysis, as indicated in Section 2. Existing and proposed CN and Tc calculations, as well as existing and proposed hydrographs are provided in Appendix A. The information below describes the methodology in which the stormwater calculations were procured.

4.1.1 Site Soils

Site soil information has been obtained from the USDA Natural Resources Conservation Service (NRCS) web soil survey database, last revised in 2015. The major soil types present on site include Penn Silt Loam, which is a somewhat poorly drained soil with 2 to 6 percent slopes. Penn soils are classified as Hydrologic Soil Group Type C soils; therefore, values used in the CN and time of concentration calculations are associated with Type C soils. For areas where the calculated time of concentration is less than 6 minutes, the calculated time was used. For impervious area, an assumed time of concentration of 6 minutes was used.

4.1.2 Rainfall Data

Rainfall data used in the stormwater calculations of this report are obtained from several different sources based on the latest NJDEP stormwater regulations. The Water Quality storm event is based on the NJDEP BMP Manual Chapter 5 definition of having a total rainfall depth of 1.25 inches and a total duration of two (2) hours. Twenty-four-hour rainfall frequency data in Somerset County for all other storms is obtained from the NOAA Atlas 14, Volume 2, Precipitation-Frequency Atlas of the United States, updated in 2006 and listed in the table below:

TABLE 4.1

| | | | | | | | |
|---------------|------|------|------|------|------|------|------|
| Event (year) | 1 | 2 | 5 | 10 | 25 | 50 | 100 |
| Rainfall (in) | 2.76 | 3.34 | 4.25 | 5.01 | 6.15 | 7.13 | 8.21 |

4.1.3 Pipe Sizing

Calculations for sizing the stormwater pipe networks associated with the proposed stormwater management conveyance system can be found in

Appendix B of this report. The Rational Method has been used to size the storm piping for the 25-year storm event. The calculations are conservatively based on a time of concentration of 6 minutes to any inlet. An Inlet Area Map is included in Appendix C.

4.2 Water Quality Controls

Water quality analysis is based on the requirements of NJAC § 7:8-5.5, which requires 80% TSS removal of post-development runoff from new impervious areas before discharging the runoff. Additionally, 50% TSS removal in post-development runoff from replaced impervious areas must be achieved prior to discharging the runoff. Three bioretention basins are used in the proposed condition that achieves 80% TSS removal which have been designed according to standards in Chapter 9.1 of the latest *New Jersey Stormwater Best Management Practices Manual*.

4.3 Groundwater Recharge

Per the Geotechnical Report, the subject site has poor permeability test rate of < 1 inches/hour. Also, the subsurface geology of the site includes karst topography. Introducing groundwater recharge to the site, could have a negative impact on the subsurface geology. Due to the conditions described above, no groundwater recharge is proposed as part of the stormwater management facilities on site.

4.4 Soil Erosion and Sediment Control

The Soil Erosion and Sediment Control plans and details are included within the Site Plan documents prepared by Bohler Engineering and must be followed throughout construction. Silt fences, stabilized construction entrances, a temporary stockpile and inlet filters are proposed during construction. It is noted that stormwater from the site during construction will discharge to Block 507.17, Lot 236 and the existing Raritan River tributary therefore, the offsite stability is considered stable. This report and the Site Plan documents prepared by Bohler Engineering are being submitted to the Somerset-Union Soil Conservation District for approval.

4.5 Low-Impact Development and Non-Structural Stormwater Management Facilities

In accordance with the NJDEP regulations and the latest *New Jersey Stormwater Best Management Practices Manual*, several non-structural stormwater management strategies have been incorporated into the design of the site and are listed below:

4.5.1 Vegetation and Landscaping

A comprehensive Landscape Plan has been incorporated into the design of the proposed improvements on the site that provides low maintenance landscaping. The use of lawn areas has been minimized where applicable and fertilizers and pesticides are to be used sparingly.

4.5.1.1 Native Ground Cover

Native plants including ground cover, shrubs and trees instead of turf grass have been proposed as part of the landscape design for the site. The native plantings will also require little or no irrigation once they are established.

4.5.2 Minimize Land Disturbance

The proposed design of the site incorporates the preservation of existing vegetative areas that will remain undisturbed. The undisturbed areas will be protected during construction and will have easements and/or deed restrictions established as required by other NJDEP regulations and permits to ensure these areas remain undisturbed in the future

4.5.3 Impervious Area Management

Impervious areas are the primary source of additional runoff in the post-development site condition. The sections below describe the measures that have been taken in the proposed site design to minimize the amount of impervious proposed on site

4.5.3.1 Streets, Sidewalks, and Parking, Driveway Areas

As part of the proposed site design, the minimum allowable parking and drive aisle sizes, in accordance with local ordinances, are used in lieu of larger stalls and aisles to reduce the amount of impervious surface in the post-development condition.

4.5.4 Preventative Source Controls

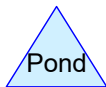
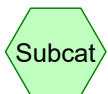
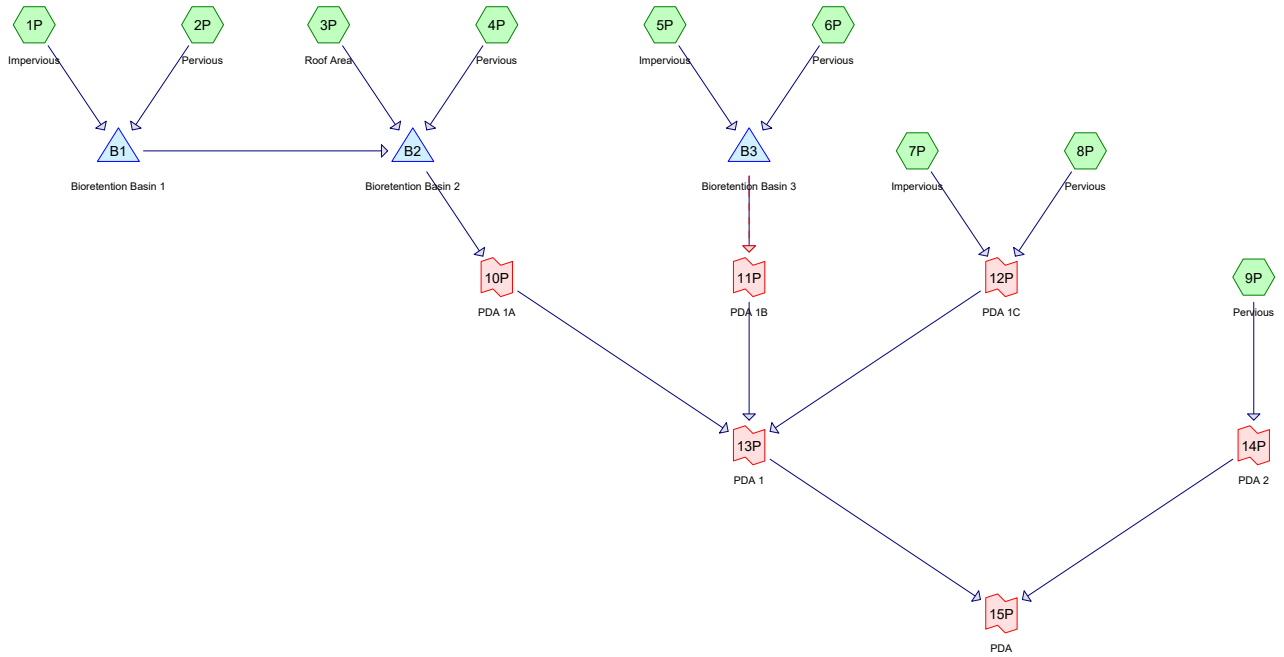
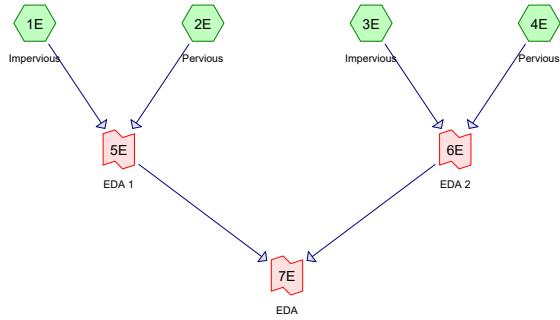
The proposed development complies with this strategy by providing dumpster areas. Additionally, floatable and total suspended solids are routinely eliminated using two bio-detention basins between the last inlet in the pipe network and the above and underground ground basins, thereby intercepting floating debris

5. Conclusions

As demonstrated in the above sections, the stormwater management plan for the proposed development meets the *NJDEP Stormwater Management Regulations* of March 2020, and addresses the requirements for stormwater quantity reductions, water quality, groundwater recharge, soil erosion and sediment control, and low impact development. As a result of the design calculations contained herein, Bohler Engineering anticipates that the stormwater design will not have a negative impact to surrounding areas.

A. PRE- vs. POST-DEVELOPMENT HYDROGRAPHS

- ◆ **Water Quality Storm Event**
- ◆ **2-Year Storm Event**
- ◆ **10-Year Storm Event**
- ◆ **100-Year Storm Event**



Routing Diagram for Pre vs Post
 Prepared by {enter your company name here}, Printed 5/14/2021
 HydroCAD® 10.00-23 s/n 02612 © 2018 HydroCAD Software Solutions LLC

Pre vs Post

Prepared by {enter your company name here}

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Project Notes

Rainfall events imported from "NRCS-Rain.txt" for 6602 NJ Burlington-C

Rainfall events imported from "NRCS-Rain.txt" for 6602 NJ Burlington-C

Pre vs Post

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Area Listing (all nodes)

| Area (sq-ft) | CN | Description (subcatchment-numbers) |
|-----------------|-----------|--|
| 216,139 | 74 | >75% Grass cover, Good, HSG C (2E, 2P, 4E, 4P, 6P, 8P, 9P) |
| 40,897 | 96 | Gravel surface, HSG C (2E, 4E, 5P) |
| 41,084 | 98 | Paved parking, HSG C (1E, 1P, 3E, 5P, 7P) |
| 350 | 98 | Unconnected pavement, HSG C (3P) |
| 40,947 | 98 | Unconnected roofs, HSG C (1E, 3E, 3P) |
| 72,991 | 70 | Woods, Good, HSG C (2E, 4E, 6P, 8P, 9P) |
| 7,150 | 72 | Woods/grass comb., Good, HSG C (2E, 2P, 4E) |
| 419,558 | 80 | TOTAL AREA |

Pre vs Post

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Soil Listing (all nodes)

| Area (sq-ft) | Soil Group | Subcatchment Numbers |
|-----------------|---------------|--|
| 0 | HSG A | |
| 0 | HSG B | |
| 419,558 | HSG C | 1E, 1P, 2E, 2P, 3E, 3P, 4E, 4P, 5P, 6P, 7P, 8P, 9P |
| 0 | HSG D | |
| 0 | Other | |
| 419,558 | | TOTAL AREA |

Pre vs Post

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Ground Covers (all nodes)

| HSG-A (sq-ft) | HSG-B (sq-ft) | HSG-C (sq-ft) | HSG-D (sq-ft) | Other (sq-ft) | Total (sq-ft) | Ground Cover | Su Nu |
|------------------|------------------|------------------|------------------|------------------|------------------|----------------------------|----------|
| 0 | 0 | 216,139 | 0 | 0 | 216,139 | >75% Grass cover, Good | |
| 0 | 0 | 40,897 | 0 | 0 | 40,897 | Gravel surface | |
| 0 | 0 | 41,084 | 0 | 0 | 41,084 | Paved parking | |
| 0 | 0 | 350 | 0 | 0 | 350 | Unconnected pavement | |
| 0 | 0 | 40,947 | 0 | 0 | 40,947 | Unconnected roofs | |
| 0 | 0 | 72,991 | 0 | 0 | 72,991 | Woods, Good | |
| 0 | 0 | 7,150 | 0 | 0 | 7,150 | Woods/grass comb., Good | |
| 0 | 0 | 419,558 | 0 | 0 | 419,558 | TOTAL AREA | |

Pre vs Post

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Pipe Listing (all nodes)

| Line# | Node Number | In-Invert (feet) | Out-Invert (feet) | Length (feet) | Slope (ft/ft) | n | Diam/Width (inches) | Height (inches) | Inside-Fill (inches) |
|-------|-------------|------------------|-------------------|---------------|---------------|-------|---------------------|-----------------|----------------------|
| 1 | 2P | 0.00 | 0.00 | 255.0 | 0.0050 | 0.013 | 15.0 | 0.0 | 0.0 |
| 2 | B1 | 73.00 | 72.85 | 10.0 | 0.0150 | 0.013 | 24.0 | 0.0 | 0.0 |
| 3 | B2 | 73.00 | 72.06 | 47.0 | 0.0200 | 0.011 | 15.0 | 0.0 | 0.0 |
| 4 | B3 | 77.48 | 77.00 | 96.0 | 0.0050 | 0.013 | 15.0 | 0.0 | 0.0 |

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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

| | |
|--------------------------------------|---|
| Subcatchment 1E: Impervious | Runoff Area=10,351 sf 100.00% Impervious Runoff Depth=1.03" Tc=12.4 min CN=0/98 Runoff=0.57 cfs 892 cf |
| Subcatchment 1P: Impervious | Runoff Area=23,576 sf 100.00% Impervious Runoff Depth=1.03" Tc=10.7 min CN=0/98 Runoff=1.36 cfs 2,033 cf |
| Subcatchment 2E: Pervious | Runoff Area=167,702 sf 0.00% Impervious Runoff Depth=0.10" Flow Length=630' Tc=12.4 min CN=76/0 Runoff=0.70 cfs 1,415 cf |
| Subcatchment 2P: Pervious | Runoff Area=24,672 sf 0.00% Impervious Runoff Depth=0.07" Flow Length=426' Tc=10.7 min CN=74/0 Runoff=0.07 cfs 152 cf |
| Subcatchment 3E: Impervious | Runoff Area=5,641 sf 100.00% Impervious Runoff Depth=1.03" Tc=6.0 min CN=0/98 Runoff=0.38 cfs 486 cf |
| Subcatchment 3P: Roof Area | Runoff Area=35,418 sf 100.00% Impervious Runoff Depth=1.03" Tc=10.7 min CN=0/98 Runoff=2.05 cfs 3,054 cf |
| Subcatchment 4E: Pervious | Runoff Area=26,085 sf 0.00% Impervious Runoff Depth=0.37" Flow Length=393' Tc=6.0 min CN=87/0 Runoff=0.66 cfs 804 cf |
| Subcatchment 4P: Pervious | Runoff Area=13,613 sf 0.00% Impervious Runoff Depth=0.07" Tc=10.7 min CN=74/0 Runoff=0.04 cfs 84 cf |
| Subcatchment 5P: Impervious | Runoff Area=5,021 sf 97.63% Impervious Runoff Depth=1.03" Tc=20.8 min CN=96/98 Runoff=0.21 cfs 431 cf |
| Subcatchment 6P: Pervious | Runoff Area=6,701 sf 0.00% Impervious Runoff Depth=0.06" Flow Length=172' Tc=20.8 min CN=73/0 Runoff=0.01 cfs 35 cf |
| Subcatchment 7P: Impervious | Runoff Area=2,493 sf 100.00% Impervious Runoff Depth=1.03" Tc=13.9 min CN=0/98 Runoff=0.13 cfs 215 cf |
| Subcatchment 8P: Pervious | Runoff Area=61,889 sf 0.00% Impervious Runoff Depth=0.05" Flow Length=409' Tc=13.9 min CN=72/0 Runoff=0.10 cfs 264 cf |
| Subcatchment 9P: Pervious | Runoff Area=36,396 sf 0.00% Impervious Runoff Depth=0.06" Flow Length=471' Tc=12.2 min CN=73/0 Runoff=0.08 cfs 188 cf |
| Pond B1: Bioretention Basin 1 | Peak Elev=77.51' Storage=2,184 cf Inflow=1.39 cfs 2,184 cf Outflow=0.00 cfs 0 cf |
| Pond B2: Bioretention Basin 2 | Peak Elev=76.94' Storage=3,137 cf Inflow=2.06 cfs 3,137 cf Outflow=0.00 cfs 0 cf |
| Pond B3: Bioretention Basin 3 | Peak Elev=80.73' Storage=466 cf Inflow=0.22 cfs 466 cf Primary=0.00 cfs 0 cf Secondary=0.00 cfs 0 cf Outflow=0.00 cfs 0 cf |

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NJ DEP 2-hr WQ Rainfall=1.25"

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Link 5E: EDA 1

Inflow=1.15 cfs 2,308 cf
Primary=1.15 cfs 2,308 cf

Link 6E: EDA 2

Inflow=1.03 cfs 1,291 cf
Primary=1.03 cfs 1,291 cf

Link 7E: EDA

Inflow=1.82 cfs 3,598 cf
Primary=1.82 cfs 3,598 cf

Link 10P: PDA 1A

Inflow=0.00 cfs 0 cf
Primary=0.00 cfs 0 cf

Link 11P: PDA 1B

Inflow=0.00 cfs 0 cf
Primary=0.00 cfs 0 cf

Link 12P: PDA 1C

Inflow=0.19 cfs 479 cf
Primary=0.19 cfs 479 cf

Link 13P: PDA 1

Inflow=0.19 cfs 479 cf
Primary=0.19 cfs 479 cf

Link 14P: PDA 2

Inflow=0.08 cfs 188 cf
Primary=0.08 cfs 188 cf

Link 15P: PDA

Inflow=0.27 cfs 666 cf
Primary=0.27 cfs 666 cf

Total Runoff Area = 419,558 sf Runoff Volume = 10,052 cf Average Runoff Depth = 0.29"
80.36% Pervious = 337,177 sf 19.64% Impervious = 82,381 sf

Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Subcatchment 1E: Impervious

Runoff = 0.57 cfs @ 1.17 hrs, Volume= 892 cf, Depth= 1.03"

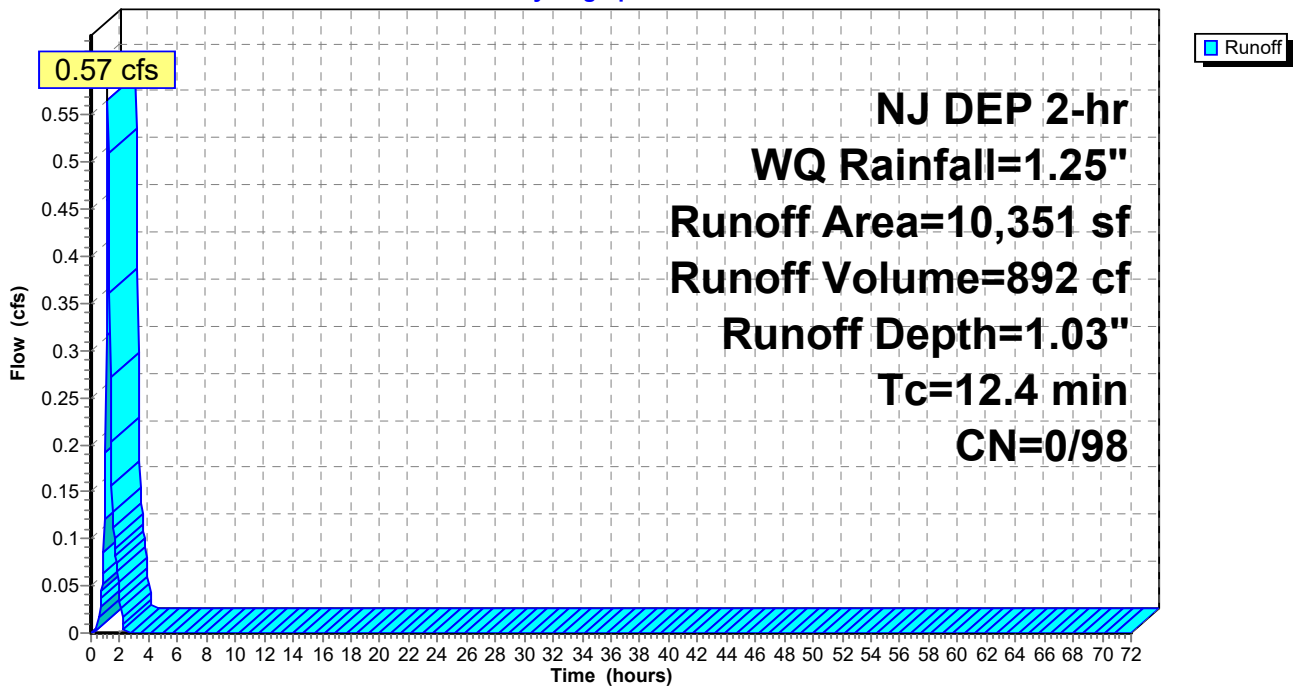
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 3,299 | 98 | Unconnected roofs, HSG C |
| 7,052 | 98 | Paved parking, HSG C |
| 10,351 | 98 | Weighted Average |
| 10,351 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 12.4 | | | | | Direct Entry, Tc |

Subcatchment 1E: Impervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

Summary for Subcatchment 1P: Impervious

Runoff = 1.36 cfs @ 1.15 hrs, Volume= 2,033 cf, Depth= 1.03"

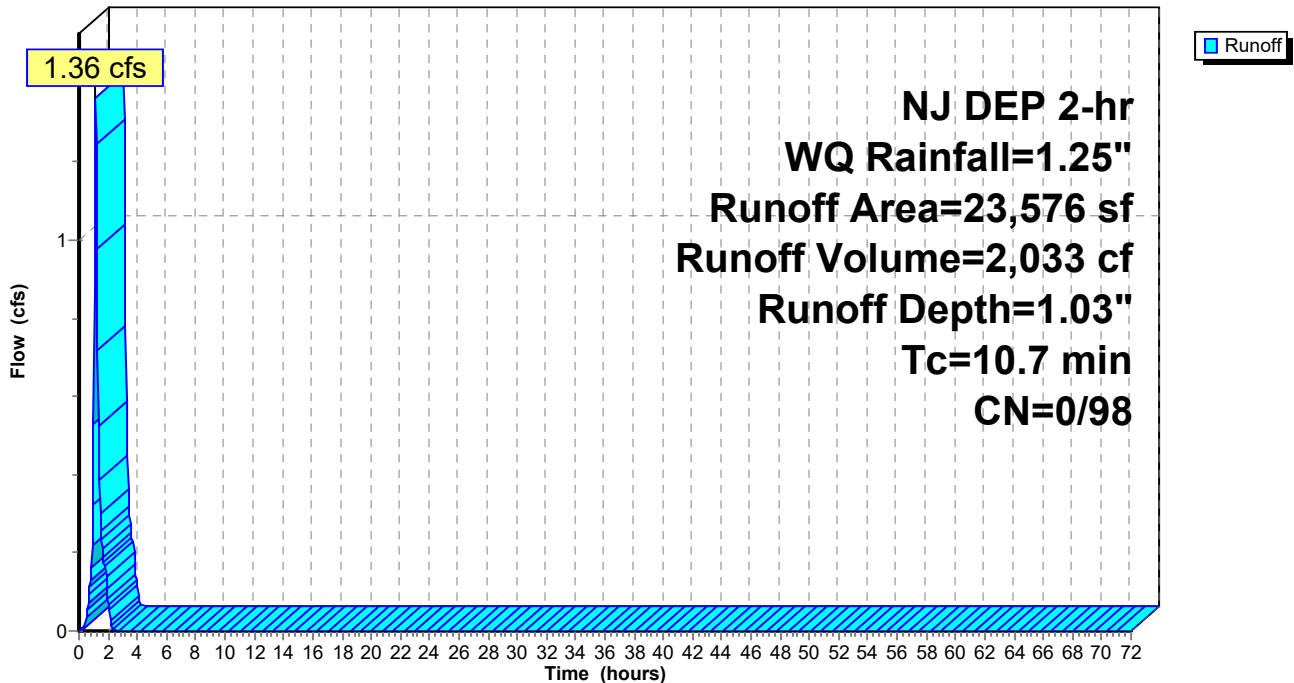
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 23,576 | 98 | Paved parking, HSG C |
| 23,576 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 1P: Impervious

Hydrograph



Pre vs Post

NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Subcatchment 2E: Pervious

Runoff = 0.70 cfs @ 1.28 hrs, Volume= 1,415 cf, Depth= 0.10"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 24,589 | 96 | Gravel surface, HSG C |
| 36,591 | 70 | Woods, Good, HSG C |
| 105,816 | 74 | >75% Grass cover, Good, HSG C |
| 706 | 72 | Woods/grass comb., Good, HSG C |
| 167,702 | 76 | Weighted Average |
| 167,702 | 76 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 0.3 | 27 | 0.0490 | 1.55 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 8.8 | 73 | 0.0130 | 0.14 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.4 | 54 | 0.0180 | 2.16 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 1.2 | 207 | 0.0340 | 2.97 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.5 | 59 | 0.0170 | 2.10 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 0.2 | 43 | 0.0470 | 3.49 | | Shallow Concentrated Flow, F-G Unpaved Kv= 16.1 fps |
| 1.0 | 167 | 0.0280 | 2.69 | | Shallow Concentrated Flow, G-H Unpaved Kv= 16.1 fps |
| 12.4 | 630 | Total | | | |

Pre vs Post

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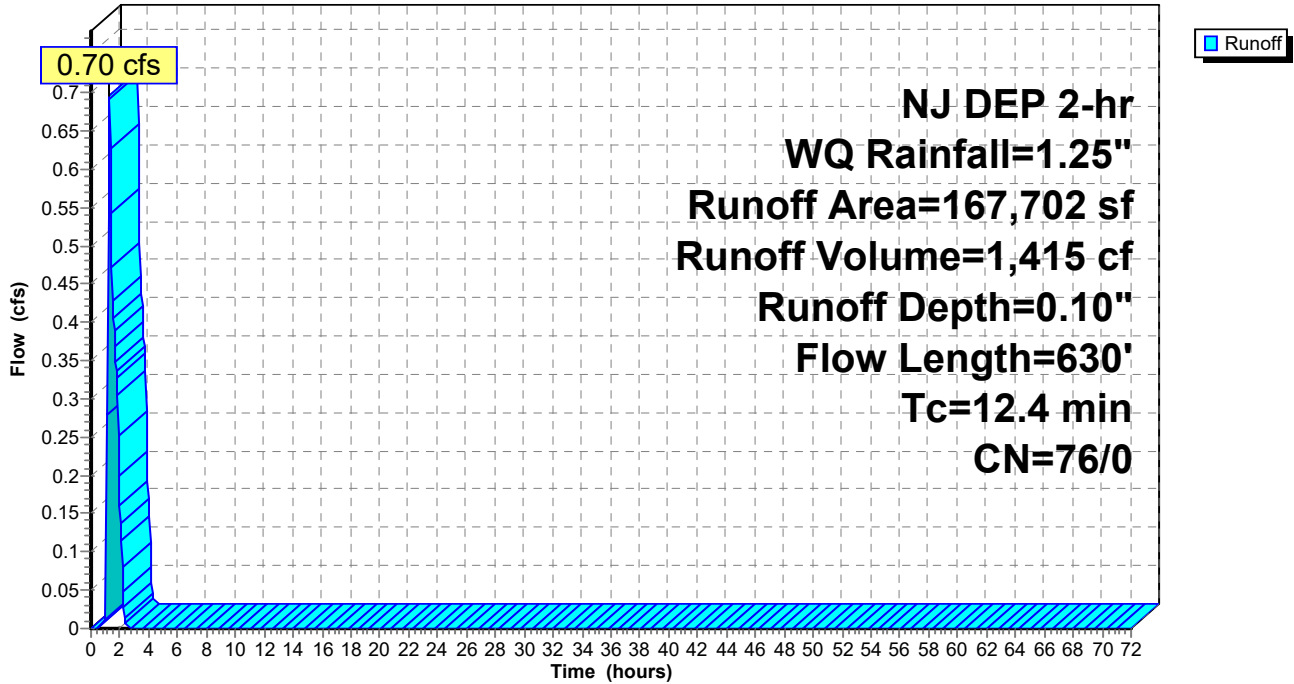
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NJ DEP 2-hr WQ Rainfall=1.25"

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Subcatchment 2E: Pervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

Summary for Subcatchment 2P: Pervious

Runoff = 0.07 cfs @ 1.28 hrs, Volume= 152 cf, Depth= 0.07"

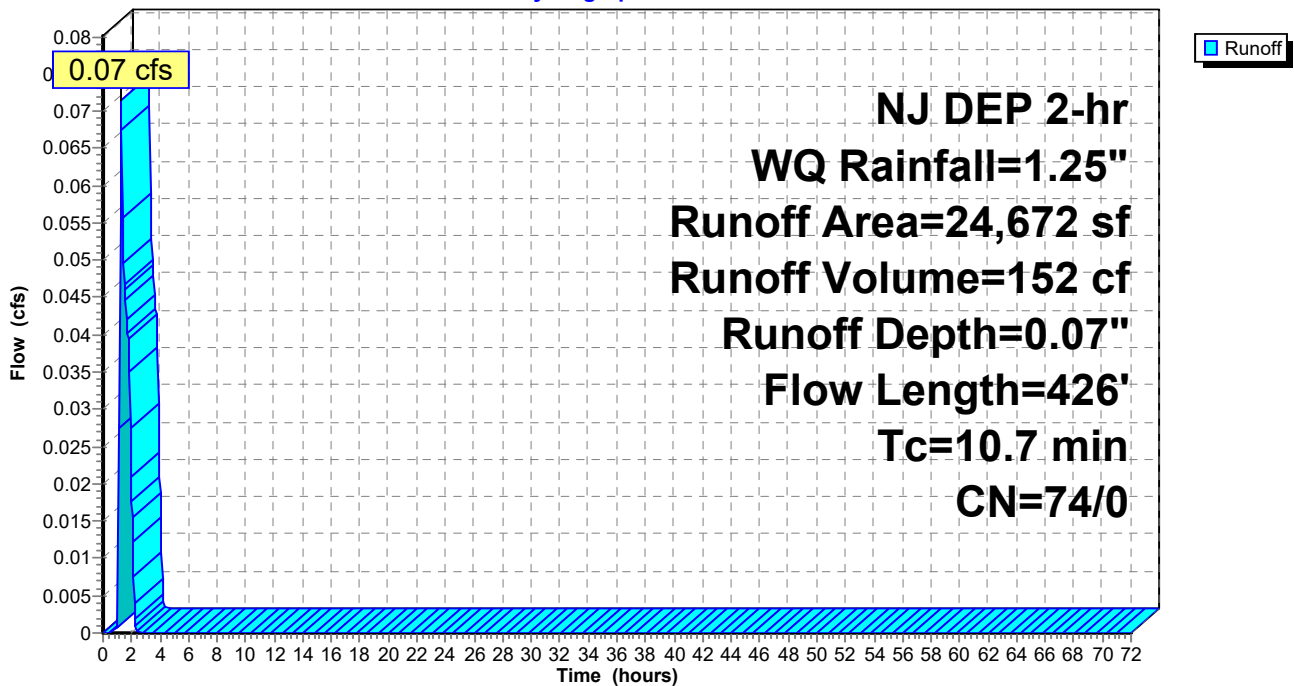
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 22,852 | 74 | >75% Grass cover, Good, HSG C |
| 1,820 | 72 | Woods/grass comb., Good, HSG C |
| 24,672 | 74 | Weighted Average |
| 24,672 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 9.2 | 100 | 0.0222 | 0.18 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.1 | 23 | 0.0730 | 4.35 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.3 | 48 | 0.0210 | 2.94 | | Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps |
| 1.1 | 255 | 0.0050 | 3.72 | 4.57 | Pipe Channel, D-E 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013 Concrete pipe, bends & connections |
| 10.7 | 426 | Total | | | |

Subcatchment 2P: Pervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Subcatchment 3E: Impervious

Runoff = 0.38 cfs @ 1.09 hrs, Volume= 486 cf, Depth= 1.03"

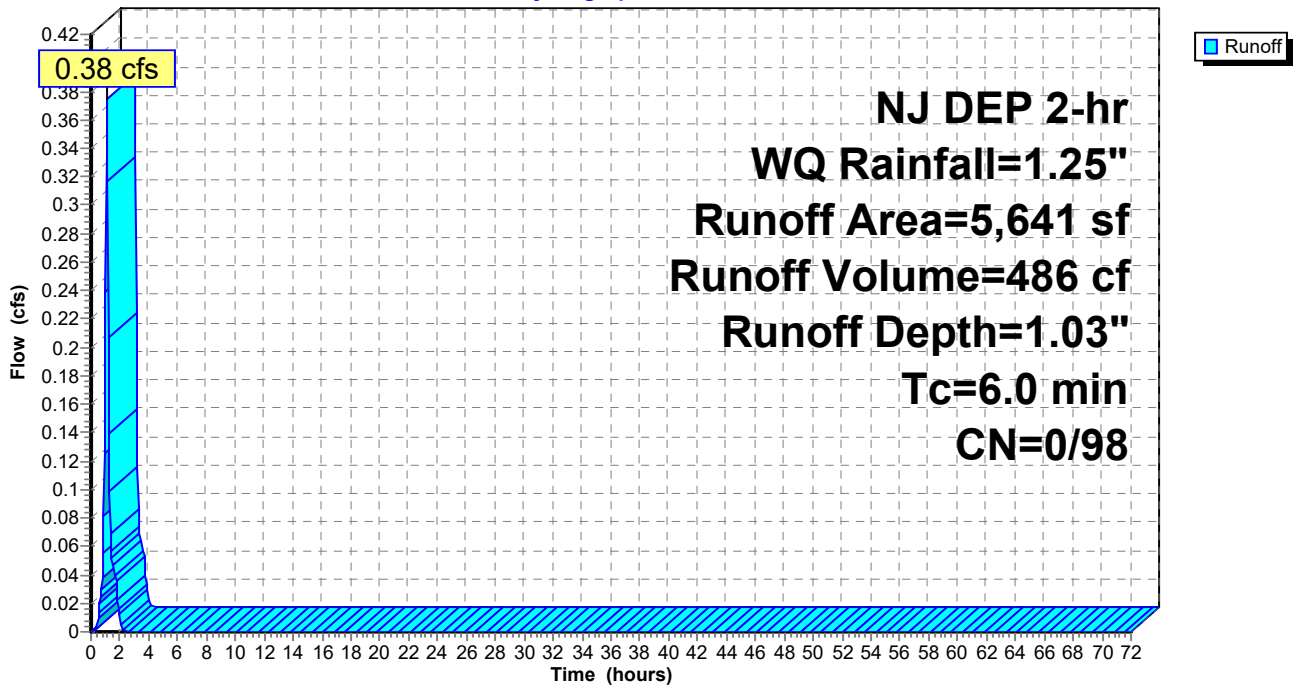
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 2,580 | 98 | Unconnected roofs, HSG C |
| 3,061 | 98 | Paved parking, HSG C |
| 5,641 | 98 | Weighted Average |
| 5,641 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|-------------------------|
| 3.0 | | | | | Direct Entry, Tc |
| 3.0 | 0 | Total, Increased to minimum Tc = 6.0 min | | | |

Subcatchment 3E: Impervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Subcatchment 3P: Roof Area

Runoff = 2.05 cfs @ 1.15 hrs, Volume= 3,054 cf, Depth= 1.03"

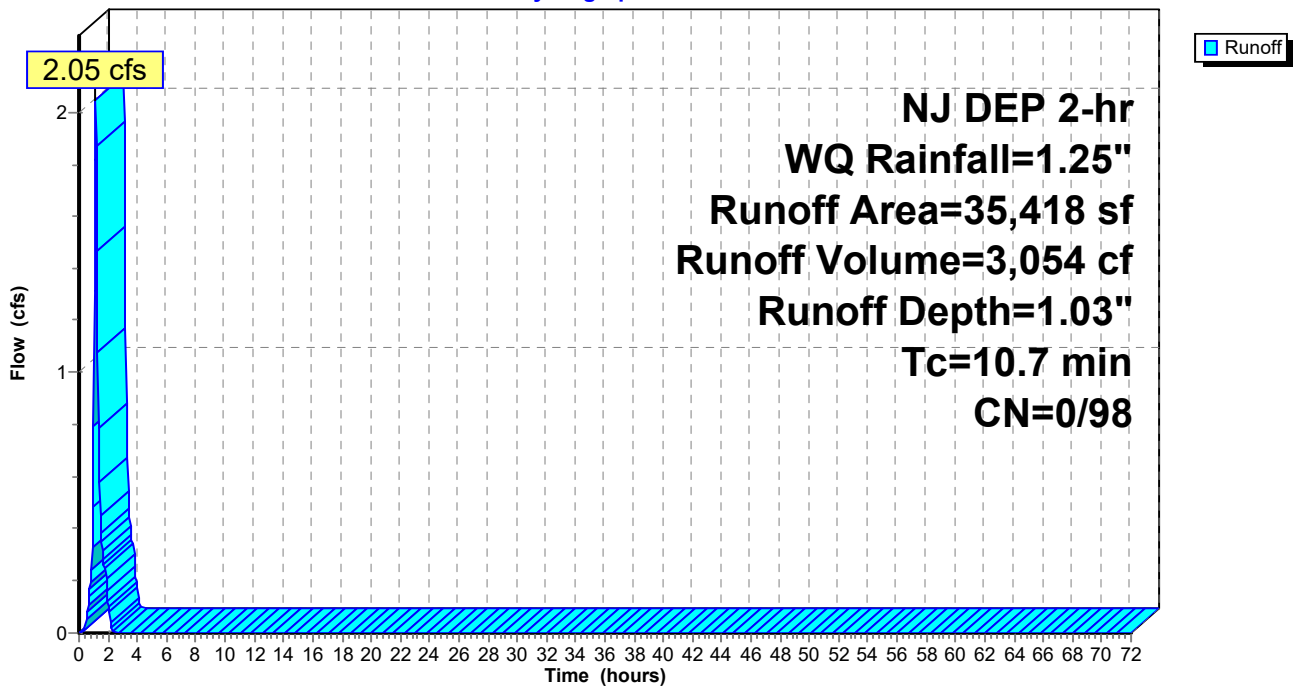
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|-----------------------------|
| 35,068 | 98 | Unconnected roofs, HSG C |
| 350 | 98 | Unconnected pavement, HSG C |
| 35,418 | 98 | Weighted Average |
| 35,418 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 3P: Roof Area

Hydrograph



Pre vs Post

NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Subcatchment 4E: Pervious

Runoff = 0.66 cfs @ 1.13 hrs, Volume= 804 cf, Depth= 0.37"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 164 | 70 | Woods, Good, HSG C |
| 16,189 | 96 | Gravel surface, HSG C |
| 5,108 | 74 | >75% Grass cover, Good, HSG C |
| 4,624 | 72 | Woods/grass comb., Good, HSG C |
| 26,085 | 87 | Weighted Average |
| 26,085 | 87 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|---|
| 1.3 | 100 | 0.0160 | 1.29 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 0.6 | 97 | 0.0200 | 2.87 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 1.0 | 175 | 0.0330 | 2.92 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.1 | 13 | 0.0230 | 2.44 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.0 | 8 | 0.0480 | 3.53 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 3.0 | 393 | Total, Increased to minimum Tc = 6.0 min | | | |

Pre vs Post

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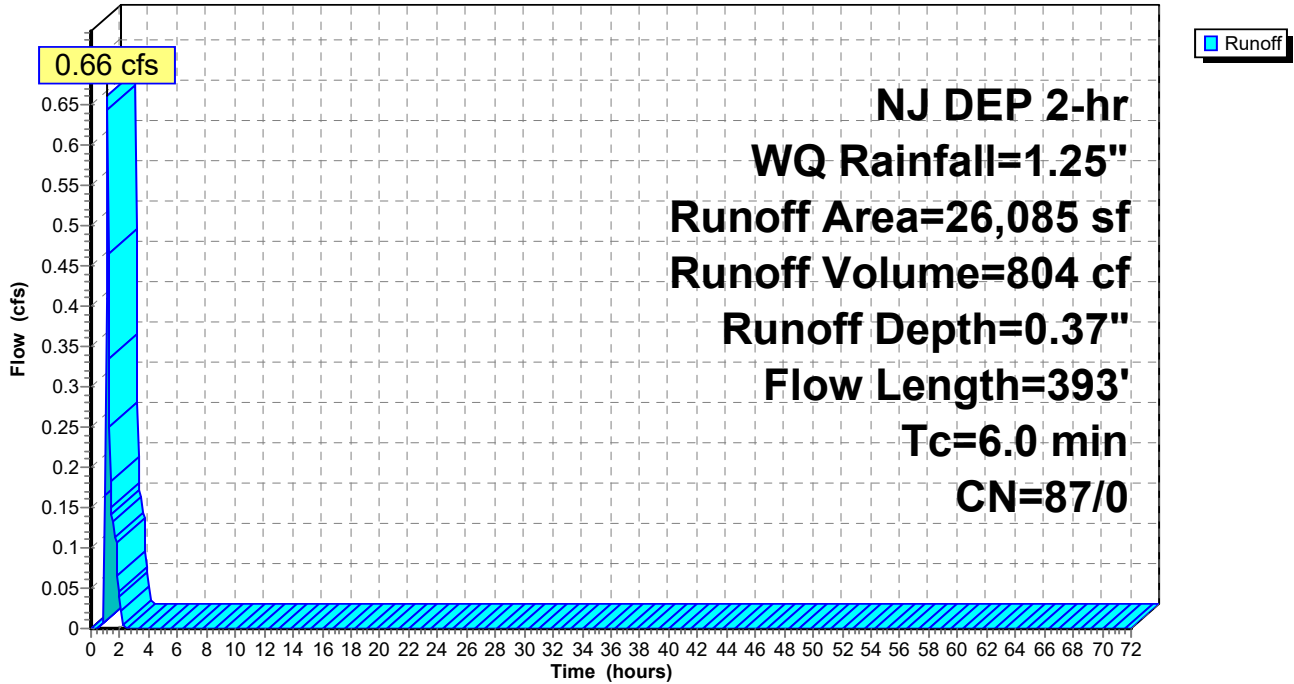
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NJ DEP 2-hr WQ Rainfall=1.25"

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Subcatchment 4E: Pervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

Summary for Subcatchment 4P: Pervious

Runoff = 0.04 cfs @ 1.28 hrs, Volume= 84 cf, Depth= 0.07"

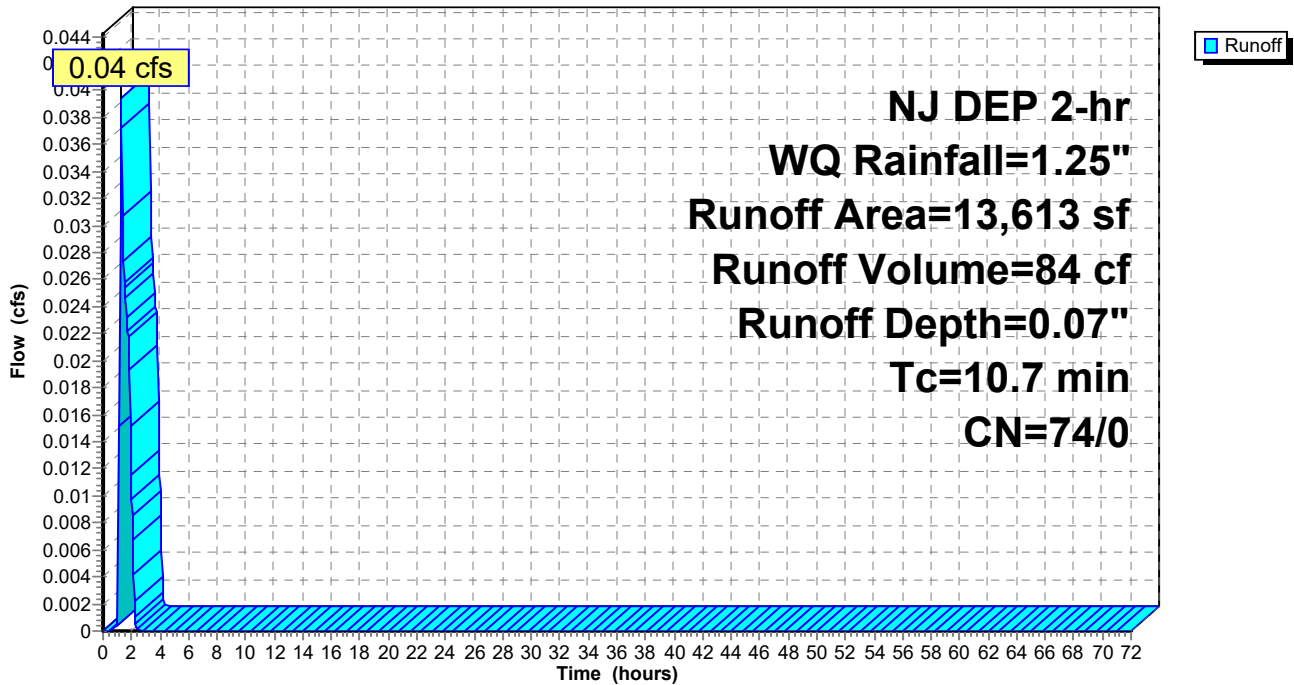
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 13,613 | 74 | >75% Grass cover, Good, HSG C |
| 13,613 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 4P: Pervious

Hydrograph



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NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Subcatchment 5P: Impervious

Runoff = 0.21 cfs @ 1.28 hrs, Volume= 431 cf, Depth= 1.03"

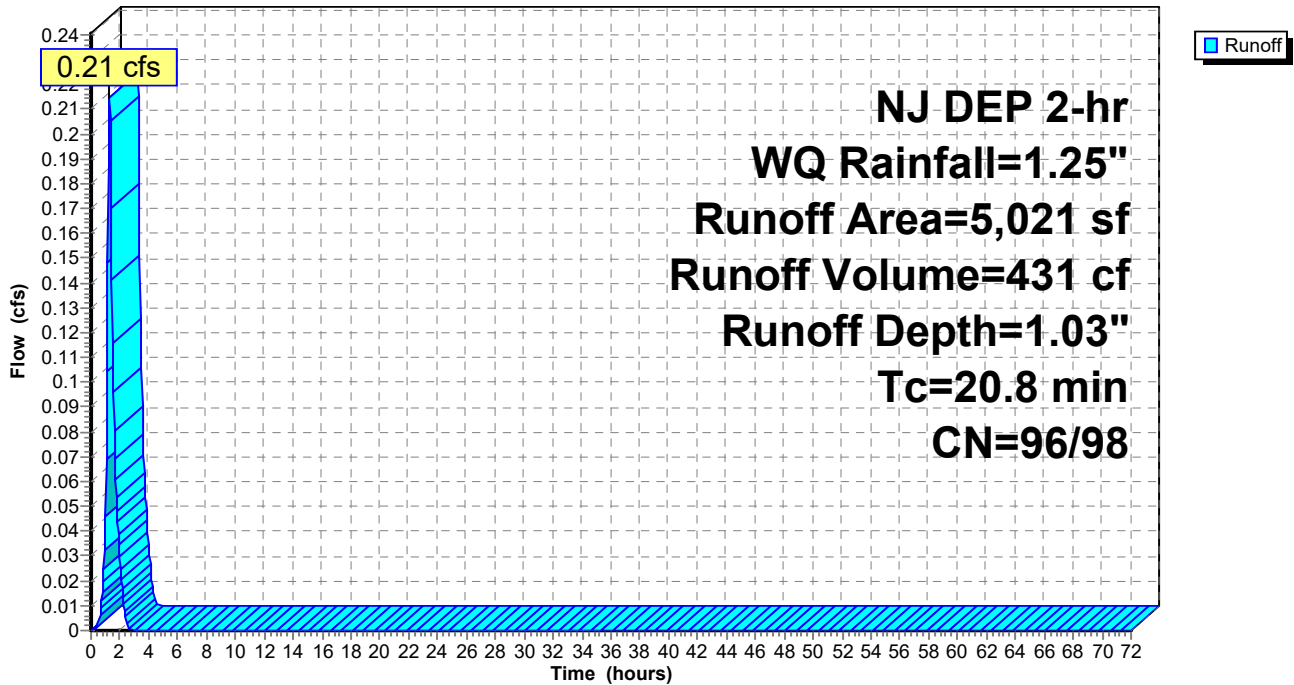
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|------------------------|
| 4,902 | 98 | Paved parking, HSG C |
| 119 | 96 | Gravel surface, HSG C |
| 5,021 | 98 | Weighted Average |
| 119 | 96 | 2.37% Pervious Area |
| 4,902 | 98 | 97.63% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 20.8 | | | | | Direct Entry, Tc |

Subcatchment 5P: Impervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

Summary for Subcatchment 6P: Pervious

Runoff = 0.01 cfs @ 1.47 hrs, Volume= 35 cf, Depth= 0.06"

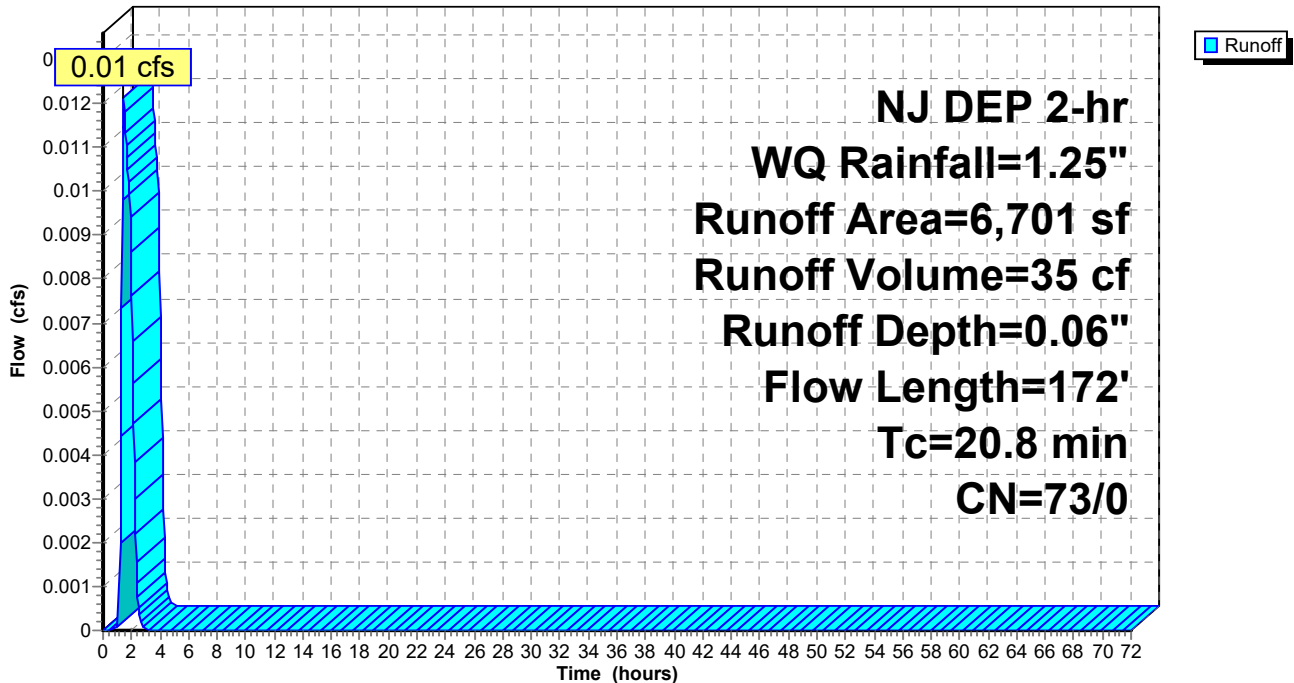
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 4,509 | 74 | >75% Grass cover, Good, HSG C |
| 2,192 | 70 | Woods, Good, HSG C |
| 6,701 | 73 | Weighted Average |
| 6,701 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 20.4 | 104 | 0.0230 | 0.08 | | Sheet Flow, A-B Woods: Light underbrush n= 0.400 P2= 3.36" |
| 0.3 | 57 | 0.0230 | 3.08 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 0.1 | 11 | 0.0200 | 2.28 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 20.8 | 172 | Total | | | |

Subcatchment 6P: Pervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

Summary for Subcatchment 7P: Impervious

Runoff = 0.13 cfs @ 1.19 hrs, Volume= 215 cf, Depth= 1.03"

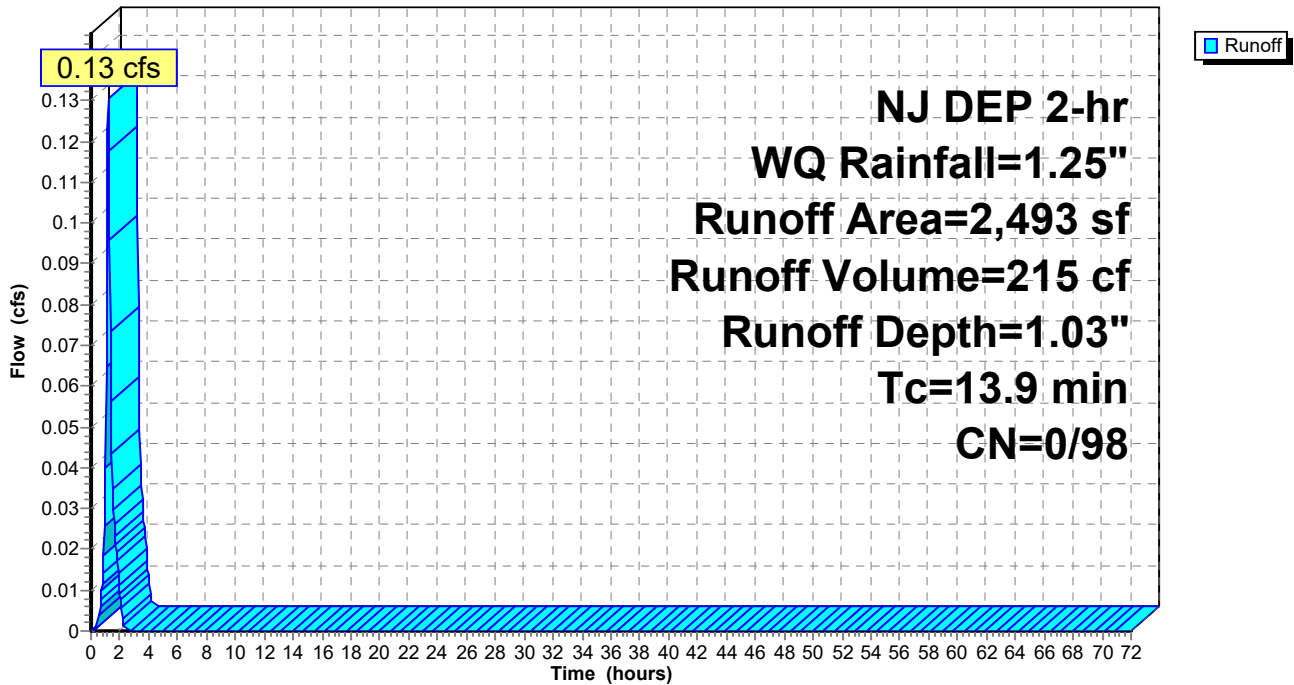
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,493 | 98 | Paved parking, HSG C |
| 2,493 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 13.9 | | | | | Direct Entry, Tc |

Subcatchment 7P: Impervious

Hydrograph



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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

Summary for Subcatchment 8P: Pervious

Runoff = 0.10 cfs @ 1.37 hrs, Volume= 264 cf, Depth= 0.05"

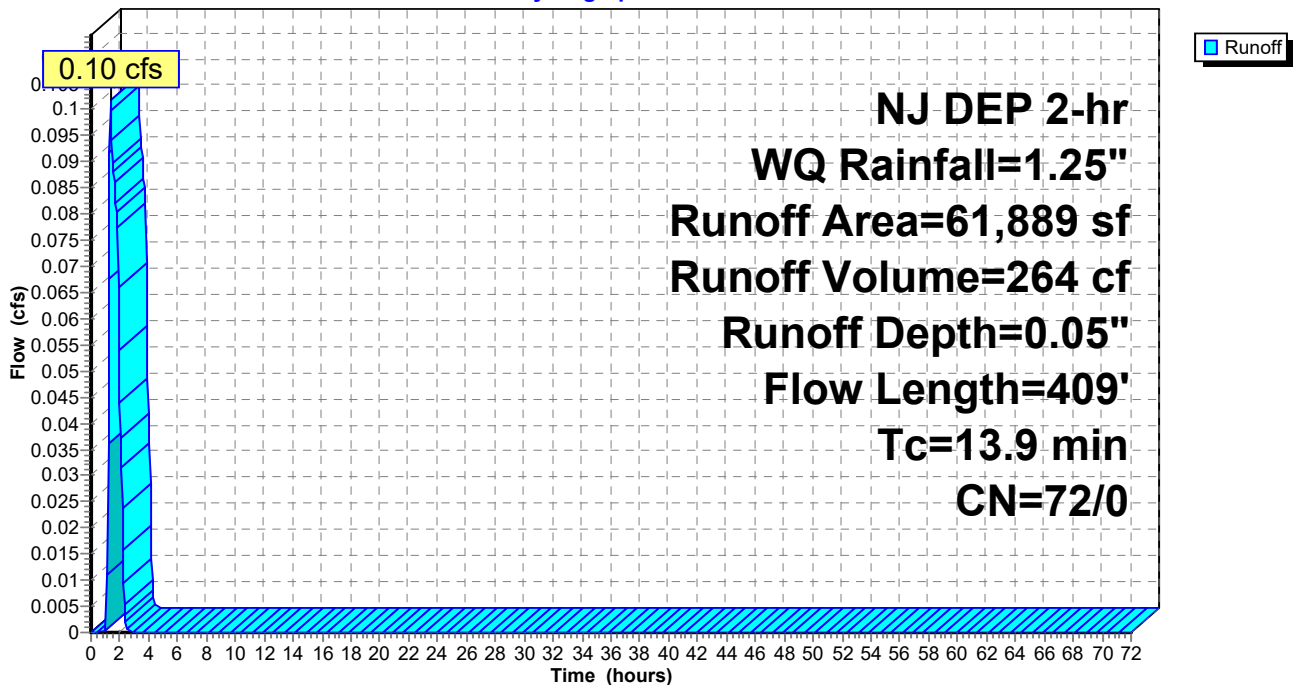
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 28,675 | 70 | Woods, Good, HSG C |
| 33,214 | 74 | >75% Grass cover, Good, HSG C |
| 61,889 | 72 | Weighted Average |
| 61,889 | 72 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 2.8 | 36 | 0.0560 | 0.21 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 4.3 | 51 | 0.0390 | 0.20 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.3 | 25 | 0.0800 | 1.41 | | Shallow Concentrated Flow, C-D Woodland Kv= 5.0 fps |
| 6.5 | 297 | 0.0230 | 0.76 | | Shallow Concentrated Flow, D-E Woodland Kv= 5.0 fps |
| 13.9 | 409 | Total | | | |

Subcatchment 8P: Pervious

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Subcatchment 9P: Pervious

Runoff = 0.08 cfs @ 1.32 hrs, Volume= 188 cf, Depth= 0.06"

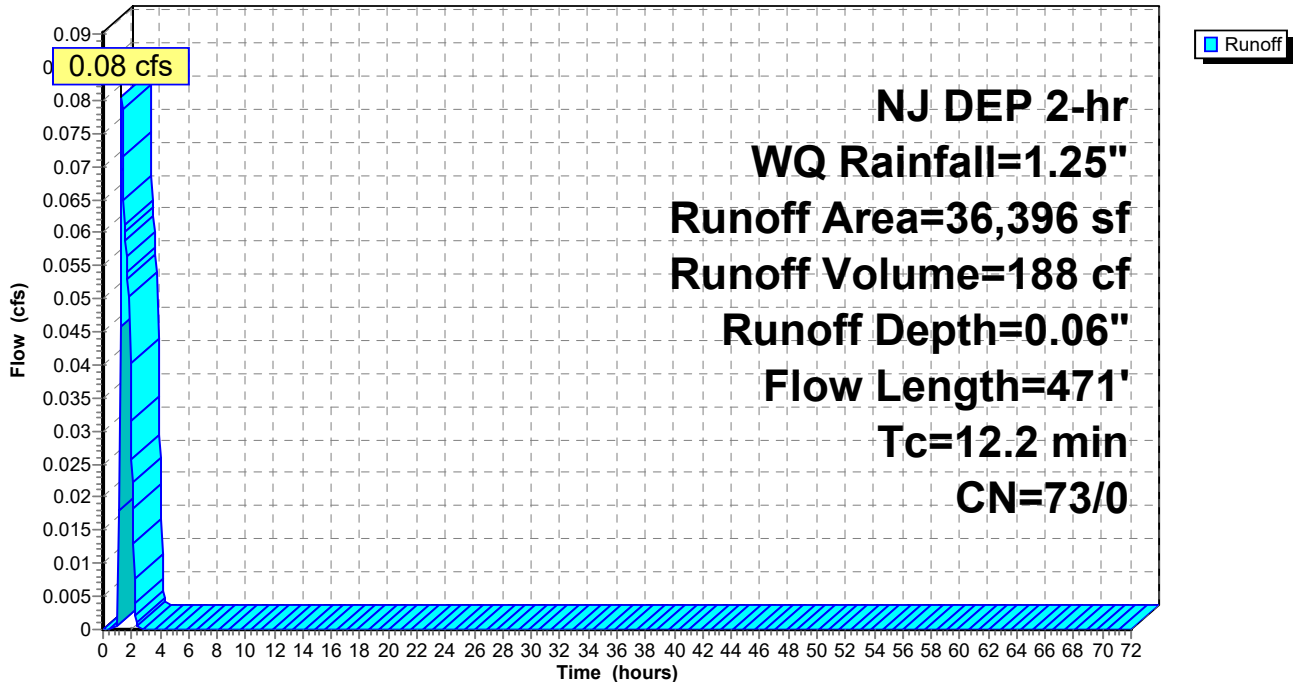
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr WQ Rainfall=1.25"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 5,369 | 70 | Woods, Good, HSG C |
| 31,027 | 74 | >75% Grass cover, Good, HSG C |
| 36,396 | 73 | Weighted Average |
| 36,396 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 9.8 | 100 | 0.0190 | 0.17 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.7 | 102 | 0.0240 | 2.49 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.8 | 128 | 0.0310 | 2.83 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.8 | 120 | 0.0250 | 2.55 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.1 | 21 | 0.0310 | 2.83 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 12.2 | 471 | Total | | | |

Subcatchment 9P: Pervious

Hydrograph



Pre vs Post

NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Pond B1: Bioretention Basin 1

[92] Warning: Device #2 is above defined storage

Inflow Area = 48,248 sf, 48.86% Impervious, Inflow Depth = 0.54" for WQ event
 Inflow = 1.39 cfs @ 1.16 hrs, Volume= 2,184 cf
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 77.51' @ 2.65 hrs Surf.Area= 2,466 sf Storage= 2,184 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)
 Center-of-Mass det. time= (not calculated: no outflow)

| Volume | Invert | Avail.Storage | Storage Description | |
|------------------|-------------------|------------------------|--|------------------|
| #1 | 76.50' | 4,938 cf | Custom Stage Data (Conic) Listed below (Recalc) | |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
| 76.50 | 1,883 | 0 | 0 | 1,883 |
| 77.50 | 2,461 | 2,166 | 2,166 | 2,484 |
| 78.50 | 3,096 | 2,772 | 4,938 | 3,146 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|---|
| #1 | Primary | 73.00' | 24.0" Round CMP_Round 24" L= 10.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.85' S= 0.0150 ' S Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf |
| #2 | Device 1 | 78.50' | 10.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 78.15' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=76.50' (Free Discharge)
 1=CMP_Round 24" (Passes 0.00 cfs of 18.88 cfs potential flow)
 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
 3=Orifice/Grate (Controls 0.00 cfs)

Pre vs Post

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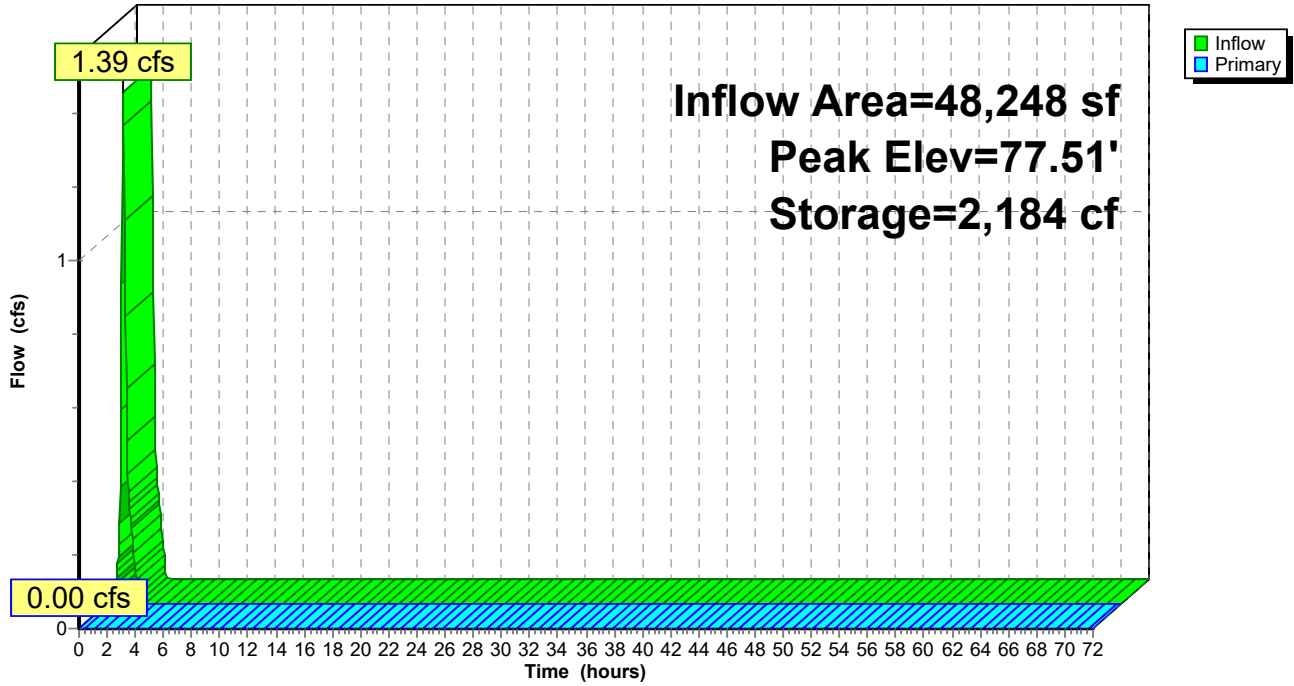
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NJ DEP 2-hr WQ Rainfall=1.25"

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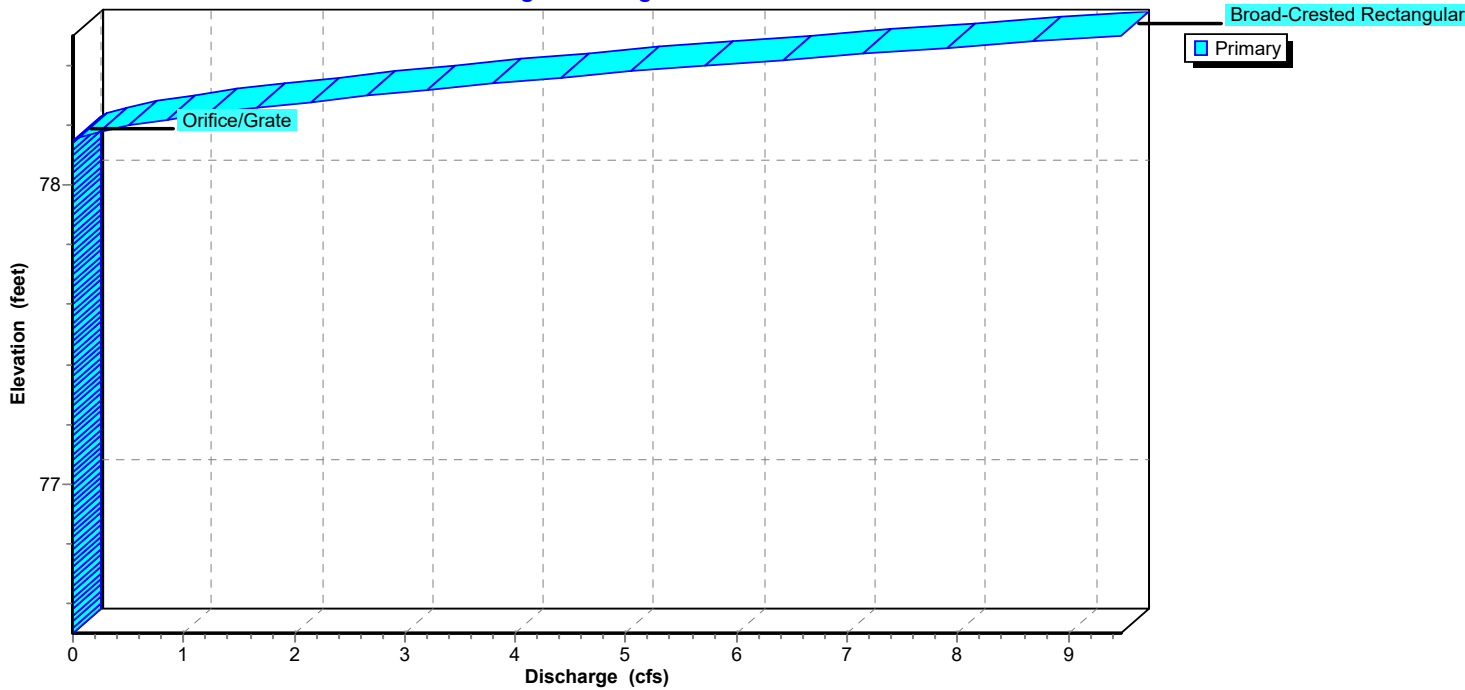
Pond B1: Bioretention Basin 1

Hydrograph



Pond B1: Bioretention Basin 1

Stage-Discharge



Pre vs Post

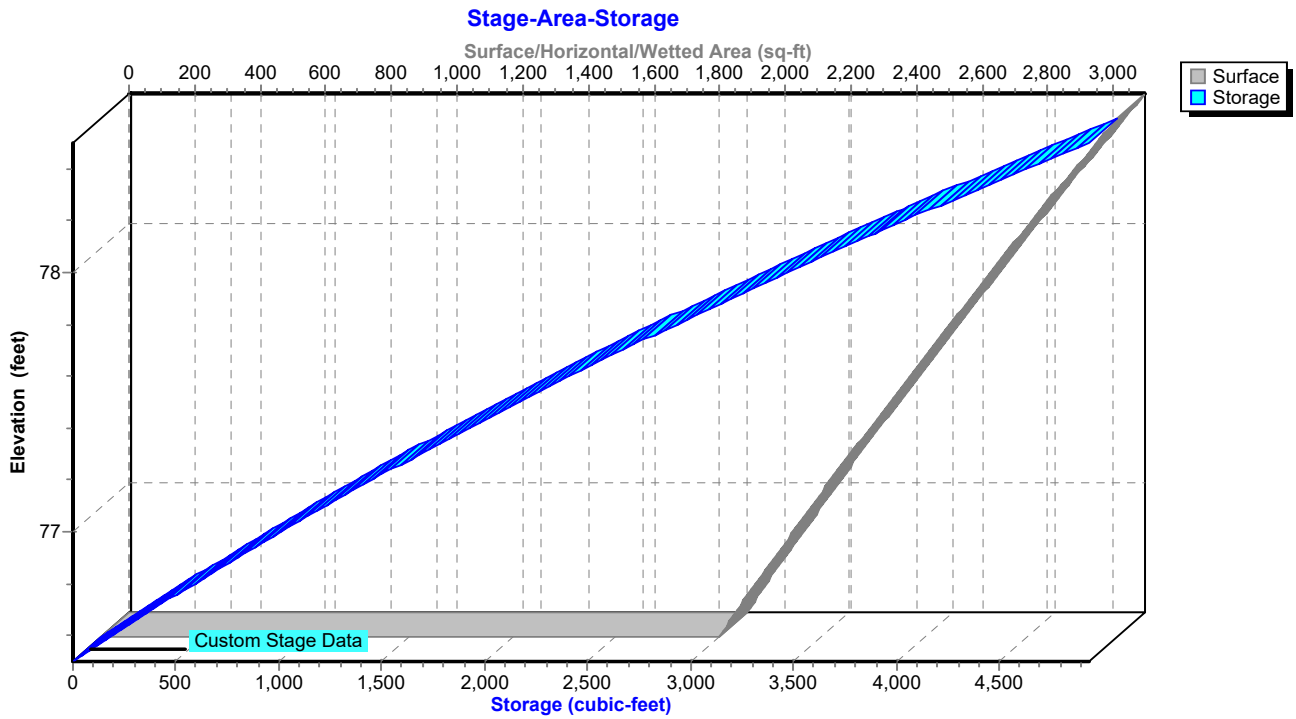
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Pond B1: Bioretention Basin 1



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Stage-Discharge for Pond B1: Bioretention Basin 1

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.03 | 0.00 | 77.56 | 0.00 | 78.09 | 0.00 |
| 76.51 | 0.00 | 77.04 | 0.00 | 77.57 | 0.00 | 78.10 | 0.00 |
| 76.52 | 0.00 | 77.05 | 0.00 | 77.58 | 0.00 | 78.11 | 0.00 |
| 76.53 | 0.00 | 77.06 | 0.00 | 77.59 | 0.00 | 78.12 | 0.00 |
| 76.54 | 0.00 | 77.07 | 0.00 | 77.60 | 0.00 | 78.13 | 0.00 |
| 76.55 | 0.00 | 77.08 | 0.00 | 77.61 | 0.00 | 78.14 | 0.00 |
| 76.56 | 0.00 | 77.09 | 0.00 | 77.62 | 0.00 | 78.15 | 0.00 |
| 76.57 | 0.00 | 77.10 | 0.00 | 77.63 | 0.00 | 78.16 | 0.05 |
| 76.58 | 0.00 | 77.11 | 0.00 | 77.64 | 0.00 | 78.17 | 0.13 |
| 76.59 | 0.00 | 77.12 | 0.00 | 77.65 | 0.00 | 78.18 | 0.24 |
| 76.60 | 0.00 | 77.13 | 0.00 | 77.66 | 0.00 | 78.19 | 0.37 |
| 76.61 | 0.00 | 77.14 | 0.00 | 77.67 | 0.00 | 78.20 | 0.51 |
| 76.62 | 0.00 | 77.15 | 0.00 | 77.68 | 0.00 | 78.21 | 0.67 |
| 76.63 | 0.00 | 77.16 | 0.00 | 77.69 | 0.00 | 78.22 | 0.85 |
| 76.64 | 0.00 | 77.17 | 0.00 | 77.70 | 0.00 | 78.23 | 1.04 |
| 76.65 | 0.00 | 77.18 | 0.00 | 77.71 | 0.00 | 78.24 | 1.24 |
| 76.66 | 0.00 | 77.19 | 0.00 | 77.72 | 0.00 | 78.25 | 1.45 |
| 76.67 | 0.00 | 77.20 | 0.00 | 77.73 | 0.00 | 78.26 | 1.67 |
| 76.68 | 0.00 | 77.21 | 0.00 | 77.74 | 0.00 | 78.27 | 1.90 |
| 76.69 | 0.00 | 77.22 | 0.00 | 77.75 | 0.00 | 78.28 | 2.15 |
| 76.70 | 0.00 | 77.23 | 0.00 | 77.76 | 0.00 | 78.29 | 2.40 |
| 76.71 | 0.00 | 77.24 | 0.00 | 77.77 | 0.00 | 78.30 | 2.66 |
| 76.72 | 0.00 | 77.25 | 0.00 | 77.78 | 0.00 | 78.31 | 2.93 |
| 76.73 | 0.00 | 77.26 | 0.00 | 77.79 | 0.00 | 78.32 | 3.21 |
| 76.74 | 0.00 | 77.27 | 0.00 | 77.80 | 0.00 | 78.33 | 3.50 |
| 76.75 | 0.00 | 77.28 | 0.00 | 77.81 | 0.00 | 78.34 | 3.79 |
| 76.76 | 0.00 | 77.29 | 0.00 | 77.82 | 0.00 | 78.35 | 4.09 |
| 76.77 | 0.00 | 77.30 | 0.00 | 77.83 | 0.00 | 78.36 | 4.41 |
| 76.78 | 0.00 | 77.31 | 0.00 | 77.84 | 0.00 | 78.37 | 4.72 |
| 76.79 | 0.00 | 77.32 | 0.00 | 77.85 | 0.00 | 78.38 | 5.05 |
| 76.80 | 0.00 | 77.33 | 0.00 | 77.86 | 0.00 | 78.39 | 5.38 |
| 76.81 | 0.00 | 77.34 | 0.00 | 77.87 | 0.00 | 78.40 | 5.72 |
| 76.82 | 0.00 | 77.35 | 0.00 | 77.88 | 0.00 | 78.41 | 6.07 |
| 76.83 | 0.00 | 77.36 | 0.00 | 77.89 | 0.00 | 78.42 | 6.42 |
| 76.84 | 0.00 | 77.37 | 0.00 | 77.90 | 0.00 | 78.43 | 6.78 |
| 76.85 | 0.00 | 77.38 | 0.00 | 77.91 | 0.00 | 78.44 | 7.15 |
| 76.86 | 0.00 | 77.39 | 0.00 | 77.92 | 0.00 | 78.45 | 7.52 |
| 76.87 | 0.00 | 77.40 | 0.00 | 77.93 | 0.00 | 78.46 | 7.90 |
| 76.88 | 0.00 | 77.41 | 0.00 | 77.94 | 0.00 | 78.47 | 8.29 |
| 76.89 | 0.00 | 77.42 | 0.00 | 77.95 | 0.00 | 78.48 | 8.68 |
| 76.90 | 0.00 | 77.43 | 0.00 | 77.96 | 0.00 | 78.49 | 9.08 |
| 76.91 | 0.00 | 77.44 | 0.00 | 77.97 | 0.00 | 78.50 | 9.48 |
| 76.92 | 0.00 | 77.45 | 0.00 | 77.98 | 0.00 | | |
| 76.93 | 0.00 | 77.46 | 0.00 | 77.99 | 0.00 | | |
| 76.94 | 0.00 | 77.47 | 0.00 | 78.00 | 0.00 | | |
| 76.95 | 0.00 | 77.48 | 0.00 | 78.01 | 0.00 | | |
| 76.96 | 0.00 | 77.49 | 0.00 | 78.02 | 0.00 | | |
| 76.97 | 0.00 | 77.50 | 0.00 | 78.03 | 0.00 | | |
| 76.98 | 0.00 | 77.51 | 0.00 | 78.04 | 0.00 | | |
| 76.99 | 0.00 | 77.52 | 0.00 | 78.05 | 0.00 | | |
| 77.00 | 0.00 | 77.53 | 0.00 | 78.06 | 0.00 | | |
| 77.01 | 0.00 | 77.54 | 0.00 | 78.07 | 0.00 | | |
| 77.02 | 0.00 | 77.55 | 0.00 | 78.08 | 0.00 | | |

Pre vs Post

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Stage-Area-Storage for Pond B1: Bioretention Basin 1

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 1,883 | 0 | 77.56 | 2,497 | 2,314 |
| 76.52 | 1,894 | 38 | 77.58 | 2,509 | 2,364 |
| 76.54 | 1,905 | 76 | 77.60 | 2,521 | 2,415 |
| 76.56 | 1,916 | 114 | 77.62 | 2,533 | 2,465 |
| 76.58 | 1,926 | 152 | 77.64 | 2,546 | 2,516 |
| 76.60 | 1,937 | 191 | 77.66 | 2,558 | 2,567 |
| 76.62 | 1,948 | 230 | 77.68 | 2,570 | 2,618 |
| 76.64 | 1,959 | 269 | 77.70 | 2,582 | 2,670 |
| 76.66 | 1,970 | 308 | 77.72 | 2,594 | 2,722 |
| 76.68 | 1,981 | 348 | 77.74 | 2,607 | 2,774 |
| 76.70 | 1,992 | 387 | 77.76 | 2,619 | 2,826 |
| 76.72 | 2,004 | 427 | 77.78 | 2,631 | 2,878 |
| 76.74 | 2,015 | 468 | 77.80 | 2,644 | 2,931 |
| 76.76 | 2,026 | 508 | 77.82 | 2,656 | 2,984 |
| 76.78 | 2,037 | 549 | 77.84 | 2,669 | 3,037 |
| 76.80 | 2,048 | 590 | 77.86 | 2,681 | 3,091 |
| 76.82 | 2,060 | 631 | 77.88 | 2,694 | 3,145 |
| 76.84 | 2,071 | 672 | 77.90 | 2,706 | 3,199 |
| 76.86 | 2,082 | 713 | 77.92 | 2,719 | 3,253 |
| 76.88 | 2,094 | 755 | 77.94 | 2,731 | 3,307 |
| 76.90 | 2,105 | 797 | 77.96 | 2,744 | 3,362 |
| 76.92 | 2,116 | 839 | 77.98 | 2,757 | 3,417 |
| 76.94 | 2,128 | 882 | 78.00 | 2,769 | 3,472 |
| 76.96 | 2,139 | 924 | 78.02 | 2,782 | 3,528 |
| 76.98 | 2,151 | 967 | 78.04 | 2,795 | 3,584 |
| 77.00 | 2,162 | 1,011 | 78.06 | 2,808 | 3,640 |
| 77.02 | 2,174 | 1,054 | 78.08 | 2,820 | 3,696 |
| 77.04 | 2,186 | 1,097 | 78.10 | 2,833 | 3,753 |
| 77.06 | 2,197 | 1,141 | 78.12 | 2,846 | 3,809 |
| 77.08 | 2,209 | 1,185 | 78.14 | 2,859 | 3,866 |
| 77.10 | 2,221 | 1,230 | 78.16 | 2,872 | 3,924 |
| 77.12 | 2,232 | 1,274 | 78.18 | 2,885 | 3,981 |
| 77.14 | 2,244 | 1,319 | 78.20 | 2,898 | 4,039 |
| 77.16 | 2,256 | 1,364 | 78.22 | 2,911 | 4,097 |
| 77.18 | 2,268 | 1,409 | 78.24 | 2,924 | 4,156 |
| 77.20 | 2,279 | 1,455 | 78.26 | 2,937 | 4,214 |
| 77.22 | 2,291 | 1,500 | 78.28 | 2,950 | 4,273 |
| 77.24 | 2,303 | 1,546 | 78.30 | 2,963 | 4,332 |
| 77.26 | 2,315 | 1,593 | 78.32 | 2,976 | 4,392 |
| 77.28 | 2,327 | 1,639 | 78.34 | 2,990 | 4,451 |
| 77.30 | 2,339 | 1,686 | 78.36 | 3,003 | 4,511 |
| 77.32 | 2,351 | 1,732 | 78.38 | 3,016 | 4,571 |
| 77.34 | 2,363 | 1,780 | 78.40 | 3,029 | 4,632 |
| 77.36 | 2,375 | 1,827 | 78.42 | 3,043 | 4,692 |
| 77.38 | 2,388 | 1,875 | 78.44 | 3,056 | 4,753 |
| 77.40 | 2,400 | 1,923 | 78.46 | 3,069 | 4,815 |
| 77.42 | 2,412 | 1,971 | 78.48 | 3,083 | 4,876 |
| 77.44 | 2,424 | 2,019 | 78.50 | 3,096 | 4,938 |
| 77.46 | 2,436 | 2,068 | | | |
| 77.48 | 2,449 | 2,116 | | | |
| 77.50 | 2,461 | 2,166 | | | |
| 77.52 | 2,473 | 2,215 | | | |
| 77.54 | 2,485 | 2,264 | | | |

Pre vs Post

NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Pond B2: Bioretention Basin 2

[79] Warning: Submerged Pond B1 Primary device # 1 INLET by 3.94'

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 0.39" for WQ event
 Inflow = 2.06 cfs @ 1.16 hrs, Volume= 3,137 cf
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 76.94' @ 2.65 hrs Surf.Area= 7,437 sf Storage= 3,137 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)
 Center-of-Mass det. time= (not calculated: no outflow)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 76.50' | 26,647 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|------------------|-------------------|------------------------|------------------------|
| 76.50 | 6,877 | 0 | 0 |
| 77.50 | 8,155 | 7,516 | 7,516 |
| 78.50 | 9,522 | 8,839 | 16,355 |
| 79.50 | 11,063 | 10,293 | 26,647 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|--|
| #1 | Primary | 73.00' | 15.0" Round Culvert L= 47.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.06' S= 0.0200 ' S= 0.0200 ' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf |
| #2 | Device 1 | 76.94' | 6.0" Vert. Orifice/Grate X 3.00 C= 0.600 |
| #3 | Device 1 | 77.78' | 4.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |
| #4 | Device 1 | 79.25' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=76.50' (Free Discharge)

- 1=Culvert (Passes 0.00 cfs of 7.91 cfs potential flow)
- 2=Orifice/Grate (Controls 0.00 cfs)
- 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
- 4=Orifice/Grate (Controls 0.00 cfs)

Pre vs Post

Prepared by {enter your company name here}

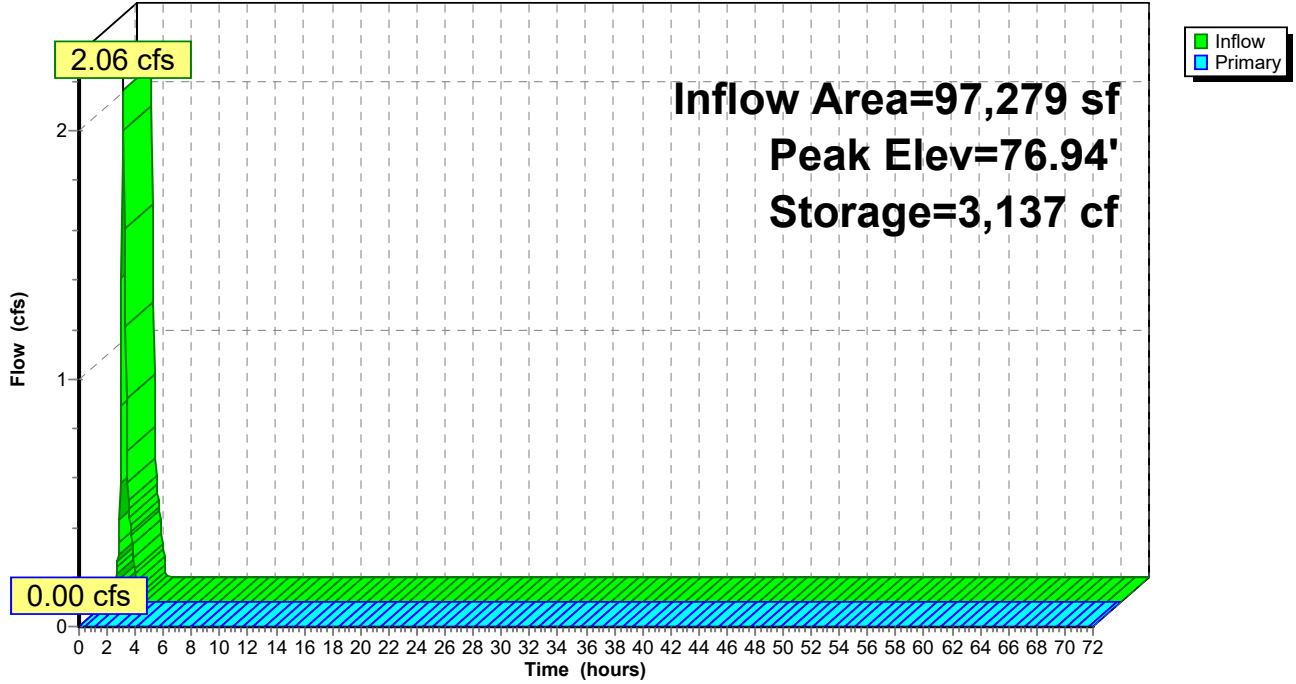
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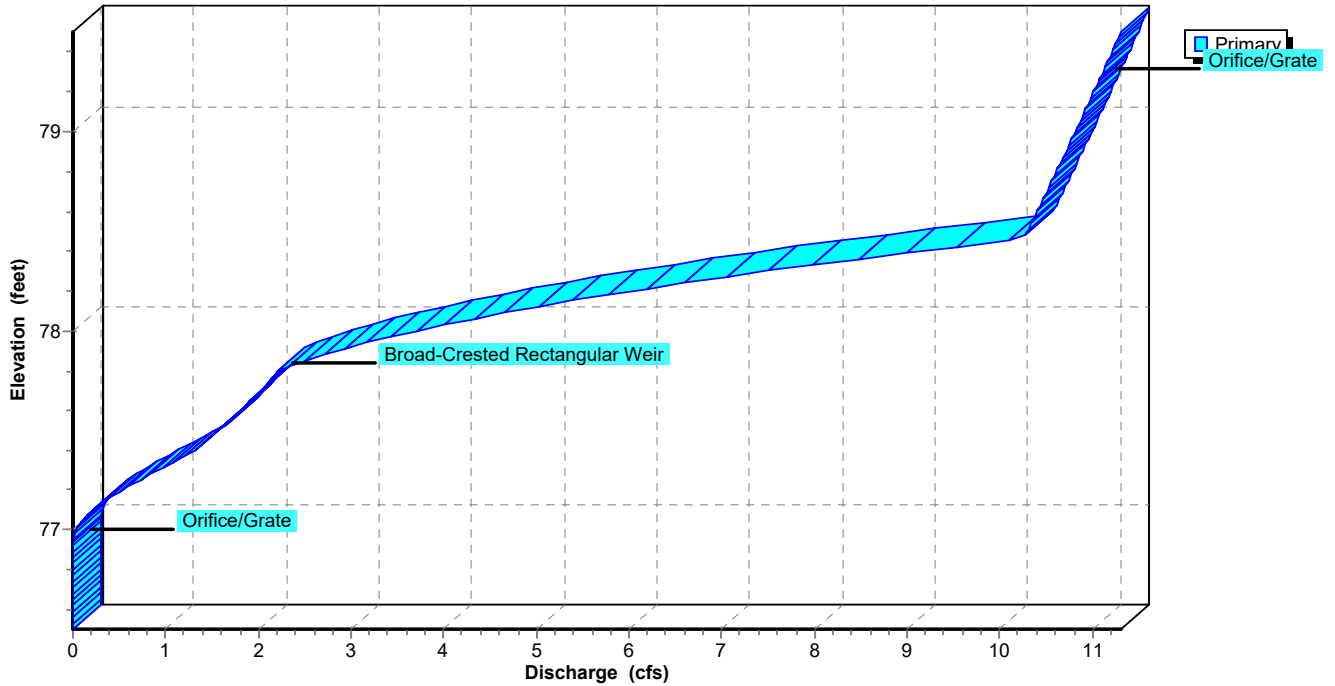
Pond B2: Bioretention Basin 2

Hydrograph



Pond B2: Bioretention Basin 2

Stage-Discharge



Pre vs Post

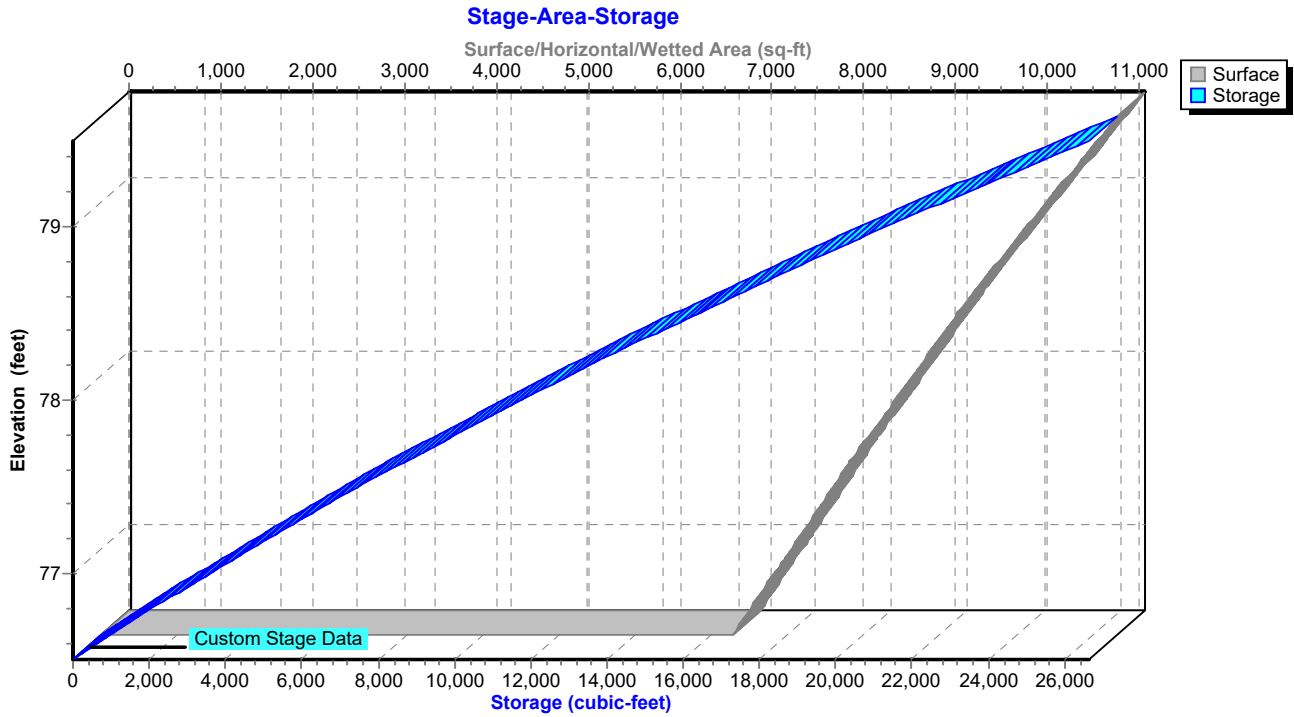
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Pond B2: Bioretention Basin 2



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

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Stage-Discharge for Pond B2: Bioretention Basin 2

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.56 | 1.73 | 78.62 | 10.43 |
| 76.52 | 0.00 | 77.58 | 1.77 | 78.64 | 10.45 |
| 76.54 | 0.00 | 77.60 | 1.82 | 78.66 | 10.47 |
| 76.56 | 0.00 | 77.62 | 1.86 | 78.68 | 10.49 |
| 76.58 | 0.00 | 77.64 | 1.90 | 78.70 | 10.51 |
| 76.60 | 0.00 | 77.66 | 1.94 | 78.72 | 10.53 |
| 76.62 | 0.00 | 77.68 | 1.99 | 78.74 | 10.55 |
| 76.64 | 0.00 | 77.70 | 2.03 | 78.76 | 10.57 |
| 76.66 | 0.00 | 77.72 | 2.06 | 78.78 | 10.59 |
| 76.68 | 0.00 | 77.74 | 2.10 | 78.80 | 10.61 |
| 76.70 | 0.00 | 77.76 | 2.14 | 78.82 | 10.63 |
| 76.72 | 0.00 | 77.78 | 2.18 | 78.84 | 10.65 |
| 76.74 | 0.00 | 77.80 | 2.25 | 78.86 | 10.67 |
| 76.76 | 0.00 | 77.82 | 2.34 | 78.88 | 10.69 |
| 76.78 | 0.00 | 77.84 | 2.45 | 78.90 | 10.71 |
| 76.80 | 0.00 | 77.86 | 2.58 | 78.92 | 10.73 |
| 76.82 | 0.00 | 77.88 | 2.71 | 78.94 | 10.75 |
| 76.84 | 0.00 | 77.90 | 2.86 | 78.96 | 10.77 |
| 76.86 | 0.00 | 77.92 | 3.01 | 78.98 | 10.79 |
| 76.88 | 0.00 | 77.94 | 3.17 | 79.00 | 10.82 |
| 76.90 | 0.00 | 77.96 | 3.34 | 79.02 | 10.84 |
| 76.92 | 0.00 | 77.98 | 3.52 | 79.04 | 10.86 |
| 76.94 | 0.00 | 78.00 | 3.71 | 79.06 | 10.88 |
| 76.96 | 0.00 | 78.02 | 3.91 | 79.08 | 10.90 |
| 76.98 | 0.02 | 78.04 | 4.12 | 79.10 | 10.92 |
| 77.00 | 0.03 | 78.06 | 4.33 | 79.12 | 10.94 |
| 77.02 | 0.06 | 78.08 | 4.56 | 79.14 | 10.96 |
| 77.04 | 0.09 | 78.10 | 4.79 | 79.16 | 10.97 |
| 77.06 | 0.13 | 78.12 | 5.02 | 79.18 | 10.99 |
| 77.08 | 0.17 | 78.14 | 5.27 | 79.20 | 11.01 |
| 77.10 | 0.22 | 78.16 | 5.52 | 79.22 | 11.03 |
| 77.12 | 0.28 | 78.18 | 5.78 | 79.24 | 11.05 |
| 77.14 | 0.34 | 78.20 | 6.05 | 79.26 | 11.07 |
| 77.16 | 0.40 | 78.22 | 6.32 | 79.28 | 11.09 |
| 77.18 | 0.47 | 78.24 | 6.61 | 79.30 | 11.11 |
| 77.20 | 0.54 | 78.26 | 6.90 | 79.32 | 11.13 |
| 77.22 | 0.61 | 78.28 | 7.20 | 79.34 | 11.15 |
| 77.24 | 0.69 | 78.30 | 7.51 | 79.36 | 11.17 |
| 77.26 | 0.77 | 78.32 | 7.83 | 79.38 | 11.19 |
| 77.28 | 0.85 | 78.34 | 8.15 | 79.40 | 11.21 |
| 77.30 | 0.93 | 78.36 | 8.48 | 79.42 | 11.23 |
| 77.32 | 1.01 | 78.38 | 8.82 | 79.44 | 11.25 |
| 77.34 | 1.09 | 78.40 | 9.18 | 79.46 | 11.27 |
| 77.36 | 1.17 | 78.42 | 9.54 | 79.48 | 11.29 |
| 77.38 | 1.24 | 78.44 | 9.92 | 79.50 | 11.31 |
| 77.40 | 1.31 | 78.46 | 10.26 | | |
| 77.42 | 1.37 | 78.48 | 10.28 | | |
| 77.44 | 1.42 | 78.50 | 10.30 | | |
| 77.46 | 1.47 | 78.52 | 10.32 | | |
| 77.48 | 1.53 | 78.54 | 10.34 | | |
| 77.50 | 1.58 | 78.56 | 10.36 | | |
| 77.52 | 1.63 | 78.58 | 10.38 | | |
| 77.54 | 1.68 | 78.60 | 10.40 | | |

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Stage-Area-Storage for Pond B2: Bioretention Basin 2

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 6,877 | 0 | 79.15 | 10,524 | 22,869 |
| 76.55 | 6,941 | 345 | 79.20 | 10,601 | 23,397 |
| 76.60 | 7,005 | 694 | 79.25 | 10,678 | 23,929 |
| 76.65 | 7,069 | 1,046 | 79.30 | 10,755 | 24,465 |
| 76.70 | 7,133 | 1,401 | 79.35 | 10,832 | 25,005 |
| 76.75 | 7,197 | 1,759 | 79.40 | 10,909 | 25,548 |
| 76.80 | 7,260 | 2,121 | 79.45 | 10,986 | 26,096 |
| 76.85 | 7,324 | 2,485 | 79.50 | 11,063 | 26,647 |
| 76.90 | 7,388 | 2,853 | | | |
| 76.95 | 7,452 | 3,224 | | | |
| 77.00 | 7,516 | 3,598 | | | |
| 77.05 | 7,580 | 3,976 | | | |
| 77.10 | 7,644 | 4,356 | | | |
| 77.15 | 7,708 | 4,740 | | | |
| 77.20 | 7,772 | 5,127 | | | |
| 77.25 | 7,836 | 5,517 | | | |
| 77.30 | 7,899 | 5,911 | | | |
| 77.35 | 7,963 | 6,307 | | | |
| 77.40 | 8,027 | 6,707 | | | |
| 77.45 | 8,091 | 7,110 | | | |
| 77.50 | 8,155 | 7,516 | | | |
| 77.55 | 8,223 | 7,925 | | | |
| 77.60 | 8,292 | 8,338 | | | |
| 77.65 | 8,360 | 8,755 | | | |
| 77.70 | 8,428 | 9,174 | | | |
| 77.75 | 8,497 | 9,597 | | | |
| 77.80 | 8,565 | 10,024 | | | |
| 77.85 | 8,633 | 10,454 | | | |
| 77.90 | 8,702 | 10,887 | | | |
| 77.95 | 8,770 | 11,324 | | | |
| 78.00 | 8,839 | 11,764 | | | |
| 78.05 | 8,907 | 12,208 | | | |
| 78.10 | 8,975 | 12,655 | | | |
| 78.15 | 9,044 | 13,106 | | | |
| 78.20 | 9,112 | 13,559 | | | |
| 78.25 | 9,180 | 14,017 | | | |
| 78.30 | 9,249 | 14,477 | | | |
| 78.35 | 9,317 | 14,942 | | | |
| 78.40 | 9,385 | 15,409 | | | |
| 78.45 | 9,454 | 15,880 | | | |
| 78.50 | 9,522 | 16,355 | | | |
| 78.55 | 9,599 | 16,833 | | | |
| 78.60 | 9,676 | 17,314 | | | |
| 78.65 | 9,753 | 17,800 | | | |
| 78.70 | 9,830 | 18,290 | | | |
| 78.75 | 9,907 | 18,783 | | | |
| 78.80 | 9,984 | 19,280 | | | |
| 78.85 | 10,061 | 19,782 | | | |
| 78.90 | 10,138 | 20,287 | | | |
| 78.95 | 10,215 | 20,795 | | | |
| 79.00 | 10,293 | 21,308 | | | |
| 79.05 | 10,370 | 21,825 | | | |
| 79.10 | 10,447 | 22,345 | | | |

Pre vs Post

NJ DEP 2-hr WQ Rainfall=1.25"

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Summary for Pond B3: Bioretention Basin 3

[92] Warning: Device #2 is above defined storage

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 0.48" for WQ event
 Inflow = 0.22 cfs @ 1.29 hrs, Volume= 466 cf
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 80.73' @ 3.25 hrs Surf.Area= 832 sf Storage= 466 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)
 Center-of-Mass det. time= (not calculated: no outflow)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 79.98' | 694 cf | Custom Stage Data (Conic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|------------------|-------------------|------------------------|------------------------|------------------|
| 79.98 | 432 | 0 | 0 | 432 |
| 80.98 | 995 | 694 | 694 | 1,003 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 77.48' | 15.0" Round CMP_Round 15" L= 96.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 77.48' / 77.00' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 1.23 sf |
| #2 | Secondary | 80.98' | 15.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 80.74' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=79.98' (Free Discharge)
 ↑1=CMP_Round 15" (Passes 0.00 cfs of 6.37 cfs potential flow)
 ↑3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=79.98' (Free Discharge)
 ↑2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pre vs Post

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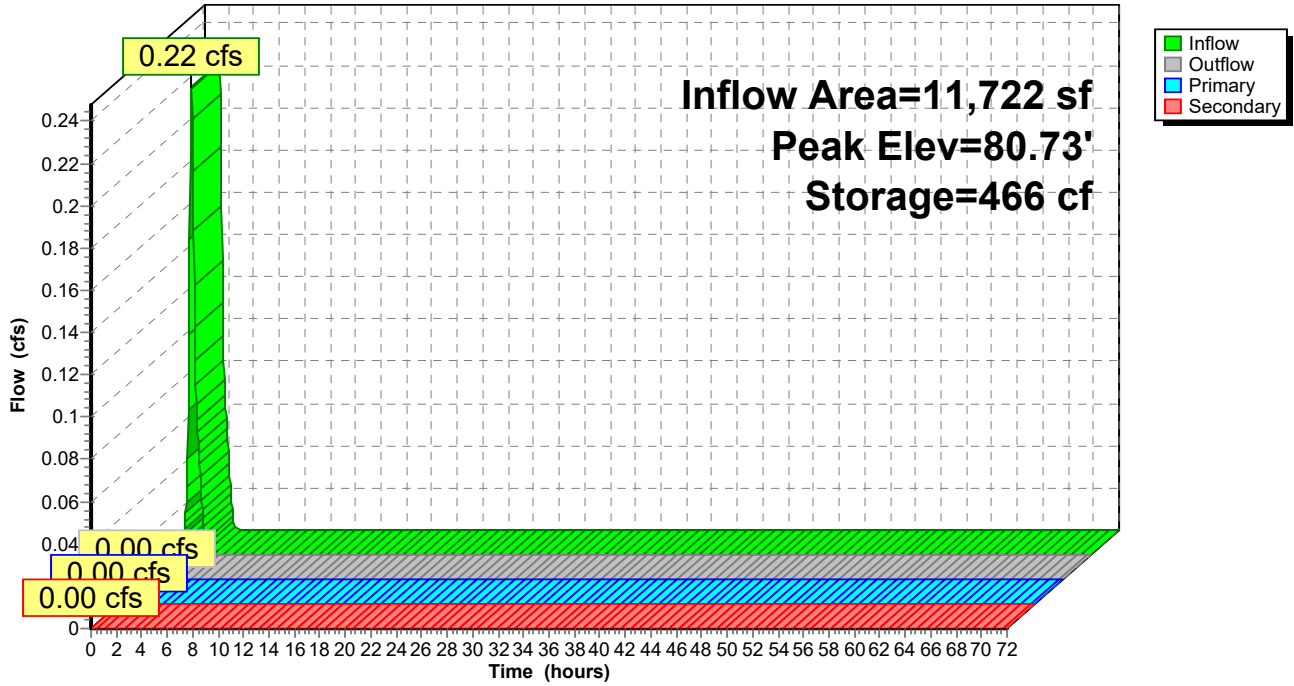
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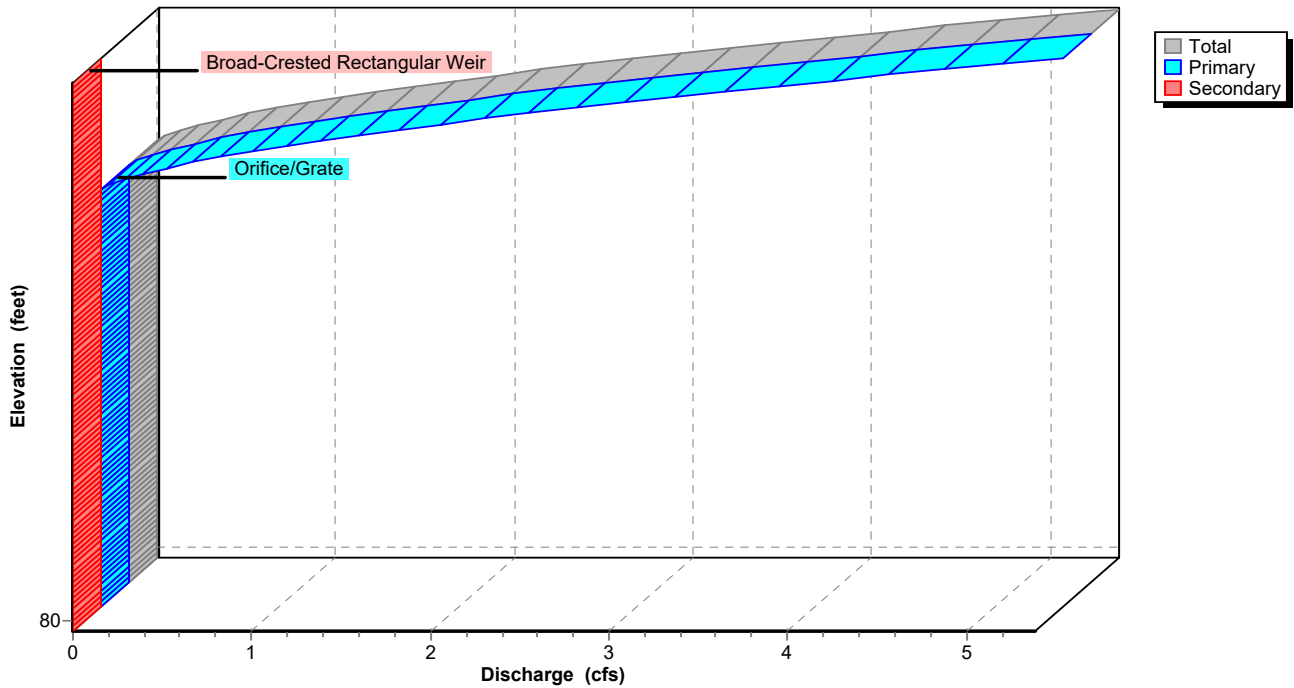
Pond B3: Bioretention Basin 3

Hydrograph



Pond B3: Bioretention Basin 3

Stage-Discharge



Pre vs Post

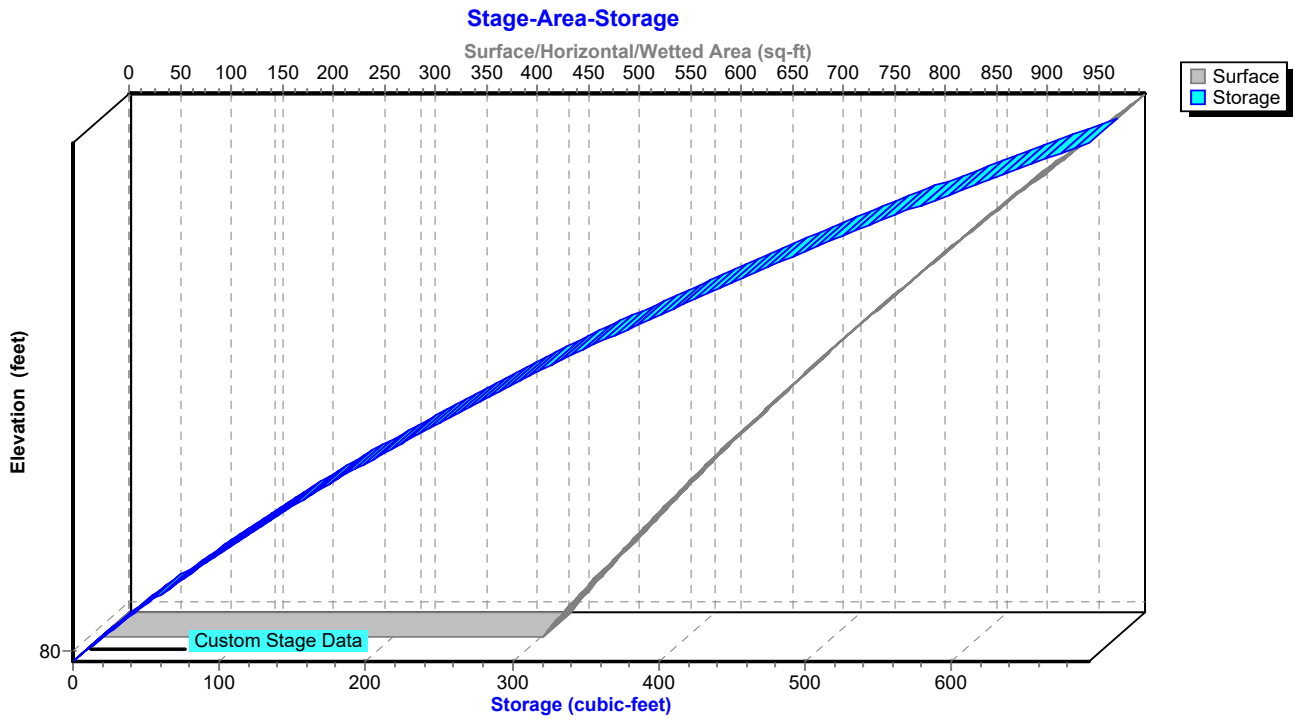
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Pond B3: Bioretention Basin 3



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Stage-Discharge for Pond B3: Bioretention Basin 3

| Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) | Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) |
|---------------------|--------------------|------------------|--------------------|---------------------|--------------------|------------------|--------------------|
| 79.98 | 0.00 | 0.00 | 0.00 | 80.51 | 0.00 | 0.00 | 0.00 |
| 79.99 | 0.00 | 0.00 | 0.00 | 80.52 | 0.00 | 0.00 | 0.00 |
| 80.00 | 0.00 | 0.00 | 0.00 | 80.53 | 0.00 | 0.00 | 0.00 |
| 80.01 | 0.00 | 0.00 | 0.00 | 80.54 | 0.00 | 0.00 | 0.00 |
| 80.02 | 0.00 | 0.00 | 0.00 | 80.55 | 0.00 | 0.00 | 0.00 |
| 80.03 | 0.00 | 0.00 | 0.00 | 80.56 | 0.00 | 0.00 | 0.00 |
| 80.04 | 0.00 | 0.00 | 0.00 | 80.57 | 0.00 | 0.00 | 0.00 |
| 80.05 | 0.00 | 0.00 | 0.00 | 80.58 | 0.00 | 0.00 | 0.00 |
| 80.06 | 0.00 | 0.00 | 0.00 | 80.59 | 0.00 | 0.00 | 0.00 |
| 80.07 | 0.00 | 0.00 | 0.00 | 80.60 | 0.00 | 0.00 | 0.00 |
| 80.08 | 0.00 | 0.00 | 0.00 | 80.61 | 0.00 | 0.00 | 0.00 |
| 80.09 | 0.00 | 0.00 | 0.00 | 80.62 | 0.00 | 0.00 | 0.00 |
| 80.10 | 0.00 | 0.00 | 0.00 | 80.63 | 0.00 | 0.00 | 0.00 |
| 80.11 | 0.00 | 0.00 | 0.00 | 80.64 | 0.00 | 0.00 | 0.00 |
| 80.12 | 0.00 | 0.00 | 0.00 | 80.65 | 0.00 | 0.00 | 0.00 |
| 80.13 | 0.00 | 0.00 | 0.00 | 80.66 | 0.00 | 0.00 | 0.00 |
| 80.14 | 0.00 | 0.00 | 0.00 | 80.67 | 0.00 | 0.00 | 0.00 |
| 80.15 | 0.00 | 0.00 | 0.00 | 80.68 | 0.00 | 0.00 | 0.00 |
| 80.16 | 0.00 | 0.00 | 0.00 | 80.69 | 0.00 | 0.00 | 0.00 |
| 80.17 | 0.00 | 0.00 | 0.00 | 80.70 | 0.00 | 0.00 | 0.00 |
| 80.18 | 0.00 | 0.00 | 0.00 | 80.71 | 0.00 | 0.00 | 0.00 |
| 80.19 | 0.00 | 0.00 | 0.00 | 80.72 | 0.00 | 0.00 | 0.00 |
| 80.20 | 0.00 | 0.00 | 0.00 | 80.73 | 0.00 | 0.00 | 0.00 |
| 80.21 | 0.00 | 0.00 | 0.00 | 80.74 | 0.00 | 0.00 | 0.00 |
| 80.22 | 0.00 | 0.00 | 0.00 | 80.75 | 0.05 | 0.05 | 0.00 |
| 80.23 | 0.00 | 0.00 | 0.00 | 80.76 | 0.13 | 0.13 | 0.00 |
| 80.24 | 0.00 | 0.00 | 0.00 | 80.77 | 0.24 | 0.24 | 0.00 |
| 80.25 | 0.00 | 0.00 | 0.00 | 80.78 | 0.37 | 0.37 | 0.00 |
| 80.26 | 0.00 | 0.00 | 0.00 | 80.79 | 0.51 | 0.51 | 0.00 |
| 80.27 | 0.00 | 0.00 | 0.00 | 80.80 | 0.67 | 0.67 | 0.00 |
| 80.28 | 0.00 | 0.00 | 0.00 | 80.81 | 0.85 | 0.85 | 0.00 |
| 80.29 | 0.00 | 0.00 | 0.00 | 80.82 | 1.04 | 1.04 | 0.00 |
| 80.30 | 0.00 | 0.00 | 0.00 | 80.83 | 1.24 | 1.24 | 0.00 |
| 80.31 | 0.00 | 0.00 | 0.00 | 80.84 | 1.45 | 1.45 | 0.00 |
| 80.32 | 0.00 | 0.00 | 0.00 | 80.85 | 1.67 | 1.67 | 0.00 |
| 80.33 | 0.00 | 0.00 | 0.00 | 80.86 | 1.90 | 1.90 | 0.00 |
| 80.34 | 0.00 | 0.00 | 0.00 | 80.87 | 2.15 | 2.15 | 0.00 |
| 80.35 | 0.00 | 0.00 | 0.00 | 80.88 | 2.40 | 2.40 | 0.00 |
| 80.36 | 0.00 | 0.00 | 0.00 | 80.89 | 2.66 | 2.66 | 0.00 |
| 80.37 | 0.00 | 0.00 | 0.00 | 80.90 | 2.93 | 2.93 | 0.00 |
| 80.38 | 0.00 | 0.00 | 0.00 | 80.91 | 3.21 | 3.21 | 0.00 |
| 80.39 | 0.00 | 0.00 | 0.00 | 80.92 | 3.50 | 3.50 | 0.00 |
| 80.40 | 0.00 | 0.00 | 0.00 | 80.93 | 3.79 | 3.79 | 0.00 |
| 80.41 | 0.00 | 0.00 | 0.00 | 80.94 | 4.09 | 4.09 | 0.00 |
| 80.42 | 0.00 | 0.00 | 0.00 | 80.95 | 4.41 | 4.41 | 0.00 |
| 80.43 | 0.00 | 0.00 | 0.00 | 80.96 | 4.72 | 4.72 | 0.00 |
| 80.44 | 0.00 | 0.00 | 0.00 | 80.97 | 5.05 | 5.05 | 0.00 |
| 80.45 | 0.00 | 0.00 | 0.00 | 80.98 | 5.38 | 5.38 | 0.00 |
| 80.46 | 0.00 | 0.00 | 0.00 | | | | |
| 80.47 | 0.00 | 0.00 | 0.00 | | | | |
| 80.48 | 0.00 | 0.00 | 0.00 | | | | |
| 80.49 | 0.00 | 0.00 | 0.00 | | | | |
| 80.50 | 0.00 | 0.00 | 0.00 | | | | |

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Stage-Area-Storage for Pond B3: Bioretention Basin 3

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 79.98 | 432 | 0 | 80.51 | 702 | 298 |
| 79.99 | 436 | 4 | 80.52 | 707 | 305 |
| 80.00 | 441 | 9 | 80.53 | 713 | 312 |
| 80.01 | 446 | 13 | 80.54 | 719 | 319 |
| 80.02 | 450 | 18 | 80.55 | 725 | 326 |
| 80.03 | 455 | 22 | 80.56 | 730 | 333 |
| 80.04 | 459 | 27 | 80.57 | 736 | 341 |
| 80.05 | 464 | 31 | 80.58 | 742 | 348 |
| 80.06 | 469 | 36 | 80.59 | 748 | 355 |
| 80.07 | 473 | 41 | 80.60 | 754 | 363 |
| 80.08 | 478 | 45 | 80.61 | 760 | 371 |
| 80.09 | 483 | 50 | 80.62 | 766 | 378 |
| 80.10 | 487 | 55 | 80.63 | 772 | 386 |
| 80.11 | 492 | 60 | 80.64 | 778 | 394 |
| 80.12 | 497 | 65 | 80.65 | 784 | 401 |
| 80.13 | 502 | 70 | 80.66 | 790 | 409 |
| 80.14 | 507 | 75 | 80.67 | 796 | 417 |
| 80.15 | 511 | 80 | 80.68 | 802 | 425 |
| 80.16 | 516 | 85 | 80.69 | 808 | 433 |
| 80.17 | 521 | 90 | 80.70 | 814 | 441 |
| 80.18 | 526 | 96 | 80.71 | 820 | 450 |
| 80.19 | 531 | 101 | 80.72 | 826 | 458 |
| 80.20 | 536 | 106 | 80.73 | 833 | 466 |
| 80.21 | 541 | 112 | 80.74 | 839 | 474 |
| 80.22 | 546 | 117 | 80.75 | 845 | 483 |
| 80.23 | 551 | 123 | 80.76 | 851 | 491 |
| 80.24 | 556 | 128 | 80.77 | 858 | 500 |
| 80.25 | 561 | 134 | 80.78 | 864 | 508 |
| 80.26 | 566 | 139 | 80.79 | 870 | 517 |
| 80.27 | 571 | 145 | 80.80 | 877 | 526 |
| 80.28 | 577 | 151 | 80.81 | 883 | 535 |
| 80.29 | 582 | 157 | 80.82 | 889 | 544 |
| 80.30 | 587 | 162 | 80.83 | 896 | 552 |
| 80.31 | 592 | 168 | 80.84 | 902 | 561 |
| 80.32 | 597 | 174 | 80.85 | 909 | 571 |
| 80.33 | 603 | 180 | 80.86 | 915 | 580 |
| 80.34 | 608 | 186 | 80.87 | 922 | 589 |
| 80.35 | 613 | 192 | 80.88 | 928 | 598 |
| 80.36 | 619 | 199 | 80.89 | 935 | 607 |
| 80.37 | 624 | 205 | 80.90 | 941 | 617 |
| 80.38 | 629 | 211 | 80.91 | 948 | 626 |
| 80.39 | 635 | 217 | 80.92 | 955 | 636 |
| 80.40 | 640 | 224 | 80.93 | 961 | 645 |
| 80.41 | 646 | 230 | 80.94 | 968 | 655 |
| 80.42 | 651 | 237 | 80.95 | 975 | 665 |
| 80.43 | 657 | 243 | 80.96 | 981 | 674 |
| 80.44 | 662 | 250 | 80.97 | 988 | 684 |
| 80.45 | 668 | 256 | 80.98 | 995 | 694 |
| 80.46 | 673 | 263 | | | |
| 80.47 | 679 | 270 | | | |
| 80.48 | 685 | 277 | | | |
| 80.49 | 690 | 284 | | | |
| 80.50 | 696 | 291 | | | |

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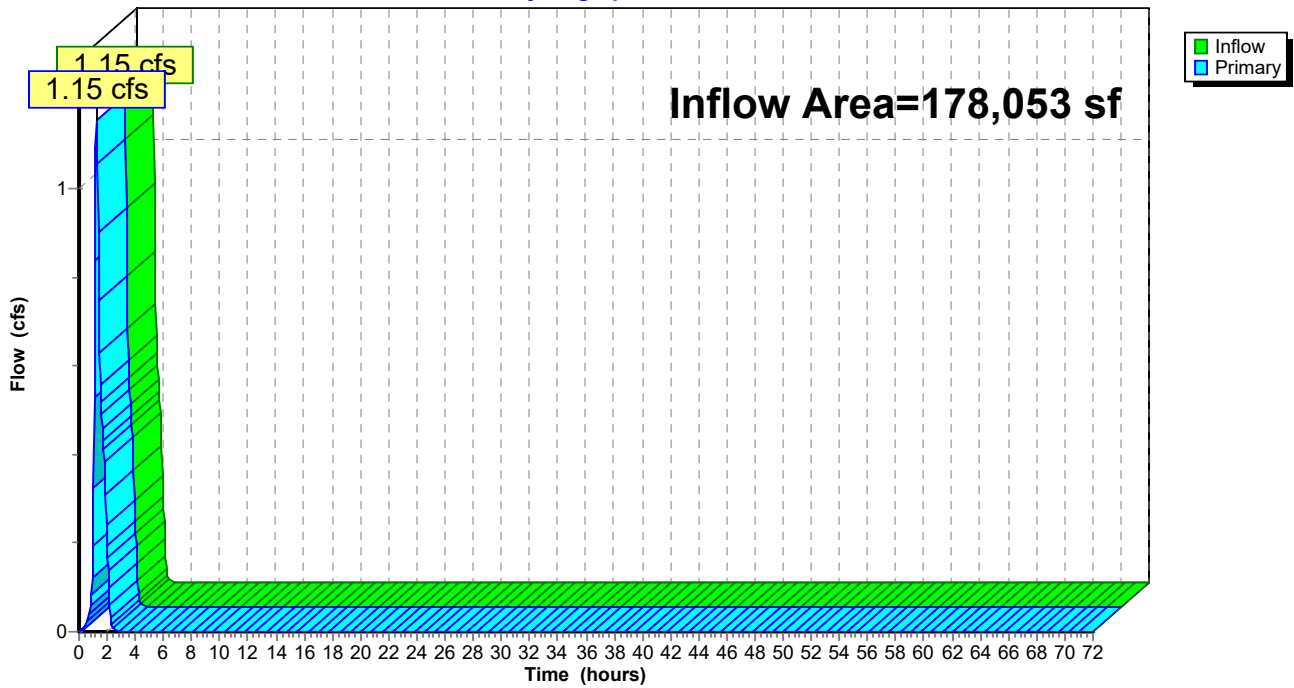
Summary for Link 5E: EDA 1

Inflow Area = 178,053 sf, 5.81% Impervious, Inflow Depth = 0.16" for WQ event
Inflow = 1.15 cfs @ 1.24 hrs, Volume= 2,308 cf
Primary = 1.15 cfs @ 1.24 hrs, Volume= 2,308 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5E: EDA 1

Hydrograph



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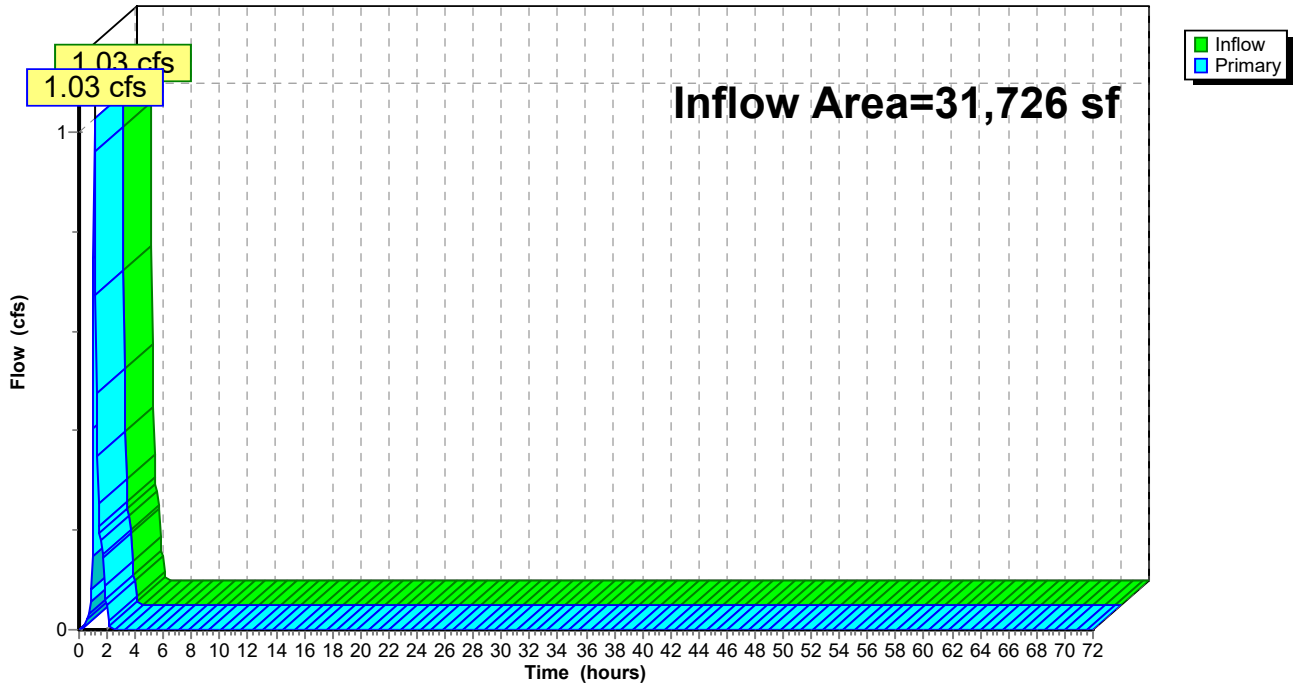
Summary for Link 6E: EDA 2

Inflow Area = 31,726 sf, 17.78% Impervious, Inflow Depth = 0.49" for WQ event
Inflow = 1.03 cfs @ 1.12 hrs, Volume= 1,291 cf
Primary = 1.03 cfs @ 1.12 hrs, Volume= 1,291 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 6E: EDA 2

Hydrograph



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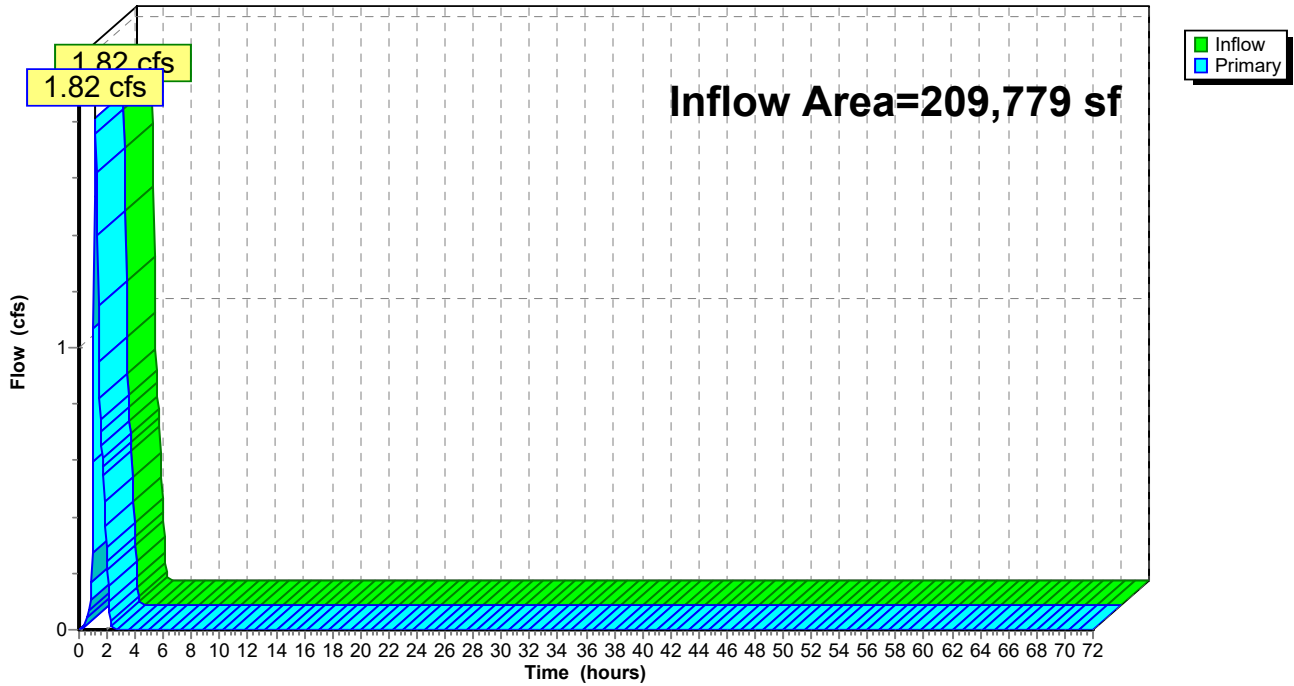
Summary for Link 7E: EDA

Inflow Area = 209,779 sf, 7.62% Impervious, Inflow Depth = 0.21" for WQ event
Inflow = 1.82 cfs @ 1.17 hrs, Volume= 3,598 cf
Primary = 1.82 cfs @ 1.17 hrs, Volume= 3,598 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 7E: EDA

Hydrograph



Pre vs Post

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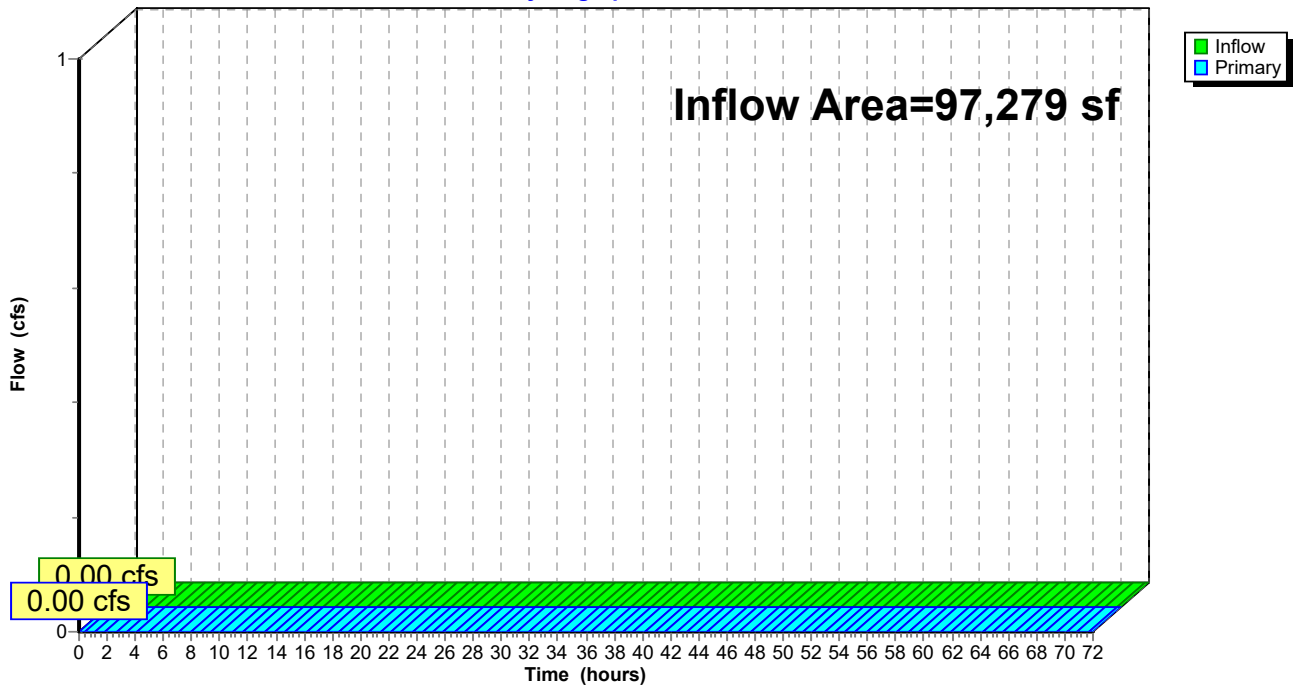
Summary for Link 10P: PDA 1A

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 0.00" for WQ event
Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 10P: PDA 1A

Hydrograph



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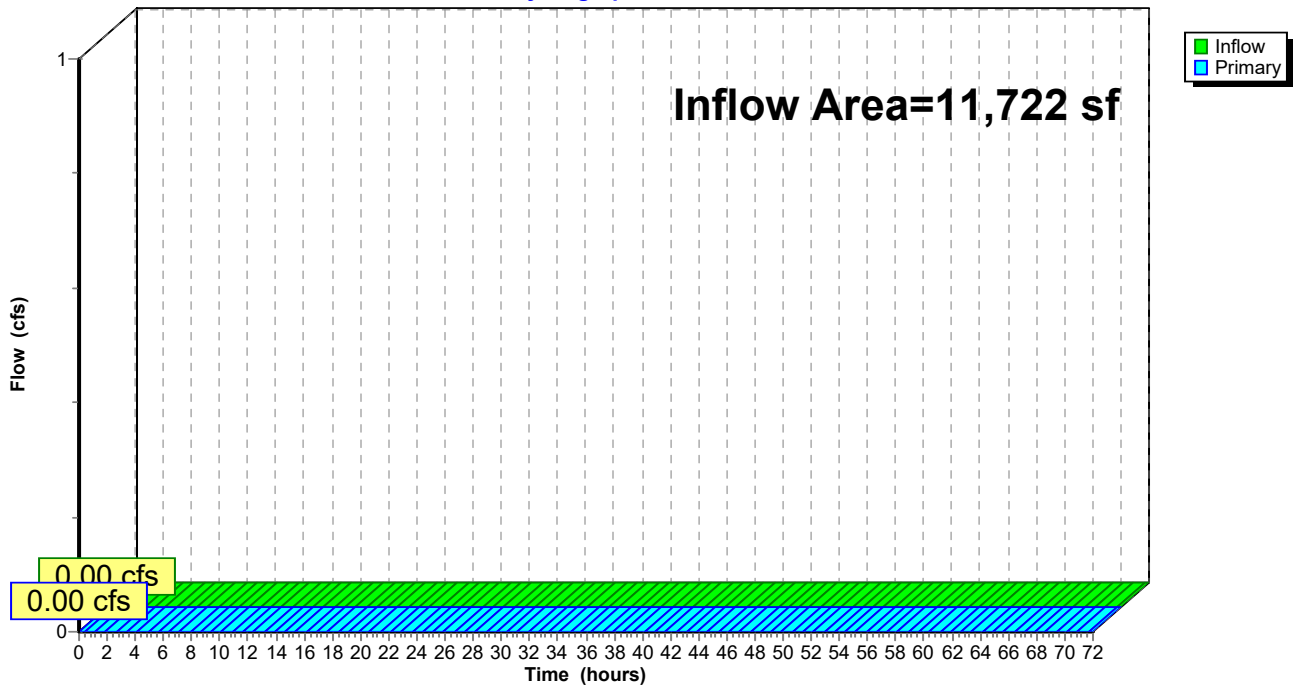
Summary for Link 11P: PDA 1B

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 0.00" for WQ event
Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0 cf
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 11P: PDA 1B

Hydrograph



Pre vs Post

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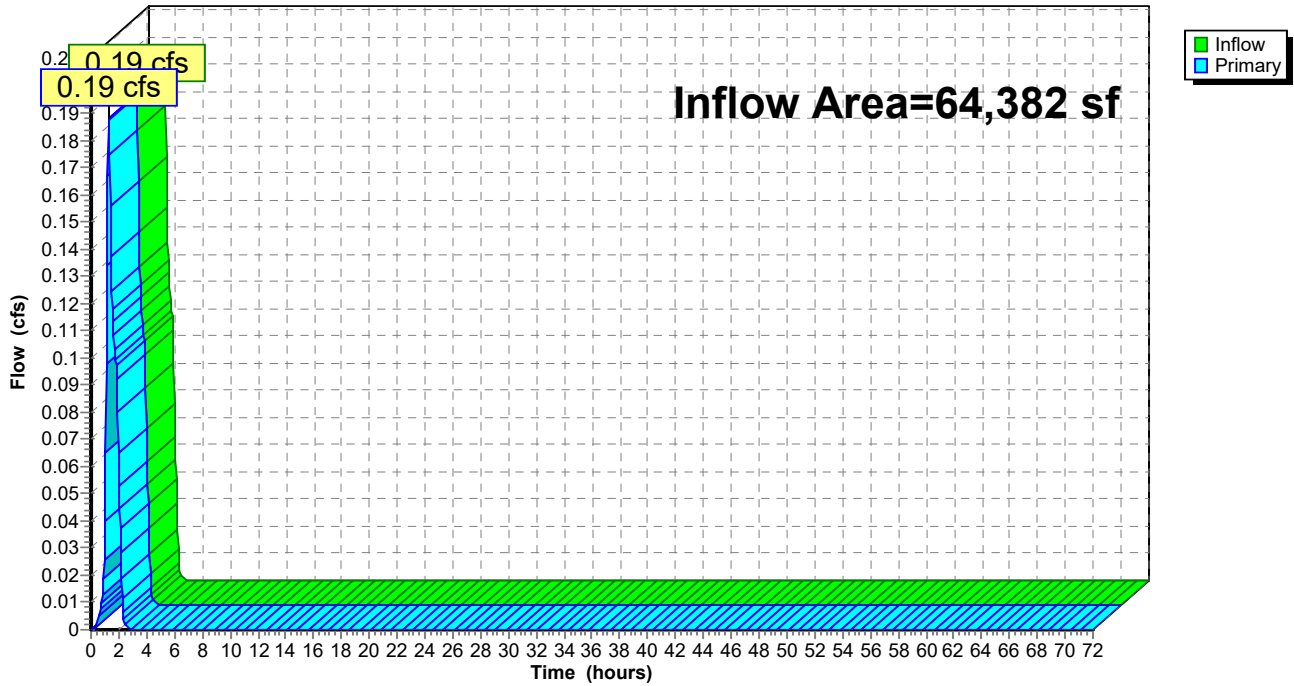
Summary for Link 12P: PDA 1C

Inflow Area = 64,382 sf, 3.87% Impervious, Inflow Depth = 0.09" for WQ event
Inflow = 0.19 cfs @ 1.28 hrs, Volume= 479 cf
Primary = 0.19 cfs @ 1.28 hrs, Volume= 479 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 12P: PDA 1C

Hydrograph



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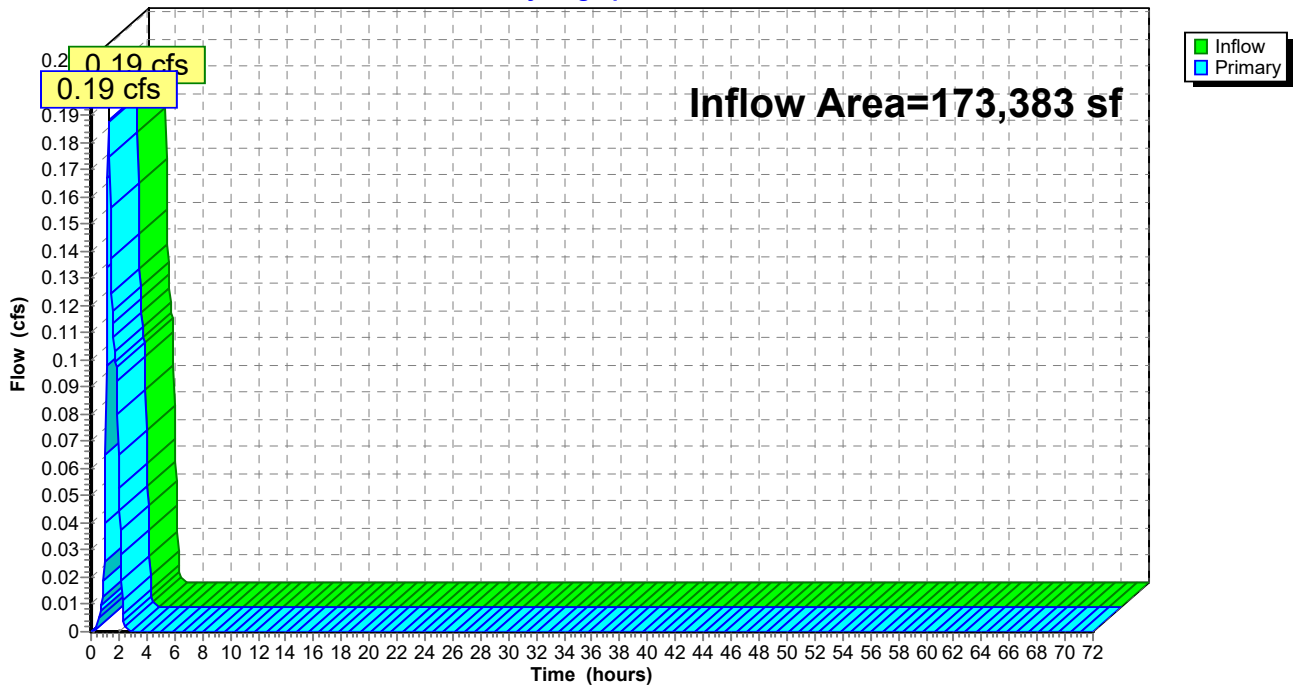
Summary for Link 13P: PDA 1

Inflow Area = 173,383 sf, 38.29% Impervious, Inflow Depth = 0.03" for WQ event
Inflow = 0.19 cfs @ 1.28 hrs, Volume= 479 cf
Primary = 0.19 cfs @ 1.28 hrs, Volume= 479 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 13P: PDA 1

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

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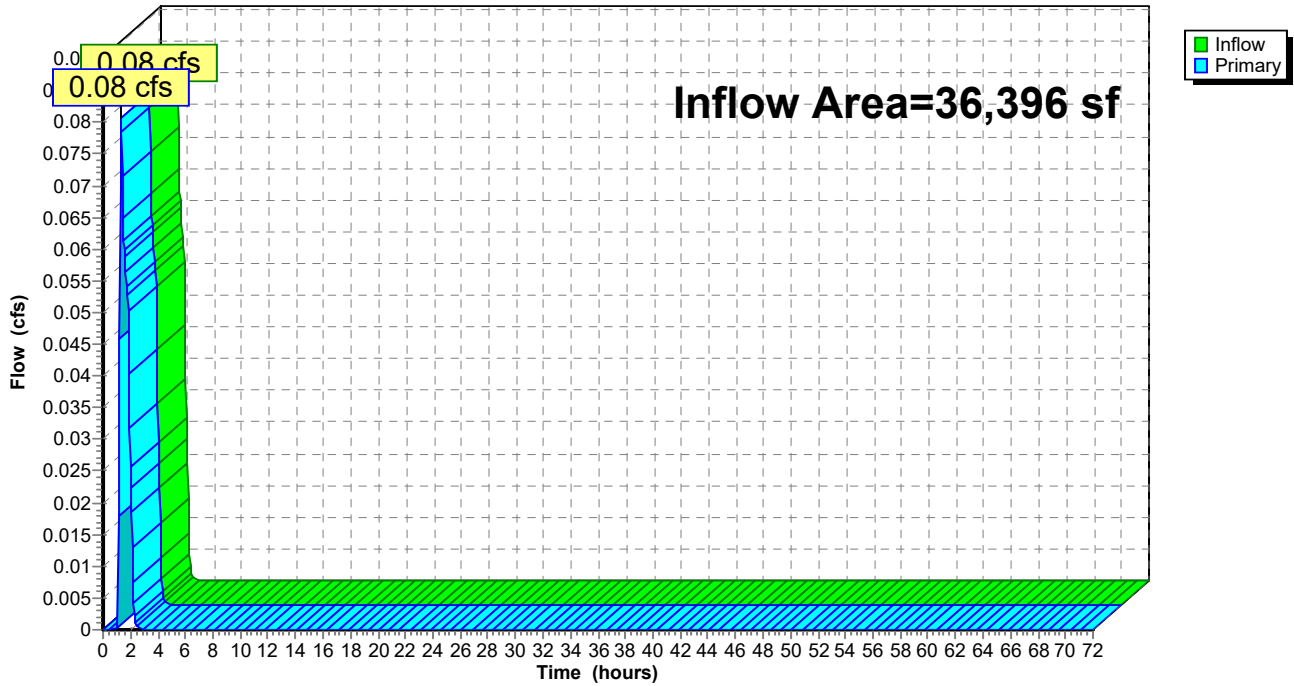
Summary for Link 14P: PDA 2

Inflow Area = 36,396 sf, 0.00% Impervious, Inflow Depth = 0.06" for WQ event
Inflow = 0.08 cfs @ 1.32 hrs, Volume= 188 cf
Primary = 0.08 cfs @ 1.32 hrs, Volume= 188 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 14P: PDA 2

Hydrograph



Pre vs Post

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NJ DEP 2-hr WQ Rainfall=1.25"

Printed 5/14/2021

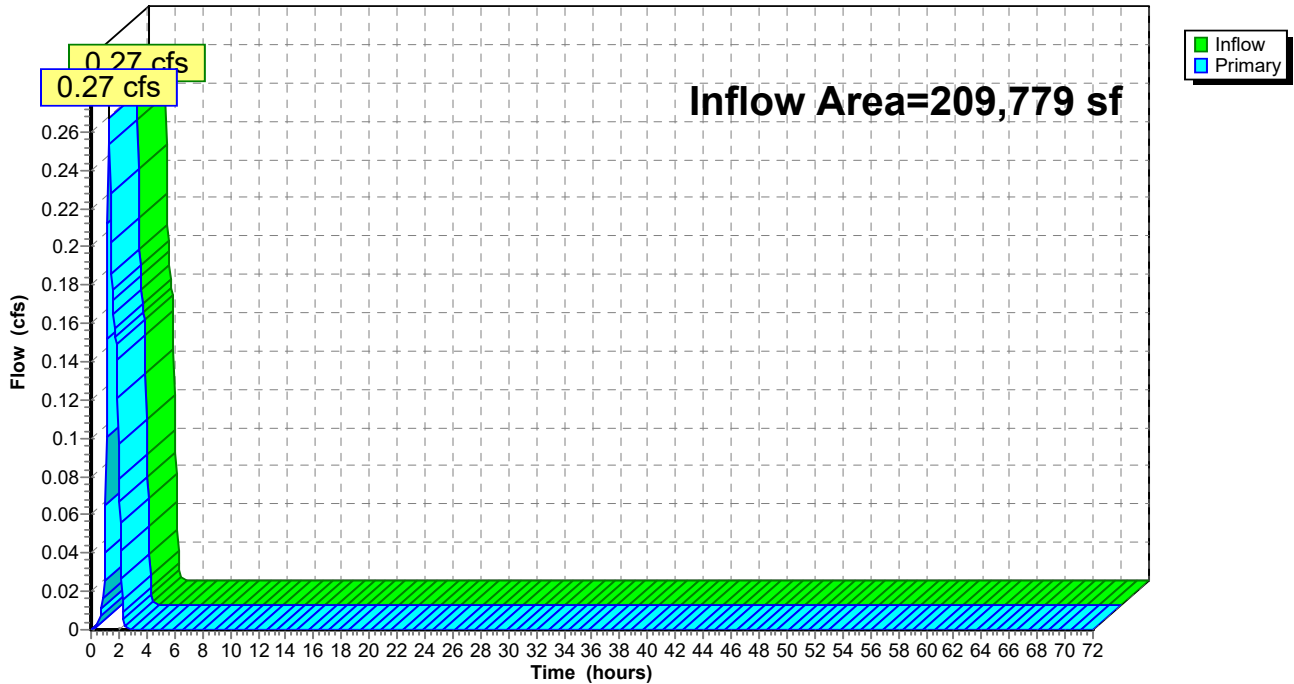
Summary for Link 15P: PDA

Inflow Area = 209,779 sf, 31.65% Impervious, Inflow Depth = 0.04" for WQ event
Inflow = 0.27 cfs @ 1.30 hrs, Volume= 666 cf
Primary = 0.27 cfs @ 1.30 hrs, Volume= 666 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 15P: PDA

Hydrograph



Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

| | |
|--------------------------------------|---|
| Subcatchment 1E: Impervious | Runoff Area=10,351 sf 100.00% Impervious Runoff Depth=3.13" Tc=12.4 min CN=0/98 Runoff=0.68 cfs 2,697 cf |
| Subcatchment 1P: Impervious | Runoff Area=23,576 sf 100.00% Impervious Runoff Depth=3.13" Tc=10.7 min CN=0/98 Runoff=1.61 cfs 6,143 cf |
| Subcatchment 2E: Pervious | Runoff Area=167,702 sf 0.00% Impervious Runoff Depth=1.26" Flow Length=630' Tc=12.4 min CN=76/0 Runoff=4.94 cfs 17,674 cf |
| Subcatchment 2P: Pervious | Runoff Area=24,672 sf 0.00% Impervious Runoff Depth=1.14" Flow Length=426' Tc=10.7 min CN=74/0 Runoff=0.68 cfs 2,353 cf |
| Subcatchment 3E: Impervious | Runoff Area=5,641 sf 100.00% Impervious Runoff Depth=3.13" Tc=6.0 min CN=0/98 Runoff=0.45 cfs 1,470 cf |
| Subcatchment 3P: Roof Area | Runoff Area=35,418 sf 100.00% Impervious Runoff Depth=3.13" Tc=10.7 min CN=0/98 Runoff=2.42 cfs 9,229 cf |
| Subcatchment 4E: Pervious | Runoff Area=26,085 sf 0.00% Impervious Runoff Depth=2.06" Flow Length=393' Tc=6.0 min CN=87/0 Runoff=1.55 cfs 4,471 cf |
| Subcatchment 4P: Pervious | Runoff Area=13,613 sf 0.00% Impervious Runoff Depth=1.14" Tc=10.7 min CN=74/0 Runoff=0.38 cfs 1,298 cf |
| Subcatchment 5P: Impervious | Runoff Area=5,021 sf 97.63% Impervious Runoff Depth=3.12" Tc=20.8 min CN=96/98 Runoff=0.27 cfs 1,306 cf |
| Subcatchment 6P: Pervious | Runoff Area=6,701 sf 0.00% Impervious Runoff Depth=1.09" Flow Length=172' Tc=20.8 min CN=73/0 Runoff=0.13 cfs 607 cf |
| Subcatchment 7P: Impervious | Runoff Area=2,493 sf 100.00% Impervious Runoff Depth=3.13" Tc=13.9 min CN=0/98 Runoff=0.16 cfs 650 cf |
| Subcatchment 8P: Pervious | Runoff Area=61,889 sf 0.00% Impervious Runoff Depth=1.03" Flow Length=409' Tc=13.9 min CN=72/0 Runoff=1.36 cfs 5,314 cf |
| Subcatchment 9P: Pervious | Runoff Area=36,396 sf 0.00% Impervious Runoff Depth=1.09" Flow Length=471' Tc=12.2 min CN=73/0 Runoff=0.91 cfs 3,296 cf |
| Pond B1: Bioretention Basin 1 | Peak Elev=78.24' Storage=4,156 cf Inflow=2.29 cfs 8,496 cf Outflow=1.24 cfs 4,601 cf |
| Pond B2: Bioretention Basin 2 | Peak Elev=77.37' Storage=6,451 cf Inflow=2.75 cfs 15,128 cf Outflow=1.20 cfs 11,962 cf |
| Pond B3: Bioretention Basin 3 | Peak Elev=80.78' Storage=510 cf Inflow=0.40 cfs 1,913 cf Primary=0.40 cfs 1,439 cf Secondary=0.00 cfs 0 cf Outflow=0.40 cfs 1,439 cf |

Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Link 5E: EDA 1

Inflow=5.61 cfs 20,371 cf
Primary=5.61 cfs 20,371 cf

Link 6E: EDA 2

Inflow=2.00 cfs 5,941 cf
Primary=2.00 cfs 5,941 cf

Link 7E: EDA

Inflow=6.99 cfs 26,313 cf
Primary=6.99 cfs 26,313 cf

Link 10P: PDA 1A

Inflow=1.20 cfs 11,962 cf
Primary=1.20 cfs 11,962 cf

Link 11P: PDA 1B

Inflow=0.40 cfs 1,439 cf
Primary=0.40 cfs 1,439 cf

Link 12P: PDA 1C

Inflow=1.52 cfs 5,964 cf
Primary=1.52 cfs 5,964 cf

Link 13P: PDA 1

Inflow=2.43 cfs 19,365 cf
Primary=2.43 cfs 19,365 cf

Link 14P: PDA 2

Inflow=0.91 cfs 3,296 cf
Primary=0.91 cfs 3,296 cf

Link 15P: PDA

Inflow=3.25 cfs 22,660 cf
Primary=3.25 cfs 22,660 cf

Total Runoff Area = 419,558 sf Runoff Volume = 56,508 cf Average Runoff Depth = 1.62"
80.36% Pervious = 337,177 sf 19.64% Impervious = 82,381 sf

Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Summary for Subcatchment 1E: Impervious

Runoff = 0.68 cfs @ 12.20 hrs, Volume= 2,697 cf, Depth= 3.13"

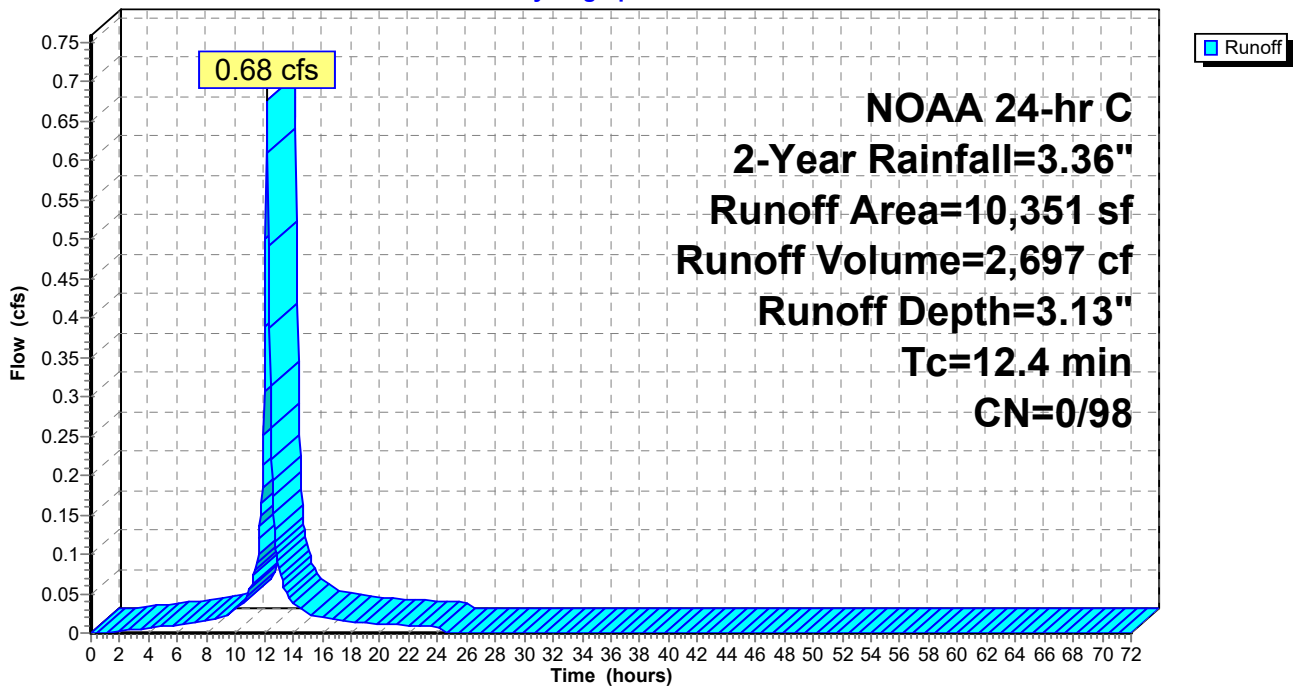
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 3,299 | 98 | Unconnected roofs, HSG C |
| 7,052 | 98 | Paved parking, HSG C |
| 10,351 | 98 | Weighted Average |
| 10,351 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 12.4 | | | | | Direct Entry, Tc |

Subcatchment 1E: Impervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Summary for Subcatchment 1P: Impervious

Runoff = 1.61 cfs @ 12.18 hrs, Volume= 6,143 cf, Depth= 3.13"

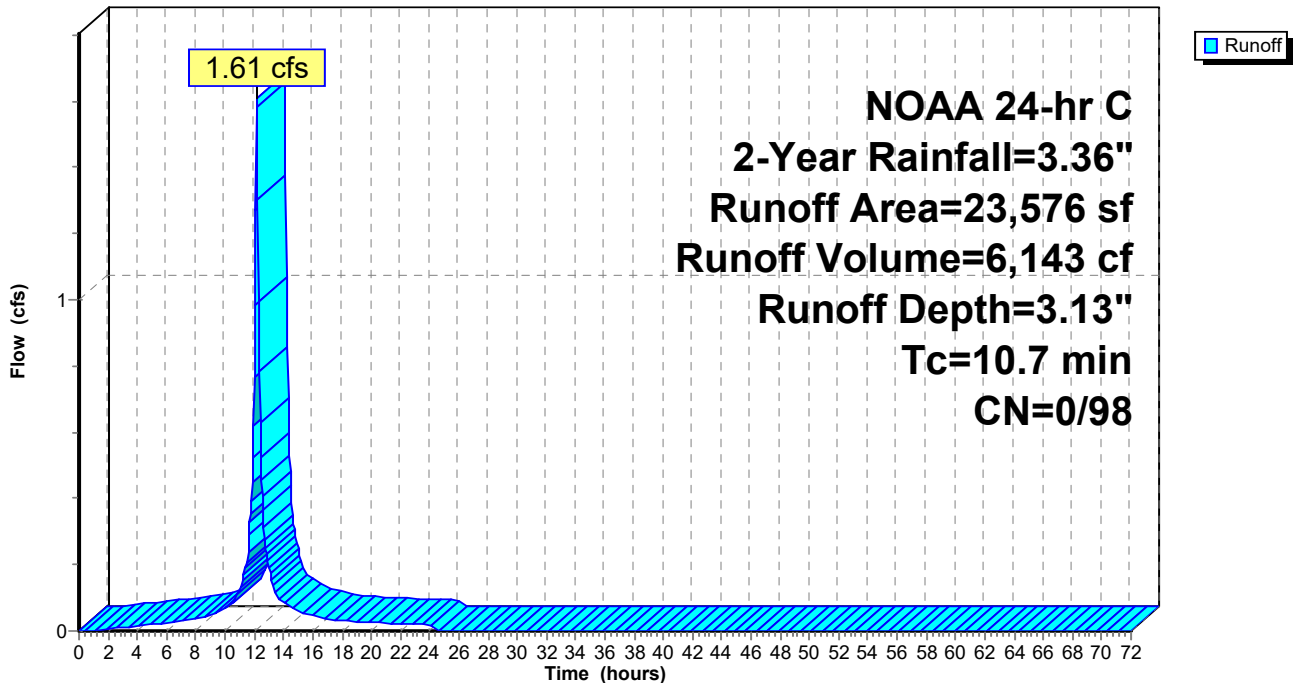
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 23,576 | 98 | Paved parking, HSG C |
| 23,576 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 1P: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Subcatchment 2E: Pervious

Runoff = 4.94 cfs @ 12.21 hrs, Volume= 17,674 cf, Depth= 1.26"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 24,589 | 96 | Gravel surface, HSG C |
| 36,591 | 70 | Woods, Good, HSG C |
| 105,816 | 74 | >75% Grass cover, Good, HSG C |
| 706 | 72 | Woods/grass comb., Good, HSG C |
| 167,702 | 76 | Weighted Average |
| 167,702 | 76 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 0.3 | 27 | 0.0490 | 1.55 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 8.8 | 73 | 0.0130 | 0.14 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.4 | 54 | 0.0180 | 2.16 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 1.2 | 207 | 0.0340 | 2.97 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.5 | 59 | 0.0170 | 2.10 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 0.2 | 43 | 0.0470 | 3.49 | | Shallow Concentrated Flow, F-G Unpaved Kv= 16.1 fps |
| 1.0 | 167 | 0.0280 | 2.69 | | Shallow Concentrated Flow, G-H Unpaved Kv= 16.1 fps |
| 12.4 | 630 | Total | | | |

Pre vs Post

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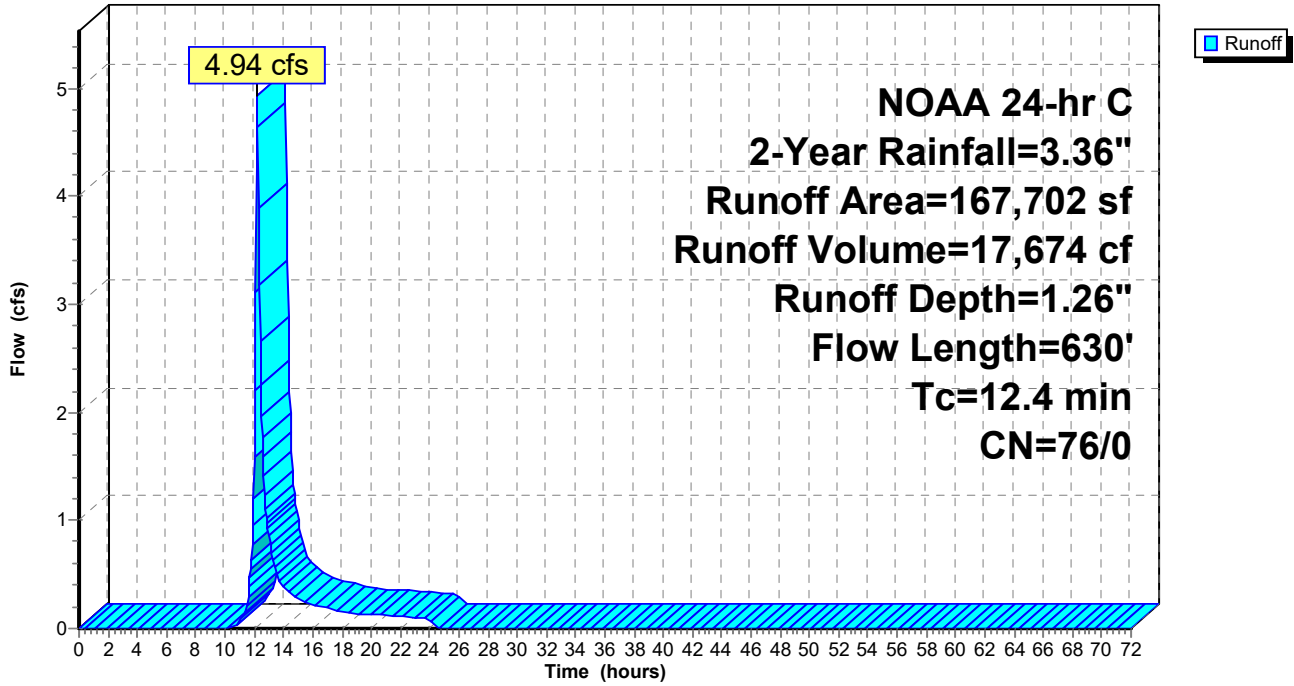
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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Subcatchment 2E: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Subcatchment 2P: Pervious

Runoff = 0.68 cfs @ 12.19 hrs, Volume= 2,353 cf, Depth= 1.14"

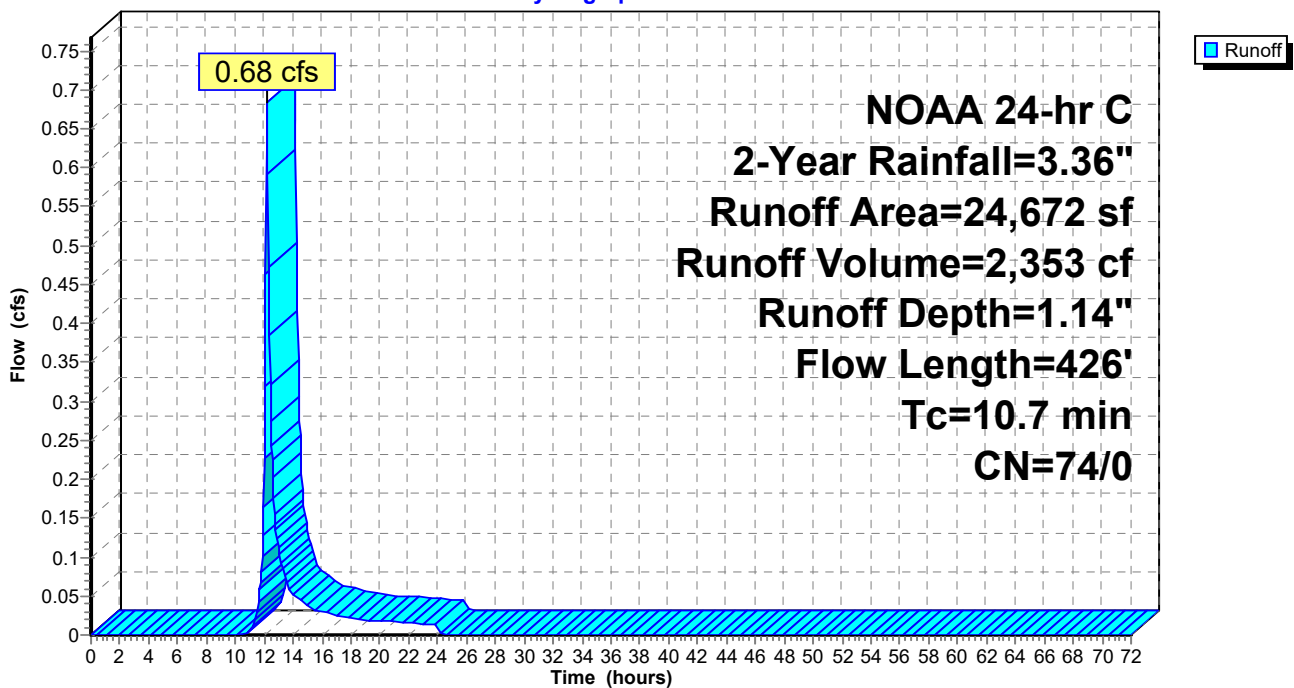
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 22,852 | 74 | >75% Grass cover, Good, HSG C |
| 1,820 | 72 | Woods/grass comb., Good, HSG C |
| 24,672 | 74 | Weighted Average |
| 24,672 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 9.2 | 100 | 0.0222 | 0.18 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.1 | 23 | 0.0730 | 4.35 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.3 | 48 | 0.0210 | 2.94 | | Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps |
| 1.1 | 255 | 0.0050 | 3.72 | 4.57 | Pipe Channel, D-E 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013 Concrete pipe, bends & connections |
| 10.7 | 426 | Total | | | |

Subcatchment 2P: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Subcatchment 3E: Impervious

Runoff = 0.45 cfs @ 12.13 hrs, Volume= 1,470 cf, Depth= 3.13"

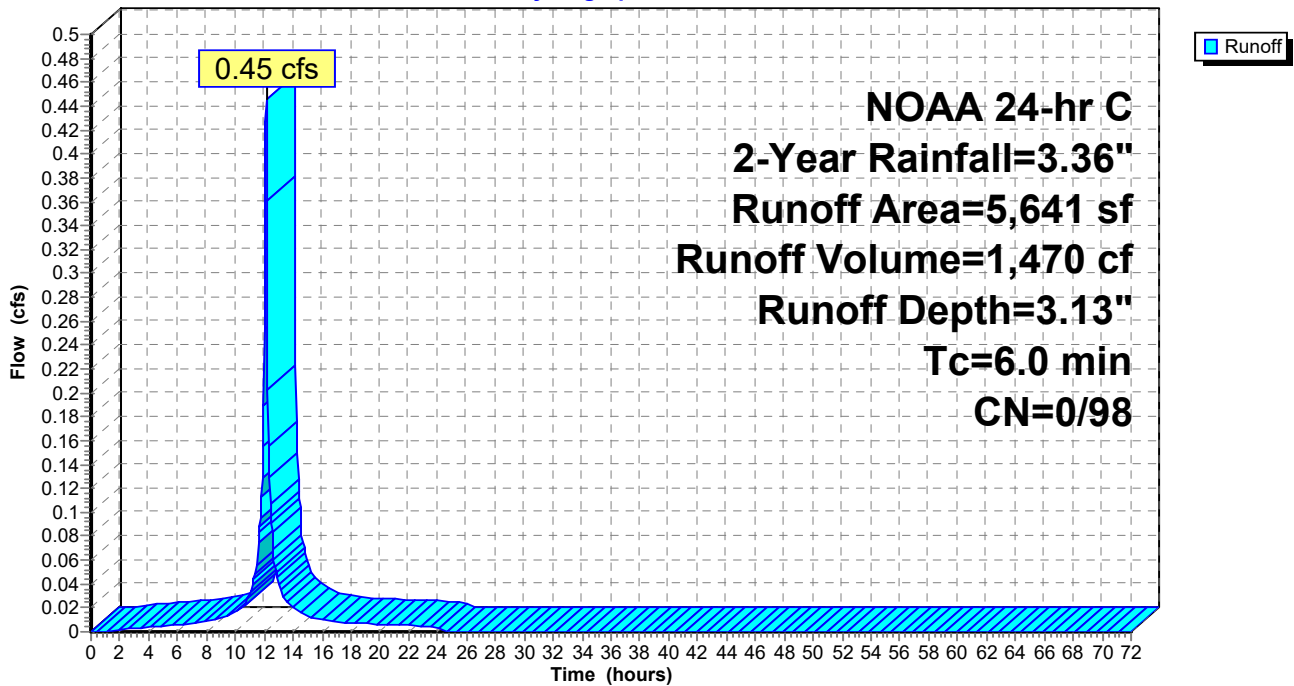
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 2,580 | 98 | Unconnected roofs, HSG C |
| 3,061 | 98 | Paved parking, HSG C |
| 5,641 | 98 | Weighted Average |
| 5,641 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|-------------------------|
| 3.0 | | | | | Direct Entry, Tc |
| 3.0 | 0 | Total, Increased to minimum Tc = 6.0 min | | | |

Subcatchment 3E: Impervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Summary for Subcatchment 3P: Roof Area

Runoff = 2.42 cfs @ 12.18 hrs, Volume= 9,229 cf, Depth= 3.13"

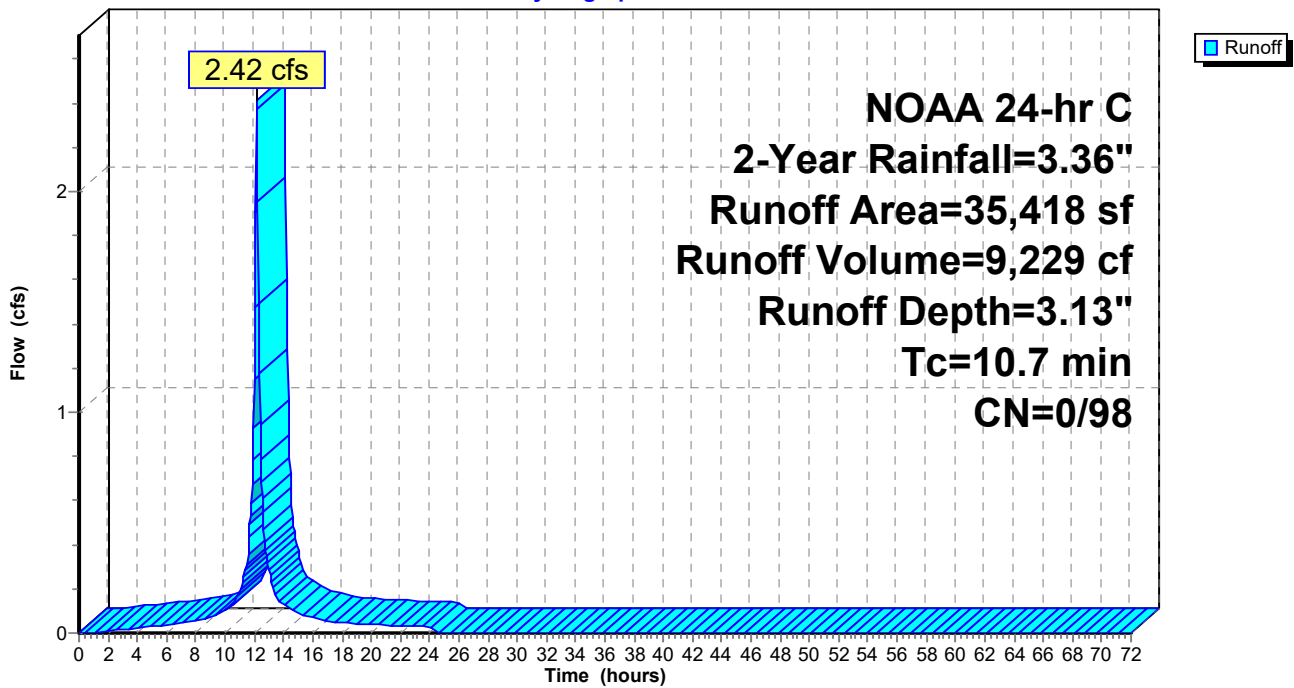
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|-----------------------------|
| 35,068 | 98 | Unconnected roofs, HSG C |
| 350 | 98 | Unconnected pavement, HSG C |
| 35,418 | 98 | Weighted Average |
| 35,418 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 3P: Roof Area

Hydrograph



Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Subcatchment 4E: Pervious

Runoff = 1.55 cfs @ 12.13 hrs, Volume= 4,471 cf, Depth= 2.06"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 164 | 70 | Woods, Good, HSG C |
| 16,189 | 96 | Gravel surface, HSG C |
| 5,108 | 74 | >75% Grass cover, Good, HSG C |
| 4,624 | 72 | Woods/grass comb., Good, HSG C |
| 26,085 | 87 | Weighted Average |
| 26,085 | 87 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|---|
| 1.3 | 100 | 0.0160 | 1.29 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 0.6 | 97 | 0.0200 | 2.87 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 1.0 | 175 | 0.0330 | 2.92 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.1 | 13 | 0.0230 | 2.44 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.0 | 8 | 0.0480 | 3.53 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 3.0 | 393 | Total, Increased to minimum Tc = 6.0 min | | | |

Pre vs Post

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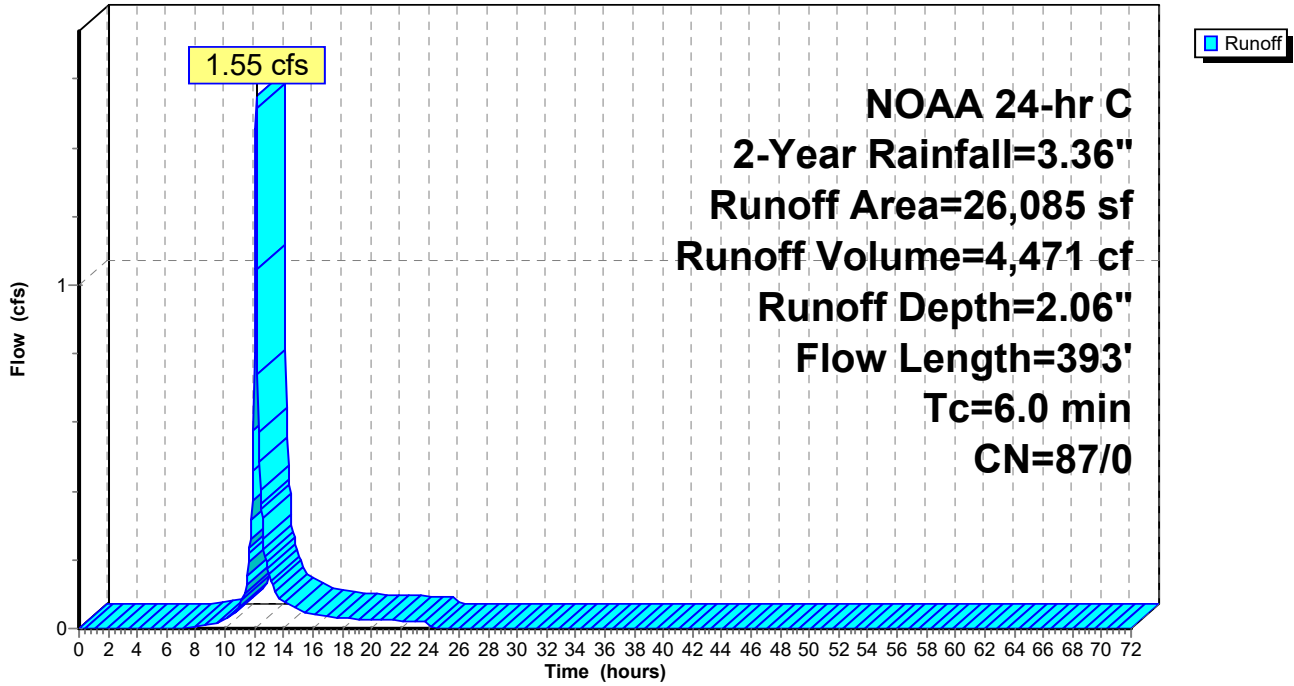
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NOAA 24-hr C 2-Year Rainfall=3.36"

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Subcatchment 4E: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Summary for Subcatchment 4P: Pervious

Runoff = 0.38 cfs @ 12.19 hrs, Volume= 1,298 cf, Depth= 1.14"

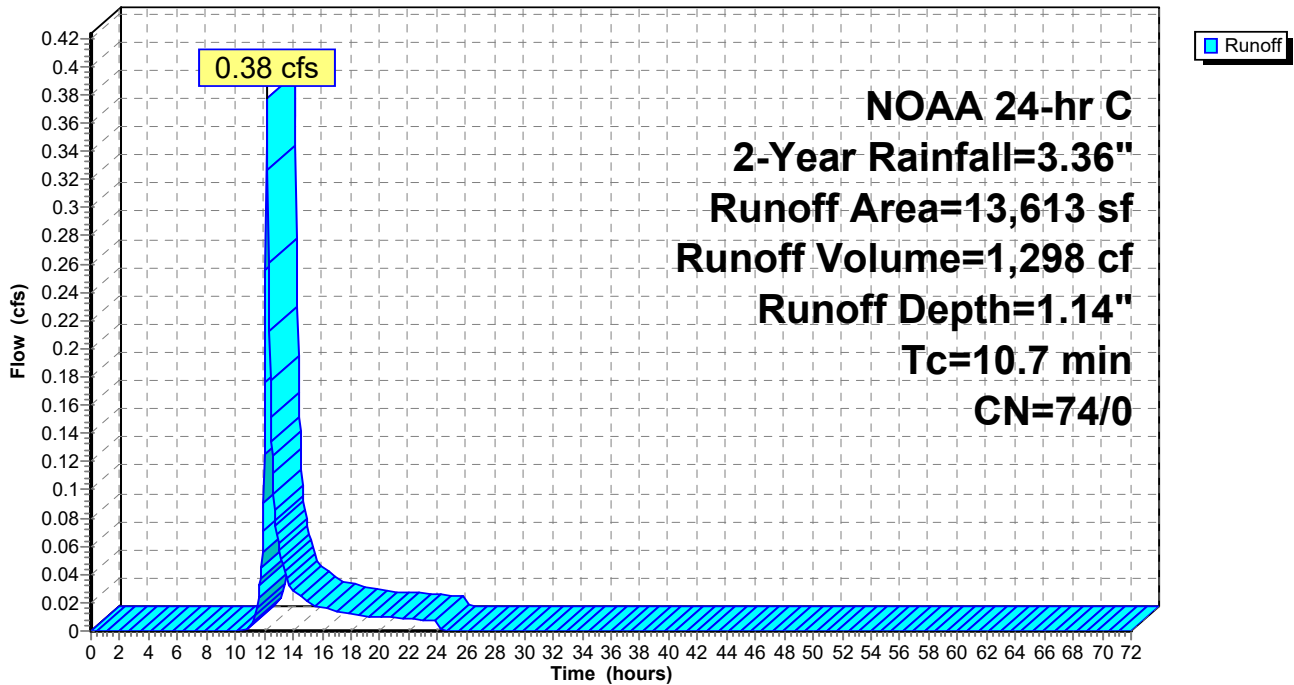
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 13,613 | 74 | >75% Grass cover, Good, HSG C |
| 13,613 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 4P: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Summary for Subcatchment 5P: Impervious

Runoff = 0.27 cfs @ 12.29 hrs, Volume= 1,306 cf, Depth= 3.12"

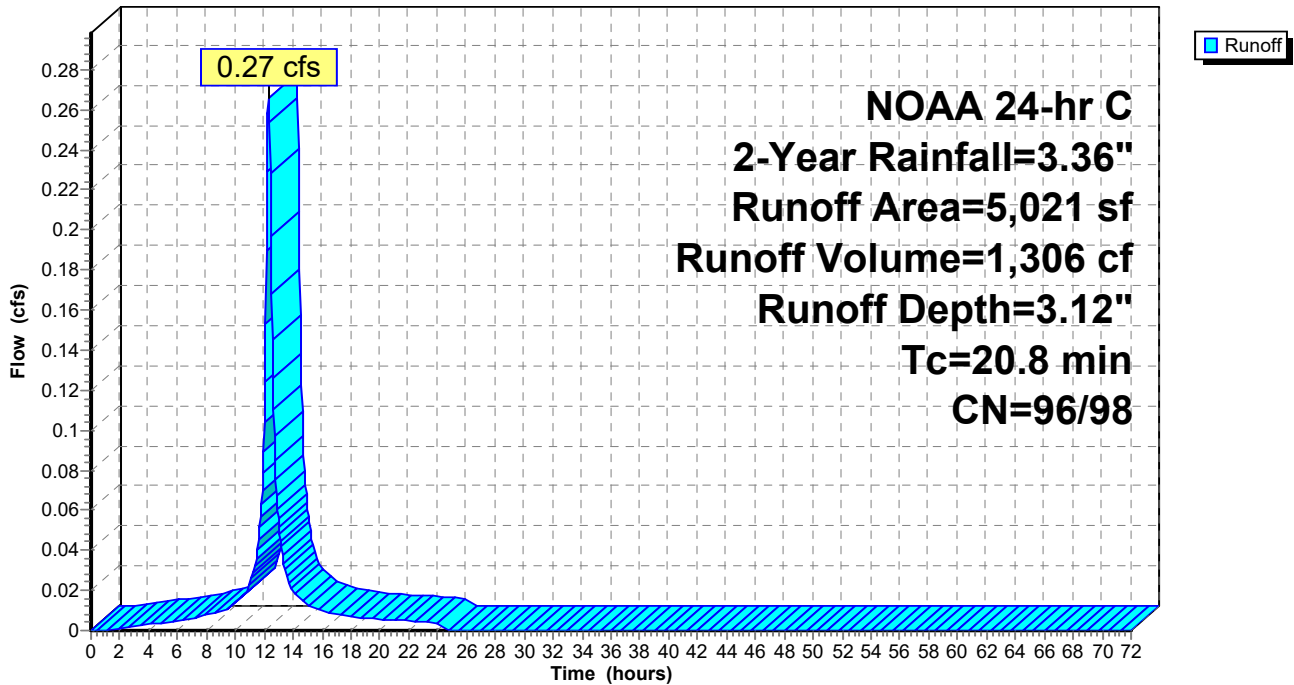
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|------------------------|
| 4,902 | 98 | Paved parking, HSG C |
| 119 | 96 | Gravel surface, HSG C |
| 5,021 | 98 | Weighted Average |
| 119 | 96 | 2.37% Pervious Area |
| 4,902 | 98 | 97.63% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 20.8 | | | | | Direct Entry, Tc |

Subcatchment 5P: Impervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Summary for Subcatchment 6P: Pervious

Runoff = 0.13 cfs @ 12.32 hrs, Volume= 607 cf, Depth= 1.09"

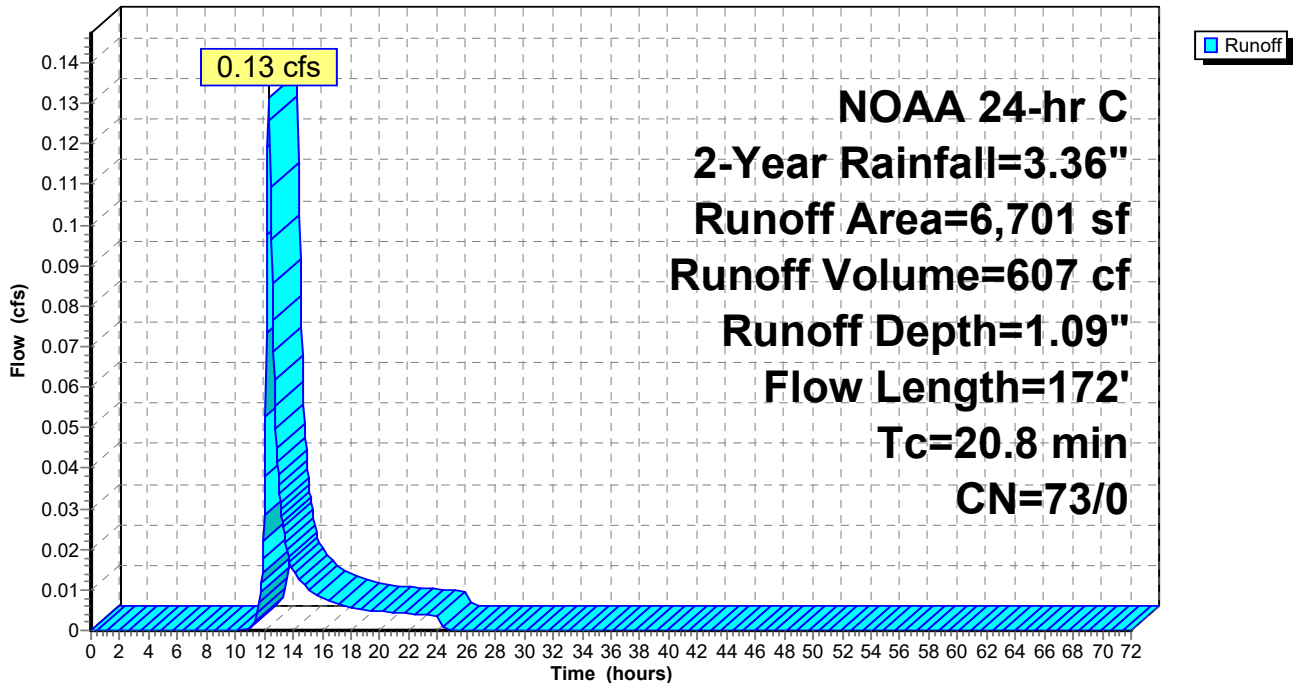
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 4,509 | 74 | >75% Grass cover, Good, HSG C |
| 2,192 | 70 | Woods, Good, HSG C |
| 6,701 | 73 | Weighted Average |
| 6,701 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 20.4 | 104 | 0.0230 | 0.08 | | Sheet Flow, A-B Woods: Light underbrush n= 0.400 P2= 3.36" |
| 0.3 | 57 | 0.0230 | 3.08 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 0.1 | 11 | 0.0200 | 2.28 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 20.8 | 172 | Total | | | |

Subcatchment 6P: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Subcatchment 7P: Impervious

Runoff = 0.16 cfs @ 12.21 hrs, Volume= 650 cf, Depth= 3.13"

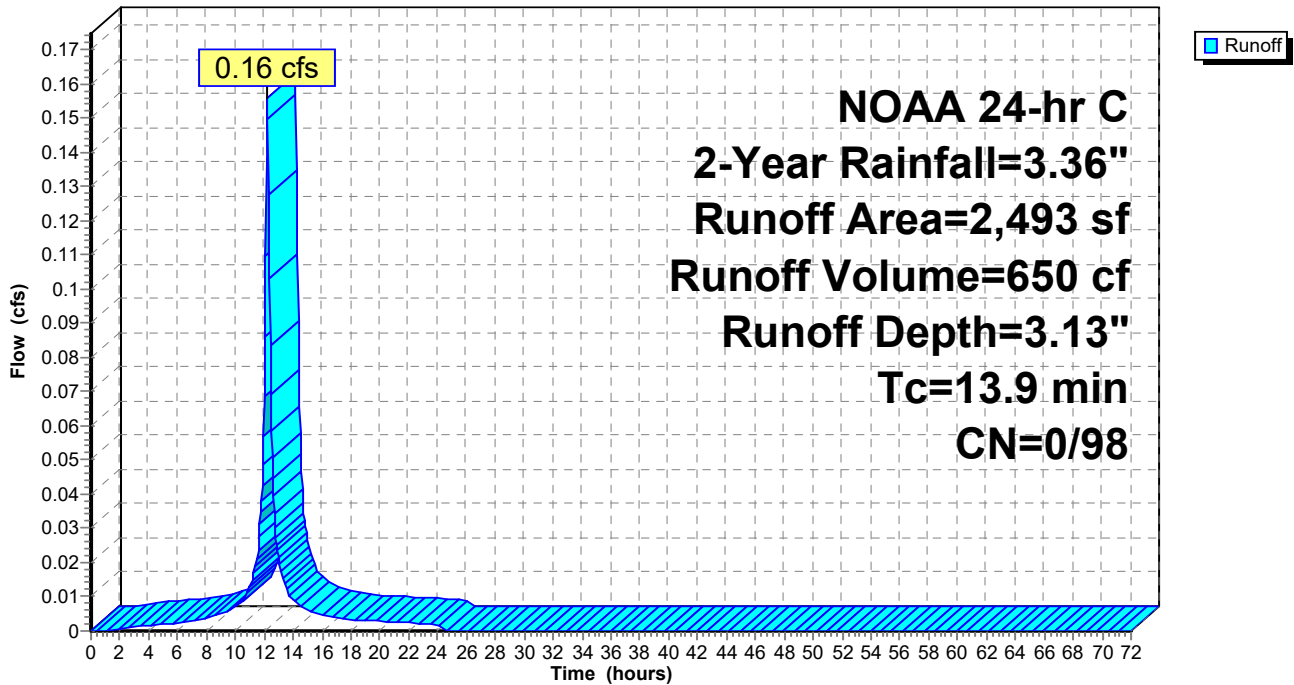
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,493 | 98 | Paved parking, HSG C |
| 2,493 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 13.9 | | | | | Direct Entry, Tc |

Subcatchment 7P: Impervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Summary for Subcatchment 8P: Pervious

Runoff = 1.36 cfs @ 12.24 hrs, Volume= 5,314 cf, Depth= 1.03"

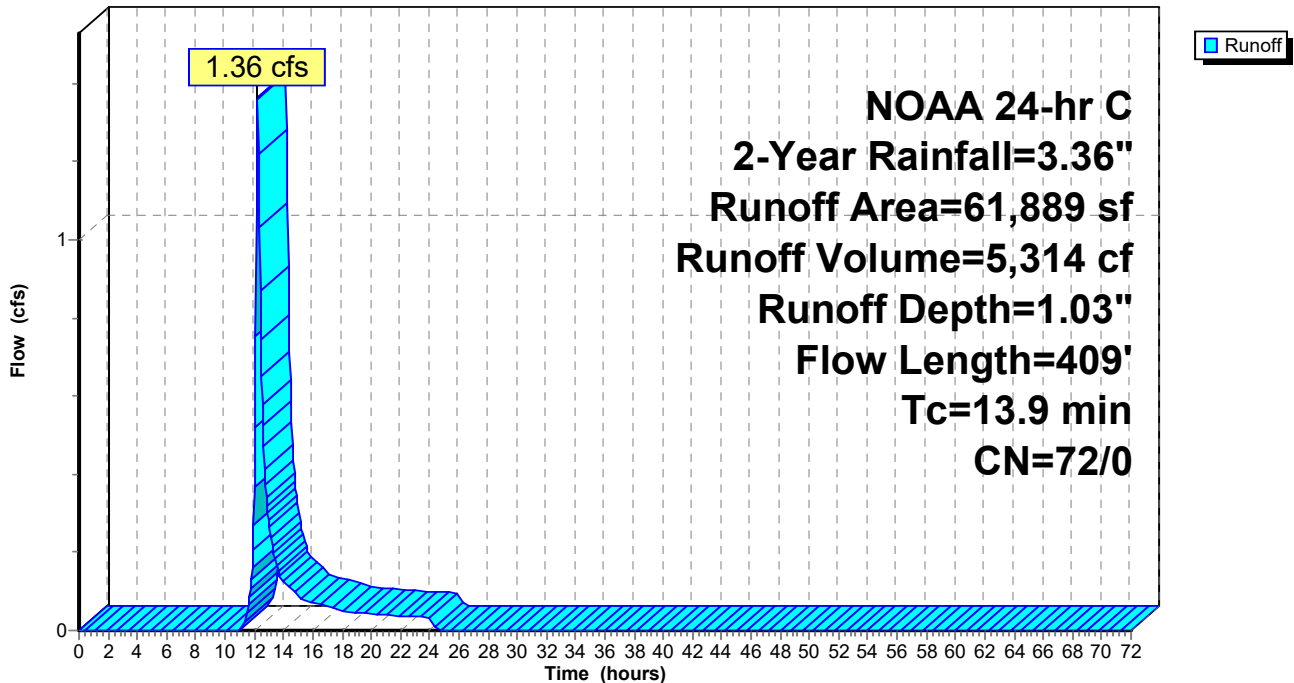
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 28,675 | 70 | Woods, Good, HSG C |
| 33,214 | 74 | >75% Grass cover, Good, HSG C |
| 61,889 | 72 | Weighted Average |
| 61,889 | 72 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 2.8 | 36 | 0.0560 | 0.21 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 4.3 | 51 | 0.0390 | 0.20 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.3 | 25 | 0.0800 | 1.41 | | Shallow Concentrated Flow, C-D Woodland Kv= 5.0 fps |
| 6.5 | 297 | 0.0230 | 0.76 | | Shallow Concentrated Flow, D-E Woodland Kv= 5.0 fps |
| 13.9 | 409 | Total | | | |

Subcatchment 8P: Pervious

Hydrograph



Pre vs Post

Prepared by {enter your company name here}

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NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Subcatchment 9P: Pervious

Runoff = 0.91 cfs @ 12.21 hrs, Volume= 3,296 cf, Depth= 1.09"

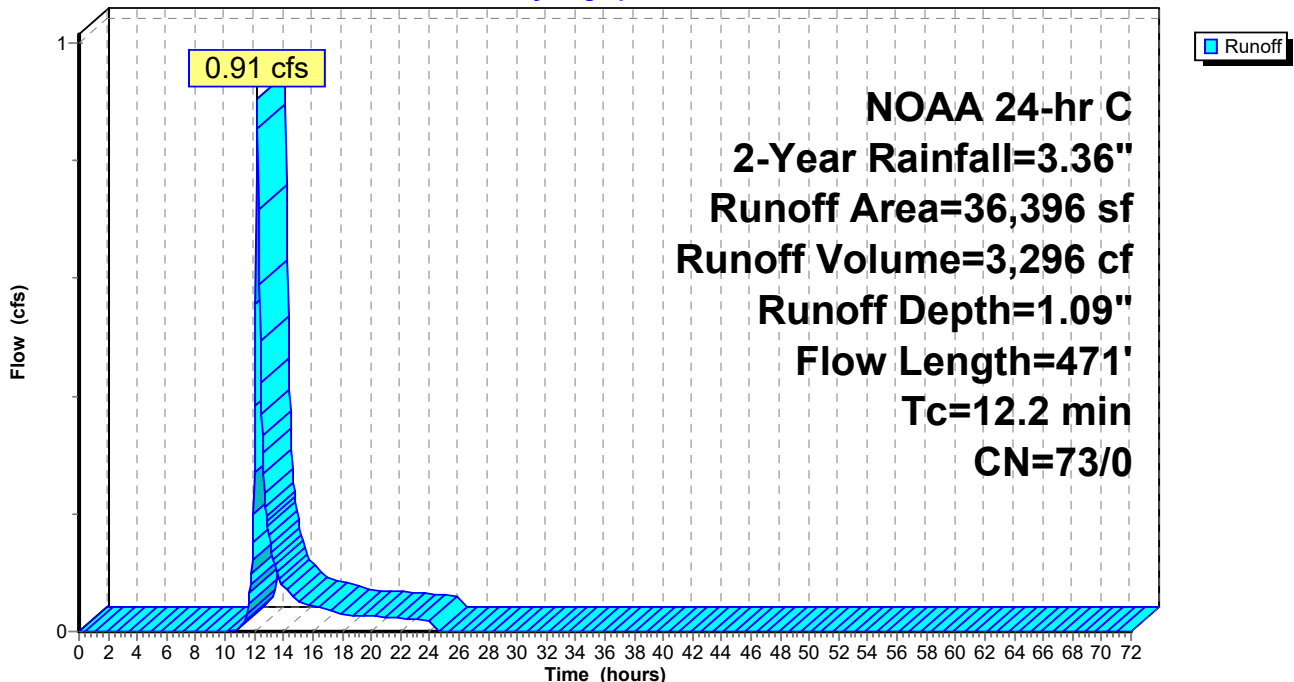
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 2-Year Rainfall=3.36"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 5,369 | 70 | Woods, Good, HSG C |
| 31,027 | 74 | >75% Grass cover, Good, HSG C |
| 36,396 | 73 | Weighted Average |
| 36,396 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 9.8 | 100 | 0.0190 | 0.17 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.7 | 102 | 0.0240 | 2.49 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.8 | 128 | 0.0310 | 2.83 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.8 | 120 | 0.0250 | 2.55 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.1 | 21 | 0.0310 | 2.83 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 12.2 | 471 | Total | | | |

Subcatchment 9P: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Pond B1: Bioretention Basin 1

[92] Warning: Device #2 is above defined storage

Inflow Area = 48,248 sf, 48.86% Impervious, Inflow Depth = 2.11" for 2-Year event
 Inflow = 2.29 cfs @ 12.18 hrs, Volume= 8,496 cf
 Outflow = 1.24 cfs @ 12.36 hrs, Volume= 4,601 cf, Atten= 46%, Lag= 10.5 min
 Primary = 1.24 cfs @ 12.36 hrs, Volume= 4,601 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 78.24' @ 12.36 hrs Surf.Area= 2,924 sf Storage= 4,156 cf

Plug-Flow detention time= 247.9 min calculated for 4,598 cf (54% of inflow)
 Center-of-Mass det. time= 123.7 min (913.9 - 790.2)

| Volume | Invert | Avail.Storage | Storage Description | |
|------------------|-------------------|------------------------|--|------------------|
| #1 | 76.50' | 4,938 cf | Custom Stage Data (Conic) Listed below (Recalc) | |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
| 76.50 | 1,883 | 0 | 0 | 1,883 |
| 77.50 | 2,461 | 2,166 | 2,166 | 2,484 |
| 78.50 | 3,096 | 2,772 | 4,938 | 3,146 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|---|
| #1 | Primary | 73.00' | 24.0" Round CMP_Round 24" L= 10.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.85' S= 0.0150 1' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf |
| #2 | Device 1 | 78.50' | 10.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 78.15' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=1.21 cfs @ 12.36 hrs HW=78.24' (Free Discharge)
 1=CMP_Round 24" (Passes 1.21 cfs of 24.59 cfs potential flow)
 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
 3=Orifice/Grate (Weir Controls 1.21 cfs @ 0.97 fps)

Pre vs Post

Prepared by {enter your company name here}

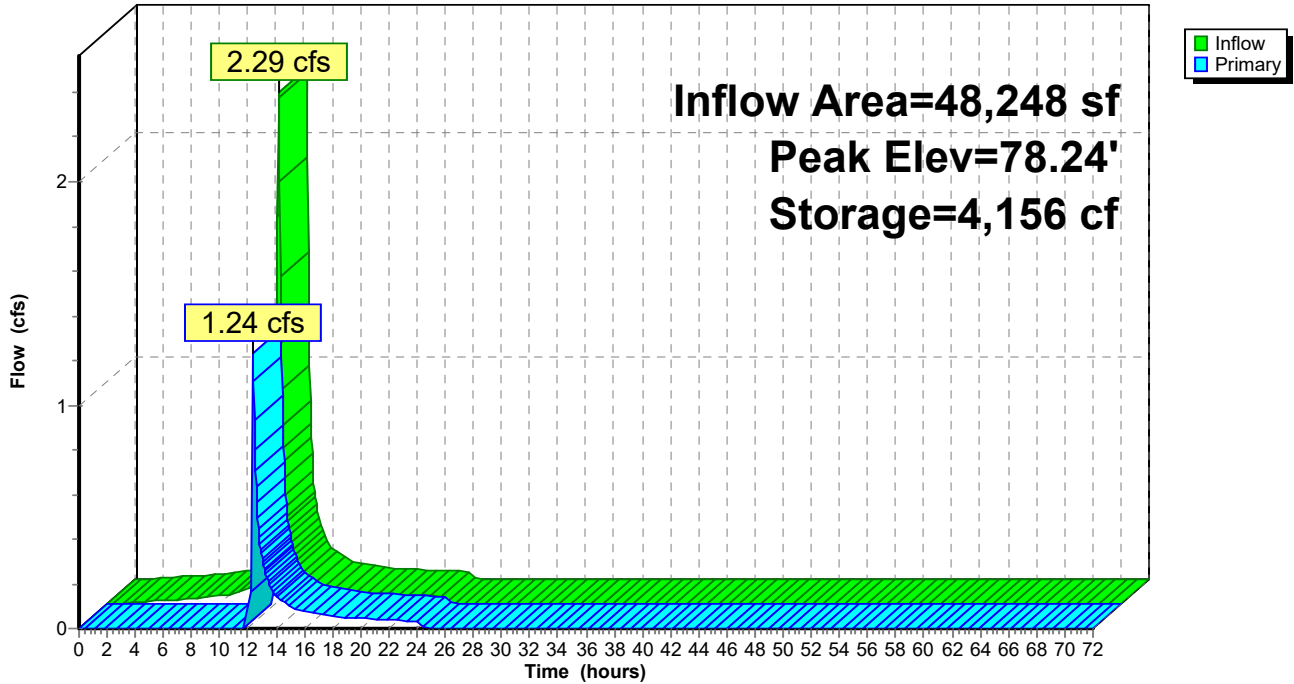
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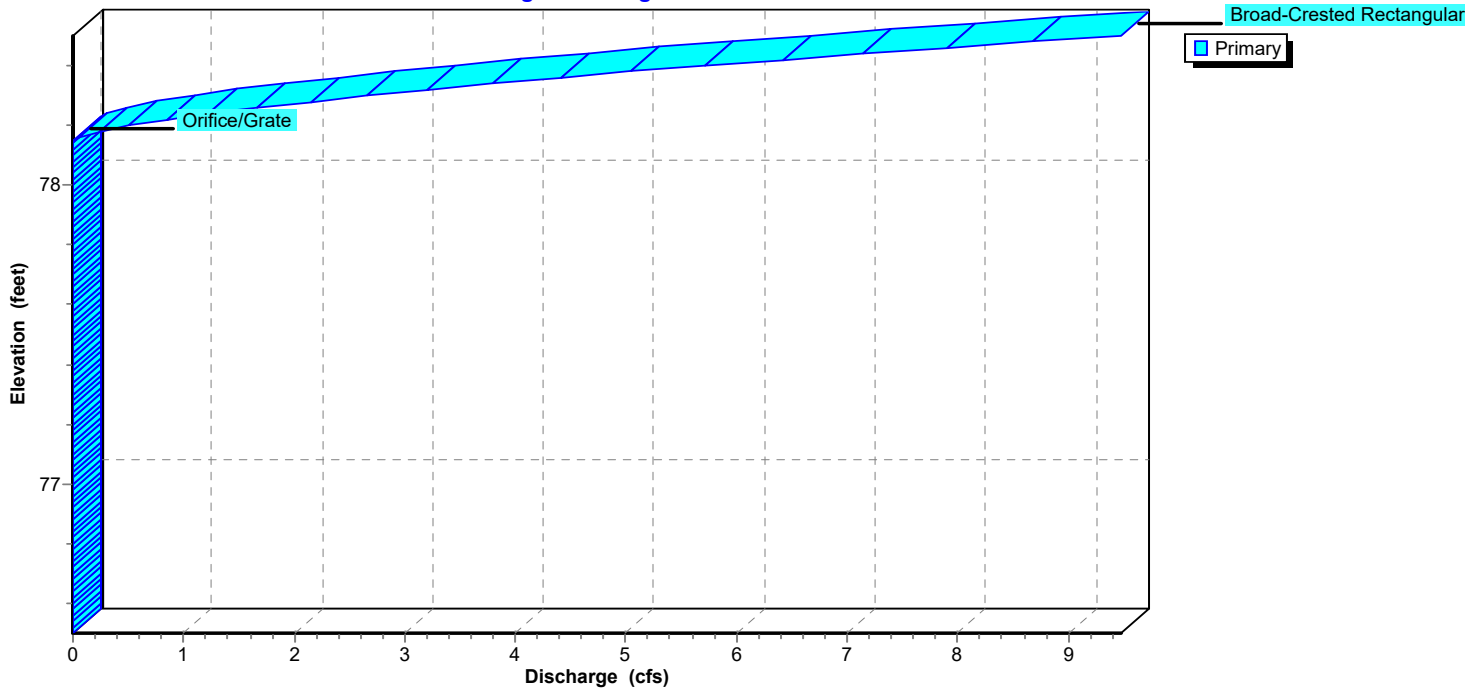
Pond B1: Bioretention Basin 1

Hydrograph



Pond B1: Bioretention Basin 1

Stage-Discharge



Pre vs Post

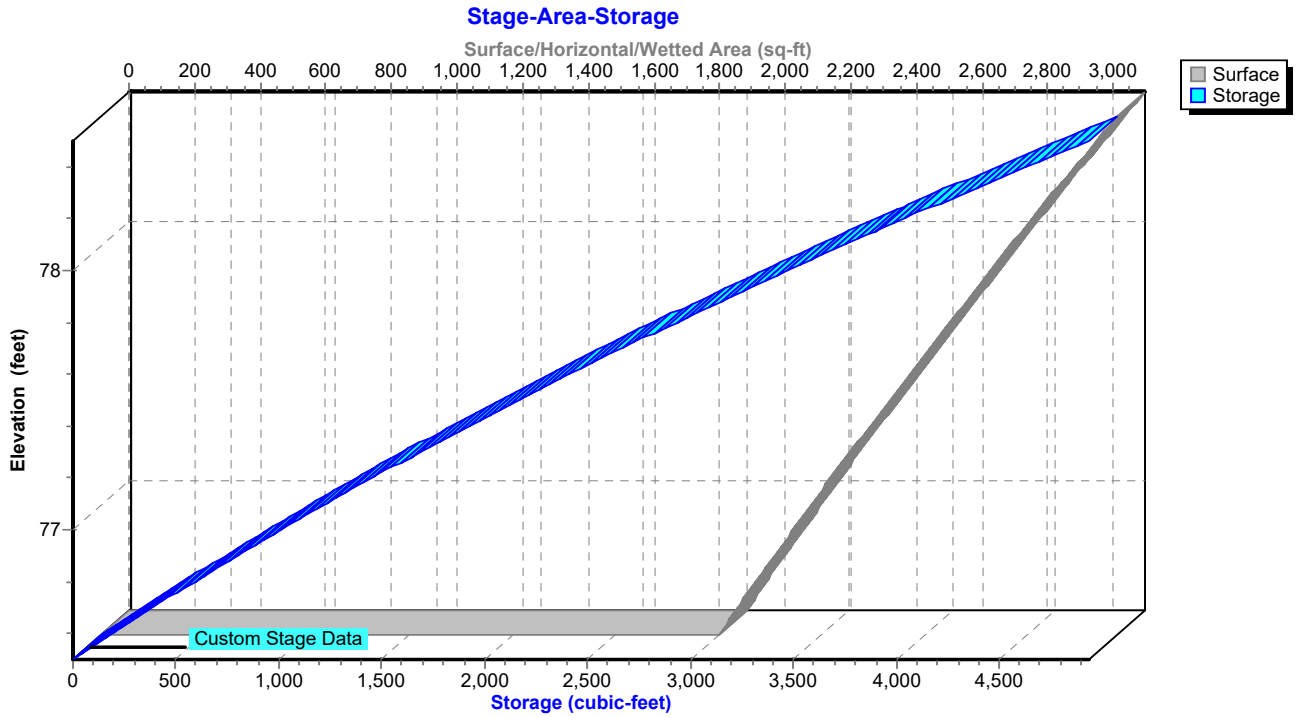
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Pond B1: Bioretention Basin 1



Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Stage-Discharge for Pond B1: Bioretention Basin 1

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.03 | 0.00 | 77.56 | 0.00 | 78.09 | 0.00 |
| 76.51 | 0.00 | 77.04 | 0.00 | 77.57 | 0.00 | 78.10 | 0.00 |
| 76.52 | 0.00 | 77.05 | 0.00 | 77.58 | 0.00 | 78.11 | 0.00 |
| 76.53 | 0.00 | 77.06 | 0.00 | 77.59 | 0.00 | 78.12 | 0.00 |
| 76.54 | 0.00 | 77.07 | 0.00 | 77.60 | 0.00 | 78.13 | 0.00 |
| 76.55 | 0.00 | 77.08 | 0.00 | 77.61 | 0.00 | 78.14 | 0.00 |
| 76.56 | 0.00 | 77.09 | 0.00 | 77.62 | 0.00 | 78.15 | 0.00 |
| 76.57 | 0.00 | 77.10 | 0.00 | 77.63 | 0.00 | 78.16 | 0.05 |
| 76.58 | 0.00 | 77.11 | 0.00 | 77.64 | 0.00 | 78.17 | 0.13 |
| 76.59 | 0.00 | 77.12 | 0.00 | 77.65 | 0.00 | 78.18 | 0.24 |
| 76.60 | 0.00 | 77.13 | 0.00 | 77.66 | 0.00 | 78.19 | 0.37 |
| 76.61 | 0.00 | 77.14 | 0.00 | 77.67 | 0.00 | 78.20 | 0.51 |
| 76.62 | 0.00 | 77.15 | 0.00 | 77.68 | 0.00 | 78.21 | 0.67 |
| 76.63 | 0.00 | 77.16 | 0.00 | 77.69 | 0.00 | 78.22 | 0.85 |
| 76.64 | 0.00 | 77.17 | 0.00 | 77.70 | 0.00 | 78.23 | 1.04 |
| 76.65 | 0.00 | 77.18 | 0.00 | 77.71 | 0.00 | 78.24 | 1.24 |
| 76.66 | 0.00 | 77.19 | 0.00 | 77.72 | 0.00 | 78.25 | 1.45 |
| 76.67 | 0.00 | 77.20 | 0.00 | 77.73 | 0.00 | 78.26 | 1.67 |
| 76.68 | 0.00 | 77.21 | 0.00 | 77.74 | 0.00 | 78.27 | 1.90 |
| 76.69 | 0.00 | 77.22 | 0.00 | 77.75 | 0.00 | 78.28 | 2.15 |
| 76.70 | 0.00 | 77.23 | 0.00 | 77.76 | 0.00 | 78.29 | 2.40 |
| 76.71 | 0.00 | 77.24 | 0.00 | 77.77 | 0.00 | 78.30 | 2.66 |
| 76.72 | 0.00 | 77.25 | 0.00 | 77.78 | 0.00 | 78.31 | 2.93 |
| 76.73 | 0.00 | 77.26 | 0.00 | 77.79 | 0.00 | 78.32 | 3.21 |
| 76.74 | 0.00 | 77.27 | 0.00 | 77.80 | 0.00 | 78.33 | 3.50 |
| 76.75 | 0.00 | 77.28 | 0.00 | 77.81 | 0.00 | 78.34 | 3.79 |
| 76.76 | 0.00 | 77.29 | 0.00 | 77.82 | 0.00 | 78.35 | 4.09 |
| 76.77 | 0.00 | 77.30 | 0.00 | 77.83 | 0.00 | 78.36 | 4.41 |
| 76.78 | 0.00 | 77.31 | 0.00 | 77.84 | 0.00 | 78.37 | 4.72 |
| 76.79 | 0.00 | 77.32 | 0.00 | 77.85 | 0.00 | 78.38 | 5.05 |
| 76.80 | 0.00 | 77.33 | 0.00 | 77.86 | 0.00 | 78.39 | 5.38 |
| 76.81 | 0.00 | 77.34 | 0.00 | 77.87 | 0.00 | 78.40 | 5.72 |
| 76.82 | 0.00 | 77.35 | 0.00 | 77.88 | 0.00 | 78.41 | 6.07 |
| 76.83 | 0.00 | 77.36 | 0.00 | 77.89 | 0.00 | 78.42 | 6.42 |
| 76.84 | 0.00 | 77.37 | 0.00 | 77.90 | 0.00 | 78.43 | 6.78 |
| 76.85 | 0.00 | 77.38 | 0.00 | 77.91 | 0.00 | 78.44 | 7.15 |
| 76.86 | 0.00 | 77.39 | 0.00 | 77.92 | 0.00 | 78.45 | 7.52 |
| 76.87 | 0.00 | 77.40 | 0.00 | 77.93 | 0.00 | 78.46 | 7.90 |
| 76.88 | 0.00 | 77.41 | 0.00 | 77.94 | 0.00 | 78.47 | 8.29 |
| 76.89 | 0.00 | 77.42 | 0.00 | 77.95 | 0.00 | 78.48 | 8.68 |
| 76.90 | 0.00 | 77.43 | 0.00 | 77.96 | 0.00 | 78.49 | 9.08 |
| 76.91 | 0.00 | 77.44 | 0.00 | 77.97 | 0.00 | 78.50 | 9.48 |
| 76.92 | 0.00 | 77.45 | 0.00 | 77.98 | 0.00 | | |
| 76.93 | 0.00 | 77.46 | 0.00 | 77.99 | 0.00 | | |
| 76.94 | 0.00 | 77.47 | 0.00 | 78.00 | 0.00 | | |
| 76.95 | 0.00 | 77.48 | 0.00 | 78.01 | 0.00 | | |
| 76.96 | 0.00 | 77.49 | 0.00 | 78.02 | 0.00 | | |
| 76.97 | 0.00 | 77.50 | 0.00 | 78.03 | 0.00 | | |
| 76.98 | 0.00 | 77.51 | 0.00 | 78.04 | 0.00 | | |
| 76.99 | 0.00 | 77.52 | 0.00 | 78.05 | 0.00 | | |
| 77.00 | 0.00 | 77.53 | 0.00 | 78.06 | 0.00 | | |
| 77.01 | 0.00 | 77.54 | 0.00 | 78.07 | 0.00 | | |
| 77.02 | 0.00 | 77.55 | 0.00 | 78.08 | 0.00 | | |

Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Stage-Area-Storage for Pond B1: Bioretention Basin 1

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 1,883 | 0 | 77.56 | 2,497 | 2,314 |
| 76.52 | 1,894 | 38 | 77.58 | 2,509 | 2,364 |
| 76.54 | 1,905 | 76 | 77.60 | 2,521 | 2,415 |
| 76.56 | 1,916 | 114 | 77.62 | 2,533 | 2,465 |
| 76.58 | 1,926 | 152 | 77.64 | 2,546 | 2,516 |
| 76.60 | 1,937 | 191 | 77.66 | 2,558 | 2,567 |
| 76.62 | 1,948 | 230 | 77.68 | 2,570 | 2,618 |
| 76.64 | 1,959 | 269 | 77.70 | 2,582 | 2,670 |
| 76.66 | 1,970 | 308 | 77.72 | 2,594 | 2,722 |
| 76.68 | 1,981 | 348 | 77.74 | 2,607 | 2,774 |
| 76.70 | 1,992 | 387 | 77.76 | 2,619 | 2,826 |
| 76.72 | 2,004 | 427 | 77.78 | 2,631 | 2,878 |
| 76.74 | 2,015 | 468 | 77.80 | 2,644 | 2,931 |
| 76.76 | 2,026 | 508 | 77.82 | 2,656 | 2,984 |
| 76.78 | 2,037 | 549 | 77.84 | 2,669 | 3,037 |
| 76.80 | 2,048 | 590 | 77.86 | 2,681 | 3,091 |
| 76.82 | 2,060 | 631 | 77.88 | 2,694 | 3,145 |
| 76.84 | 2,071 | 672 | 77.90 | 2,706 | 3,199 |
| 76.86 | 2,082 | 713 | 77.92 | 2,719 | 3,253 |
| 76.88 | 2,094 | 755 | 77.94 | 2,731 | 3,307 |
| 76.90 | 2,105 | 797 | 77.96 | 2,744 | 3,362 |
| 76.92 | 2,116 | 839 | 77.98 | 2,757 | 3,417 |
| 76.94 | 2,128 | 882 | 78.00 | 2,769 | 3,472 |
| 76.96 | 2,139 | 924 | 78.02 | 2,782 | 3,528 |
| 76.98 | 2,151 | 967 | 78.04 | 2,795 | 3,584 |
| 77.00 | 2,162 | 1,011 | 78.06 | 2,808 | 3,640 |
| 77.02 | 2,174 | 1,054 | 78.08 | 2,820 | 3,696 |
| 77.04 | 2,186 | 1,097 | 78.10 | 2,833 | 3,753 |
| 77.06 | 2,197 | 1,141 | 78.12 | 2,846 | 3,809 |
| 77.08 | 2,209 | 1,185 | 78.14 | 2,859 | 3,866 |
| 77.10 | 2,221 | 1,230 | 78.16 | 2,872 | 3,924 |
| 77.12 | 2,232 | 1,274 | 78.18 | 2,885 | 3,981 |
| 77.14 | 2,244 | 1,319 | 78.20 | 2,898 | 4,039 |
| 77.16 | 2,256 | 1,364 | 78.22 | 2,911 | 4,097 |
| 77.18 | 2,268 | 1,409 | 78.24 | 2,924 | 4,156 |
| 77.20 | 2,279 | 1,455 | 78.26 | 2,937 | 4,214 |
| 77.22 | 2,291 | 1,500 | 78.28 | 2,950 | 4,273 |
| 77.24 | 2,303 | 1,546 | 78.30 | 2,963 | 4,332 |
| 77.26 | 2,315 | 1,593 | 78.32 | 2,976 | 4,392 |
| 77.28 | 2,327 | 1,639 | 78.34 | 2,990 | 4,451 |
| 77.30 | 2,339 | 1,686 | 78.36 | 3,003 | 4,511 |
| 77.32 | 2,351 | 1,732 | 78.38 | 3,016 | 4,571 |
| 77.34 | 2,363 | 1,780 | 78.40 | 3,029 | 4,632 |
| 77.36 | 2,375 | 1,827 | 78.42 | 3,043 | 4,692 |
| 77.38 | 2,388 | 1,875 | 78.44 | 3,056 | 4,753 |
| 77.40 | 2,400 | 1,923 | 78.46 | 3,069 | 4,815 |
| 77.42 | 2,412 | 1,971 | 78.48 | 3,083 | 4,876 |
| 77.44 | 2,424 | 2,019 | 78.50 | 3,096 | 4,938 |
| 77.46 | 2,436 | 2,068 | | | |
| 77.48 | 2,449 | 2,116 | | | |
| 77.50 | 2,461 | 2,166 | | | |
| 77.52 | 2,473 | 2,215 | | | |
| 77.54 | 2,485 | 2,264 | | | |

Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Pond B2: Bioretention Basin 2

[79] Warning: Submerged Pond B1 Primary device # 1 INLET by 4.37'

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 1.87" for 2-Year event
 Inflow = 2.75 cfs @ 12.20 hrs, Volume= 15,128 cf
 Outflow = 1.20 cfs @ 12.63 hrs, Volume= 11,962 cf, Atten= 57%, Lag= 25.9 min
 Primary = 1.20 cfs @ 12.63 hrs, Volume= 11,962 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 77.37' @ 12.63 hrs Surf.Area= 7,986 sf Storage= 6,451 cf

Plug-Flow detention time= 240.9 min calculated for 11,962 cf (79% of inflow)
 Center-of-Mass det. time= 150.5 min (967.0 - 816.5)

| Volume | Invert | Avail.Storage | Storage Description |
|---------------------|----------------------|---------------------------|--|
| #1 | 76.50' | 26,647 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 76.50 | 6,877 | 0 | 0 |
| 77.50 | 8,155 | 7,516 | 7,516 |
| 78.50 | 9,522 | 8,839 | 16,355 |
| 79.50 | 11,063 | 10,293 | 26,647 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|--|
| #1 | Primary | 73.00' | 15.0" Round Culvert L= 47.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.06' S= 0.0200 ' S Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf |
| #2 | Device 1 | 76.94' | 6.0" Vert. Orifice/Grate X 3.00 C= 0.600 |
| #3 | Device 1 | 77.78' | 4.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |
| #4 | Device 1 | 79.25' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=1.19 cfs @ 12.63 hrs HW=77.37' (Free Discharge)

- 1=Culvert (Passes 1.19 cfs of 9.02 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 1.19 cfs @ 2.23 fps)
- 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
- 4=Orifice/Grate (Controls 0.00 cfs)

Pre vs Post

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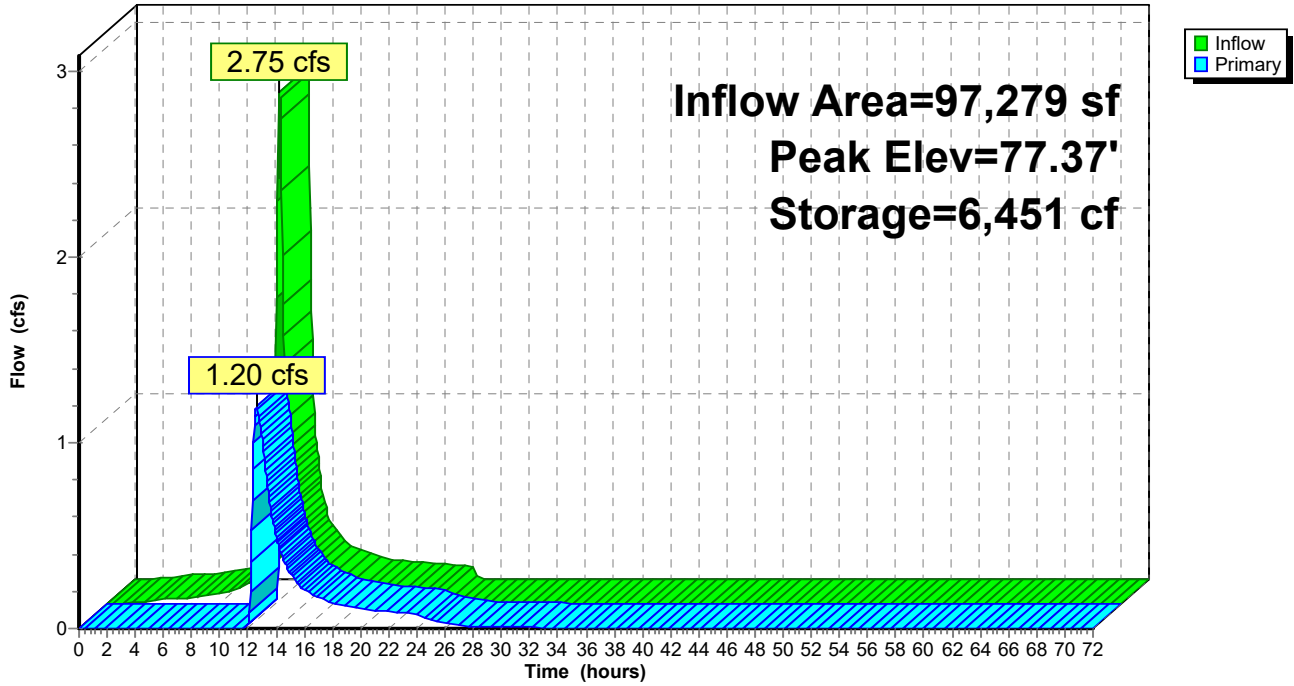
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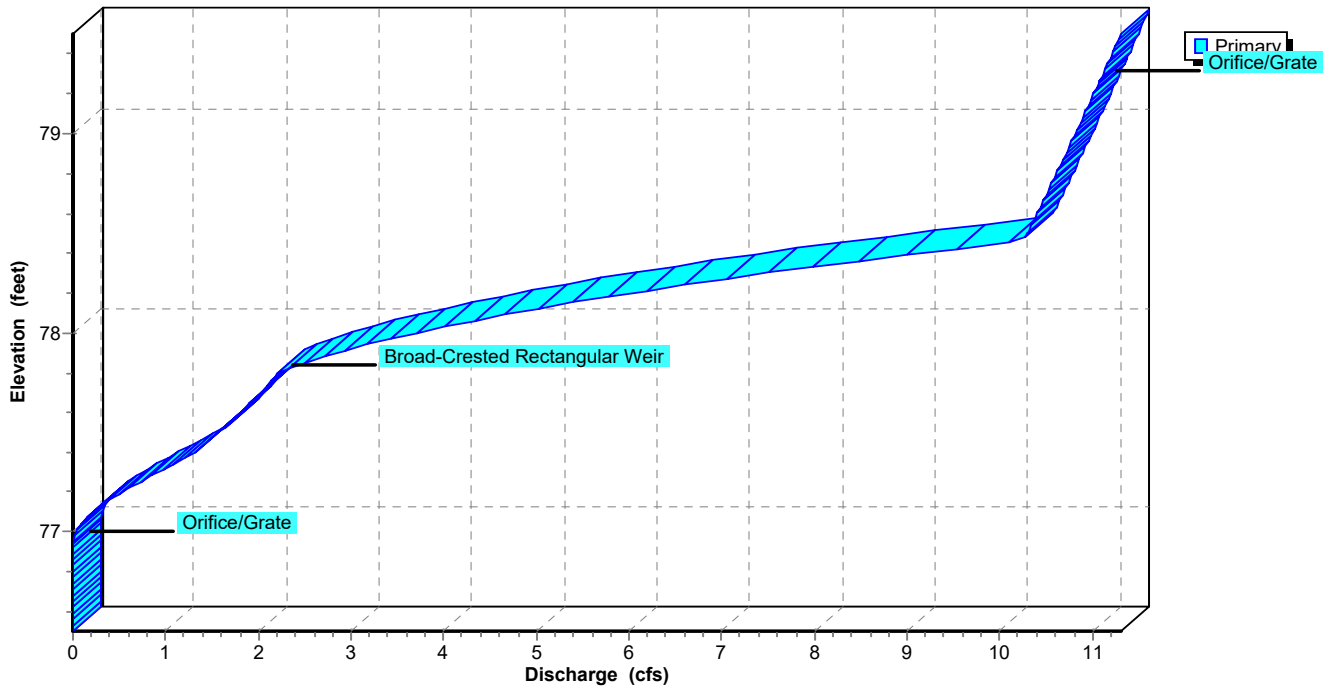
Pond B2: Bioretention Basin 2

Hydrograph



Pond B2: Bioretention Basin 2

Stage-Discharge



Pre vs Post

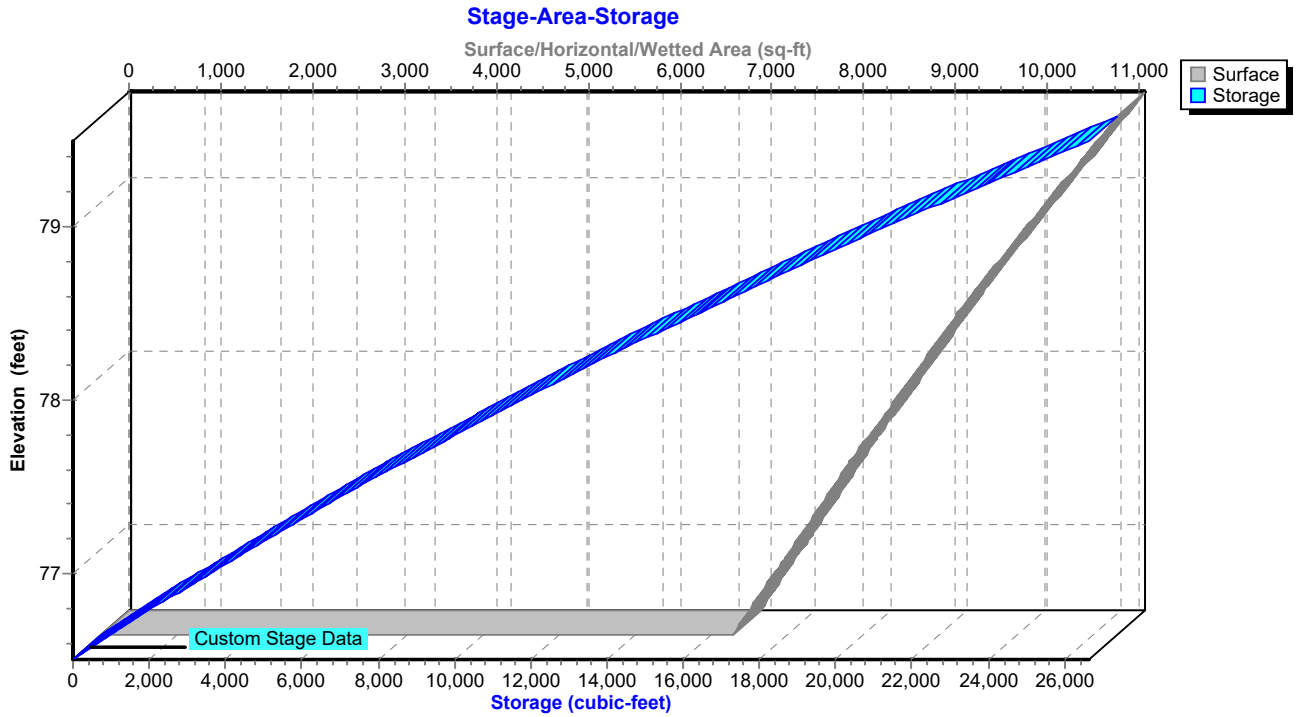
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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

Pond B2: Bioretention Basin 2



Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

Prepared by {enter your company name here}

Printed 5/14/2021

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Stage-Discharge for Pond B2: Bioretention Basin 2

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.56 | 1.73 | 78.62 | 10.43 |
| 76.52 | 0.00 | 77.58 | 1.77 | 78.64 | 10.45 |
| 76.54 | 0.00 | 77.60 | 1.82 | 78.66 | 10.47 |
| 76.56 | 0.00 | 77.62 | 1.86 | 78.68 | 10.49 |
| 76.58 | 0.00 | 77.64 | 1.90 | 78.70 | 10.51 |
| 76.60 | 0.00 | 77.66 | 1.94 | 78.72 | 10.53 |
| 76.62 | 0.00 | 77.68 | 1.99 | 78.74 | 10.55 |
| 76.64 | 0.00 | 77.70 | 2.03 | 78.76 | 10.57 |
| 76.66 | 0.00 | 77.72 | 2.06 | 78.78 | 10.59 |
| 76.68 | 0.00 | 77.74 | 2.10 | 78.80 | 10.61 |
| 76.70 | 0.00 | 77.76 | 2.14 | 78.82 | 10.63 |
| 76.72 | 0.00 | 77.78 | 2.18 | 78.84 | 10.65 |
| 76.74 | 0.00 | 77.80 | 2.25 | 78.86 | 10.67 |
| 76.76 | 0.00 | 77.82 | 2.34 | 78.88 | 10.69 |
| 76.78 | 0.00 | 77.84 | 2.45 | 78.90 | 10.71 |
| 76.80 | 0.00 | 77.86 | 2.58 | 78.92 | 10.73 |
| 76.82 | 0.00 | 77.88 | 2.71 | 78.94 | 10.75 |
| 76.84 | 0.00 | 77.90 | 2.86 | 78.96 | 10.77 |
| 76.86 | 0.00 | 77.92 | 3.01 | 78.98 | 10.79 |
| 76.88 | 0.00 | 77.94 | 3.17 | 79.00 | 10.82 |
| 76.90 | 0.00 | 77.96 | 3.34 | 79.02 | 10.84 |
| 76.92 | 0.00 | 77.98 | 3.52 | 79.04 | 10.86 |
| 76.94 | 0.00 | 78.00 | 3.71 | 79.06 | 10.88 |
| 76.96 | 0.00 | 78.02 | 3.91 | 79.08 | 10.90 |
| 76.98 | 0.02 | 78.04 | 4.12 | 79.10 | 10.92 |
| 77.00 | 0.03 | 78.06 | 4.33 | 79.12 | 10.94 |
| 77.02 | 0.06 | 78.08 | 4.56 | 79.14 | 10.96 |
| 77.04 | 0.09 | 78.10 | 4.79 | 79.16 | 10.97 |
| 77.06 | 0.13 | 78.12 | 5.02 | 79.18 | 10.99 |
| 77.08 | 0.17 | 78.14 | 5.27 | 79.20 | 11.01 |
| 77.10 | 0.22 | 78.16 | 5.52 | 79.22 | 11.03 |
| 77.12 | 0.28 | 78.18 | 5.78 | 79.24 | 11.05 |
| 77.14 | 0.34 | 78.20 | 6.05 | 79.26 | 11.07 |
| 77.16 | 0.40 | 78.22 | 6.32 | 79.28 | 11.09 |
| 77.18 | 0.47 | 78.24 | 6.61 | 79.30 | 11.11 |
| 77.20 | 0.54 | 78.26 | 6.90 | 79.32 | 11.13 |
| 77.22 | 0.61 | 78.28 | 7.20 | 79.34 | 11.15 |
| 77.24 | 0.69 | 78.30 | 7.51 | 79.36 | 11.17 |
| 77.26 | 0.77 | 78.32 | 7.83 | 79.38 | 11.19 |
| 77.28 | 0.85 | 78.34 | 8.15 | 79.40 | 11.21 |
| 77.30 | 0.93 | 78.36 | 8.48 | 79.42 | 11.23 |
| 77.32 | 1.01 | 78.38 | 8.82 | 79.44 | 11.25 |
| 77.34 | 1.09 | 78.40 | 9.18 | 79.46 | 11.27 |
| 77.36 | 1.17 | 78.42 | 9.54 | 79.48 | 11.29 |
| 77.38 | 1.24 | 78.44 | 9.92 | 79.50 | 11.31 |
| 77.40 | 1.31 | 78.46 | 10.26 | | |
| 77.42 | 1.37 | 78.48 | 10.28 | | |
| 77.44 | 1.42 | 78.50 | 10.30 | | |
| 77.46 | 1.47 | 78.52 | 10.32 | | |
| 77.48 | 1.53 | 78.54 | 10.34 | | |
| 77.50 | 1.58 | 78.56 | 10.36 | | |
| 77.52 | 1.63 | 78.58 | 10.38 | | |
| 77.54 | 1.68 | 78.60 | 10.40 | | |

Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Stage-Area-Storage for Pond B2: Bioretention Basin 2

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 6,877 | 0 | 79.15 | 10,524 | 22,869 |
| 76.55 | 6,941 | 345 | 79.20 | 10,601 | 23,397 |
| 76.60 | 7,005 | 694 | 79.25 | 10,678 | 23,929 |
| 76.65 | 7,069 | 1,046 | 79.30 | 10,755 | 24,465 |
| 76.70 | 7,133 | 1,401 | 79.35 | 10,832 | 25,005 |
| 76.75 | 7,197 | 1,759 | 79.40 | 10,909 | 25,548 |
| 76.80 | 7,260 | 2,121 | 79.45 | 10,986 | 26,096 |
| 76.85 | 7,324 | 2,485 | 79.50 | 11,063 | 26,647 |
| 76.90 | 7,388 | 2,853 | | | |
| 76.95 | 7,452 | 3,224 | | | |
| 77.00 | 7,516 | 3,598 | | | |
| 77.05 | 7,580 | 3,976 | | | |
| 77.10 | 7,644 | 4,356 | | | |
| 77.15 | 7,708 | 4,740 | | | |
| 77.20 | 7,772 | 5,127 | | | |
| 77.25 | 7,836 | 5,517 | | | |
| 77.30 | 7,899 | 5,911 | | | |
| 77.35 | 7,963 | 6,307 | | | |
| 77.40 | 8,027 | 6,707 | | | |
| 77.45 | 8,091 | 7,110 | | | |
| 77.50 | 8,155 | 7,516 | | | |
| 77.55 | 8,223 | 7,925 | | | |
| 77.60 | 8,292 | 8,338 | | | |
| 77.65 | 8,360 | 8,755 | | | |
| 77.70 | 8,428 | 9,174 | | | |
| 77.75 | 8,497 | 9,597 | | | |
| 77.80 | 8,565 | 10,024 | | | |
| 77.85 | 8,633 | 10,454 | | | |
| 77.90 | 8,702 | 10,887 | | | |
| 77.95 | 8,770 | 11,324 | | | |
| 78.00 | 8,839 | 11,764 | | | |
| 78.05 | 8,907 | 12,208 | | | |
| 78.10 | 8,975 | 12,655 | | | |
| 78.15 | 9,044 | 13,106 | | | |
| 78.20 | 9,112 | 13,559 | | | |
| 78.25 | 9,180 | 14,017 | | | |
| 78.30 | 9,249 | 14,477 | | | |
| 78.35 | 9,317 | 14,942 | | | |
| 78.40 | 9,385 | 15,409 | | | |
| 78.45 | 9,454 | 15,880 | | | |
| 78.50 | 9,522 | 16,355 | | | |
| 78.55 | 9,599 | 16,833 | | | |
| 78.60 | 9,676 | 17,314 | | | |
| 78.65 | 9,753 | 17,800 | | | |
| 78.70 | 9,830 | 18,290 | | | |
| 78.75 | 9,907 | 18,783 | | | |
| 78.80 | 9,984 | 19,280 | | | |
| 78.85 | 10,061 | 19,782 | | | |
| 78.90 | 10,138 | 20,287 | | | |
| 78.95 | 10,215 | 20,795 | | | |
| 79.00 | 10,293 | 21,308 | | | |
| 79.05 | 10,370 | 21,825 | | | |
| 79.10 | 10,447 | 22,345 | | | |

Pre vs Post

NOAA 24-hr C 2-Year Rainfall=3.36"

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Summary for Pond B3: Bioretention Basin 3

[92] Warning: Device #2 is above defined storage

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 1.96" for 2-Year event
 Inflow = 0.40 cfs @ 12.30 hrs, Volume= 1,913 cf
 Outflow = 0.40 cfs @ 12.32 hrs, Volume= 1,439 cf, Atten= 0%, Lag= 1.0 min
 Primary = 0.40 cfs @ 12.32 hrs, Volume= 1,439 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 80.78' @ 12.32 hrs Surf.Area= 865 sf Storage= 510 cf

Plug-Flow detention time= 163.2 min calculated for 1,439 cf (75% of inflow)
 Center-of-Mass det. time= 68.3 min (873.5 - 805.2)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 79.98' | 694 cf | Custom Stage Data (Conic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|------------------|-------------------|------------------------|------------------------|------------------|
| 79.98 | 432 | 0 | 0 | 432 |
| 80.98 | 995 | 694 | 694 | 1,003 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 77.48' | 15.0" Round CMP_Round 15" L= 96.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 77.48' / 77.00' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 1.23 sf |
| #2 | Secondary | 80.98' | 15.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 80.74' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=0.39 cfs @ 12.32 hrs HW=80.78' (Free Discharge)
 ↑1=CMP_Round 15" (Passes 0.39 cfs of 7.63 cfs potential flow)
 ↑3=Orifice/Grate (Weir Controls 0.39 cfs @ 0.67 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=79.98' (Free Discharge)
 ↑2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pre vs Post

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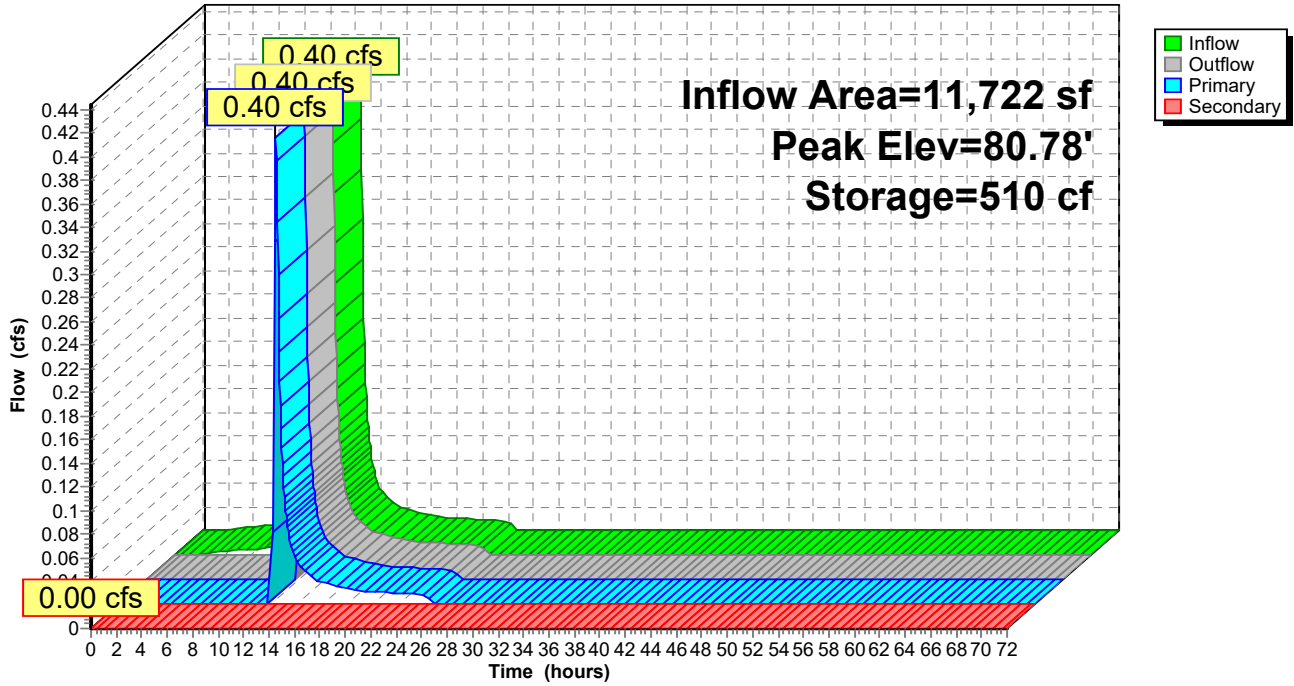
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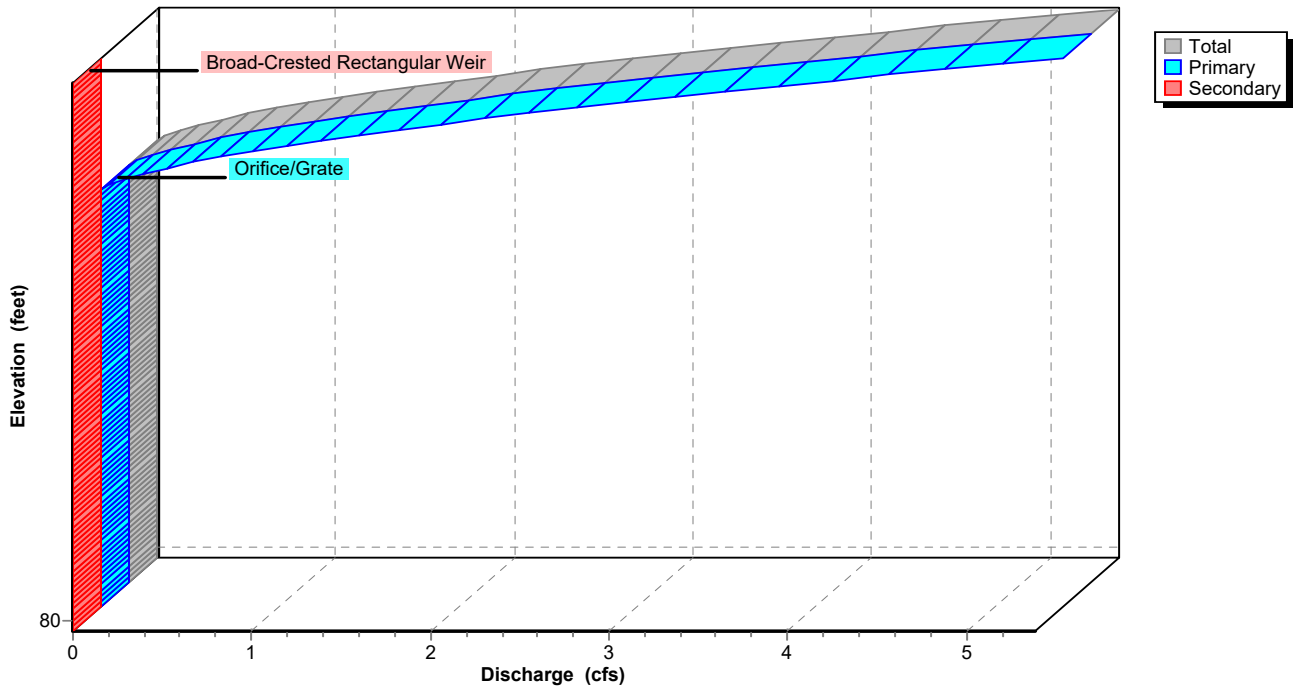
Pond B3: Bioretention Basin 3

Hydrograph



Pond B3: Bioretention Basin 3

Stage-Discharge



Pre vs Post

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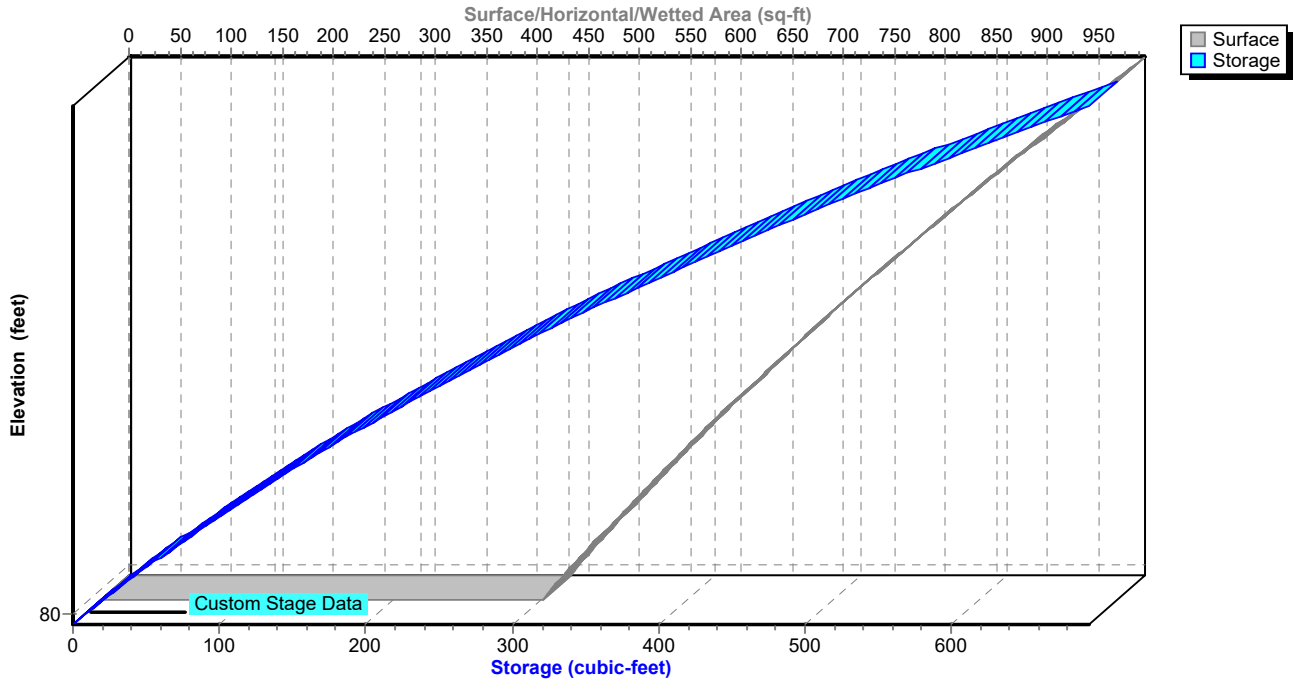
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Pond B3: Bioretention Basin 3

Stage-Area-Storage



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Stage-Discharge for Pond B3: Bioretention Basin 3

| Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) | Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) |
|---------------------|--------------------|------------------|--------------------|---------------------|--------------------|------------------|--------------------|
| 79.98 | 0.00 | 0.00 | 0.00 | 80.51 | 0.00 | 0.00 | 0.00 |
| 79.99 | 0.00 | 0.00 | 0.00 | 80.52 | 0.00 | 0.00 | 0.00 |
| 80.00 | 0.00 | 0.00 | 0.00 | 80.53 | 0.00 | 0.00 | 0.00 |
| 80.01 | 0.00 | 0.00 | 0.00 | 80.54 | 0.00 | 0.00 | 0.00 |
| 80.02 | 0.00 | 0.00 | 0.00 | 80.55 | 0.00 | 0.00 | 0.00 |
| 80.03 | 0.00 | 0.00 | 0.00 | 80.56 | 0.00 | 0.00 | 0.00 |
| 80.04 | 0.00 | 0.00 | 0.00 | 80.57 | 0.00 | 0.00 | 0.00 |
| 80.05 | 0.00 | 0.00 | 0.00 | 80.58 | 0.00 | 0.00 | 0.00 |
| 80.06 | 0.00 | 0.00 | 0.00 | 80.59 | 0.00 | 0.00 | 0.00 |
| 80.07 | 0.00 | 0.00 | 0.00 | 80.60 | 0.00 | 0.00 | 0.00 |
| 80.08 | 0.00 | 0.00 | 0.00 | 80.61 | 0.00 | 0.00 | 0.00 |
| 80.09 | 0.00 | 0.00 | 0.00 | 80.62 | 0.00 | 0.00 | 0.00 |
| 80.10 | 0.00 | 0.00 | 0.00 | 80.63 | 0.00 | 0.00 | 0.00 |
| 80.11 | 0.00 | 0.00 | 0.00 | 80.64 | 0.00 | 0.00 | 0.00 |
| 80.12 | 0.00 | 0.00 | 0.00 | 80.65 | 0.00 | 0.00 | 0.00 |
| 80.13 | 0.00 | 0.00 | 0.00 | 80.66 | 0.00 | 0.00 | 0.00 |
| 80.14 | 0.00 | 0.00 | 0.00 | 80.67 | 0.00 | 0.00 | 0.00 |
| 80.15 | 0.00 | 0.00 | 0.00 | 80.68 | 0.00 | 0.00 | 0.00 |
| 80.16 | 0.00 | 0.00 | 0.00 | 80.69 | 0.00 | 0.00 | 0.00 |
| 80.17 | 0.00 | 0.00 | 0.00 | 80.70 | 0.00 | 0.00 | 0.00 |
| 80.18 | 0.00 | 0.00 | 0.00 | 80.71 | 0.00 | 0.00 | 0.00 |
| 80.19 | 0.00 | 0.00 | 0.00 | 80.72 | 0.00 | 0.00 | 0.00 |
| 80.20 | 0.00 | 0.00 | 0.00 | 80.73 | 0.00 | 0.00 | 0.00 |
| 80.21 | 0.00 | 0.00 | 0.00 | 80.74 | 0.00 | 0.00 | 0.00 |
| 80.22 | 0.00 | 0.00 | 0.00 | 80.75 | 0.05 | 0.05 | 0.00 |
| 80.23 | 0.00 | 0.00 | 0.00 | 80.76 | 0.13 | 0.13 | 0.00 |
| 80.24 | 0.00 | 0.00 | 0.00 | 80.77 | 0.24 | 0.24 | 0.00 |
| 80.25 | 0.00 | 0.00 | 0.00 | 80.78 | 0.37 | 0.37 | 0.00 |
| 80.26 | 0.00 | 0.00 | 0.00 | 80.79 | 0.51 | 0.51 | 0.00 |
| 80.27 | 0.00 | 0.00 | 0.00 | 80.80 | 0.67 | 0.67 | 0.00 |
| 80.28 | 0.00 | 0.00 | 0.00 | 80.81 | 0.85 | 0.85 | 0.00 |
| 80.29 | 0.00 | 0.00 | 0.00 | 80.82 | 1.04 | 1.04 | 0.00 |
| 80.30 | 0.00 | 0.00 | 0.00 | 80.83 | 1.24 | 1.24 | 0.00 |
| 80.31 | 0.00 | 0.00 | 0.00 | 80.84 | 1.45 | 1.45 | 0.00 |
| 80.32 | 0.00 | 0.00 | 0.00 | 80.85 | 1.67 | 1.67 | 0.00 |
| 80.33 | 0.00 | 0.00 | 0.00 | 80.86 | 1.90 | 1.90 | 0.00 |
| 80.34 | 0.00 | 0.00 | 0.00 | 80.87 | 2.15 | 2.15 | 0.00 |
| 80.35 | 0.00 | 0.00 | 0.00 | 80.88 | 2.40 | 2.40 | 0.00 |
| 80.36 | 0.00 | 0.00 | 0.00 | 80.89 | 2.66 | 2.66 | 0.00 |
| 80.37 | 0.00 | 0.00 | 0.00 | 80.90 | 2.93 | 2.93 | 0.00 |
| 80.38 | 0.00 | 0.00 | 0.00 | 80.91 | 3.21 | 3.21 | 0.00 |
| 80.39 | 0.00 | 0.00 | 0.00 | 80.92 | 3.50 | 3.50 | 0.00 |
| 80.40 | 0.00 | 0.00 | 0.00 | 80.93 | 3.79 | 3.79 | 0.00 |
| 80.41 | 0.00 | 0.00 | 0.00 | 80.94 | 4.09 | 4.09 | 0.00 |
| 80.42 | 0.00 | 0.00 | 0.00 | 80.95 | 4.41 | 4.41 | 0.00 |
| 80.43 | 0.00 | 0.00 | 0.00 | 80.96 | 4.72 | 4.72 | 0.00 |
| 80.44 | 0.00 | 0.00 | 0.00 | 80.97 | 5.05 | 5.05 | 0.00 |
| 80.45 | 0.00 | 0.00 | 0.00 | 80.98 | 5.38 | 5.38 | 0.00 |
| 80.46 | 0.00 | 0.00 | 0.00 | | | | |
| 80.47 | 0.00 | 0.00 | 0.00 | | | | |
| 80.48 | 0.00 | 0.00 | 0.00 | | | | |
| 80.49 | 0.00 | 0.00 | 0.00 | | | | |
| 80.50 | 0.00 | 0.00 | 0.00 | | | | |

Pre vs Post

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Stage-Area-Storage for Pond B3: Bioretention Basin 3

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 79.98 | 432 | 0 | 80.51 | 702 | 298 |
| 79.99 | 436 | 4 | 80.52 | 707 | 305 |
| 80.00 | 441 | 9 | 80.53 | 713 | 312 |
| 80.01 | 446 | 13 | 80.54 | 719 | 319 |
| 80.02 | 450 | 18 | 80.55 | 725 | 326 |
| 80.03 | 455 | 22 | 80.56 | 730 | 333 |
| 80.04 | 459 | 27 | 80.57 | 736 | 341 |
| 80.05 | 464 | 31 | 80.58 | 742 | 348 |
| 80.06 | 469 | 36 | 80.59 | 748 | 355 |
| 80.07 | 473 | 41 | 80.60 | 754 | 363 |
| 80.08 | 478 | 45 | 80.61 | 760 | 371 |
| 80.09 | 483 | 50 | 80.62 | 766 | 378 |
| 80.10 | 487 | 55 | 80.63 | 772 | 386 |
| 80.11 | 492 | 60 | 80.64 | 778 | 394 |
| 80.12 | 497 | 65 | 80.65 | 784 | 401 |
| 80.13 | 502 | 70 | 80.66 | 790 | 409 |
| 80.14 | 507 | 75 | 80.67 | 796 | 417 |
| 80.15 | 511 | 80 | 80.68 | 802 | 425 |
| 80.16 | 516 | 85 | 80.69 | 808 | 433 |
| 80.17 | 521 | 90 | 80.70 | 814 | 441 |
| 80.18 | 526 | 96 | 80.71 | 820 | 450 |
| 80.19 | 531 | 101 | 80.72 | 826 | 458 |
| 80.20 | 536 | 106 | 80.73 | 833 | 466 |
| 80.21 | 541 | 112 | 80.74 | 839 | 474 |
| 80.22 | 546 | 117 | 80.75 | 845 | 483 |
| 80.23 | 551 | 123 | 80.76 | 851 | 491 |
| 80.24 | 556 | 128 | 80.77 | 858 | 500 |
| 80.25 | 561 | 134 | 80.78 | 864 | 508 |
| 80.26 | 566 | 139 | 80.79 | 870 | 517 |
| 80.27 | 571 | 145 | 80.80 | 877 | 526 |
| 80.28 | 577 | 151 | 80.81 | 883 | 535 |
| 80.29 | 582 | 157 | 80.82 | 889 | 544 |
| 80.30 | 587 | 162 | 80.83 | 896 | 552 |
| 80.31 | 592 | 168 | 80.84 | 902 | 561 |
| 80.32 | 597 | 174 | 80.85 | 909 | 571 |
| 80.33 | 603 | 180 | 80.86 | 915 | 580 |
| 80.34 | 608 | 186 | 80.87 | 922 | 589 |
| 80.35 | 613 | 192 | 80.88 | 928 | 598 |
| 80.36 | 619 | 199 | 80.89 | 935 | 607 |
| 80.37 | 624 | 205 | 80.90 | 941 | 617 |
| 80.38 | 629 | 211 | 80.91 | 948 | 626 |
| 80.39 | 635 | 217 | 80.92 | 955 | 636 |
| 80.40 | 640 | 224 | 80.93 | 961 | 645 |
| 80.41 | 646 | 230 | 80.94 | 968 | 655 |
| 80.42 | 651 | 237 | 80.95 | 975 | 665 |
| 80.43 | 657 | 243 | 80.96 | 981 | 674 |
| 80.44 | 662 | 250 | 80.97 | 988 | 684 |
| 80.45 | 668 | 256 | 80.98 | 995 | 694 |
| 80.46 | 673 | 263 | | | |
| 80.47 | 679 | 270 | | | |
| 80.48 | 685 | 277 | | | |
| 80.49 | 690 | 284 | | | |
| 80.50 | 696 | 291 | | | |

Pre vs Post

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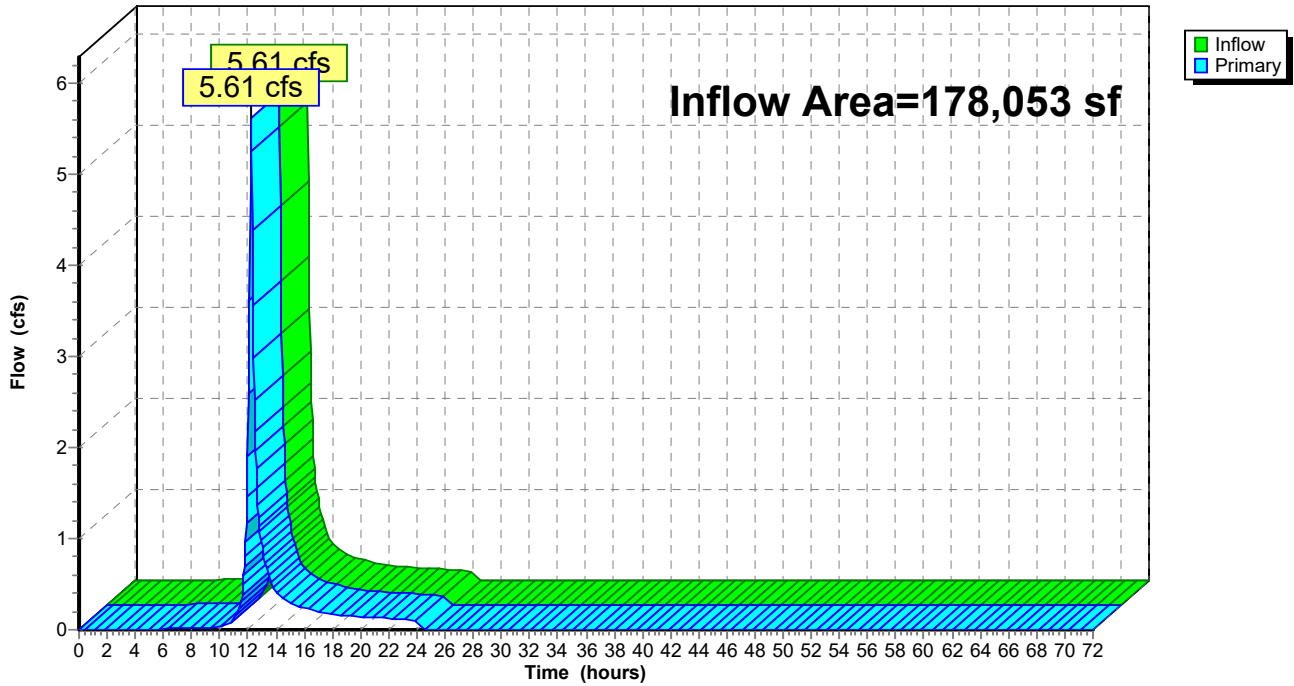
Summary for Link 5E: EDA 1

Inflow Area = 178,053 sf, 5.81% Impervious, Inflow Depth = 1.37" for 2-Year event
Inflow = 5.61 cfs @ 12.21 hrs, Volume= 20,371 cf
Primary = 5.61 cfs @ 12.21 hrs, Volume= 20,371 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5E: EDA 1

Hydrograph



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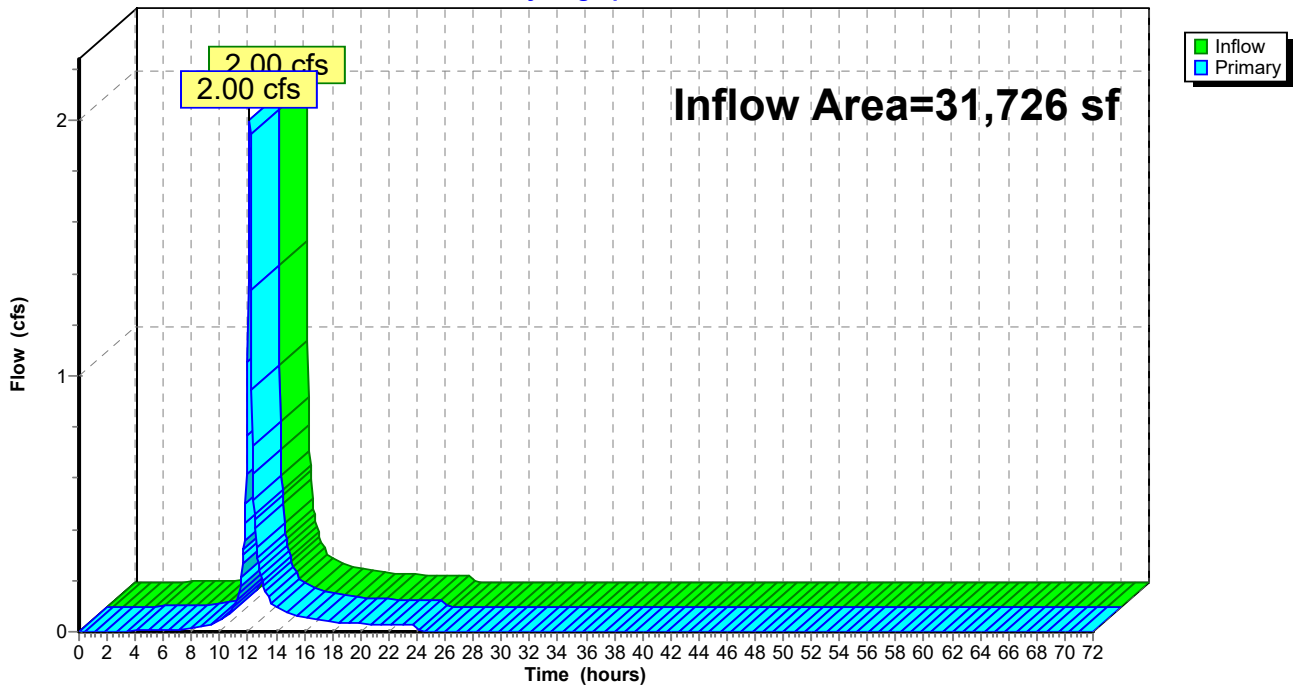
Summary for Link 6E: EDA 2

Inflow Area = 31,726 sf, 17.78% Impervious, Inflow Depth = 2.25" for 2-Year event
Inflow = 2.00 cfs @ 12.13 hrs, Volume= 5,941 cf
Primary = 2.00 cfs @ 12.13 hrs, Volume= 5,941 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 6E: EDA 2

Hydrograph



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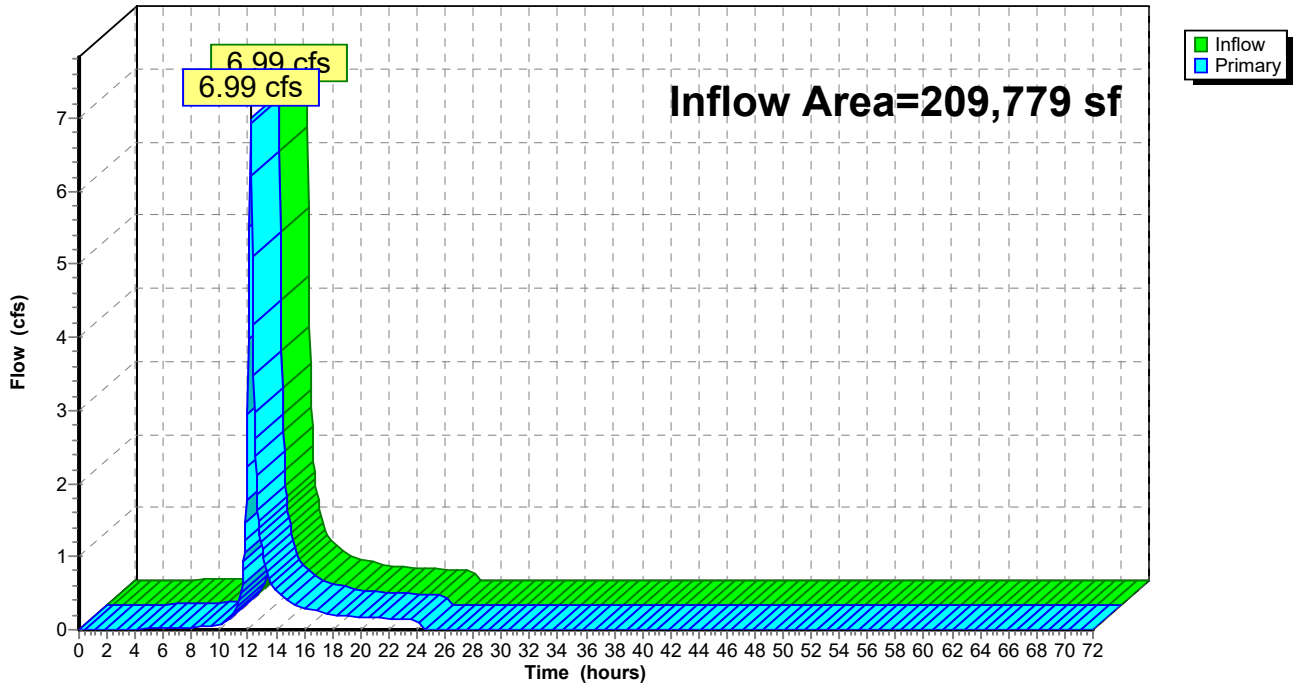
Summary for Link 7E: EDA

Inflow Area = 209,779 sf, 7.62% Impervious, Inflow Depth = 1.51" for 2-Year event
Inflow = 6.99 cfs @ 12.18 hrs, Volume= 26,313 cf
Primary = 6.99 cfs @ 12.18 hrs, Volume= 26,313 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 7E: EDA

Hydrograph



Pre vs Post

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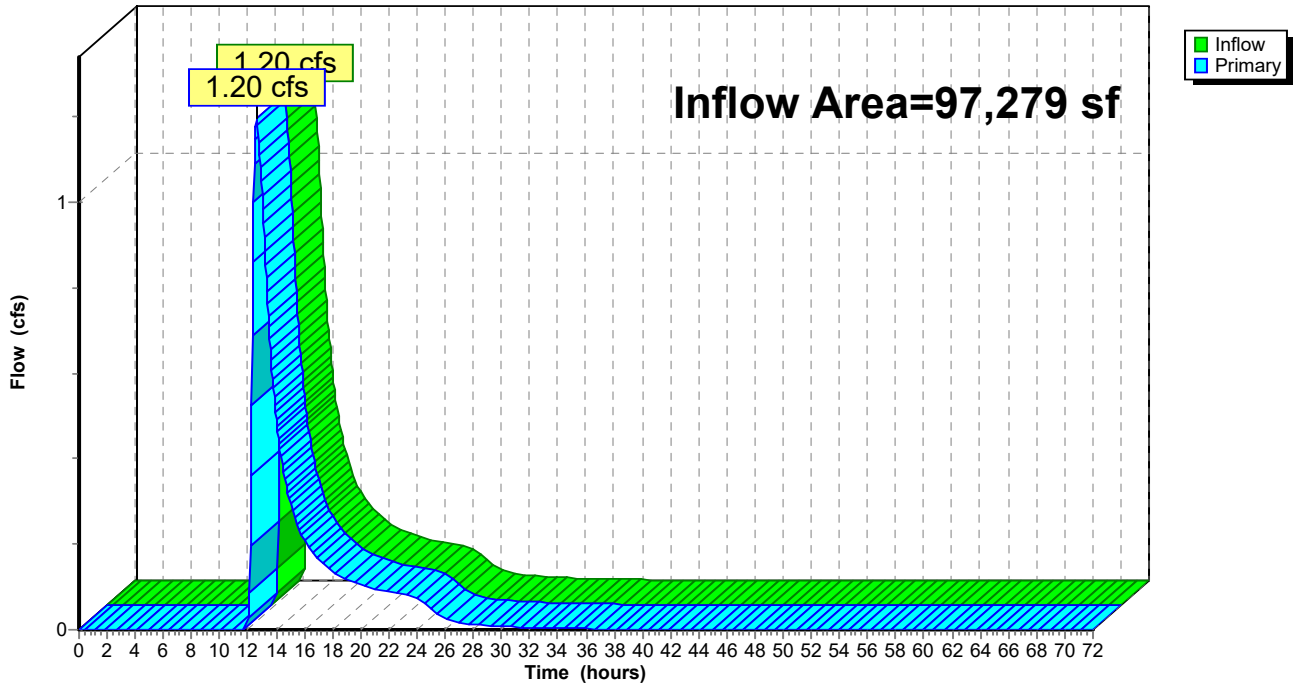
Summary for Link 10P: PDA 1A

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth > 1.48" for 2-Year event
Inflow = 1.20 cfs @ 12.63 hrs, Volume= 11,962 cf
Primary = 1.20 cfs @ 12.63 hrs, Volume= 11,962 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 10P: PDA 1A

Hydrograph



Pre vs Post

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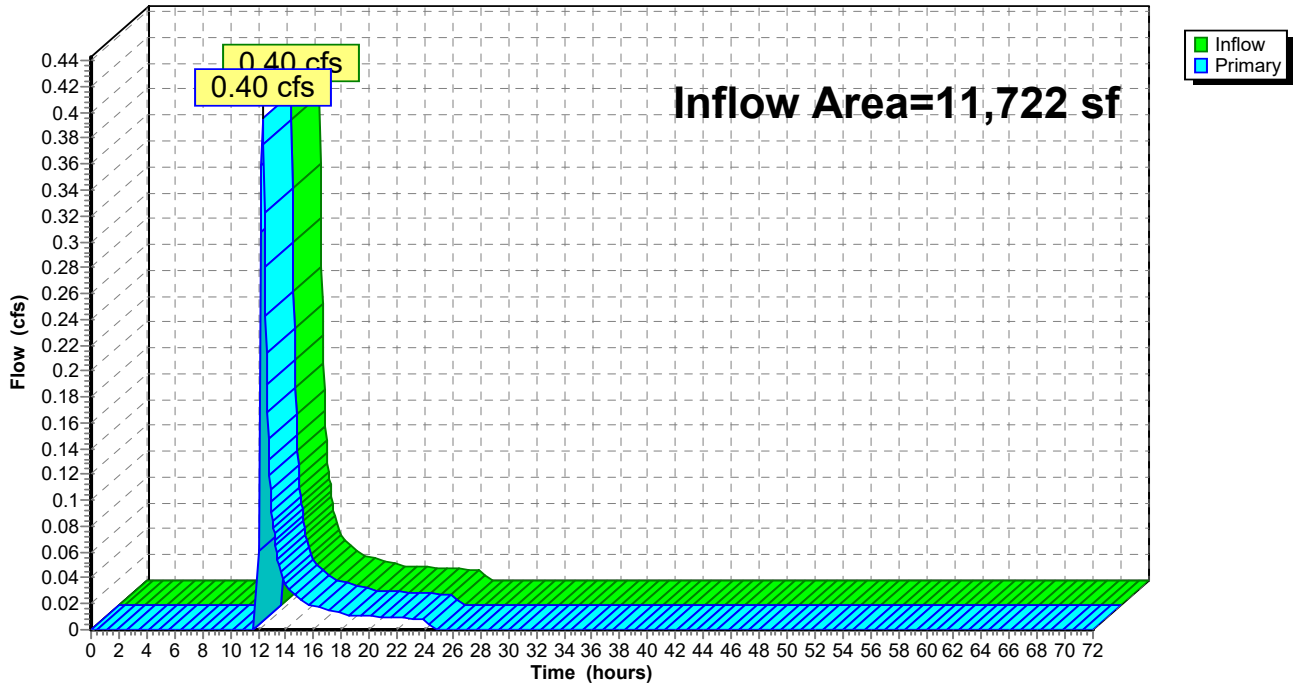
Summary for Link 11P: PDA 1B

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 1.47" for 2-Year event
Inflow = 0.40 cfs @ 12.32 hrs, Volume= 1,439 cf
Primary = 0.40 cfs @ 12.32 hrs, Volume= 1,439 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 11P: PDA 1B

Hydrograph



Pre vs Post

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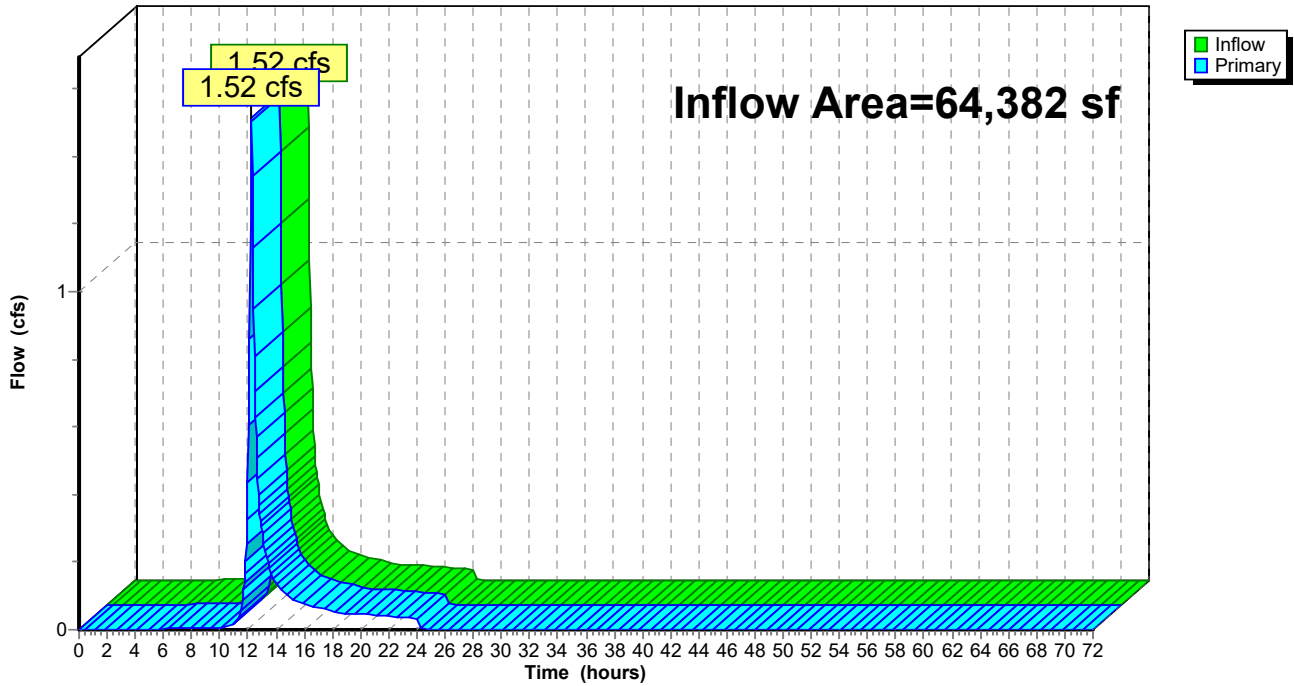
Summary for Link 12P: PDA 1C

Inflow Area = 64,382 sf, 3.87% Impervious, Inflow Depth = 1.11" for 2-Year event
Inflow = 1.52 cfs @ 12.23 hrs, Volume= 5,964 cf
Primary = 1.52 cfs @ 12.23 hrs, Volume= 5,964 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 12P: PDA 1C

Hydrograph



Pre vs Post

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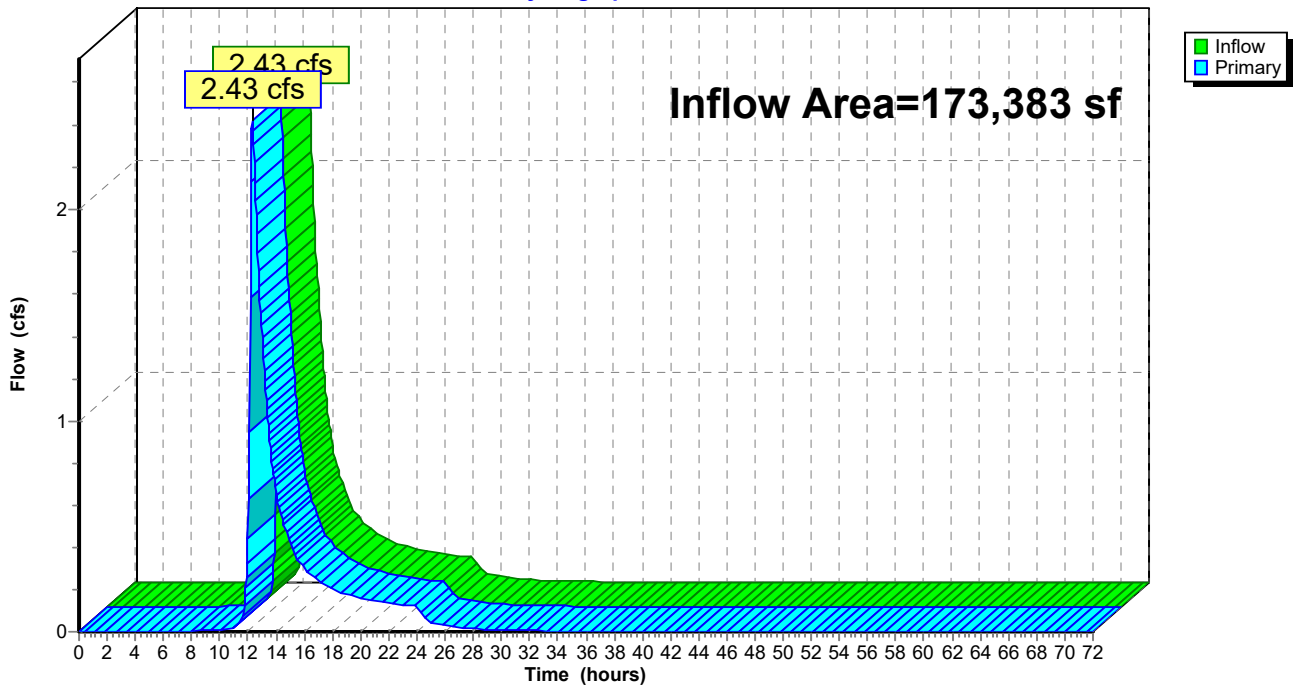
Summary for Link 13P: PDA 1

Inflow Area = 173,383 sf, 38.29% Impervious, Inflow Depth = 1.34" for 2-Year event
Inflow = 2.43 cfs @ 12.30 hrs, Volume= 19,365 cf
Primary = 2.43 cfs @ 12.30 hrs, Volume= 19,365 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 13P: PDA 1

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

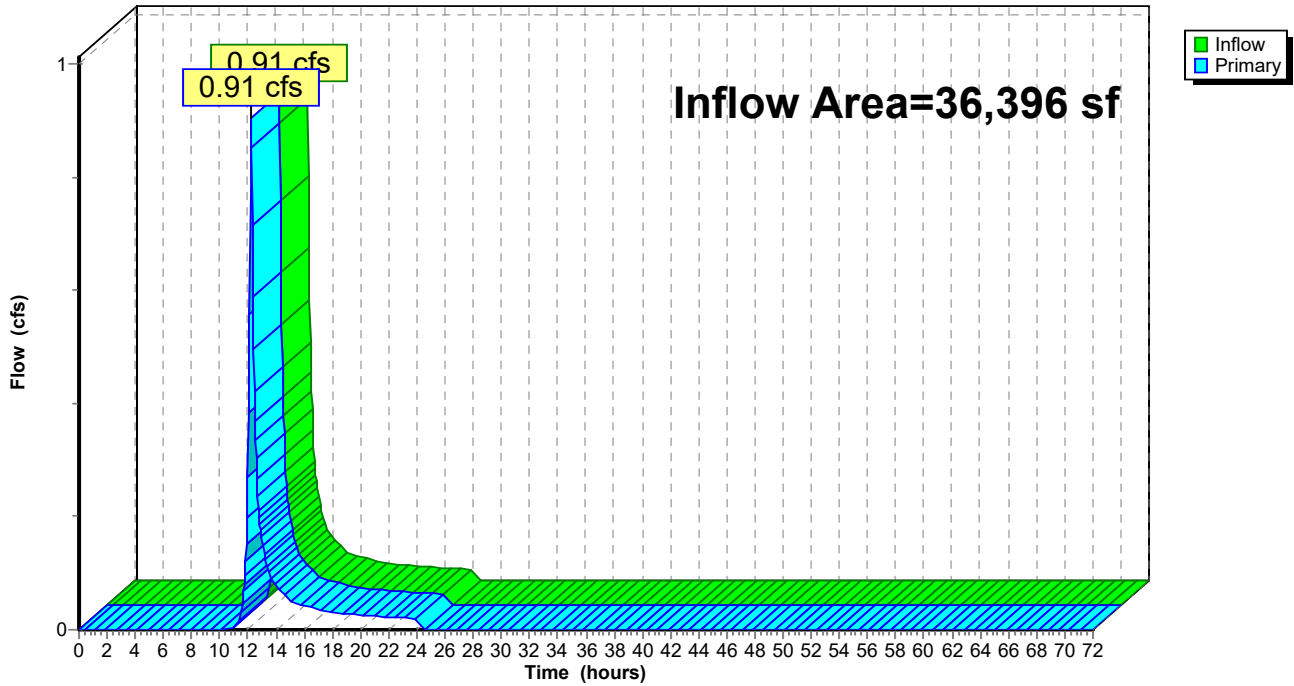
Summary for Link 14P: PDA 2

Inflow Area = 36,396 sf, 0.00% Impervious, Inflow Depth = 1.09" for 2-Year event
Inflow = 0.91 cfs @ 12.21 hrs, Volume= 3,296 cf
Primary = 0.91 cfs @ 12.21 hrs, Volume= 3,296 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 14P: PDA 2

Hydrograph



Pre vs Post

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NOAA 24-hr C 2-Year Rainfall=3.36"

Printed 5/14/2021

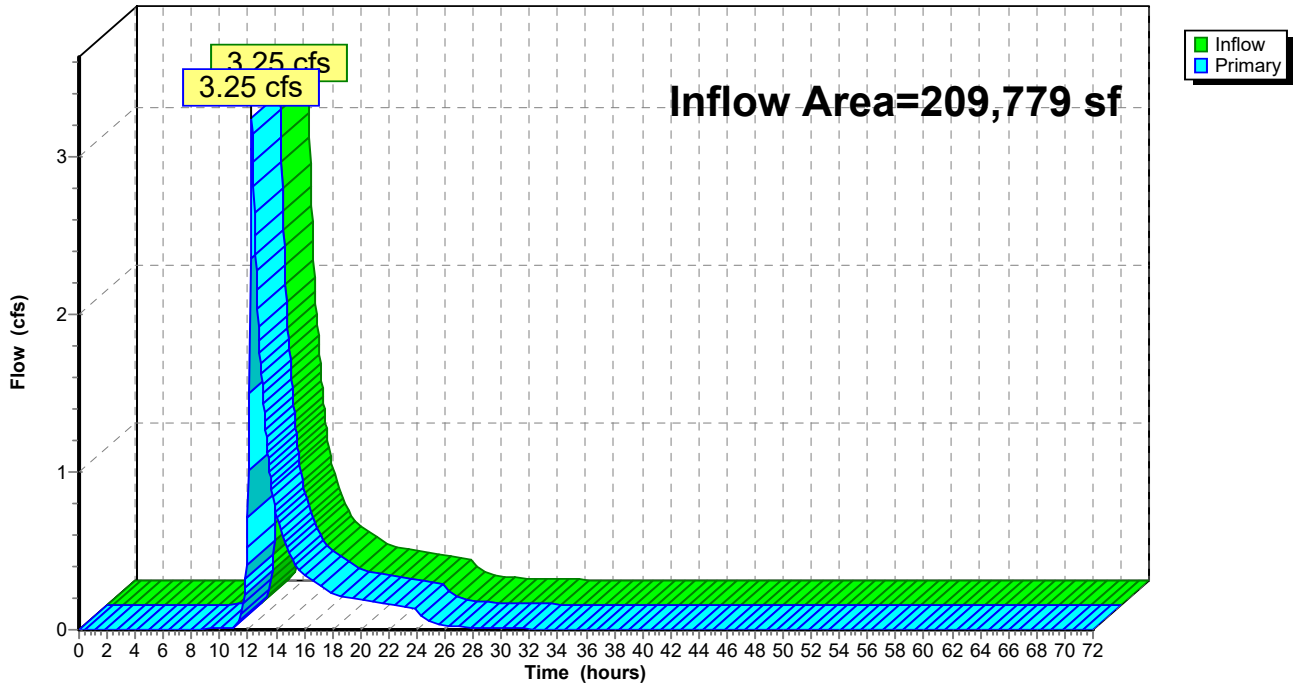
Summary for Link 15P: PDA

Inflow Area = 209,779 sf, 31.65% Impervious, Inflow Depth = 1.30" for 2-Year event
Inflow = 3.25 cfs @ 12.26 hrs, Volume= 22,660 cf
Primary = 3.25 cfs @ 12.26 hrs, Volume= 22,660 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 15P: PDA

Hydrograph



Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

Prepared by {enter your company name here}

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

| | |
|--------------------------------------|---|
| Subcatchment 1E: Impervious | Runoff Area=10,351 sf 100.00% Impervious Runoff Depth=4.94" Tc=12.4 min CN=0/98 Runoff=1.05 cfs 4,264 cf |
| Subcatchment 1P: Impervious | Runoff Area=23,576 sf 100.00% Impervious Runoff Depth=4.94" Tc=10.7 min CN=0/98 Runoff=2.50 cfs 9,711 cf |
| Subcatchment 2E: Pervious | Runoff Area=167,702 sf 0.00% Impervious Runoff Depth=2.68" Flow Length=630' Tc=12.4 min CN=76/0 Runoff=10.69 cfs 37,517 cf |
| Subcatchment 2P: Pervious | Runoff Area=24,672 sf 0.00% Impervious Runoff Depth=2.51" Flow Length=426' Tc=10.7 min CN=74/0 Runoff=1.54 cfs 5,158 cf |
| Subcatchment 3E: Impervious | Runoff Area=5,641 sf 100.00% Impervious Runoff Depth=4.94" Tc=6.0 min CN=0/98 Runoff=0.69 cfs 2,324 cf |
| Subcatchment 3P: Roof Area | Runoff Area=35,418 sf 100.00% Impervious Runoff Depth=4.94" Tc=10.7 min CN=0/98 Runoff=3.76 cfs 14,589 cf |
| Subcatchment 4E: Pervious | Runoff Area=26,085 sf 0.00% Impervious Runoff Depth=3.74" Flow Length=393' Tc=6.0 min CN=87/0 Runoff=2.75 cfs 8,124 cf |
| Subcatchment 4P: Pervious | Runoff Area=13,613 sf 0.00% Impervious Runoff Depth=2.51" Tc=10.7 min CN=74/0 Runoff=0.85 cfs 2,846 cf |
| Subcatchment 5P: Impervious | Runoff Area=5,021 sf 97.63% Impervious Runoff Depth=4.94" Tc=20.8 min CN=96/98 Runoff=0.41 cfs 2,066 cf |
| Subcatchment 6P: Pervious | Runoff Area=6,701 sf 0.00% Impervious Runoff Depth=2.42" Flow Length=172' Tc=20.8 min CN=73/0 Runoff=0.31 cfs 1,353 cf |
| Subcatchment 7P: Impervious | Runoff Area=2,493 sf 100.00% Impervious Runoff Depth=4.94" Tc=13.9 min CN=0/98 Runoff=0.24 cfs 1,027 cf |
| Subcatchment 8P: Pervious | Runoff Area=61,889 sf 0.00% Impervious Runoff Depth=2.34" Flow Length=409' Tc=13.9 min CN=72/0 Runoff=3.24 cfs 12,055 cf |
| Subcatchment 9P: Pervious | Runoff Area=36,396 sf 0.00% Impervious Runoff Depth=2.42" Flow Length=471' Tc=12.2 min CN=73/0 Runoff=2.10 cfs 7,347 cf |
| Pond B1: Bioretention Basin 1 | Peak Elev=78.34' Storage=4,464 cf Inflow=4.04 cfs 14,869 cf Outflow=3.92 cfs 10,974 cf |
| Pond B2: Bioretention Basin 2 | Peak Elev=77.94' Storage=11,272 cf Inflow=8.46 cfs 28,409 cf Outflow=3.21 cfs 25,242 cf |
| Pond B3: Bioretention Basin 3 | Peak Elev=80.80' Storage=528 cf Inflow=0.72 cfs 3,419 cf Primary=0.72 cfs 2,944 cf Secondary=0.00 cfs 0 cf Outflow=0.72 cfs 2,944 cf |

Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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| | |
|-------------------------|---|
| Link 5E: EDA 1 | Inflow=11.74 cfs 41,781 cf Primary=11.74 cfs 41,781 cf |
| Link 6E: EDA 2 | Inflow=3.44 cfs 10,447 cf Primary=3.44 cfs 10,447 cf |
| Link 7E: EDA | Inflow=14.14 cfs 52,228 cf Primary=14.14 cfs 52,228 cf |
| Link 10P: PDA 1A | Inflow=3.21 cfs 25,242 cf Primary=3.21 cfs 25,242 cf |
| Link 11P: PDA 1B | Inflow=0.72 cfs 2,944 cf Primary=0.72 cfs 2,944 cf |
| Link 12P: PDA 1C | Inflow=3.50 cfs 13,082 cf Primary=3.50 cfs 13,082 cf |
| Link 13P: PDA 1 | Inflow=6.33 cfs 41,268 cf Primary=6.33 cfs 41,268 cf |
| Link 14P: PDA 2 | Inflow=2.10 cfs 7,347 cf Primary=2.10 cfs 7,347 cf |
| Link 15P: PDA | Inflow=8.20 cfs 48,616 cf Primary=8.20 cfs 48,616 cf |

Total Runoff Area = 419,558 sf Runoff Volume = 108,380 cf Average Runoff Depth = 3.10"
80.36% Pervious = 337,177 sf 19.64% Impervious = 82,381 sf

Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

Summary for Subcatchment 1E: Impervious

Runoff = 1.05 cfs @ 12.20 hrs, Volume= 4,264 cf, Depth= 4.94"

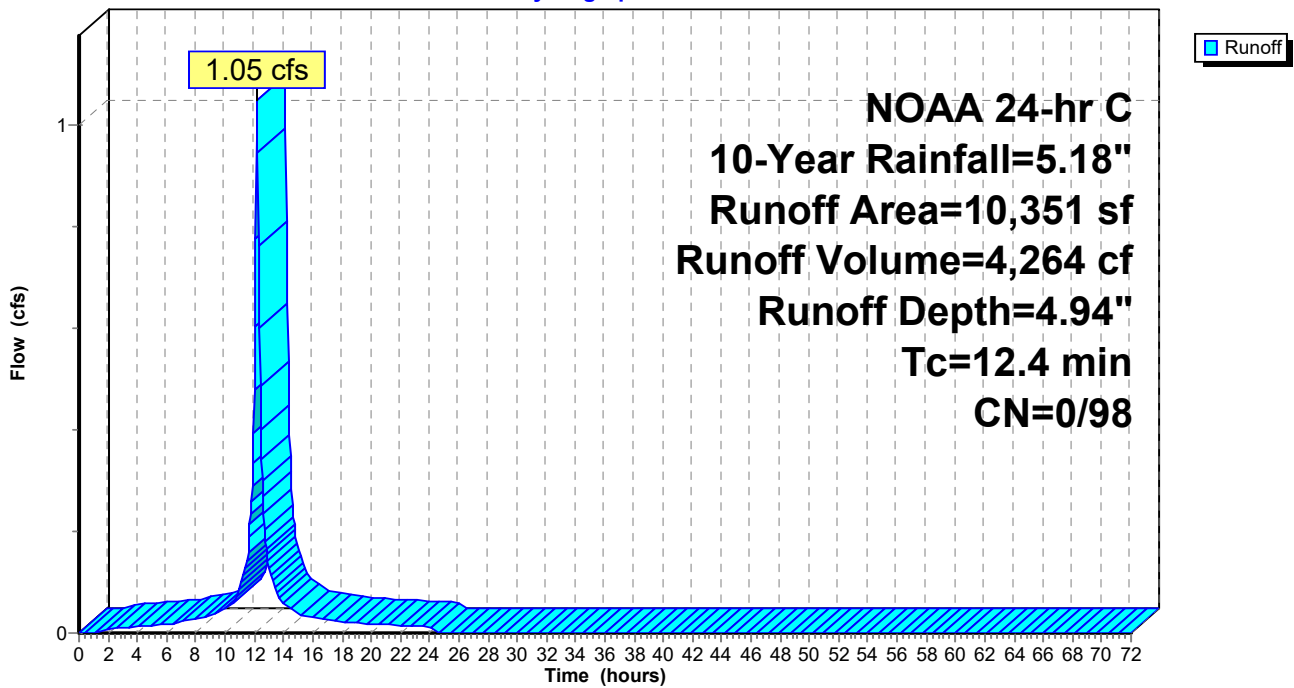
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 3,299 | 98 | Unconnected roofs, HSG C |
| 7,052 | 98 | Paved parking, HSG C |
| 10,351 | 98 | Weighted Average |
| 10,351 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 12.4 | | | | | Direct Entry, Tc |

Subcatchment 1E: Impervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 1P: Impervious

Runoff = 2.50 cfs @ 12.18 hrs, Volume= 9,711 cf, Depth= 4.94"

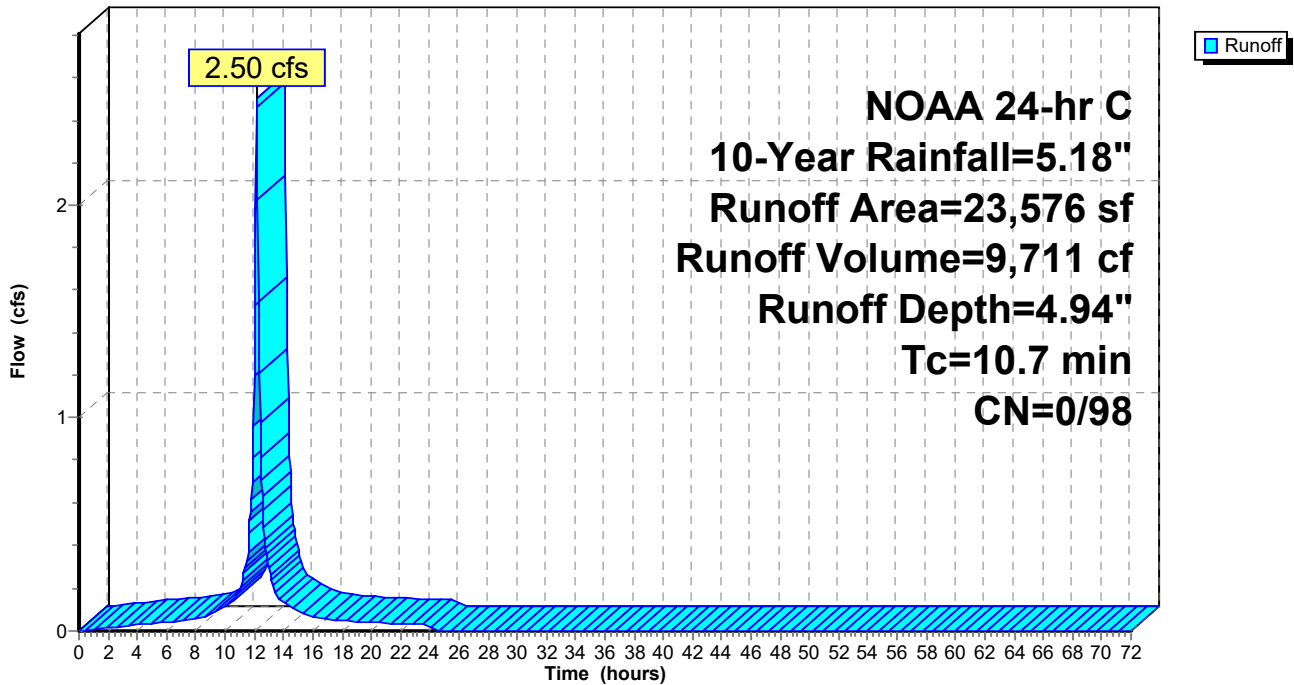
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 23,576 | 98 | Paved parking, HSG C |
| 23,576 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 1P: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 2E: Pervious

Runoff = 10.69 cfs @ 12.20 hrs, Volume= 37,517 cf, Depth= 2.68"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 24,589 | 96 | Gravel surface, HSG C |
| 36,591 | 70 | Woods, Good, HSG C |
| 105,816 | 74 | >75% Grass cover, Good, HSG C |
| 706 | 72 | Woods/grass comb., Good, HSG C |
| 167,702 | 76 | Weighted Average |
| 167,702 | 76 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 0.3 | 27 | 0.0490 | 1.55 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 8.8 | 73 | 0.0130 | 0.14 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.4 | 54 | 0.0180 | 2.16 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 1.2 | 207 | 0.0340 | 2.97 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.5 | 59 | 0.0170 | 2.10 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 0.2 | 43 | 0.0470 | 3.49 | | Shallow Concentrated Flow, F-G Unpaved Kv= 16.1 fps |
| 1.0 | 167 | 0.0280 | 2.69 | | Shallow Concentrated Flow, G-H Unpaved Kv= 16.1 fps |
| 12.4 | 630 | Total | | | |

Pre vs Post

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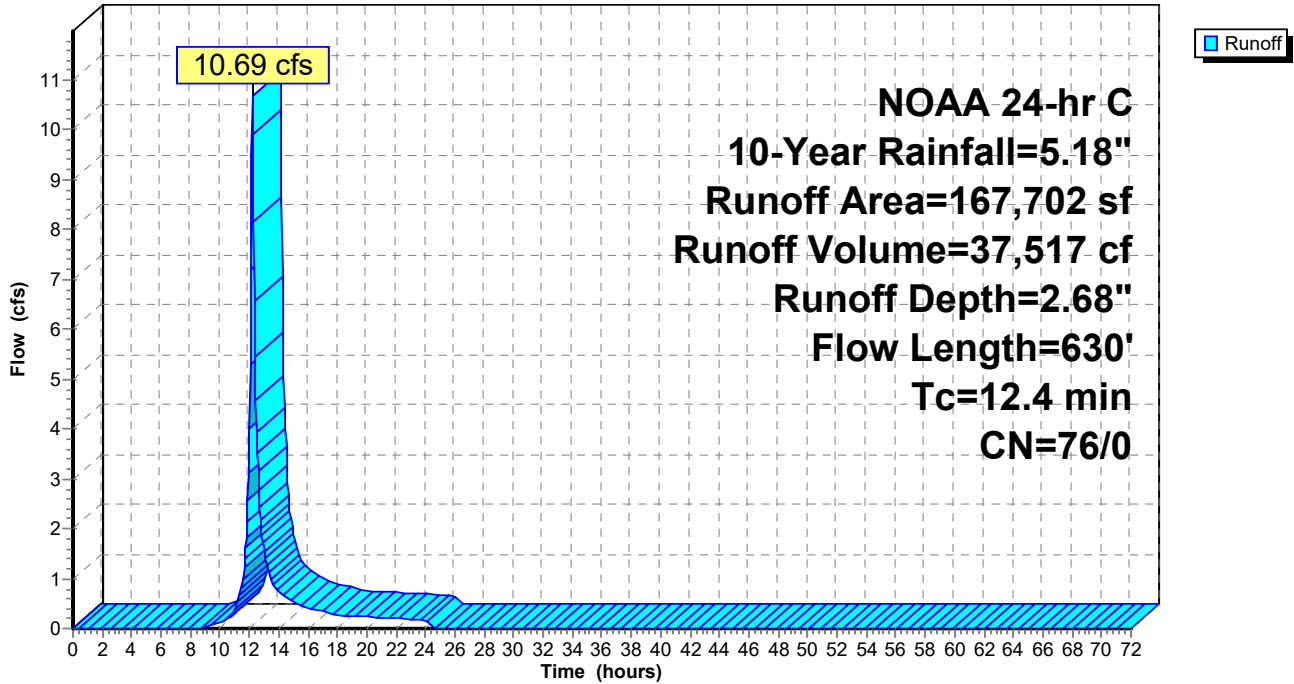
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NOAA 24-hr C 10-Year Rainfall=5.18"

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Subcatchment 2E: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

Summary for Subcatchment 2P: Pervious

Runoff = 1.54 cfs @ 12.19 hrs, Volume= 5,158 cf, Depth= 2.51"

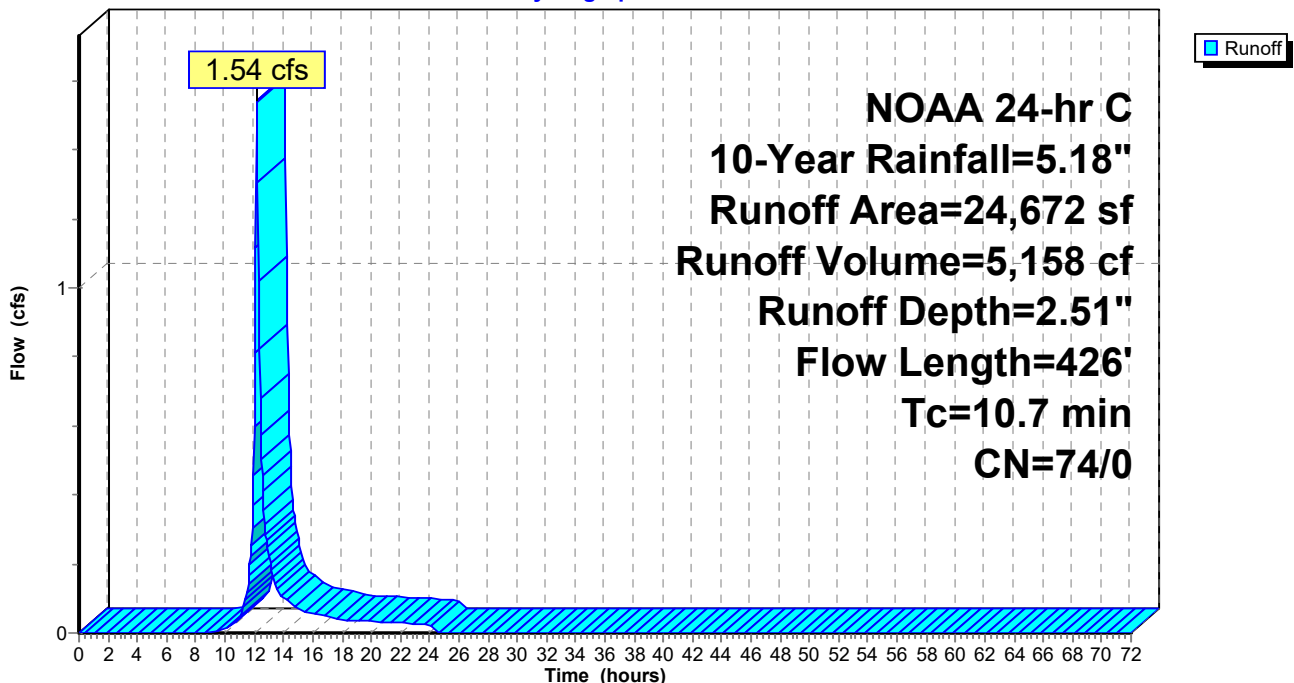
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 22,852 | 74 | >75% Grass cover, Good, HSG C |
| 1,820 | 72 | Woods/grass comb., Good, HSG C |
| 24,672 | 74 | Weighted Average |
| 24,672 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 9.2 | 100 | 0.0222 | 0.18 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.1 | 23 | 0.0730 | 4.35 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.3 | 48 | 0.0210 | 2.94 | | Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps |
| 1.1 | 255 | 0.0050 | 3.72 | 4.57 | Pipe Channel, D-E 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013 Concrete pipe, bends & connections |
| 10.7 | 426 | Total | | | |

Subcatchment 2P: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 3E: Impervious

Runoff = 0.69 cfs @ 12.13 hrs, Volume= 2,324 cf, Depth= 4.94"

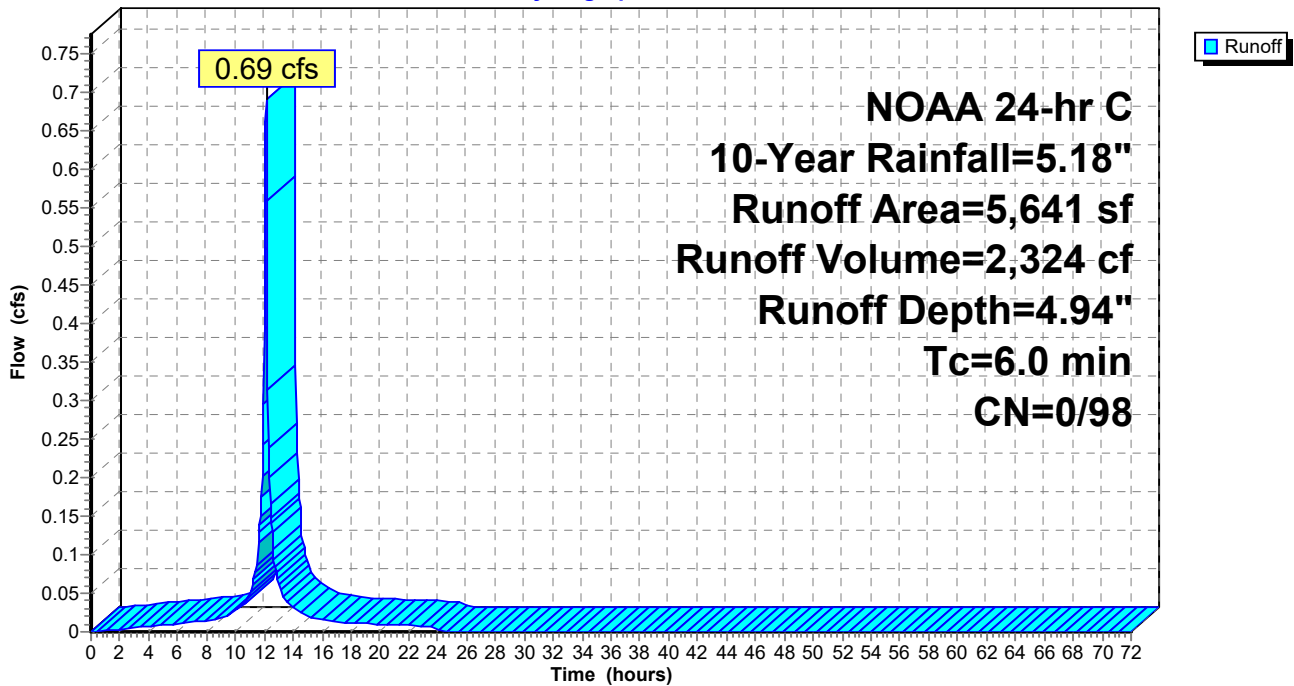
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 2,580 | 98 | Unconnected roofs, HSG C |
| 3,061 | 98 | Paved parking, HSG C |
| 5,641 | 98 | Weighted Average |
| 5,641 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|-------------------------|
| 3.0 | | | | | Direct Entry, Tc |
| 3.0 | 0 | Total, Increased to minimum Tc = 6.0 min | | | |

Subcatchment 3E: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 3P: Roof Area

Runoff = 3.76 cfs @ 12.18 hrs, Volume= 14,589 cf, Depth= 4.94"

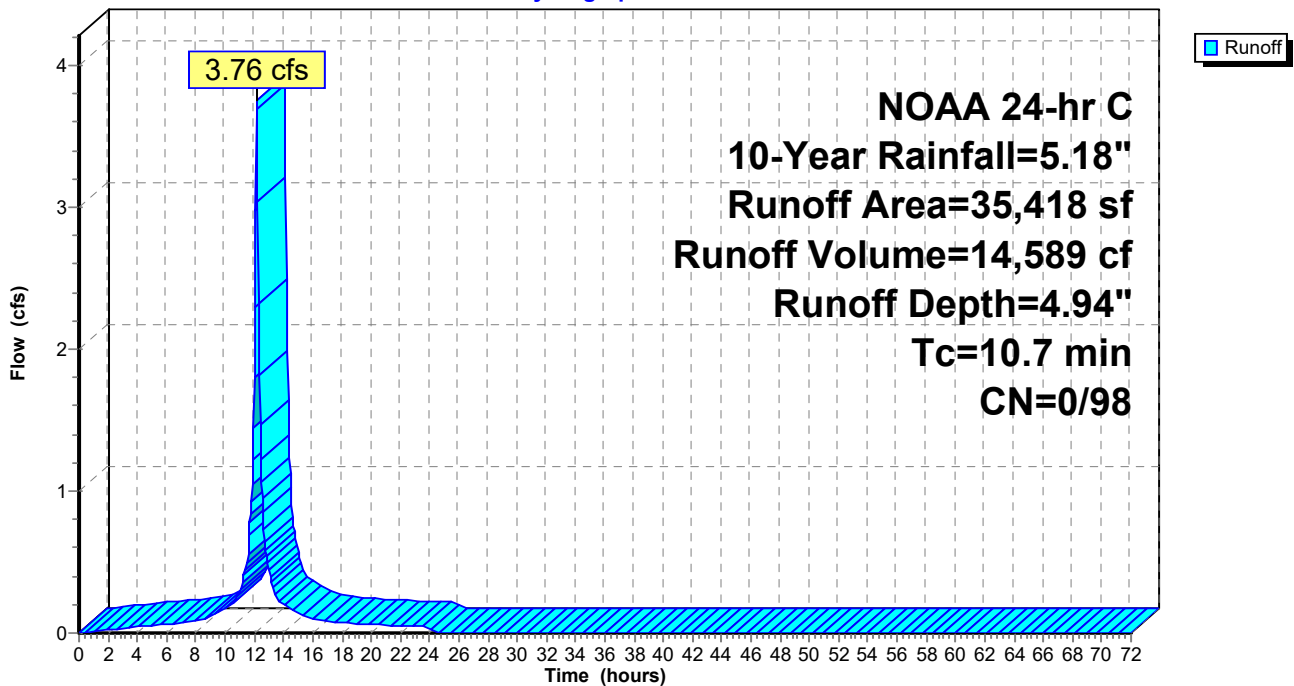
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|-----------------------------|
| 35,068 | 98 | Unconnected roofs, HSG C |
| 350 | 98 | Unconnected pavement, HSG C |
| 35,418 | 98 | Weighted Average |
| 35,418 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 3P: Roof Area

Hydrograph



Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 4E: Pervious

Runoff = 2.75 cfs @ 12.13 hrs, Volume= 8,124 cf, Depth= 3.74"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 164 | 70 | Woods, Good, HSG C |
| 16,189 | 96 | Gravel surface, HSG C |
| 5,108 | 74 | >75% Grass cover, Good, HSG C |
| 4,624 | 72 | Woods/grass comb., Good, HSG C |
| 26,085 | 87 | Weighted Average |
| 26,085 | 87 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|---|
| 1.3 | 100 | 0.0160 | 1.29 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 0.6 | 97 | 0.0200 | 2.87 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 1.0 | 175 | 0.0330 | 2.92 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.1 | 13 | 0.0230 | 2.44 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.0 | 8 | 0.0480 | 3.53 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 3.0 | 393 | Total, Increased to minimum Tc = 6.0 min | | | |

Pre vs Post

Prepared by {enter your company name here}

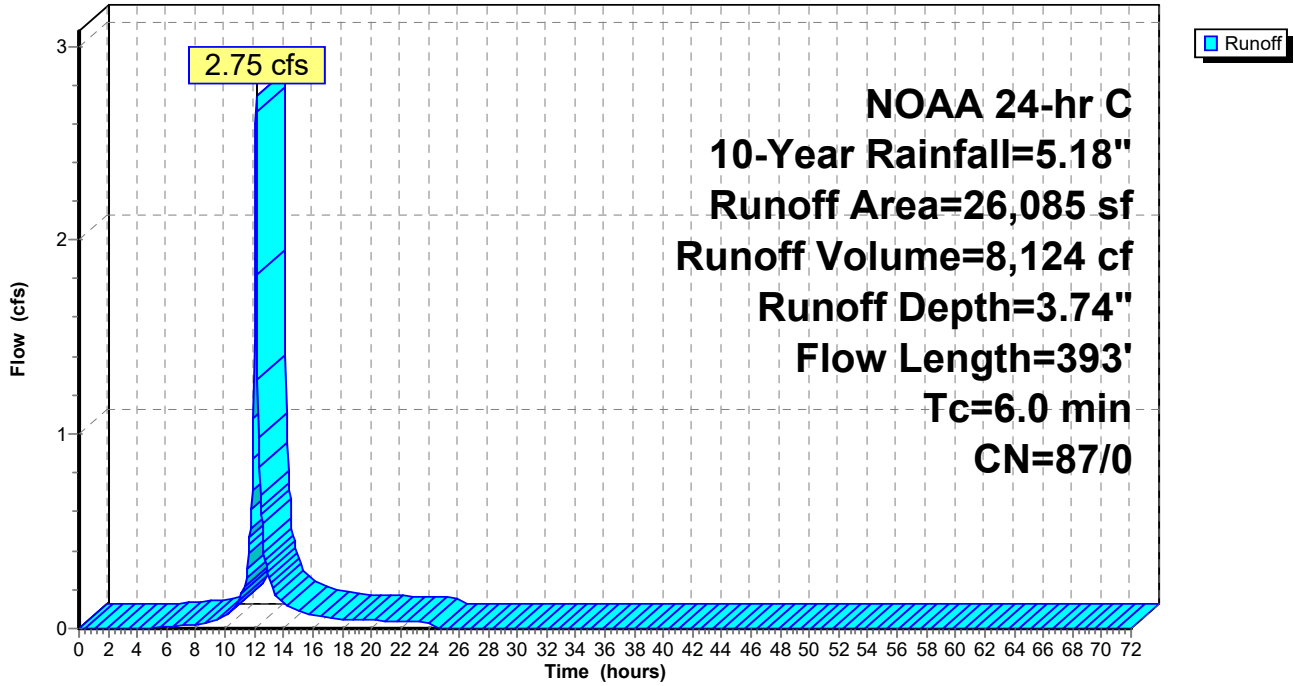
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Subcatchment 4E: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

Summary for Subcatchment 4P: Pervious

Runoff = 0.85 cfs @ 12.19 hrs, Volume= 2,846 cf, Depth= 2.51"

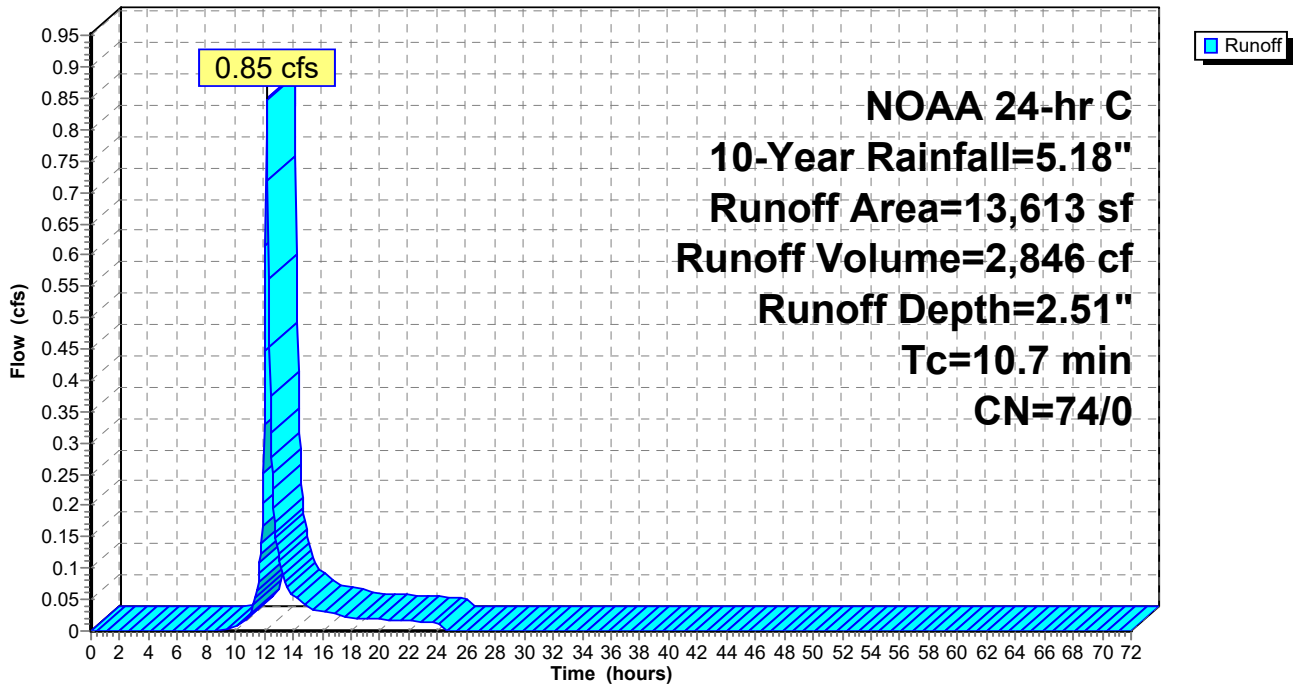
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 13,613 | 74 | >75% Grass cover, Good, HSG C |
| 13,613 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 4P: Pervious

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 5P: Impervious

Runoff = 0.41 cfs @ 12.29 hrs, Volume= 2,066 cf, Depth= 4.94"

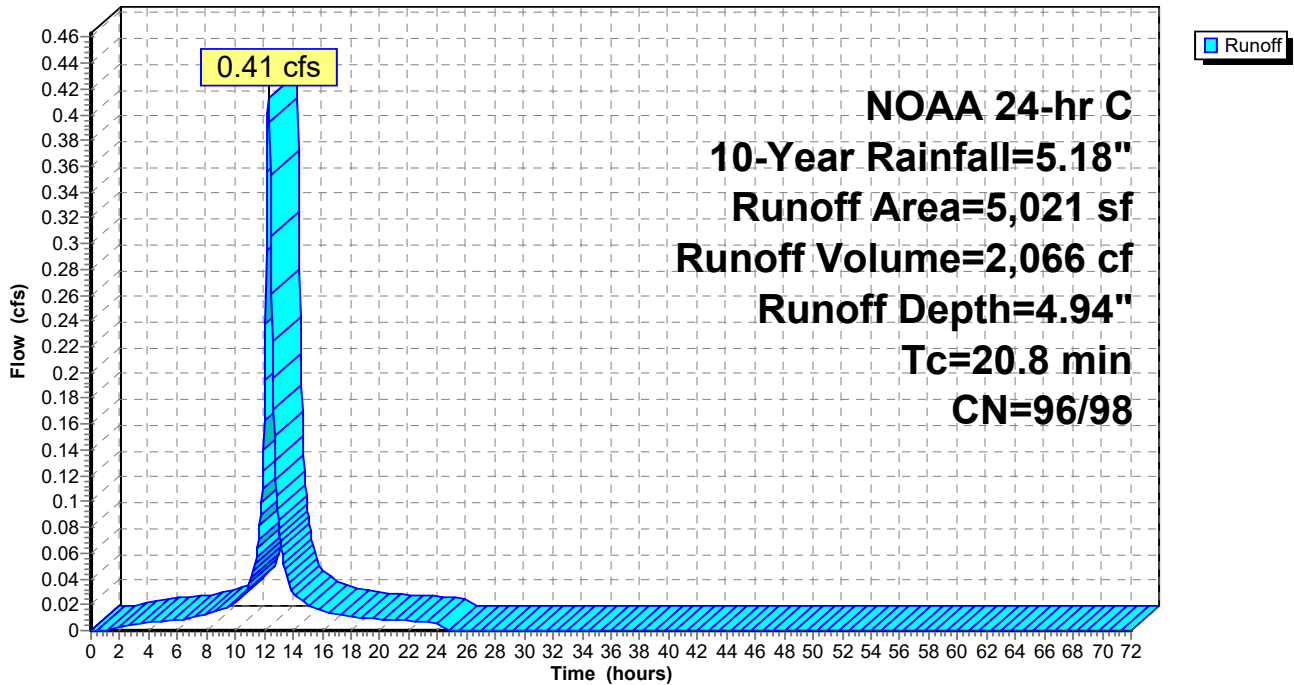
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|------------------------|
| 4,902 | 98 | Paved parking, HSG C |
| 119 | 96 | Gravel surface, HSG C |
| 5,021 | 98 | Weighted Average |
| 119 | 96 | 2.37% Pervious Area |
| 4,902 | 98 | 97.63% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 20.8 | | | | | Direct Entry, Tc |

Subcatchment 5P: Impervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

Summary for Subcatchment 6P: Pervious

Runoff = 0.31 cfs @ 12.31 hrs, Volume= 1,353 cf, Depth= 2.42"

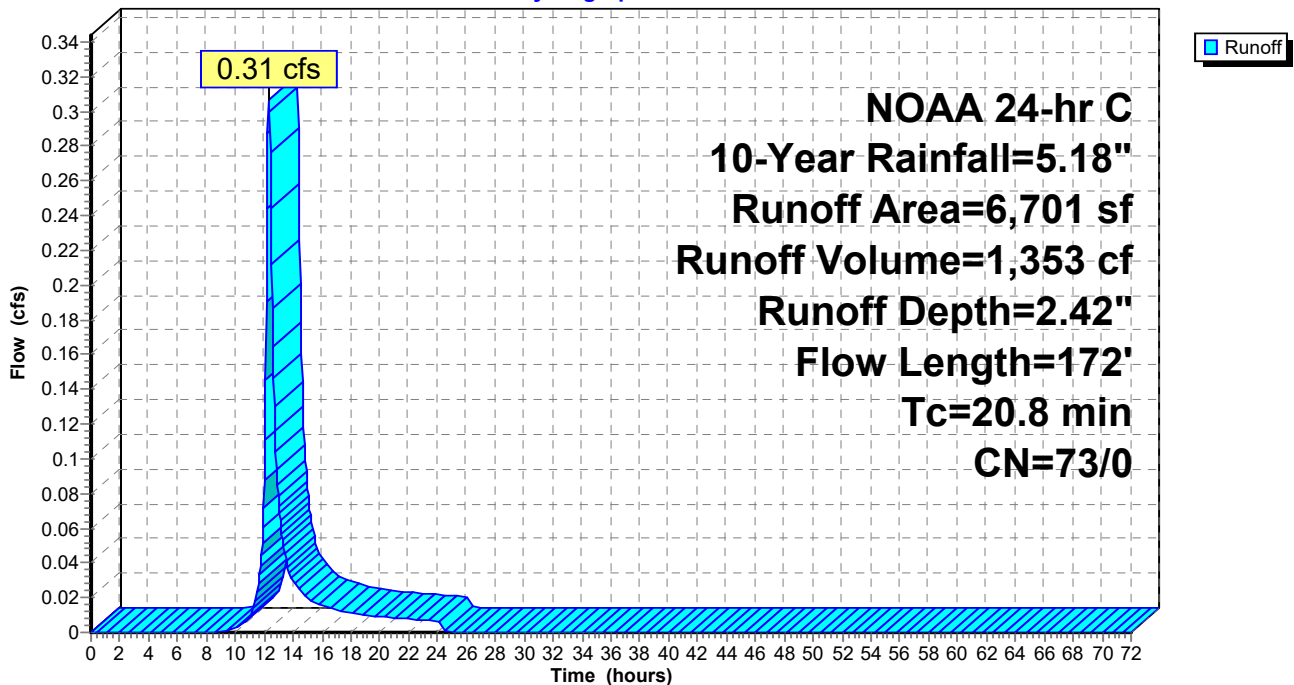
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 4,509 | 74 | >75% Grass cover, Good, HSG C |
| 2,192 | 70 | Woods, Good, HSG C |
| 6,701 | 73 | Weighted Average |
| 6,701 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 20.4 | 104 | 0.0230 | 0.08 | | Sheet Flow, A-B Woods: Light underbrush n= 0.400 P2= 3.36" |
| 0.3 | 57 | 0.0230 | 3.08 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 0.1 | 11 | 0.0200 | 2.28 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 20.8 | 172 | Total | | | |

Subcatchment 6P: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 7P: Impervious

Runoff = 0.24 cfs @ 12.21 hrs, Volume= 1,027 cf, Depth= 4.94"

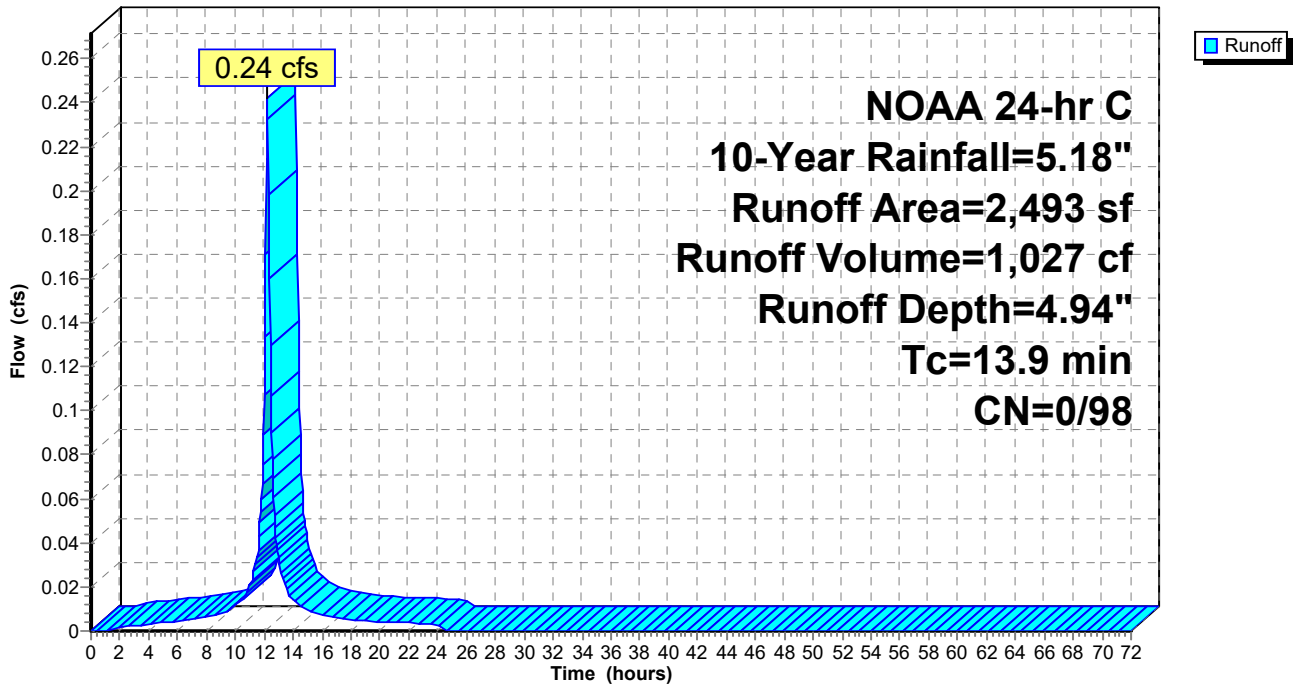
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,493 | 98 | Paved parking, HSG C |
| 2,493 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 13.9 | | | | | Direct Entry, Tc |

Subcatchment 7P: Impervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

Summary for Subcatchment 8P: Pervious

Runoff = 3.24 cfs @ 12.23 hrs, Volume= 12,055 cf, Depth= 2.34"

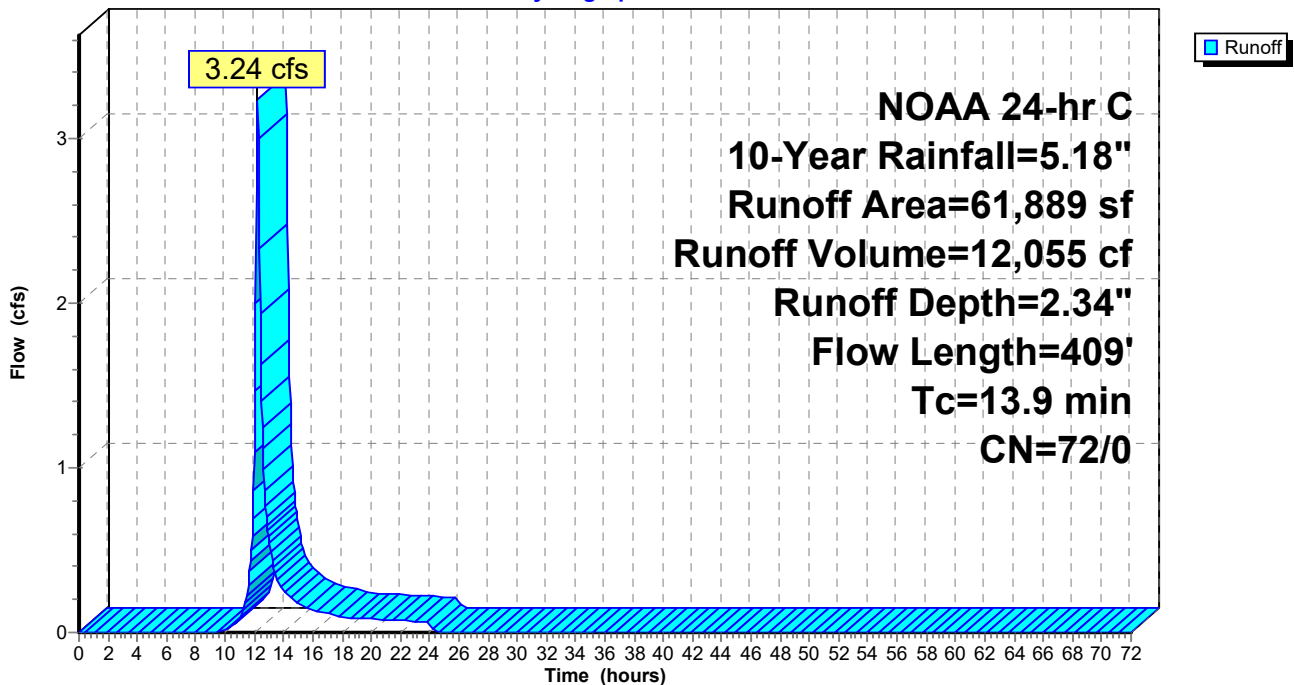
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 28,675 | 70 | Woods, Good, HSG C |
| 33,214 | 74 | >75% Grass cover, Good, HSG C |
| 61,889 | 72 | Weighted Average |
| 61,889 | 72 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 2.8 | 36 | 0.0560 | 0.21 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 4.3 | 51 | 0.0390 | 0.20 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.3 | 25 | 0.0800 | 1.41 | | Shallow Concentrated Flow, C-D Woodland Kv= 5.0 fps |
| 6.5 | 297 | 0.0230 | 0.76 | | Shallow Concentrated Flow, D-E Woodland Kv= 5.0 fps |
| 13.9 | 409 | Total | | | |

Subcatchment 8P: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Subcatchment 9P: Pervious

Runoff = 2.10 cfs @ 12.20 hrs, Volume= 7,347 cf, Depth= 2.42"

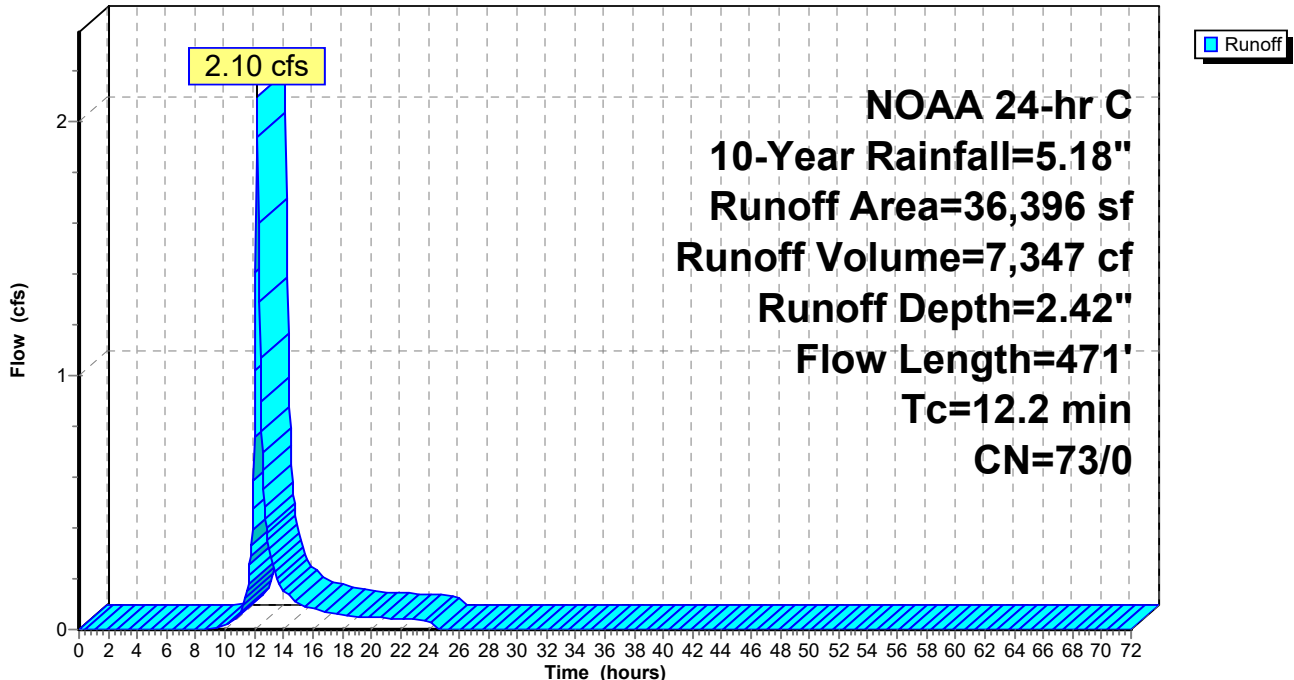
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 10-Year Rainfall=5.18"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 5,369 | 70 | Woods, Good, HSG C |
| 31,027 | 74 | >75% Grass cover, Good, HSG C |
| 36,396 | 73 | Weighted Average |
| 36,396 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 9.8 | 100 | 0.0190 | 0.17 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.7 | 102 | 0.0240 | 2.49 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.8 | 128 | 0.0310 | 2.83 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.8 | 120 | 0.0250 | 2.55 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.1 | 21 | 0.0310 | 2.83 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 12.2 | 471 | Total | | | |

Subcatchment 9P: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Pond B1: Bioretention Basin 1

[92] Warning: Device #2 is above defined storage

Inflow Area = 48,248 sf, 48.86% Impervious, Inflow Depth = 3.70" for 10-Year event
 Inflow = 4.04 cfs @ 12.18 hrs, Volume= 14,869 cf
 Outflow = 3.92 cfs @ 12.21 hrs, Volume= 10,974 cf, Atten= 3%, Lag= 1.6 min
 Primary = 3.92 cfs @ 12.21 hrs, Volume= 10,974 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 78.34' @ 12.21 hrs Surf.Area= 2,992 sf Storage= 4,464 cf

Plug-Flow detention time= 169.1 min calculated for 10,966 cf (74% of inflow)
 Center-of-Mass det. time= 74.7 min (858.8 - 784.1)

| Volume | Invert | Avail.Storage | Storage Description | |
|------------------|-------------------|------------------------|--|------------------|
| #1 | 76.50' | 4,938 cf | Custom Stage Data (Conic) Listed below (Recalc) | |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
| 76.50 | 1,883 | 0 | 0 | 1,883 |
| 77.50 | 2,461 | 2,166 | 2,166 | 2,484 |
| 78.50 | 3,096 | 2,772 | 4,938 | 3,146 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|---|
| #1 | Primary | 73.00' | 24.0" Round CMP_Round 24" L= 10.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.85' S= 0.0150 1' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf |
| #2 | Device 1 | 78.50' | 10.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 78.15' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=3.86 cfs @ 12.21 hrs HW=78.34' (Free Discharge)
 1=CMP_Round 24" (Passes 3.86 cfs of 24.89 cfs potential flow)
 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
 3=Orifice/Grate (Weir Controls 3.86 cfs @ 1.43 fps)

Pre vs Post

Prepared by {enter your company name here}

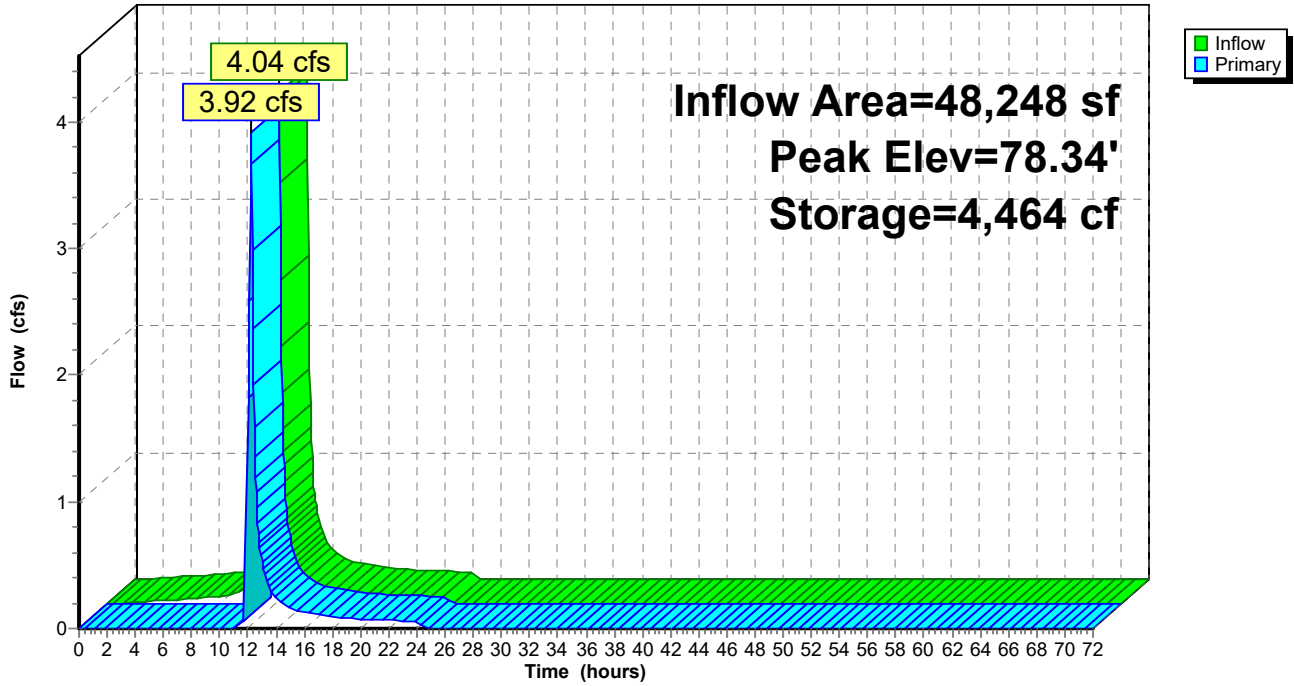
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NOAA 24-hr C 10-Year Rainfall=5.18"

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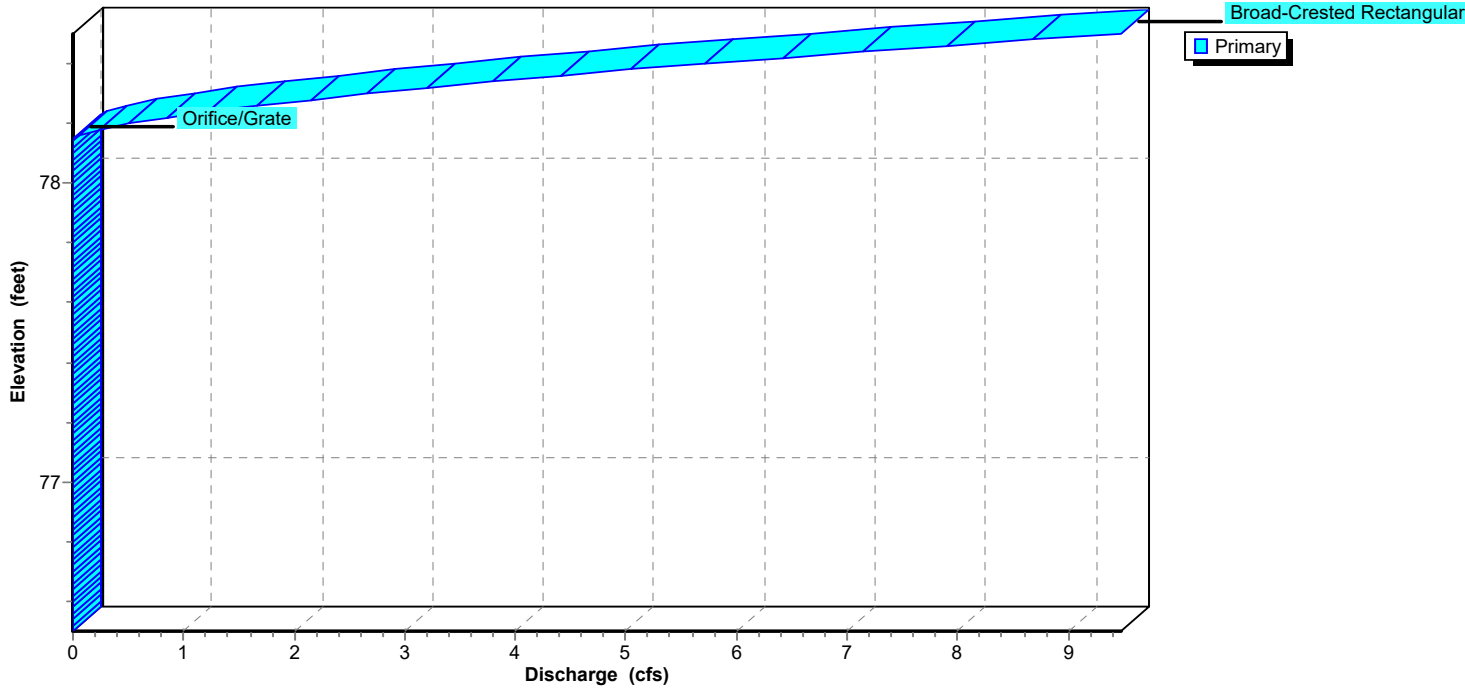
Pond B1: Bioretention Basin 1

Hydrograph



Pond B1: Bioretention Basin 1

Stage-Discharge



Pre vs Post

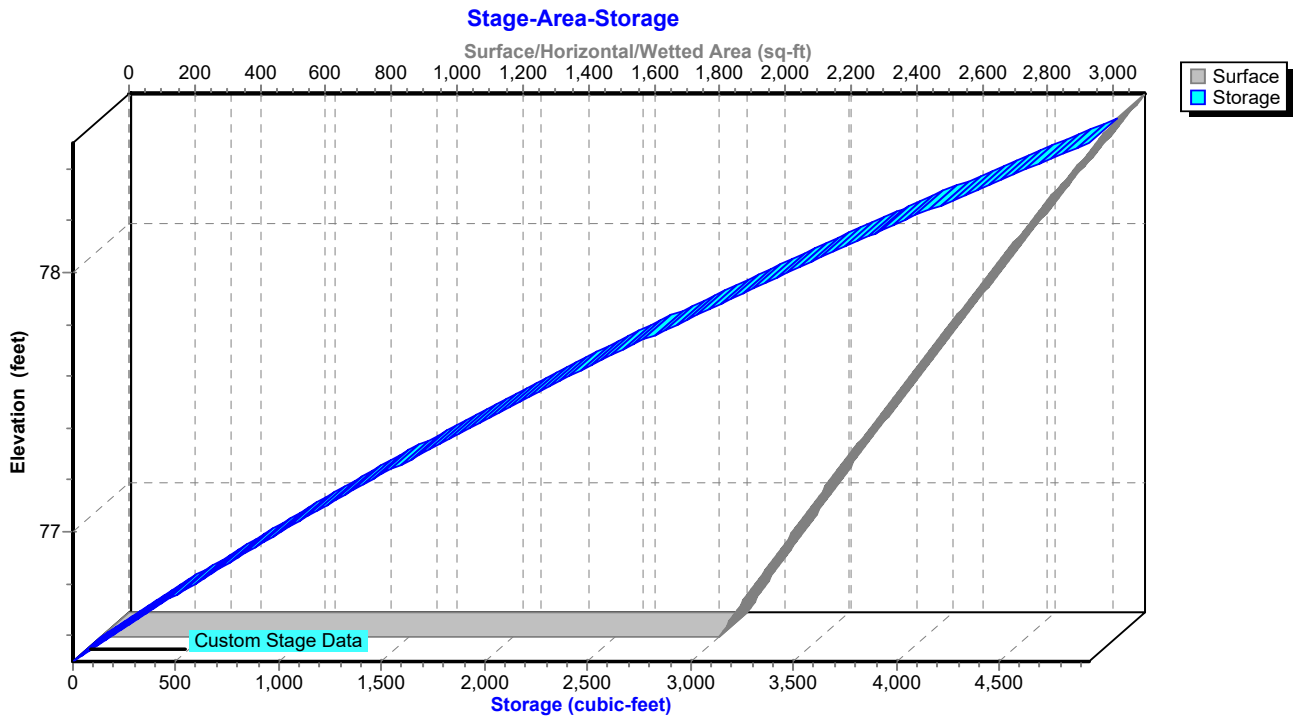
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Pond B1: Bioretention Basin 1



Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Stage-Discharge for Pond B1: Bioretention Basin 1

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.03 | 0.00 | 77.56 | 0.00 | 78.09 | 0.00 |
| 76.51 | 0.00 | 77.04 | 0.00 | 77.57 | 0.00 | 78.10 | 0.00 |
| 76.52 | 0.00 | 77.05 | 0.00 | 77.58 | 0.00 | 78.11 | 0.00 |
| 76.53 | 0.00 | 77.06 | 0.00 | 77.59 | 0.00 | 78.12 | 0.00 |
| 76.54 | 0.00 | 77.07 | 0.00 | 77.60 | 0.00 | 78.13 | 0.00 |
| 76.55 | 0.00 | 77.08 | 0.00 | 77.61 | 0.00 | 78.14 | 0.00 |
| 76.56 | 0.00 | 77.09 | 0.00 | 77.62 | 0.00 | 78.15 | 0.00 |
| 76.57 | 0.00 | 77.10 | 0.00 | 77.63 | 0.00 | 78.16 | 0.05 |
| 76.58 | 0.00 | 77.11 | 0.00 | 77.64 | 0.00 | 78.17 | 0.13 |
| 76.59 | 0.00 | 77.12 | 0.00 | 77.65 | 0.00 | 78.18 | 0.24 |
| 76.60 | 0.00 | 77.13 | 0.00 | 77.66 | 0.00 | 78.19 | 0.37 |
| 76.61 | 0.00 | 77.14 | 0.00 | 77.67 | 0.00 | 78.20 | 0.51 |
| 76.62 | 0.00 | 77.15 | 0.00 | 77.68 | 0.00 | 78.21 | 0.67 |
| 76.63 | 0.00 | 77.16 | 0.00 | 77.69 | 0.00 | 78.22 | 0.85 |
| 76.64 | 0.00 | 77.17 | 0.00 | 77.70 | 0.00 | 78.23 | 1.04 |
| 76.65 | 0.00 | 77.18 | 0.00 | 77.71 | 0.00 | 78.24 | 1.24 |
| 76.66 | 0.00 | 77.19 | 0.00 | 77.72 | 0.00 | 78.25 | 1.45 |
| 76.67 | 0.00 | 77.20 | 0.00 | 77.73 | 0.00 | 78.26 | 1.67 |
| 76.68 | 0.00 | 77.21 | 0.00 | 77.74 | 0.00 | 78.27 | 1.90 |
| 76.69 | 0.00 | 77.22 | 0.00 | 77.75 | 0.00 | 78.28 | 2.15 |
| 76.70 | 0.00 | 77.23 | 0.00 | 77.76 | 0.00 | 78.29 | 2.40 |
| 76.71 | 0.00 | 77.24 | 0.00 | 77.77 | 0.00 | 78.30 | 2.66 |
| 76.72 | 0.00 | 77.25 | 0.00 | 77.78 | 0.00 | 78.31 | 2.93 |
| 76.73 | 0.00 | 77.26 | 0.00 | 77.79 | 0.00 | 78.32 | 3.21 |
| 76.74 | 0.00 | 77.27 | 0.00 | 77.80 | 0.00 | 78.33 | 3.50 |
| 76.75 | 0.00 | 77.28 | 0.00 | 77.81 | 0.00 | 78.34 | 3.79 |
| 76.76 | 0.00 | 77.29 | 0.00 | 77.82 | 0.00 | 78.35 | 4.09 |
| 76.77 | 0.00 | 77.30 | 0.00 | 77.83 | 0.00 | 78.36 | 4.41 |
| 76.78 | 0.00 | 77.31 | 0.00 | 77.84 | 0.00 | 78.37 | 4.72 |
| 76.79 | 0.00 | 77.32 | 0.00 | 77.85 | 0.00 | 78.38 | 5.05 |
| 76.80 | 0.00 | 77.33 | 0.00 | 77.86 | 0.00 | 78.39 | 5.38 |
| 76.81 | 0.00 | 77.34 | 0.00 | 77.87 | 0.00 | 78.40 | 5.72 |
| 76.82 | 0.00 | 77.35 | 0.00 | 77.88 | 0.00 | 78.41 | 6.07 |
| 76.83 | 0.00 | 77.36 | 0.00 | 77.89 | 0.00 | 78.42 | 6.42 |
| 76.84 | 0.00 | 77.37 | 0.00 | 77.90 | 0.00 | 78.43 | 6.78 |
| 76.85 | 0.00 | 77.38 | 0.00 | 77.91 | 0.00 | 78.44 | 7.15 |
| 76.86 | 0.00 | 77.39 | 0.00 | 77.92 | 0.00 | 78.45 | 7.52 |
| 76.87 | 0.00 | 77.40 | 0.00 | 77.93 | 0.00 | 78.46 | 7.90 |
| 76.88 | 0.00 | 77.41 | 0.00 | 77.94 | 0.00 | 78.47 | 8.29 |
| 76.89 | 0.00 | 77.42 | 0.00 | 77.95 | 0.00 | 78.48 | 8.68 |
| 76.90 | 0.00 | 77.43 | 0.00 | 77.96 | 0.00 | 78.49 | 9.08 |
| 76.91 | 0.00 | 77.44 | 0.00 | 77.97 | 0.00 | 78.50 | 9.48 |
| 76.92 | 0.00 | 77.45 | 0.00 | 77.98 | 0.00 | | |
| 76.93 | 0.00 | 77.46 | 0.00 | 77.99 | 0.00 | | |
| 76.94 | 0.00 | 77.47 | 0.00 | 78.00 | 0.00 | | |
| 76.95 | 0.00 | 77.48 | 0.00 | 78.01 | 0.00 | | |
| 76.96 | 0.00 | 77.49 | 0.00 | 78.02 | 0.00 | | |
| 76.97 | 0.00 | 77.50 | 0.00 | 78.03 | 0.00 | | |
| 76.98 | 0.00 | 77.51 | 0.00 | 78.04 | 0.00 | | |
| 76.99 | 0.00 | 77.52 | 0.00 | 78.05 | 0.00 | | |
| 77.00 | 0.00 | 77.53 | 0.00 | 78.06 | 0.00 | | |
| 77.01 | 0.00 | 77.54 | 0.00 | 78.07 | 0.00 | | |
| 77.02 | 0.00 | 77.55 | 0.00 | 78.08 | 0.00 | | |

Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Stage-Area-Storage for Pond B1: Bioretention Basin 1

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 1,883 | 0 | 77.56 | 2,497 | 2,314 |
| 76.52 | 1,894 | 38 | 77.58 | 2,509 | 2,364 |
| 76.54 | 1,905 | 76 | 77.60 | 2,521 | 2,415 |
| 76.56 | 1,916 | 114 | 77.62 | 2,533 | 2,465 |
| 76.58 | 1,926 | 152 | 77.64 | 2,546 | 2,516 |
| 76.60 | 1,937 | 191 | 77.66 | 2,558 | 2,567 |
| 76.62 | 1,948 | 230 | 77.68 | 2,570 | 2,618 |
| 76.64 | 1,959 | 269 | 77.70 | 2,582 | 2,670 |
| 76.66 | 1,970 | 308 | 77.72 | 2,594 | 2,722 |
| 76.68 | 1,981 | 348 | 77.74 | 2,607 | 2,774 |
| 76.70 | 1,992 | 387 | 77.76 | 2,619 | 2,826 |
| 76.72 | 2,004 | 427 | 77.78 | 2,631 | 2,878 |
| 76.74 | 2,015 | 468 | 77.80 | 2,644 | 2,931 |
| 76.76 | 2,026 | 508 | 77.82 | 2,656 | 2,984 |
| 76.78 | 2,037 | 549 | 77.84 | 2,669 | 3,037 |
| 76.80 | 2,048 | 590 | 77.86 | 2,681 | 3,091 |
| 76.82 | 2,060 | 631 | 77.88 | 2,694 | 3,145 |
| 76.84 | 2,071 | 672 | 77.90 | 2,706 | 3,199 |
| 76.86 | 2,082 | 713 | 77.92 | 2,719 | 3,253 |
| 76.88 | 2,094 | 755 | 77.94 | 2,731 | 3,307 |
| 76.90 | 2,105 | 797 | 77.96 | 2,744 | 3,362 |
| 76.92 | 2,116 | 839 | 77.98 | 2,757 | 3,417 |
| 76.94 | 2,128 | 882 | 78.00 | 2,769 | 3,472 |
| 76.96 | 2,139 | 924 | 78.02 | 2,782 | 3,528 |
| 76.98 | 2,151 | 967 | 78.04 | 2,795 | 3,584 |
| 77.00 | 2,162 | 1,011 | 78.06 | 2,808 | 3,640 |
| 77.02 | 2,174 | 1,054 | 78.08 | 2,820 | 3,696 |
| 77.04 | 2,186 | 1,097 | 78.10 | 2,833 | 3,753 |
| 77.06 | 2,197 | 1,141 | 78.12 | 2,846 | 3,809 |
| 77.08 | 2,209 | 1,185 | 78.14 | 2,859 | 3,866 |
| 77.10 | 2,221 | 1,230 | 78.16 | 2,872 | 3,924 |
| 77.12 | 2,232 | 1,274 | 78.18 | 2,885 | 3,981 |
| 77.14 | 2,244 | 1,319 | 78.20 | 2,898 | 4,039 |
| 77.16 | 2,256 | 1,364 | 78.22 | 2,911 | 4,097 |
| 77.18 | 2,268 | 1,409 | 78.24 | 2,924 | 4,156 |
| 77.20 | 2,279 | 1,455 | 78.26 | 2,937 | 4,214 |
| 77.22 | 2,291 | 1,500 | 78.28 | 2,950 | 4,273 |
| 77.24 | 2,303 | 1,546 | 78.30 | 2,963 | 4,332 |
| 77.26 | 2,315 | 1,593 | 78.32 | 2,976 | 4,392 |
| 77.28 | 2,327 | 1,639 | 78.34 | 2,990 | 4,451 |
| 77.30 | 2,339 | 1,686 | 78.36 | 3,003 | 4,511 |
| 77.32 | 2,351 | 1,732 | 78.38 | 3,016 | 4,571 |
| 77.34 | 2,363 | 1,780 | 78.40 | 3,029 | 4,632 |
| 77.36 | 2,375 | 1,827 | 78.42 | 3,043 | 4,692 |
| 77.38 | 2,388 | 1,875 | 78.44 | 3,056 | 4,753 |
| 77.40 | 2,400 | 1,923 | 78.46 | 3,069 | 4,815 |
| 77.42 | 2,412 | 1,971 | 78.48 | 3,083 | 4,876 |
| 77.44 | 2,424 | 2,019 | 78.50 | 3,096 | 4,938 |
| 77.46 | 2,436 | 2,068 | | | |
| 77.48 | 2,449 | 2,116 | | | |
| 77.50 | 2,461 | 2,166 | | | |
| 77.52 | 2,473 | 2,215 | | | |
| 77.54 | 2,485 | 2,264 | | | |

Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Pond B2: Bioretention Basin 2

[79] Warning: Submerged Pond B1 Primary device # 1 INLET by 4.94'

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 3.50" for 10-Year event
 Inflow = 8.46 cfs @ 12.19 hrs, Volume= 28,409 cf
 Outflow = 3.21 cfs @ 12.45 hrs, Volume= 25,242 cf, Atten= 62%, Lag= 15.4 min
 Primary = 3.21 cfs @ 12.45 hrs, Volume= 25,242 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 77.94' @ 12.45 hrs Surf.Area= 8,762 sf Storage= 11,272 cf

Plug-Flow detention time= 163.2 min calculated for 25,242 cf (89% of inflow)
 Center-of-Mass det. time= 106.6 min (909.3 - 802.7)

| Volume | Invert | Avail.Storage | Storage Description |
|------------------|-------------------|------------------------|--|
| #1 | 76.50' | 26,647 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 76.50 | 6,877 | 0 | 0 |
| 77.50 | 8,155 | 7,516 | 7,516 |
| 78.50 | 9,522 | 8,839 | 16,355 |
| 79.50 | 11,063 | 10,293 | 26,647 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|--|
| #1 | Primary | 73.00' | 15.0" Round Culvert L= 47.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.06' S= 0.0200 ' S= 0.0200 ' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf |
| #2 | Device 1 | 76.94' | 6.0" Vert. Orifice/Grate X 3.00 C= 0.600 |
| #3 | Device 1 | 77.78' | 4.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |
| #4 | Device 1 | 79.25' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=3.21 cfs @ 12.45 hrs HW=77.94' (Free Discharge)
 1=Culvert (Passes 3.21 cfs of 9.69 cfs potential flow)
 2=Orifice/Grate (Orifice Controls 2.46 cfs @ 4.18 fps)
 3=Broad-Crested Rectangular Weir (Weir Controls 0.74 cfs @ 1.13 fps)
 4=Orifice/Grate (Controls 0.00 cfs)

Pre vs Post

Prepared by {enter your company name here}

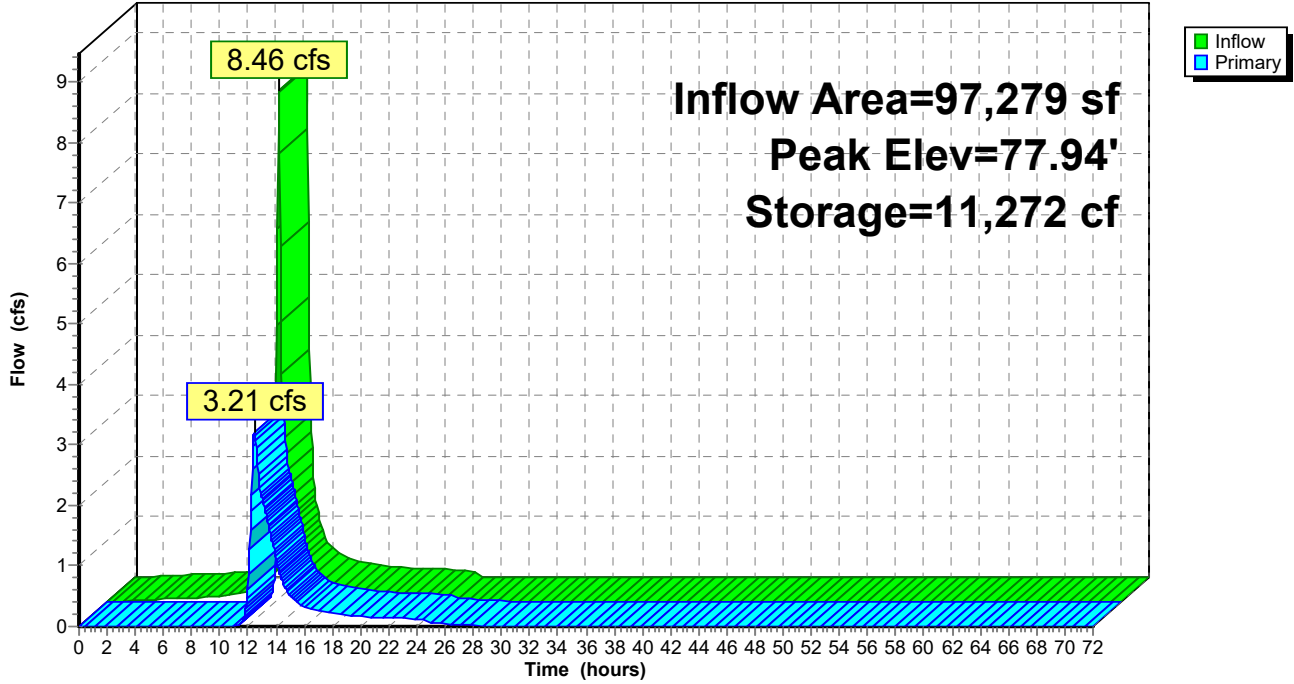
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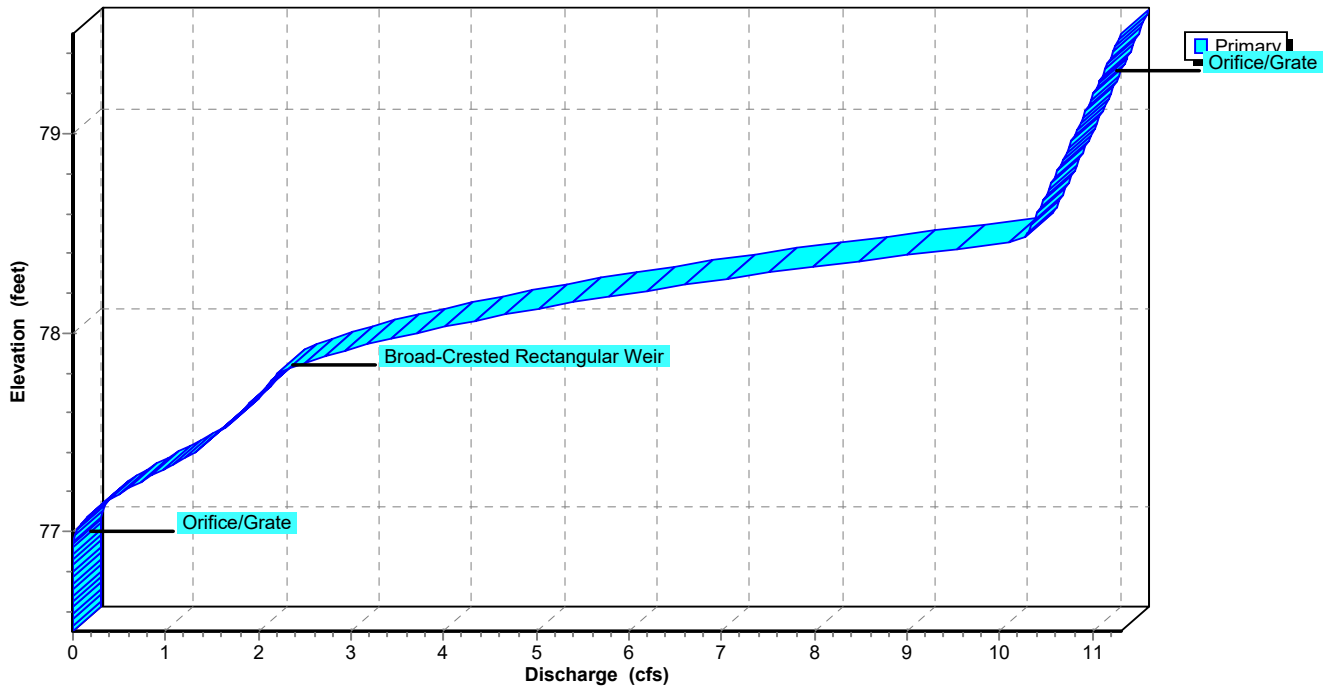
Pond B2: Bioretention Basin 2

Hydrograph



Pond B2: Bioretention Basin 2

Stage-Discharge



Pre vs Post

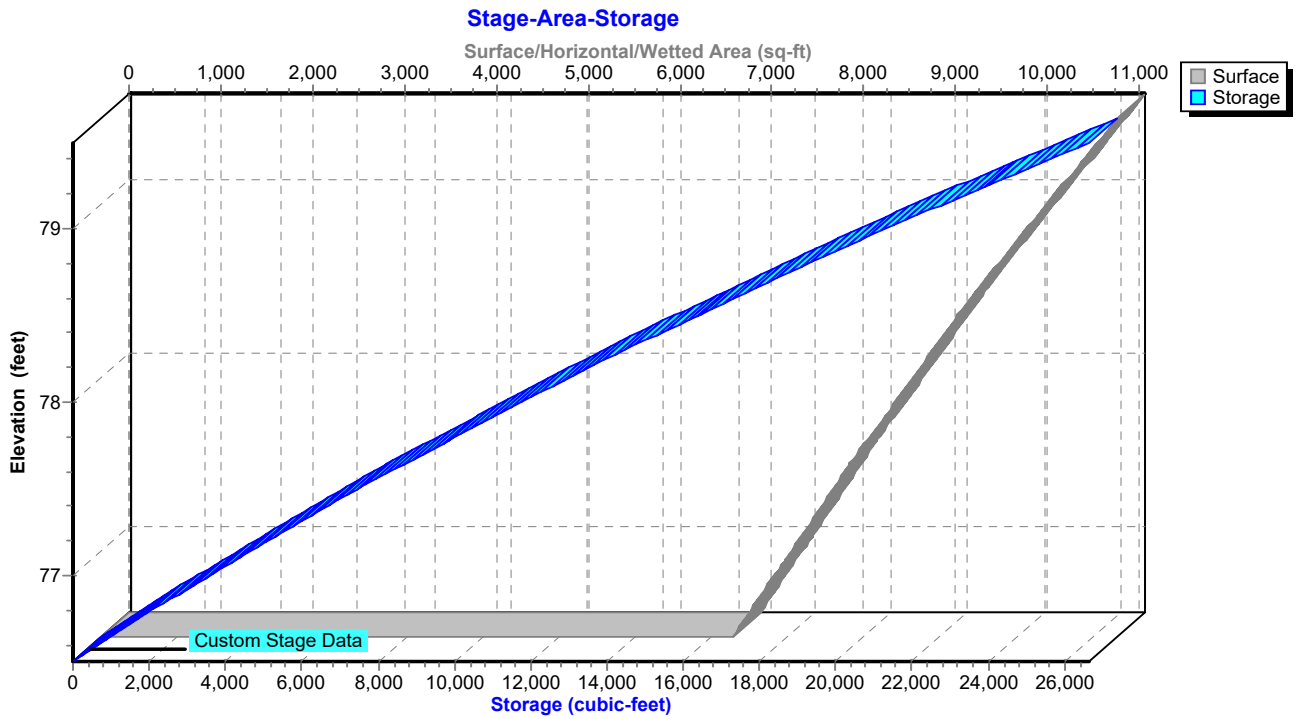
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NOAA 24-hr C 10-Year Rainfall=5.18"

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Pond B2: Bioretention Basin 2



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

Stage-Discharge for Pond B2: Bioretention Basin 2

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.56 | 1.73 | 78.62 | 10.43 |
| 76.52 | 0.00 | 77.58 | 1.77 | 78.64 | 10.45 |
| 76.54 | 0.00 | 77.60 | 1.82 | 78.66 | 10.47 |
| 76.56 | 0.00 | 77.62 | 1.86 | 78.68 | 10.49 |
| 76.58 | 0.00 | 77.64 | 1.90 | 78.70 | 10.51 |
| 76.60 | 0.00 | 77.66 | 1.94 | 78.72 | 10.53 |
| 76.62 | 0.00 | 77.68 | 1.99 | 78.74 | 10.55 |
| 76.64 | 0.00 | 77.70 | 2.03 | 78.76 | 10.57 |
| 76.66 | 0.00 | 77.72 | 2.06 | 78.78 | 10.59 |
| 76.68 | 0.00 | 77.74 | 2.10 | 78.80 | 10.61 |
| 76.70 | 0.00 | 77.76 | 2.14 | 78.82 | 10.63 |
| 76.72 | 0.00 | 77.78 | 2.18 | 78.84 | 10.65 |
| 76.74 | 0.00 | 77.80 | 2.25 | 78.86 | 10.67 |
| 76.76 | 0.00 | 77.82 | 2.34 | 78.88 | 10.69 |
| 76.78 | 0.00 | 77.84 | 2.45 | 78.90 | 10.71 |
| 76.80 | 0.00 | 77.86 | 2.58 | 78.92 | 10.73 |
| 76.82 | 0.00 | 77.88 | 2.71 | 78.94 | 10.75 |
| 76.84 | 0.00 | 77.90 | 2.86 | 78.96 | 10.77 |
| 76.86 | 0.00 | 77.92 | 3.01 | 78.98 | 10.79 |
| 76.88 | 0.00 | 77.94 | 3.17 | 79.00 | 10.82 |
| 76.90 | 0.00 | 77.96 | 3.34 | 79.02 | 10.84 |
| 76.92 | 0.00 | 77.98 | 3.52 | 79.04 | 10.86 |
| 76.94 | 0.00 | 78.00 | 3.71 | 79.06 | 10.88 |
| 76.96 | 0.00 | 78.02 | 3.91 | 79.08 | 10.90 |
| 76.98 | 0.02 | 78.04 | 4.12 | 79.10 | 10.92 |
| 77.00 | 0.03 | 78.06 | 4.33 | 79.12 | 10.94 |
| 77.02 | 0.06 | 78.08 | 4.56 | 79.14 | 10.96 |
| 77.04 | 0.09 | 78.10 | 4.79 | 79.16 | 10.97 |
| 77.06 | 0.13 | 78.12 | 5.02 | 79.18 | 10.99 |
| 77.08 | 0.17 | 78.14 | 5.27 | 79.20 | 11.01 |
| 77.10 | 0.22 | 78.16 | 5.52 | 79.22 | 11.03 |
| 77.12 | 0.28 | 78.18 | 5.78 | 79.24 | 11.05 |
| 77.14 | 0.34 | 78.20 | 6.05 | 79.26 | 11.07 |
| 77.16 | 0.40 | 78.22 | 6.32 | 79.28 | 11.09 |
| 77.18 | 0.47 | 78.24 | 6.61 | 79.30 | 11.11 |
| 77.20 | 0.54 | 78.26 | 6.90 | 79.32 | 11.13 |
| 77.22 | 0.61 | 78.28 | 7.20 | 79.34 | 11.15 |
| 77.24 | 0.69 | 78.30 | 7.51 | 79.36 | 11.17 |
| 77.26 | 0.77 | 78.32 | 7.83 | 79.38 | 11.19 |
| 77.28 | 0.85 | 78.34 | 8.15 | 79.40 | 11.21 |
| 77.30 | 0.93 | 78.36 | 8.48 | 79.42 | 11.23 |
| 77.32 | 1.01 | 78.38 | 8.82 | 79.44 | 11.25 |
| 77.34 | 1.09 | 78.40 | 9.18 | 79.46 | 11.27 |
| 77.36 | 1.17 | 78.42 | 9.54 | 79.48 | 11.29 |
| 77.38 | 1.24 | 78.44 | 9.92 | 79.50 | 11.31 |
| 77.40 | 1.31 | 78.46 | 10.26 | | |
| 77.42 | 1.37 | 78.48 | 10.28 | | |
| 77.44 | 1.42 | 78.50 | 10.30 | | |
| 77.46 | 1.47 | 78.52 | 10.32 | | |
| 77.48 | 1.53 | 78.54 | 10.34 | | |
| 77.50 | 1.58 | 78.56 | 10.36 | | |
| 77.52 | 1.63 | 78.58 | 10.38 | | |
| 77.54 | 1.68 | 78.60 | 10.40 | | |

Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Stage-Area-Storage for Pond B2: Bioretention Basin 2

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 6,877 | 0 | 79.15 | 10,524 | 22,869 |
| 76.55 | 6,941 | 345 | 79.20 | 10,601 | 23,397 |
| 76.60 | 7,005 | 694 | 79.25 | 10,678 | 23,929 |
| 76.65 | 7,069 | 1,046 | 79.30 | 10,755 | 24,465 |
| 76.70 | 7,133 | 1,401 | 79.35 | 10,832 | 25,005 |
| 76.75 | 7,197 | 1,759 | 79.40 | 10,909 | 25,548 |
| 76.80 | 7,260 | 2,121 | 79.45 | 10,986 | 26,096 |
| 76.85 | 7,324 | 2,485 | 79.50 | 11,063 | 26,647 |
| 76.90 | 7,388 | 2,853 | | | |
| 76.95 | 7,452 | 3,224 | | | |
| 77.00 | 7,516 | 3,598 | | | |
| 77.05 | 7,580 | 3,976 | | | |
| 77.10 | 7,644 | 4,356 | | | |
| 77.15 | 7,708 | 4,740 | | | |
| 77.20 | 7,772 | 5,127 | | | |
| 77.25 | 7,836 | 5,517 | | | |
| 77.30 | 7,899 | 5,911 | | | |
| 77.35 | 7,963 | 6,307 | | | |
| 77.40 | 8,027 | 6,707 | | | |
| 77.45 | 8,091 | 7,110 | | | |
| 77.50 | 8,155 | 7,516 | | | |
| 77.55 | 8,223 | 7,925 | | | |
| 77.60 | 8,292 | 8,338 | | | |
| 77.65 | 8,360 | 8,755 | | | |
| 77.70 | 8,428 | 9,174 | | | |
| 77.75 | 8,497 | 9,597 | | | |
| 77.80 | 8,565 | 10,024 | | | |
| 77.85 | 8,633 | 10,454 | | | |
| 77.90 | 8,702 | 10,887 | | | |
| 77.95 | 8,770 | 11,324 | | | |
| 78.00 | 8,839 | 11,764 | | | |
| 78.05 | 8,907 | 12,208 | | | |
| 78.10 | 8,975 | 12,655 | | | |
| 78.15 | 9,044 | 13,106 | | | |
| 78.20 | 9,112 | 13,559 | | | |
| 78.25 | 9,180 | 14,017 | | | |
| 78.30 | 9,249 | 14,477 | | | |
| 78.35 | 9,317 | 14,942 | | | |
| 78.40 | 9,385 | 15,409 | | | |
| 78.45 | 9,454 | 15,880 | | | |
| 78.50 | 9,522 | 16,355 | | | |
| 78.55 | 9,599 | 16,833 | | | |
| 78.60 | 9,676 | 17,314 | | | |
| 78.65 | 9,753 | 17,800 | | | |
| 78.70 | 9,830 | 18,290 | | | |
| 78.75 | 9,907 | 18,783 | | | |
| 78.80 | 9,984 | 19,280 | | | |
| 78.85 | 10,061 | 19,782 | | | |
| 78.90 | 10,138 | 20,287 | | | |
| 78.95 | 10,215 | 20,795 | | | |
| 79.00 | 10,293 | 21,308 | | | |
| 79.05 | 10,370 | 21,825 | | | |
| 79.10 | 10,447 | 22,345 | | | |

Pre vs Post

NOAA 24-hr C 10-Year Rainfall=5.18"

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Summary for Pond B3: Bioretention Basin 3

[92] Warning: Device #2 is above defined storage

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 3.50" for 10-Year event
 Inflow = 0.72 cfs @ 12.30 hrs, Volume= 3,419 cf
 Outflow = 0.72 cfs @ 12.32 hrs, Volume= 2,944 cf, Atten= 0%, Lag= 0.8 min
 Primary = 0.72 cfs @ 12.32 hrs, Volume= 2,944 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 80.80' @ 12.32 hrs Surf.Area= 878 sf Storage= 528 cf

Plug-Flow detention time= 114.2 min calculated for 2,942 cf (86% of inflow)
 Center-of-Mass det. time= 48.3 min (847.4 - 799.1)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 79.98' | 694 cf | Custom Stage Data (Conic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|------------------|-------------------|------------------------|------------------------|------------------|
| 79.98 | 432 | 0 | 0 | 432 |
| 80.98 | 995 | 694 | 694 | 1,003 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 77.48' | 15.0" Round CMP_Round 15" L= 96.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 77.48' / 77.00' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 1.23 sf |
| #2 | Secondary | 80.98' | 15.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 80.74' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=0.71 cfs @ 12.32 hrs HW=80.80' (Free Discharge)
 ↑1=CMP_Round 15" (Passes 0.71 cfs of 7.66 cfs potential flow)
 ↑3=Orifice/Grate (Weir Controls 0.71 cfs @ 0.82 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=79.98' (Free Discharge)
 ↑2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pre vs Post

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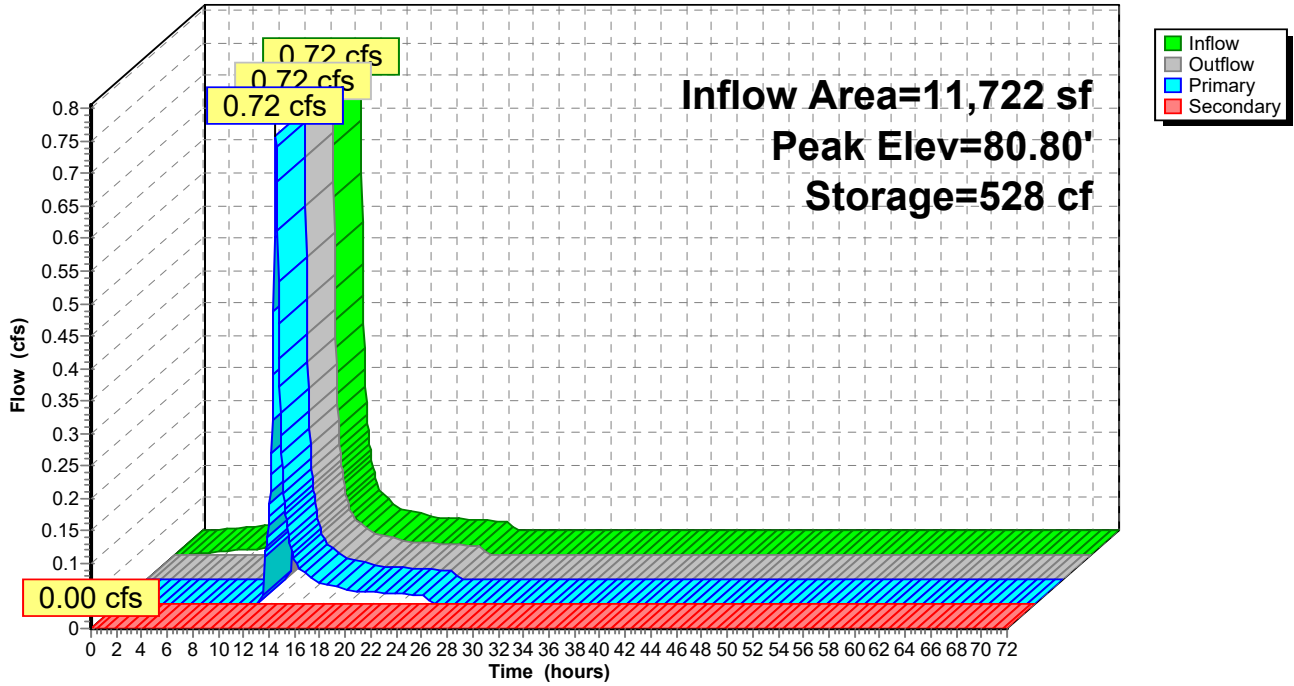
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NOAA 24-hr C 10-Year Rainfall=5.18"

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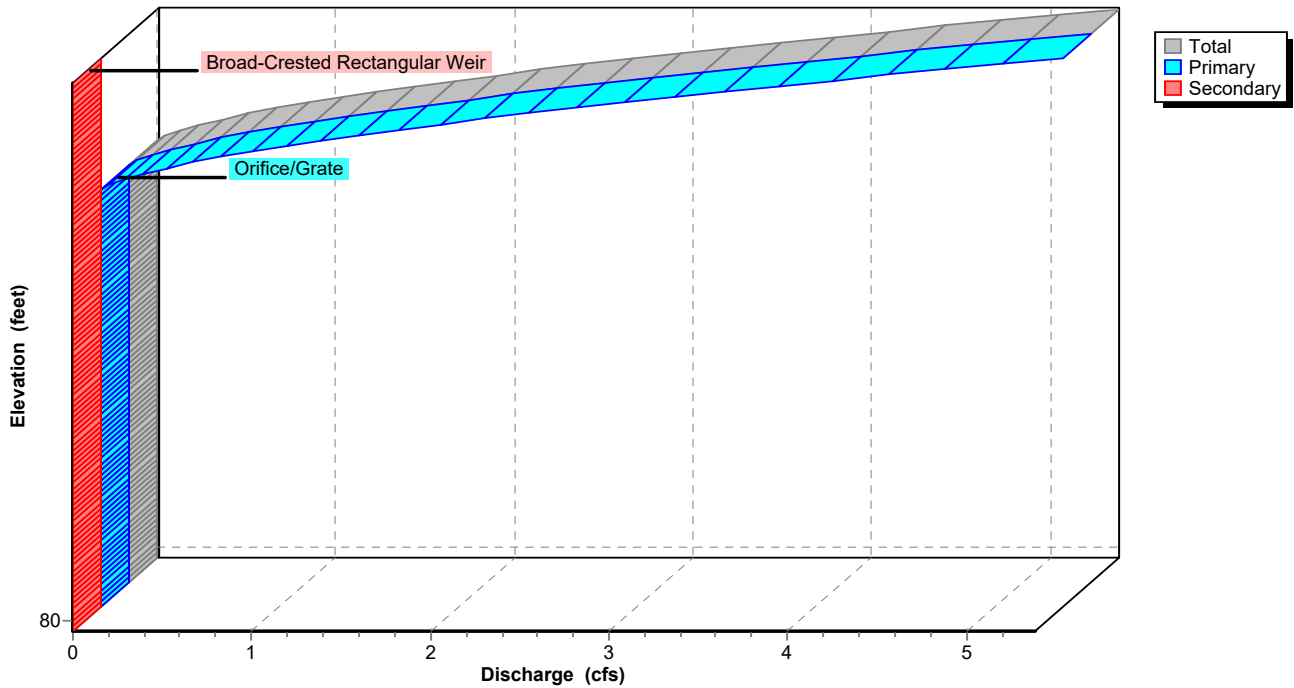
Pond B3: Bioretention Basin 3

Hydrograph



Pond B3: Bioretention Basin 3

Stage-Discharge



Pre vs Post

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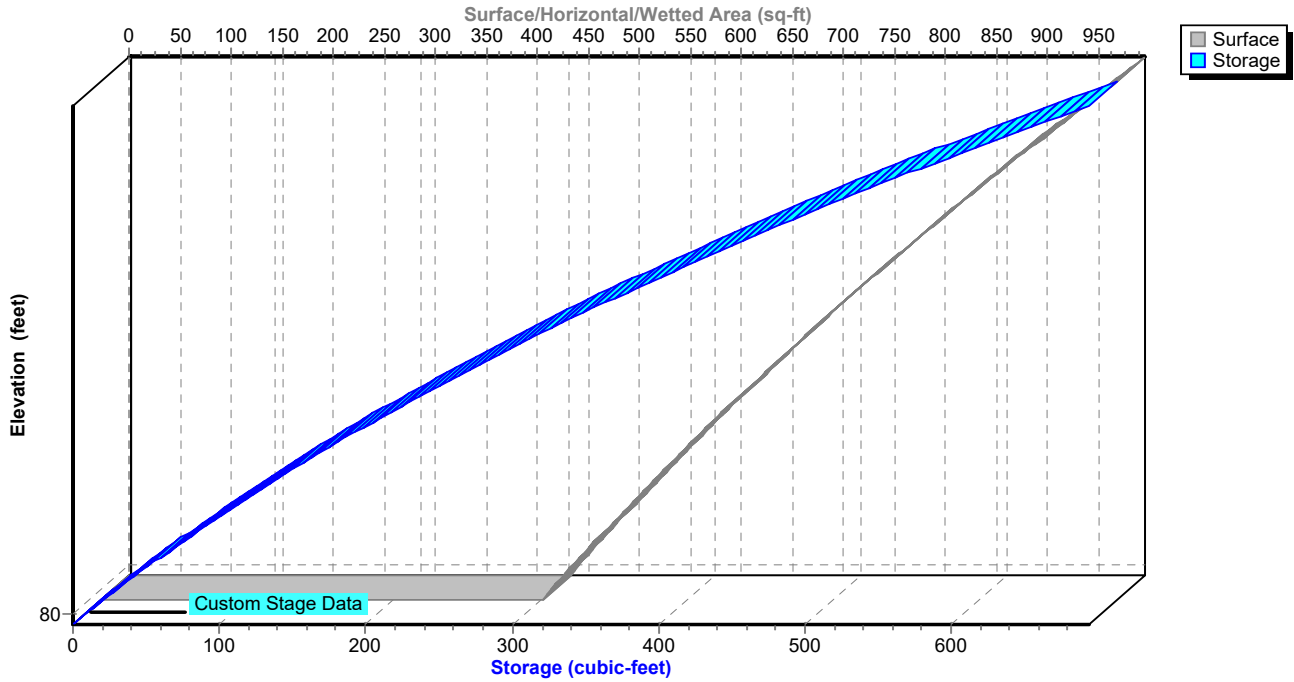
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Pond B3: Bioretention Basin 3

Stage-Area-Storage



Pre vs Post

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Stage-Discharge for Pond B3: Bioretention Basin 3

| Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) | Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) |
|---------------------|--------------------|------------------|--------------------|---------------------|--------------------|------------------|--------------------|
| 79.98 | 0.00 | 0.00 | 0.00 | 80.51 | 0.00 | 0.00 | 0.00 |
| 79.99 | 0.00 | 0.00 | 0.00 | 80.52 | 0.00 | 0.00 | 0.00 |
| 80.00 | 0.00 | 0.00 | 0.00 | 80.53 | 0.00 | 0.00 | 0.00 |
| 80.01 | 0.00 | 0.00 | 0.00 | 80.54 | 0.00 | 0.00 | 0.00 |
| 80.02 | 0.00 | 0.00 | 0.00 | 80.55 | 0.00 | 0.00 | 0.00 |
| 80.03 | 0.00 | 0.00 | 0.00 | 80.56 | 0.00 | 0.00 | 0.00 |
| 80.04 | 0.00 | 0.00 | 0.00 | 80.57 | 0.00 | 0.00 | 0.00 |
| 80.05 | 0.00 | 0.00 | 0.00 | 80.58 | 0.00 | 0.00 | 0.00 |
| 80.06 | 0.00 | 0.00 | 0.00 | 80.59 | 0.00 | 0.00 | 0.00 |
| 80.07 | 0.00 | 0.00 | 0.00 | 80.60 | 0.00 | 0.00 | 0.00 |
| 80.08 | 0.00 | 0.00 | 0.00 | 80.61 | 0.00 | 0.00 | 0.00 |
| 80.09 | 0.00 | 0.00 | 0.00 | 80.62 | 0.00 | 0.00 | 0.00 |
| 80.10 | 0.00 | 0.00 | 0.00 | 80.63 | 0.00 | 0.00 | 0.00 |
| 80.11 | 0.00 | 0.00 | 0.00 | 80.64 | 0.00 | 0.00 | 0.00 |
| 80.12 | 0.00 | 0.00 | 0.00 | 80.65 | 0.00 | 0.00 | 0.00 |
| 80.13 | 0.00 | 0.00 | 0.00 | 80.66 | 0.00 | 0.00 | 0.00 |
| 80.14 | 0.00 | 0.00 | 0.00 | 80.67 | 0.00 | 0.00 | 0.00 |
| 80.15 | 0.00 | 0.00 | 0.00 | 80.68 | 0.00 | 0.00 | 0.00 |
| 80.16 | 0.00 | 0.00 | 0.00 | 80.69 | 0.00 | 0.00 | 0.00 |
| 80.17 | 0.00 | 0.00 | 0.00 | 80.70 | 0.00 | 0.00 | 0.00 |
| 80.18 | 0.00 | 0.00 | 0.00 | 80.71 | 0.00 | 0.00 | 0.00 |
| 80.19 | 0.00 | 0.00 | 0.00 | 80.72 | 0.00 | 0.00 | 0.00 |
| 80.20 | 0.00 | 0.00 | 0.00 | 80.73 | 0.00 | 0.00 | 0.00 |
| 80.21 | 0.00 | 0.00 | 0.00 | 80.74 | 0.00 | 0.00 | 0.00 |
| 80.22 | 0.00 | 0.00 | 0.00 | 80.75 | 0.05 | 0.05 | 0.00 |
| 80.23 | 0.00 | 0.00 | 0.00 | 80.76 | 0.13 | 0.13 | 0.00 |
| 80.24 | 0.00 | 0.00 | 0.00 | 80.77 | 0.24 | 0.24 | 0.00 |
| 80.25 | 0.00 | 0.00 | 0.00 | 80.78 | 0.37 | 0.37 | 0.00 |
| 80.26 | 0.00 | 0.00 | 0.00 | 80.79 | 0.51 | 0.51 | 0.00 |
| 80.27 | 0.00 | 0.00 | 0.00 | 80.80 | 0.67 | 0.67 | 0.00 |
| 80.28 | 0.00 | 0.00 | 0.00 | 80.81 | 0.85 | 0.85 | 0.00 |
| 80.29 | 0.00 | 0.00 | 0.00 | 80.82 | 1.04 | 1.04 | 0.00 |
| 80.30 | 0.00 | 0.00 | 0.00 | 80.83 | 1.24 | 1.24 | 0.00 |
| 80.31 | 0.00 | 0.00 | 0.00 | 80.84 | 1.45 | 1.45 | 0.00 |
| 80.32 | 0.00 | 0.00 | 0.00 | 80.85 | 1.67 | 1.67 | 0.00 |
| 80.33 | 0.00 | 0.00 | 0.00 | 80.86 | 1.90 | 1.90 | 0.00 |
| 80.34 | 0.00 | 0.00 | 0.00 | 80.87 | 2.15 | 2.15 | 0.00 |
| 80.35 | 0.00 | 0.00 | 0.00 | 80.88 | 2.40 | 2.40 | 0.00 |
| 80.36 | 0.00 | 0.00 | 0.00 | 80.89 | 2.66 | 2.66 | 0.00 |
| 80.37 | 0.00 | 0.00 | 0.00 | 80.90 | 2.93 | 2.93 | 0.00 |
| 80.38 | 0.00 | 0.00 | 0.00 | 80.91 | 3.21 | 3.21 | 0.00 |
| 80.39 | 0.00 | 0.00 | 0.00 | 80.92 | 3.50 | 3.50 | 0.00 |
| 80.40 | 0.00 | 0.00 | 0.00 | 80.93 | 3.79 | 3.79 | 0.00 |
| 80.41 | 0.00 | 0.00 | 0.00 | 80.94 | 4.09 | 4.09 | 0.00 |
| 80.42 | 0.00 | 0.00 | 0.00 | 80.95 | 4.41 | 4.41 | 0.00 |
| 80.43 | 0.00 | 0.00 | 0.00 | 80.96 | 4.72 | 4.72 | 0.00 |
| 80.44 | 0.00 | 0.00 | 0.00 | 80.97 | 5.05 | 5.05 | 0.00 |
| 80.45 | 0.00 | 0.00 | 0.00 | 80.98 | 5.38 | 5.38 | 0.00 |
| 80.46 | 0.00 | 0.00 | 0.00 | | | | |
| 80.47 | 0.00 | 0.00 | 0.00 | | | | |
| 80.48 | 0.00 | 0.00 | 0.00 | | | | |
| 80.49 | 0.00 | 0.00 | 0.00 | | | | |
| 80.50 | 0.00 | 0.00 | 0.00 | | | | |

Pre vs Post

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Stage-Area-Storage for Pond B3: Bioretention Basin 3

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 79.98 | 432 | 0 | 80.51 | 702 | 298 |
| 79.99 | 436 | 4 | 80.52 | 707 | 305 |
| 80.00 | 441 | 9 | 80.53 | 713 | 312 |
| 80.01 | 446 | 13 | 80.54 | 719 | 319 |
| 80.02 | 450 | 18 | 80.55 | 725 | 326 |
| 80.03 | 455 | 22 | 80.56 | 730 | 333 |
| 80.04 | 459 | 27 | 80.57 | 736 | 341 |
| 80.05 | 464 | 31 | 80.58 | 742 | 348 |
| 80.06 | 469 | 36 | 80.59 | 748 | 355 |
| 80.07 | 473 | 41 | 80.60 | 754 | 363 |
| 80.08 | 478 | 45 | 80.61 | 760 | 371 |
| 80.09 | 483 | 50 | 80.62 | 766 | 378 |
| 80.10 | 487 | 55 | 80.63 | 772 | 386 |
| 80.11 | 492 | 60 | 80.64 | 778 | 394 |
| 80.12 | 497 | 65 | 80.65 | 784 | 401 |
| 80.13 | 502 | 70 | 80.66 | 790 | 409 |
| 80.14 | 507 | 75 | 80.67 | 796 | 417 |
| 80.15 | 511 | 80 | 80.68 | 802 | 425 |
| 80.16 | 516 | 85 | 80.69 | 808 | 433 |
| 80.17 | 521 | 90 | 80.70 | 814 | 441 |
| 80.18 | 526 | 96 | 80.71 | 820 | 450 |
| 80.19 | 531 | 101 | 80.72 | 826 | 458 |
| 80.20 | 536 | 106 | 80.73 | 833 | 466 |
| 80.21 | 541 | 112 | 80.74 | 839 | 474 |
| 80.22 | 546 | 117 | 80.75 | 845 | 483 |
| 80.23 | 551 | 123 | 80.76 | 851 | 491 |
| 80.24 | 556 | 128 | 80.77 | 858 | 500 |
| 80.25 | 561 | 134 | 80.78 | 864 | 508 |
| 80.26 | 566 | 139 | 80.79 | 870 | 517 |
| 80.27 | 571 | 145 | 80.80 | 877 | 526 |
| 80.28 | 577 | 151 | 80.81 | 883 | 535 |
| 80.29 | 582 | 157 | 80.82 | 889 | 544 |
| 80.30 | 587 | 162 | 80.83 | 896 | 552 |
| 80.31 | 592 | 168 | 80.84 | 902 | 561 |
| 80.32 | 597 | 174 | 80.85 | 909 | 571 |
| 80.33 | 603 | 180 | 80.86 | 915 | 580 |
| 80.34 | 608 | 186 | 80.87 | 922 | 589 |
| 80.35 | 613 | 192 | 80.88 | 928 | 598 |
| 80.36 | 619 | 199 | 80.89 | 935 | 607 |
| 80.37 | 624 | 205 | 80.90 | 941 | 617 |
| 80.38 | 629 | 211 | 80.91 | 948 | 626 |
| 80.39 | 635 | 217 | 80.92 | 955 | 636 |
| 80.40 | 640 | 224 | 80.93 | 961 | 645 |
| 80.41 | 646 | 230 | 80.94 | 968 | 655 |
| 80.42 | 651 | 237 | 80.95 | 975 | 665 |
| 80.43 | 657 | 243 | 80.96 | 981 | 674 |
| 80.44 | 662 | 250 | 80.97 | 988 | 684 |
| 80.45 | 668 | 256 | 80.98 | 995 | 694 |
| 80.46 | 673 | 263 | | | |
| 80.47 | 679 | 270 | | | |
| 80.48 | 685 | 277 | | | |
| 80.49 | 690 | 284 | | | |
| 80.50 | 696 | 291 | | | |

Pre vs Post

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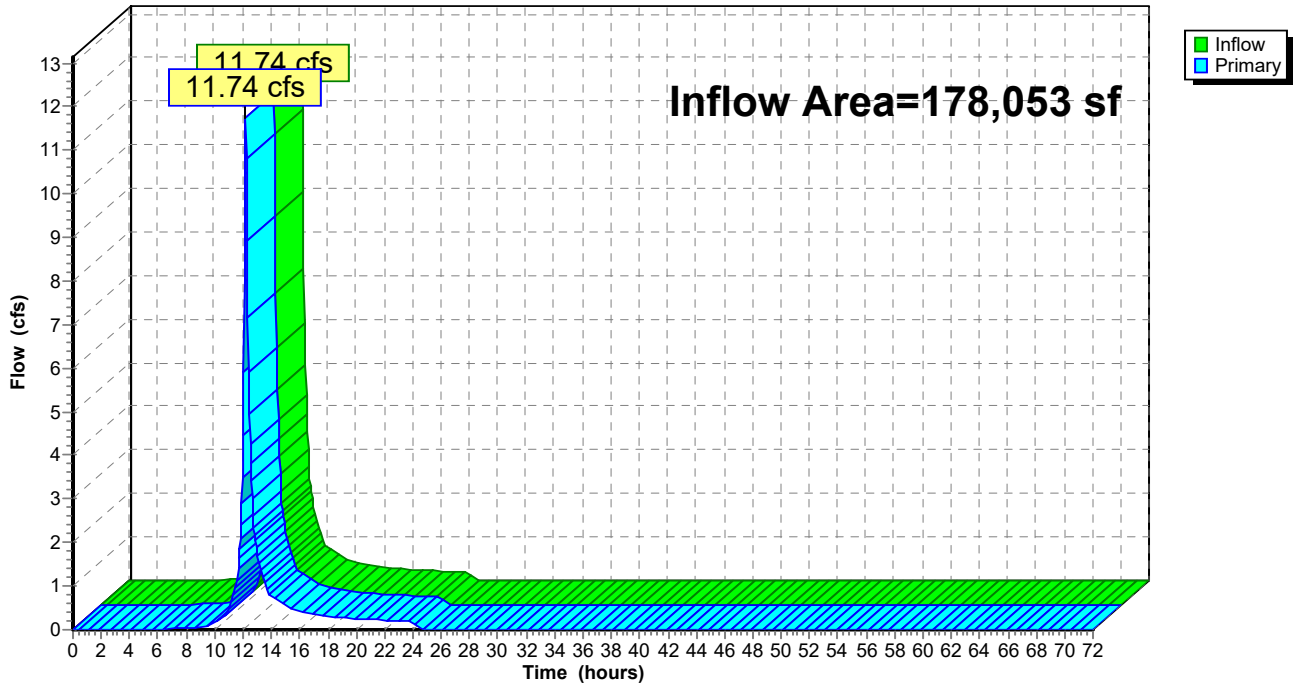
Summary for Link 5E: EDA 1

Inflow Area = 178,053 sf, 5.81% Impervious, Inflow Depth = 2.82" for 10-Year event
Inflow = 11.74 cfs @ 12.20 hrs, Volume= 41,781 cf
Primary = 11.74 cfs @ 12.20 hrs, Volume= 41,781 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5E: EDA 1

Hydrograph



Pre vs Post

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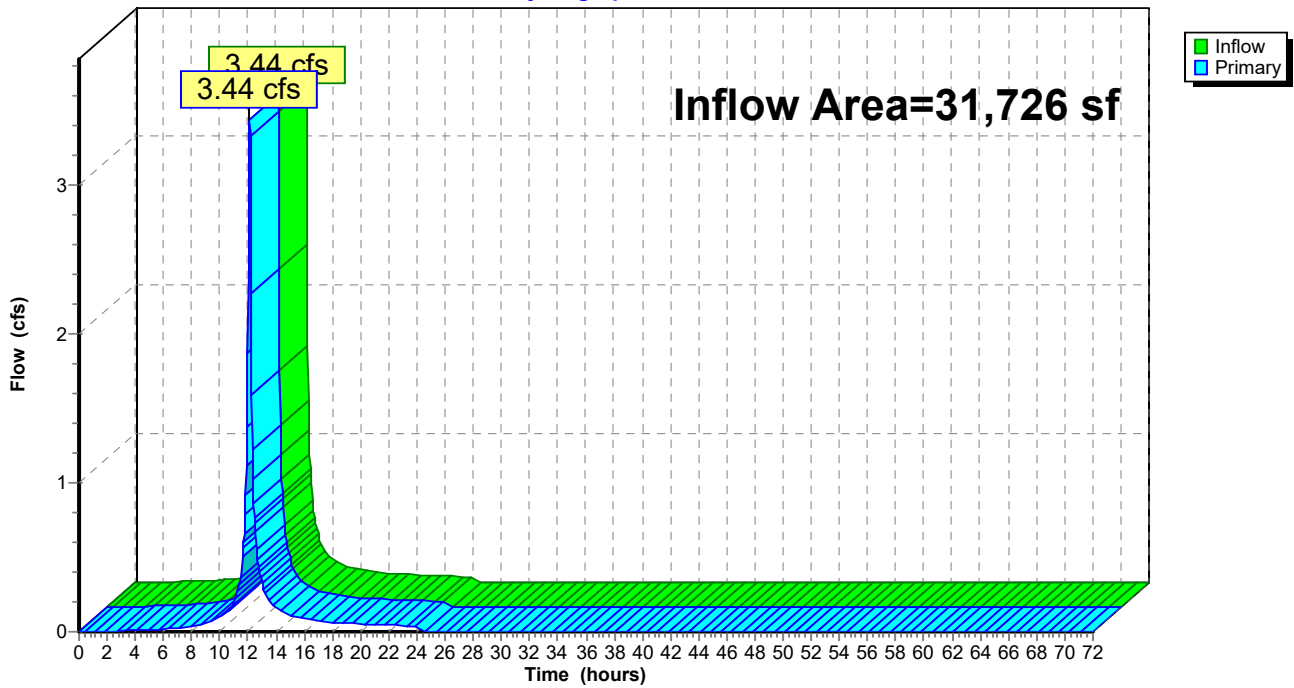
Summary for Link 6E: EDA 2

Inflow Area = 31,726 sf, 17.78% Impervious, Inflow Depth = 3.95" for 10-Year event
Inflow = 3.44 cfs @ 12.13 hrs, Volume= 10,447 cf
Primary = 3.44 cfs @ 12.13 hrs, Volume= 10,447 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 6E: EDA 2

Hydrograph



Pre vs Post

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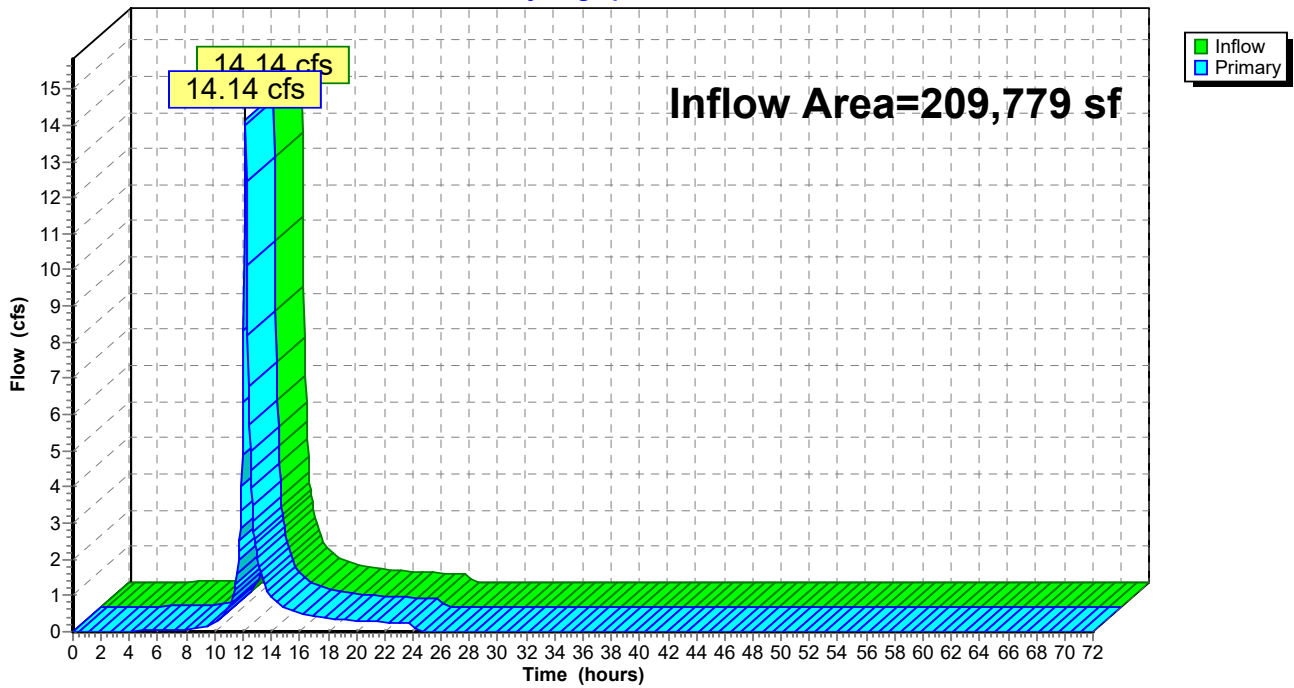
Summary for Link 7E: EDA

Inflow Area = 209,779 sf, 7.62% Impervious, Inflow Depth = 2.99" for 10-Year event
Inflow = 14.14 cfs @ 12.18 hrs, Volume= 52,228 cf
Primary = 14.14 cfs @ 12.18 hrs, Volume= 52,228 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 7E: EDA

Hydrograph



Pre vs Post

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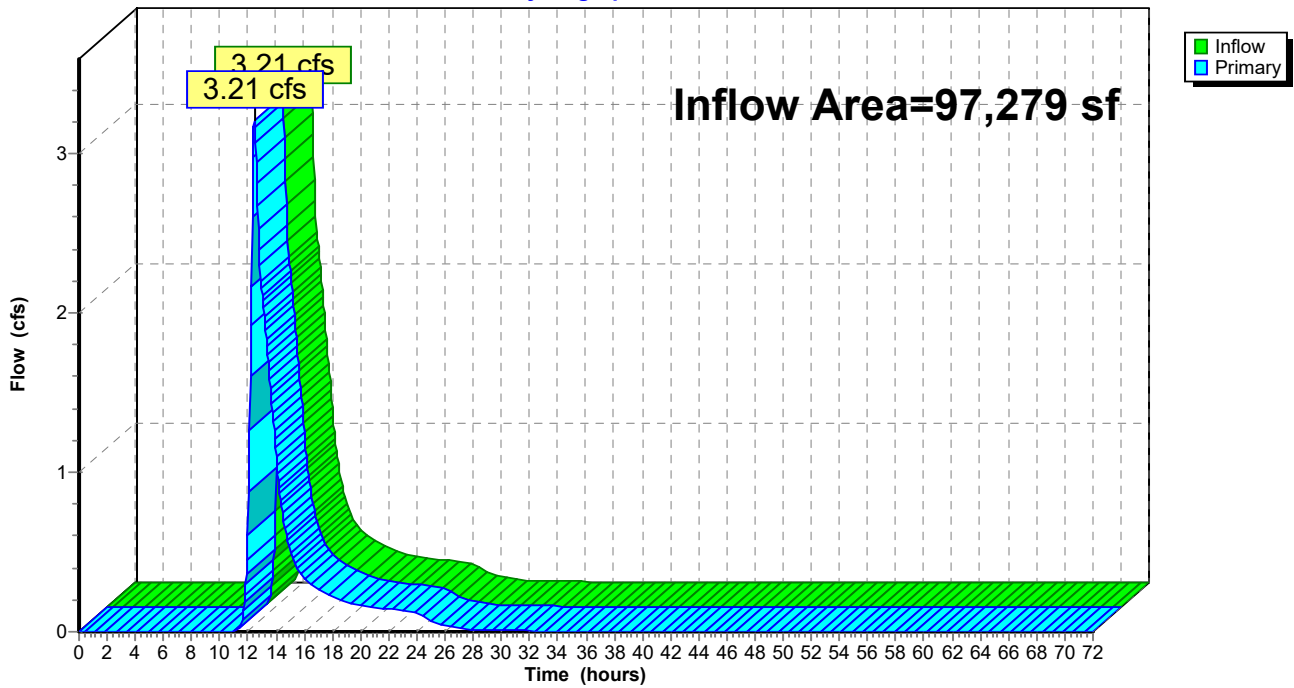
Summary for Link 10P: PDA 1A

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 3.11" for 10-Year event
Inflow = 3.21 cfs @ 12.45 hrs, Volume= 25,242 cf
Primary = 3.21 cfs @ 12.45 hrs, Volume= 25,242 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 10P: PDA 1A

Hydrograph



Pre vs Post

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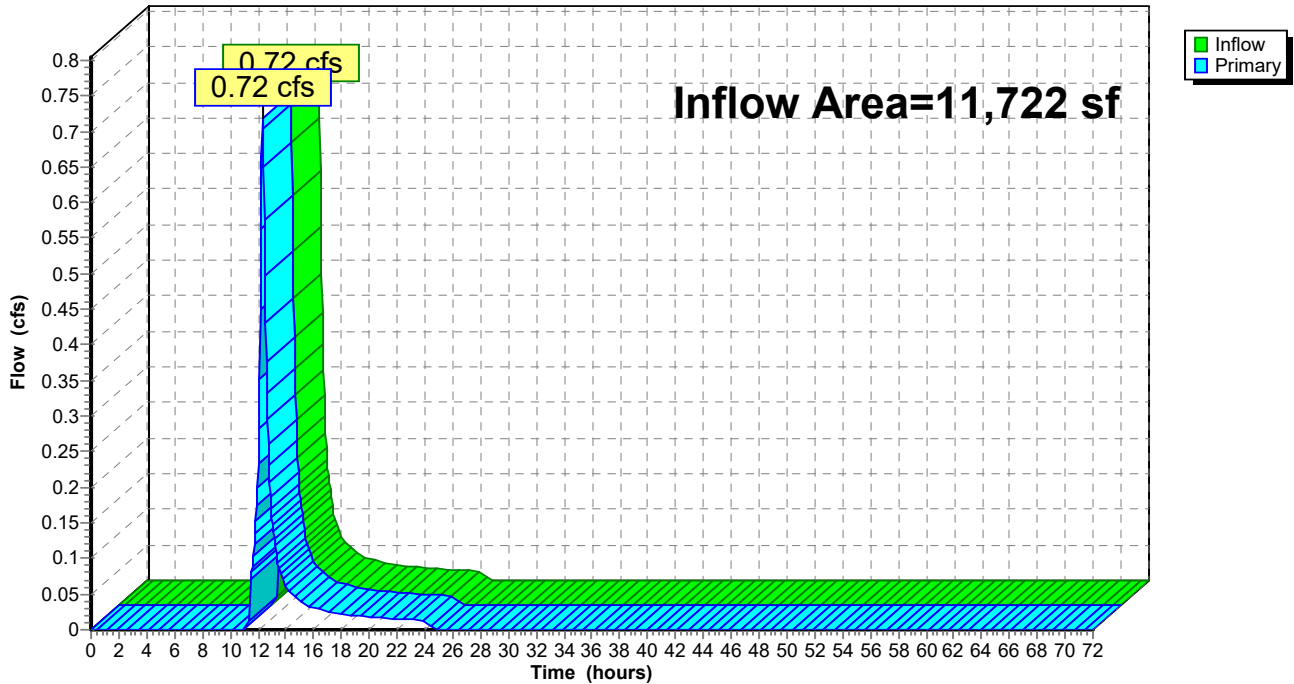
Summary for Link 11P: PDA 1B

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 3.01" for 10-Year event
Inflow = 0.72 cfs @ 12.32 hrs, Volume= 2,944 cf
Primary = 0.72 cfs @ 12.32 hrs, Volume= 2,944 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 11P: PDA 1B

Hydrograph



Pre vs Post

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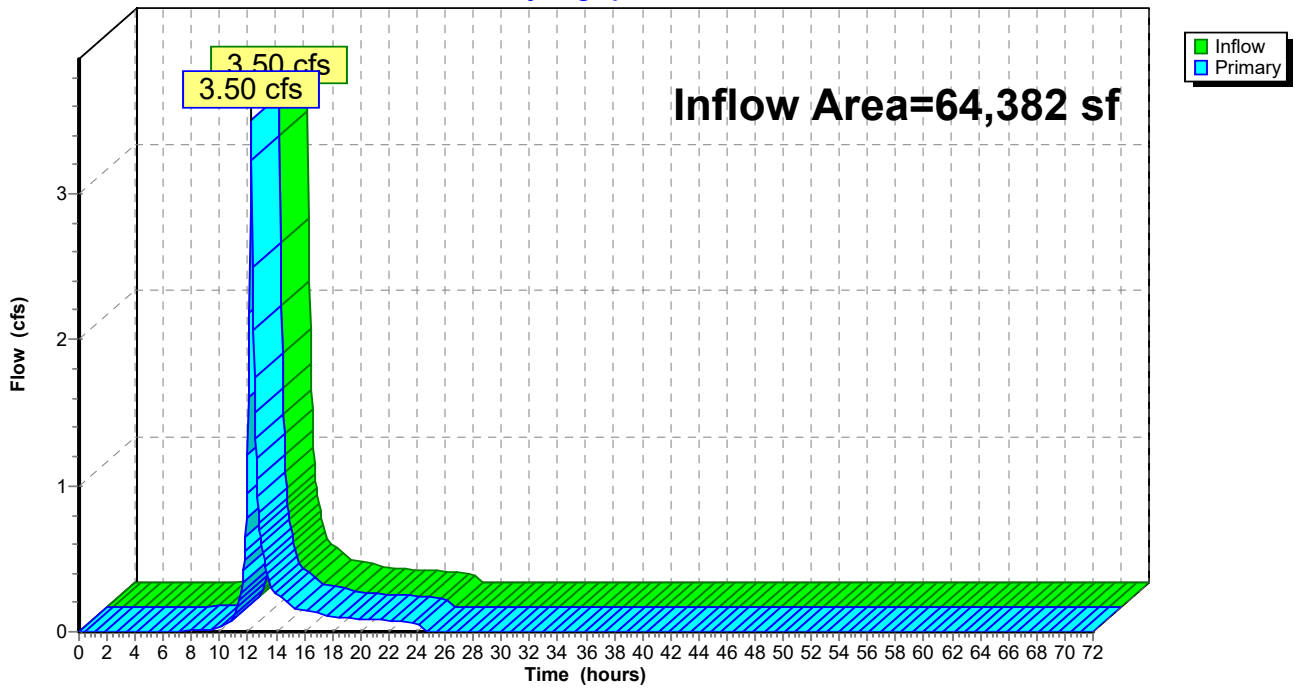
Summary for Link 12P: PDA 1C

Inflow Area = 64,382 sf, 3.87% Impervious, Inflow Depth = 2.44" for 10-Year event
Inflow = 3.50 cfs @ 12.22 hrs, Volume= 13,082 cf
Primary = 3.50 cfs @ 12.22 hrs, Volume= 13,082 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 12P: PDA 1C

Hydrograph



Pre vs Post

Prepared by {enter your company name here}

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

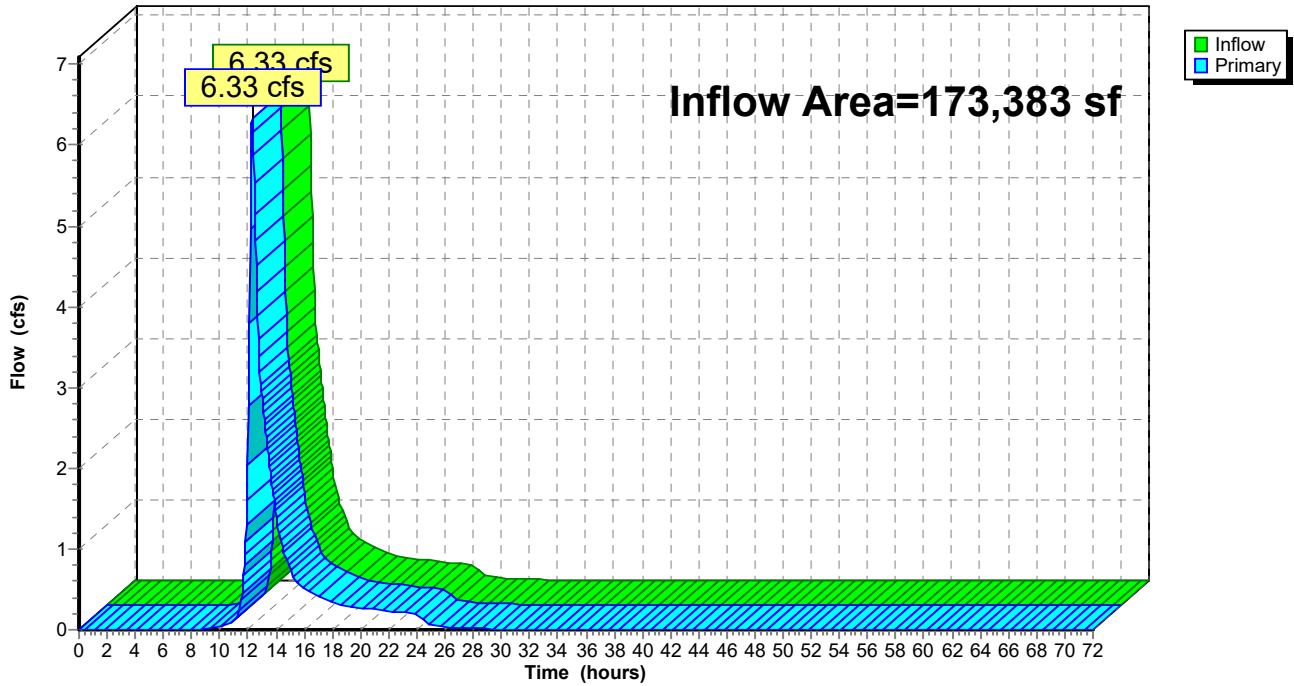
Summary for Link 13P: PDA 1

Inflow Area = 173,383 sf, 38.29% Impervious, Inflow Depth = 2.86" for 10-Year event
Inflow = 6.33 cfs @ 12.29 hrs, Volume= 41,268 cf
Primary = 6.33 cfs @ 12.29 hrs, Volume= 41,268 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 13P: PDA 1

Hydrograph



Pre vs Post

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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

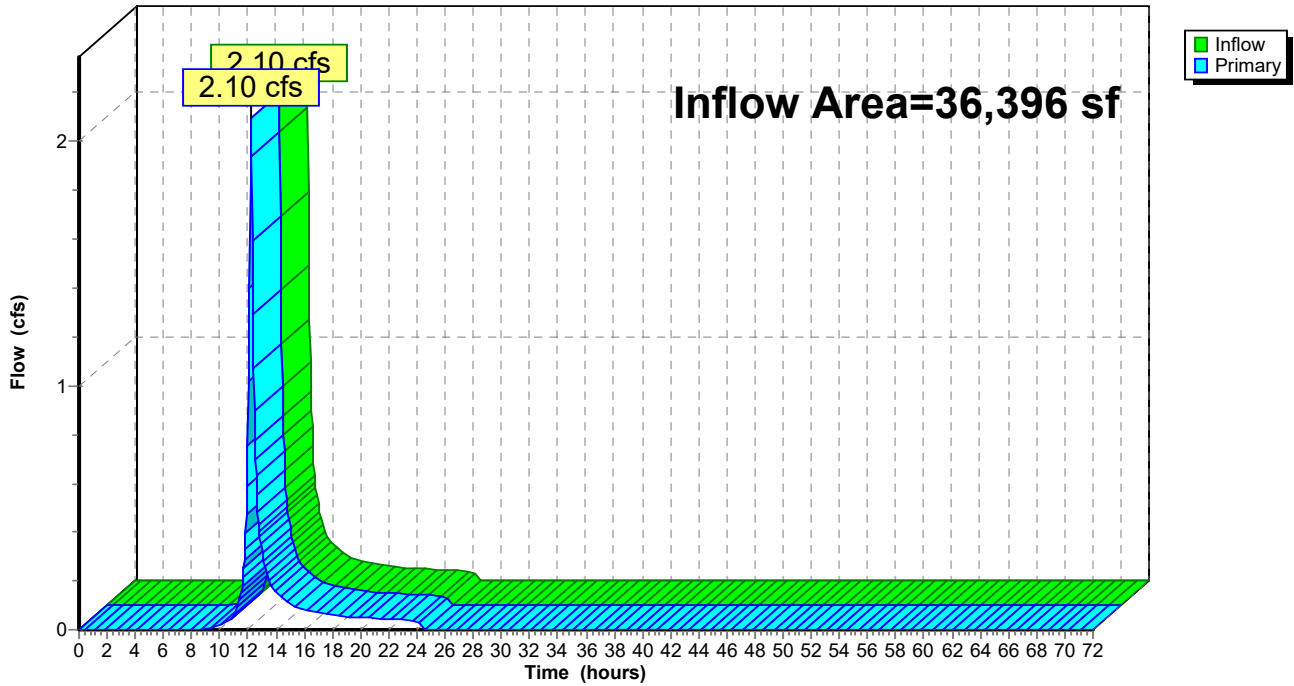
Summary for Link 14P: PDA 2

Inflow Area = 36,396 sf, 0.00% Impervious, Inflow Depth = 2.42" for 10-Year event
Inflow = 2.10 cfs @ 12.20 hrs, Volume= 7,347 cf
Primary = 2.10 cfs @ 12.20 hrs, Volume= 7,347 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 14P: PDA 2

Hydrograph



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NOAA 24-hr C 10-Year Rainfall=5.18"

Printed 5/14/2021

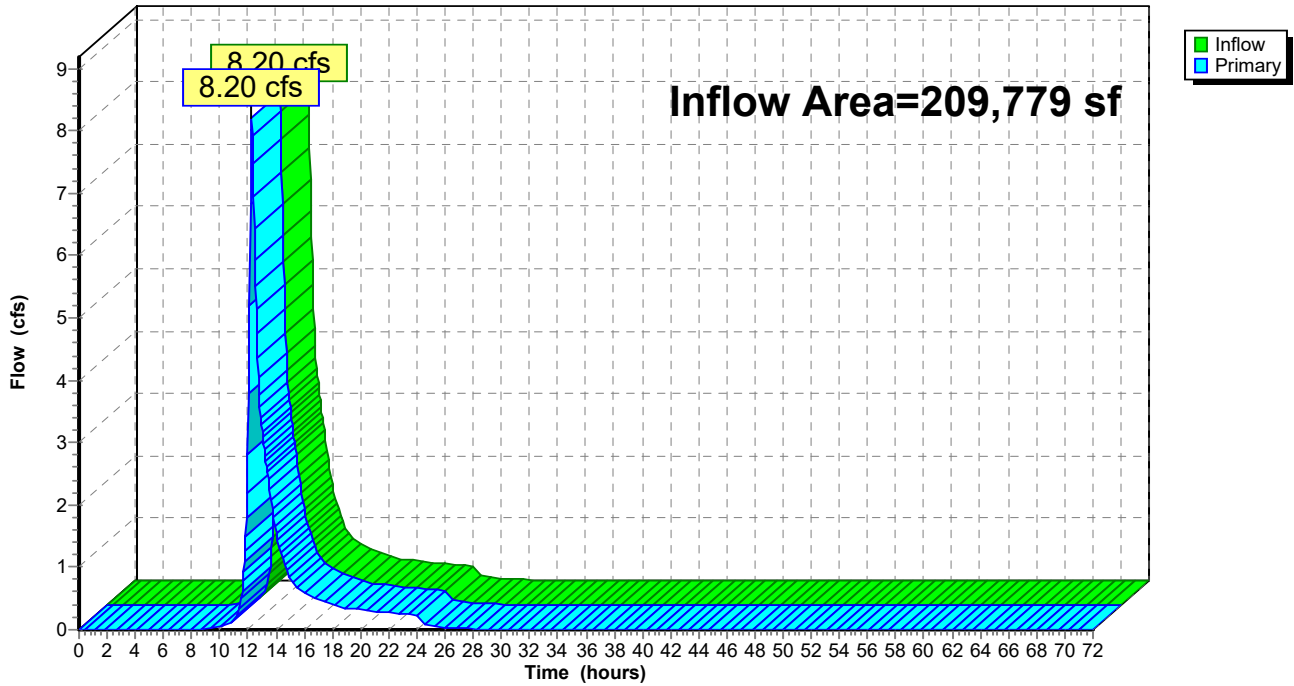
Summary for Link 15P: PDA

Inflow Area = 209,779 sf, 31.65% Impervious, Inflow Depth = 2.78" for 10-Year event
Inflow = 8.20 cfs @ 12.25 hrs, Volume= 48,616 cf
Primary = 8.20 cfs @ 12.25 hrs, Volume= 48,616 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 15P: PDA

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

Prepared by {enter your company name here}

Printed 5/14/2021

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv.
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

| | |
|--------------------------------------|---|
| Subcatchment 1E: Impervious | Runoff Area=10,351 sf 100.00% Impervious Runoff Depth=8.57" Tc=12.4 min CN=0/98 Runoff=1.79 cfs 7,392 cf |
| Subcatchment 1P: Impervious | Runoff Area=23,576 sf 100.00% Impervious Runoff Depth=8.57" Tc=10.7 min CN=0/98 Runoff=4.27 cfs 16,837 cf |
| Subcatchment 2E: Pervious | Runoff Area=167,702 sf 0.00% Impervious Runoff Depth=5.90" Flow Length=630' Tc=12.4 min CN=76/0 Runoff=23.14 cfs 82,456 cf |
| Subcatchment 2P: Pervious | Runoff Area=24,672 sf 0.00% Impervious Runoff Depth=5.66" Flow Length=426' Tc=10.7 min CN=74/0 Runoff=3.44 cfs 11,629 cf |
| Subcatchment 3E: Impervious | Runoff Area=5,641 sf 100.00% Impervious Runoff Depth=8.57" Tc=6.0 min CN=0/98 Runoff=1.18 cfs 4,028 cf |
| Subcatchment 3P: Roof Area | Runoff Area=35,418 sf 100.00% Impervious Runoff Depth=8.57" Tc=10.7 min CN=0/98 Runoff=6.41 cfs 25,294 cf |
| Subcatchment 4E: Pervious | Runoff Area=26,085 sf 0.00% Impervious Runoff Depth=7.24" Flow Length=393' Tc=6.0 min CN=87/0 Runoff=5.11 cfs 15,738 cf |
| Subcatchment 4P: Pervious | Runoff Area=13,613 sf 0.00% Impervious Runoff Depth=5.66" Tc=10.7 min CN=74/0 Runoff=1.90 cfs 6,416 cf |
| Subcatchment 5P: Impervious | Runoff Area=5,021 sf 97.63% Impervious Runoff Depth=8.56" Tc=20.8 min CN=96/98 Runoff=0.71 cfs 3,583 cf |
| Subcatchment 6P: Pervious | Runoff Area=6,701 sf 0.00% Impervious Runoff Depth=5.53" Flow Length=172' Tc=20.8 min CN=73/0 Runoff=0.70 cfs 3,090 cf |
| Subcatchment 7P: Impervious | Runoff Area=2,493 sf 100.00% Impervious Runoff Depth=8.57" Tc=13.9 min CN=0/98 Runoff=0.41 cfs 1,780 cf |
| Subcatchment 8P: Pervious | Runoff Area=61,889 sf 0.00% Impervious Runoff Depth=5.41" Flow Length=409' Tc=13.9 min CN=72/0 Runoff=7.54 cfs 27,912 cf |
| Subcatchment 9P: Pervious | Runoff Area=36,396 sf 0.00% Impervious Runoff Depth=5.53" Flow Length=471' Tc=12.2 min CN=73/0 Runoff=4.76 cfs 16,785 cf |
| Pond B1: Bioretention Basin 1 | Peak Elev=78.45' Storage=4,786 cf Inflow=7.70 cfs 28,466 cf Outflow=7.55 cfs 24,571 cf |
| Pond B2: Bioretention Basin 2 | Peak Elev=78.50' Storage=16,324 cf Inflow=15.77 cfs 56,281 cf Outflow=10.31 cfs 53,114 cf |
| Pond B3: Bioretention Basin 3 | Peak Elev=80.84' Storage=560 cf Inflow=1.41 cfs 6,674 cf Primary=1.41 cfs 6,199 cf Secondary=0.00 cfs 0 cf Outflow=1.41 cfs 6,199 cf |

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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| | |
|-------------------------|---|
| Link 5E: EDA 1 | Inflow=24.93 cfs 89,848 cf Primary=24.93 cfs 89,848 cf |
| Link 6E: EDA 2 | Inflow=6.29 cfs 19,767 cf Primary=6.29 cfs 19,767 cf |
| Link 7E: EDA | Inflow=29.37 cfs 109,615 cf Primary=29.37 cfs 109,615 cf |
| Link 10P: PDA 1A | Inflow=10.31 cfs 53,114 cf Primary=10.31 cfs 53,114 cf |
| Link 11P: PDA 1B | Inflow=1.41 cfs 6,199 cf Primary=1.41 cfs 6,199 cf |
| Link 12P: PDA 1C | Inflow=7.95 cfs 29,692 cf Primary=7.95 cfs 29,692 cf |
| Link 13P: PDA 1 | Inflow=19.24 cfs 89,005 cf Primary=19.24 cfs 89,005 cf |
| Link 14P: PDA 2 | Inflow=4.76 cfs 16,785 cf Primary=4.76 cfs 16,785 cf |
| Link 15P: PDA | Inflow=23.53 cfs 105,790 cf Primary=23.53 cfs 105,790 cf |

Total Runoff Area = 419,558 sf Runoff Volume = 222,941 cf Average Runoff Depth = 6.38"
80.36% Pervious = 337,177 sf 19.64% Impervious = 82,381 sf

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 1E: Impervious

Runoff = 1.79 cfs @ 12.20 hrs, Volume= 7,392 cf, Depth= 8.57"

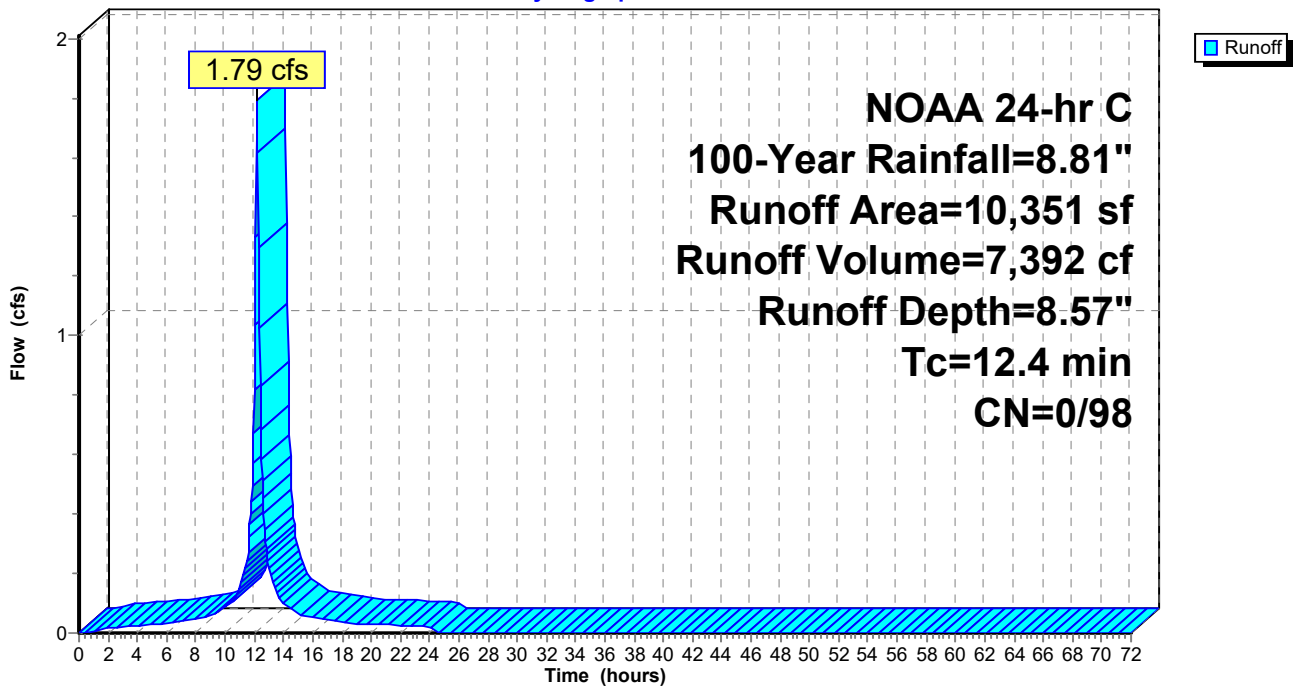
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 3,299 | 98 | Unconnected roofs, HSG C |
| 7,052 | 98 | Paved parking, HSG C |
| 10,351 | 98 | Weighted Average |
| 10,351 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 12.4 | | | | | Direct Entry, Tc |

Subcatchment 1E: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 1P: Impervious

Runoff = 4.27 cfs @ 12.18 hrs, Volume= 16,837 cf, Depth= 8.57"

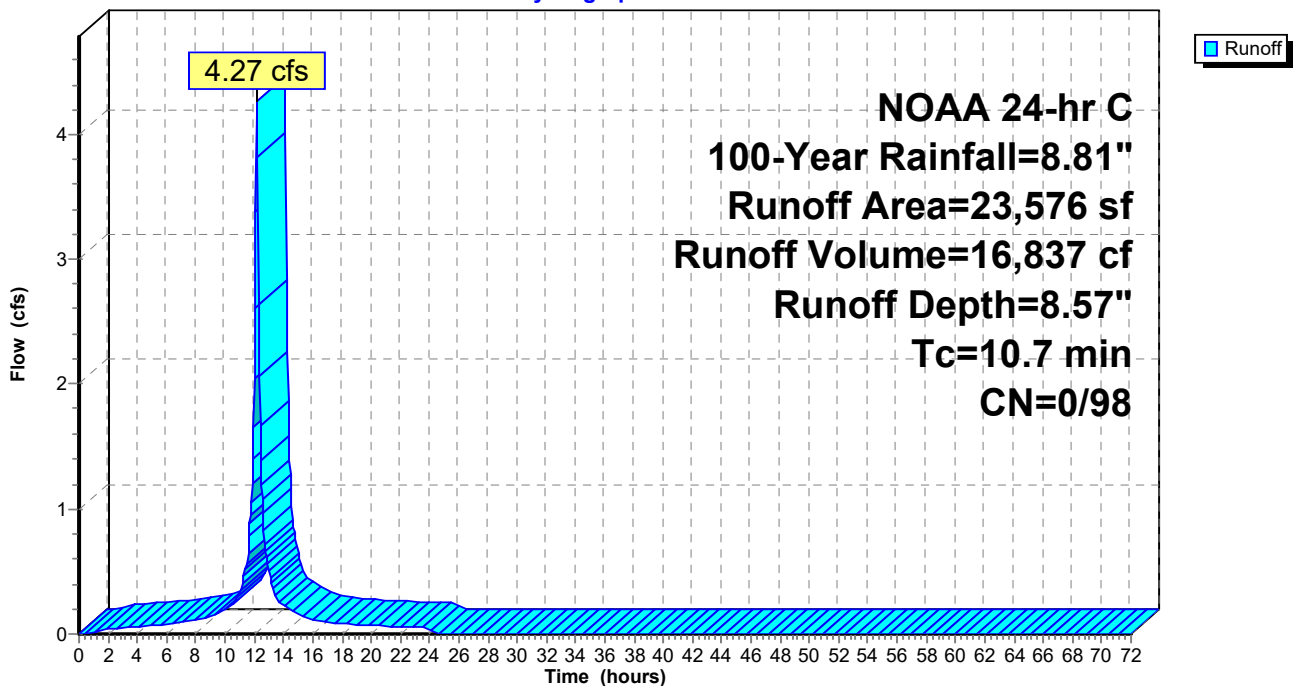
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 23,576 | 98 | Paved parking, HSG C |
| 23,576 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 1P: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 2E: Pervious

Runoff = 23.14 cfs @ 12.20 hrs, Volume= 82,456 cf, Depth= 5.90"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 24,589 | 96 | Gravel surface, HSG C |
| 36,591 | 70 | Woods, Good, HSG C |
| 105,816 | 74 | >75% Grass cover, Good, HSG C |
| 706 | 72 | Woods/grass comb., Good, HSG C |
| 167,702 | 76 | Weighted Average |
| 167,702 | 76 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 0.3 | 27 | 0.0490 | 1.55 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 8.8 | 73 | 0.0130 | 0.14 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.4 | 54 | 0.0180 | 2.16 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 1.2 | 207 | 0.0340 | 2.97 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.5 | 59 | 0.0170 | 2.10 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 0.2 | 43 | 0.0470 | 3.49 | | Shallow Concentrated Flow, F-G Unpaved Kv= 16.1 fps |
| 1.0 | 167 | 0.0280 | 2.69 | | Shallow Concentrated Flow, G-H Unpaved Kv= 16.1 fps |
| 12.4 | 630 | Total | | | |

Pre vs Post

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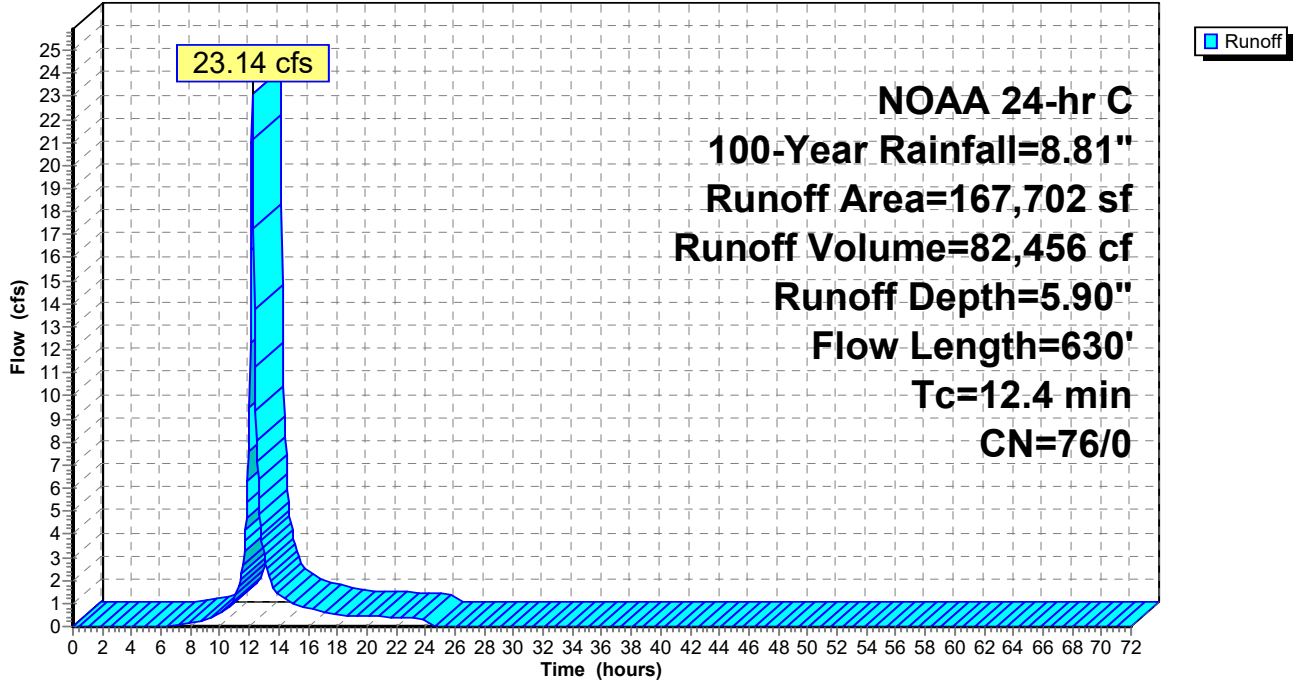
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NOAA 24-hr C 100-Year Rainfall=8.81"

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Subcatchment 2E: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 2P: Pervious

Runoff = 3.44 cfs @ 12.18 hrs, Volume= 11,629 cf, Depth= 5.66"

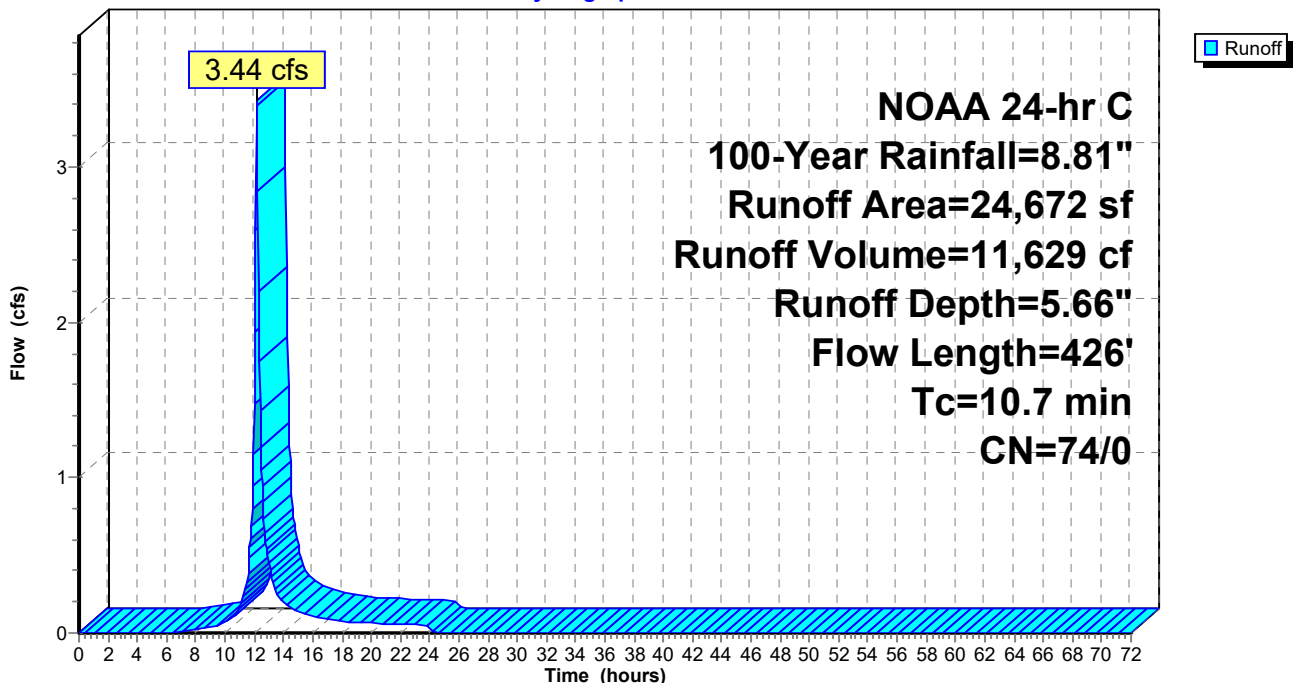
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 22,852 | 74 | >75% Grass cover, Good, HSG C |
| 1,820 | 72 | Woods/grass comb., Good, HSG C |
| 24,672 | 74 | Weighted Average |
| 24,672 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 9.2 | 100 | 0.0222 | 0.18 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.1 | 23 | 0.0730 | 4.35 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.3 | 48 | 0.0210 | 2.94 | | Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps |
| 1.1 | 255 | 0.0050 | 3.72 | 4.57 | Pipe Channel, D-E 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013 Concrete pipe, bends & connections |
| 10.7 | 426 | Total | | | |

Subcatchment 2P: Pervious

Hydrograph



Pre vs Post

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NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 3E: Impervious

Runoff = 1.18 cfs @ 12.13 hrs, Volume= 4,028 cf, Depth= 8.57"

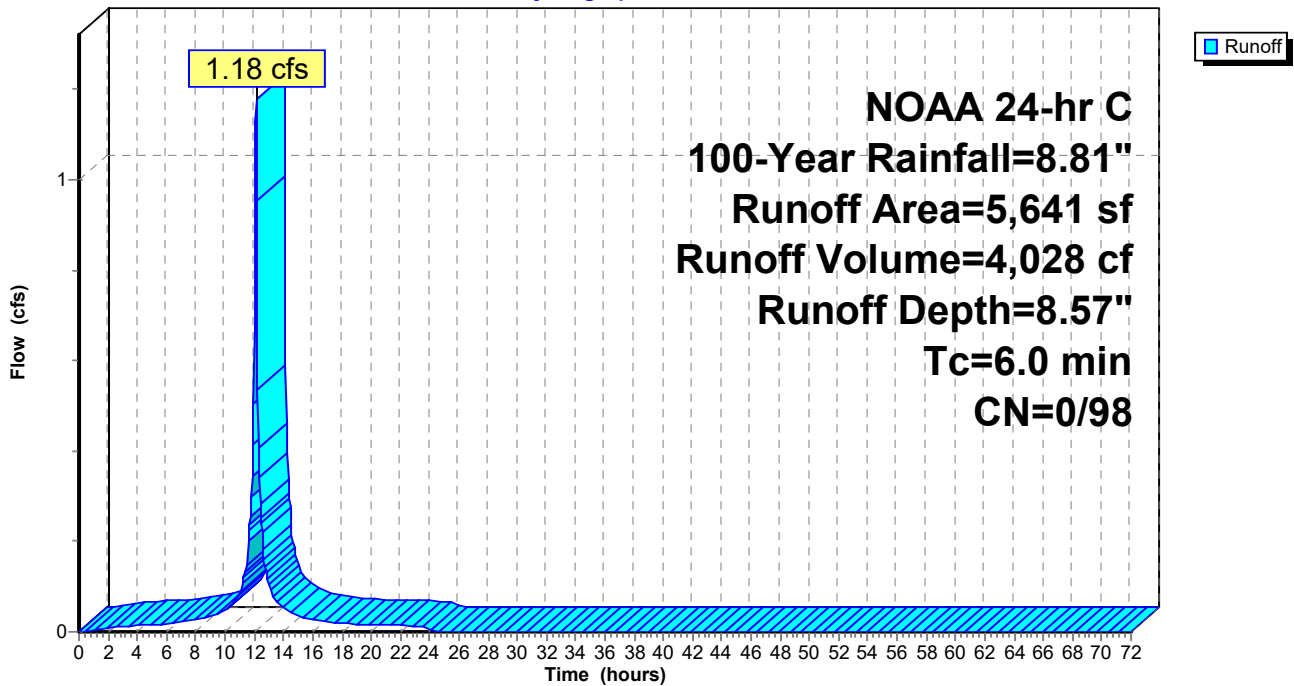
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|--------------------------|
| 2,580 | 98 | Unconnected roofs, HSG C |
| 3,061 | 98 | Paved parking, HSG C |
| 5,641 | 98 | Weighted Average |
| 5,641 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|-------------------------|
| 3.0 | | | | | Direct Entry, Tc |
| 3.0 | 0 | Total, Increased to minimum Tc = 6.0 min | | | |

Subcatchment 3E: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 3P: Roof Area

Runoff = 6.41 cfs @ 12.18 hrs, Volume= 25,294 cf, Depth= 8.57"

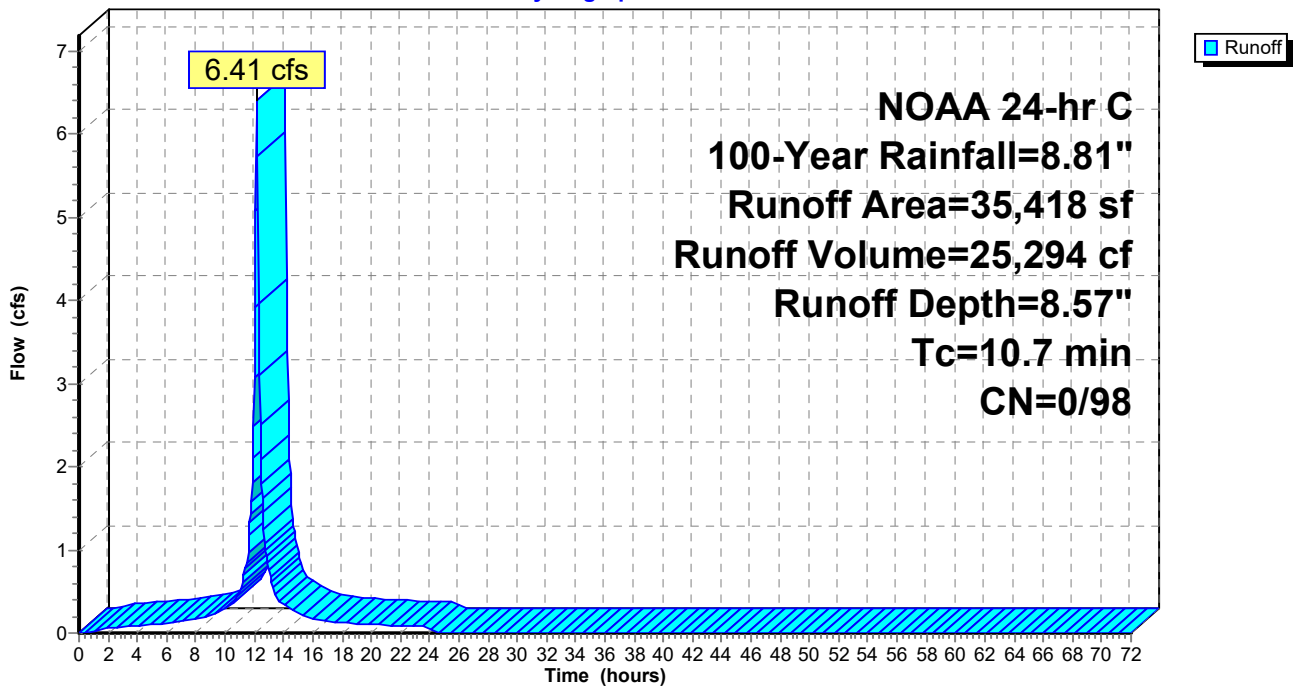
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|-----------------------------|
| 35,068 | 98 | Unconnected roofs, HSG C |
| 350 | 98 | Unconnected pavement, HSG C |
| 35,418 | 98 | Weighted Average |
| 35,418 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 3P: Roof Area

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 4E: Pervious

Runoff = 5.11 cfs @ 12.13 hrs, Volume= 15,738 cf, Depth= 7.24"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 164 | 70 | Woods, Good, HSG C |
| 16,189 | 96 | Gravel surface, HSG C |
| 5,108 | 74 | >75% Grass cover, Good, HSG C |
| 4,624 | 72 | Woods/grass comb., Good, HSG C |
| 26,085 | 87 | Weighted Average |
| 26,085 | 87 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|--|-------------------|----------------|---|
| 1.3 | 100 | 0.0160 | 1.29 | | Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.36" |
| 0.6 | 97 | 0.0200 | 2.87 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 1.0 | 175 | 0.0330 | 2.92 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.1 | 13 | 0.0230 | 2.44 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.0 | 8 | 0.0480 | 3.53 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 3.0 | 393 | Total, Increased to minimum Tc = 6.0 min | | | |

Pre vs Post

Prepared by {enter your company name here}

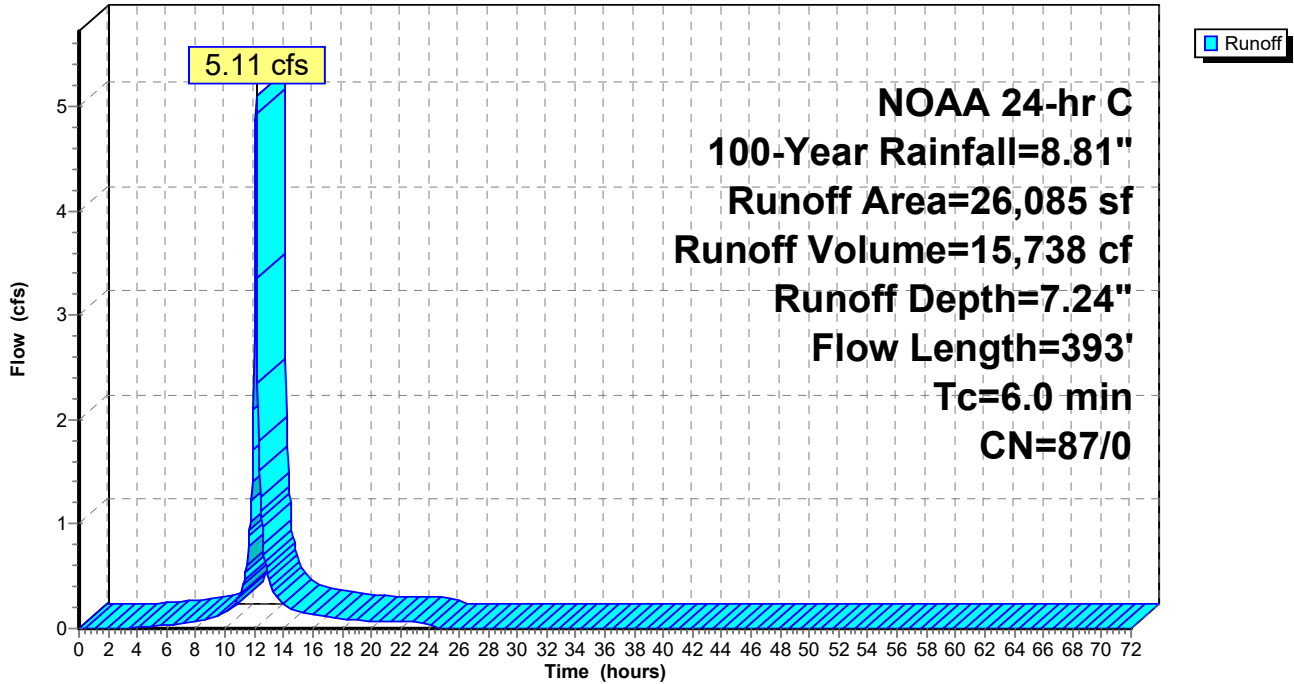
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NOAA 24-hr C 100-Year Rainfall=8.81"

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Subcatchment 4E: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 4P: Pervious

Runoff = 1.90 cfs @ 12.18 hrs, Volume= 6,416 cf, Depth= 5.66"

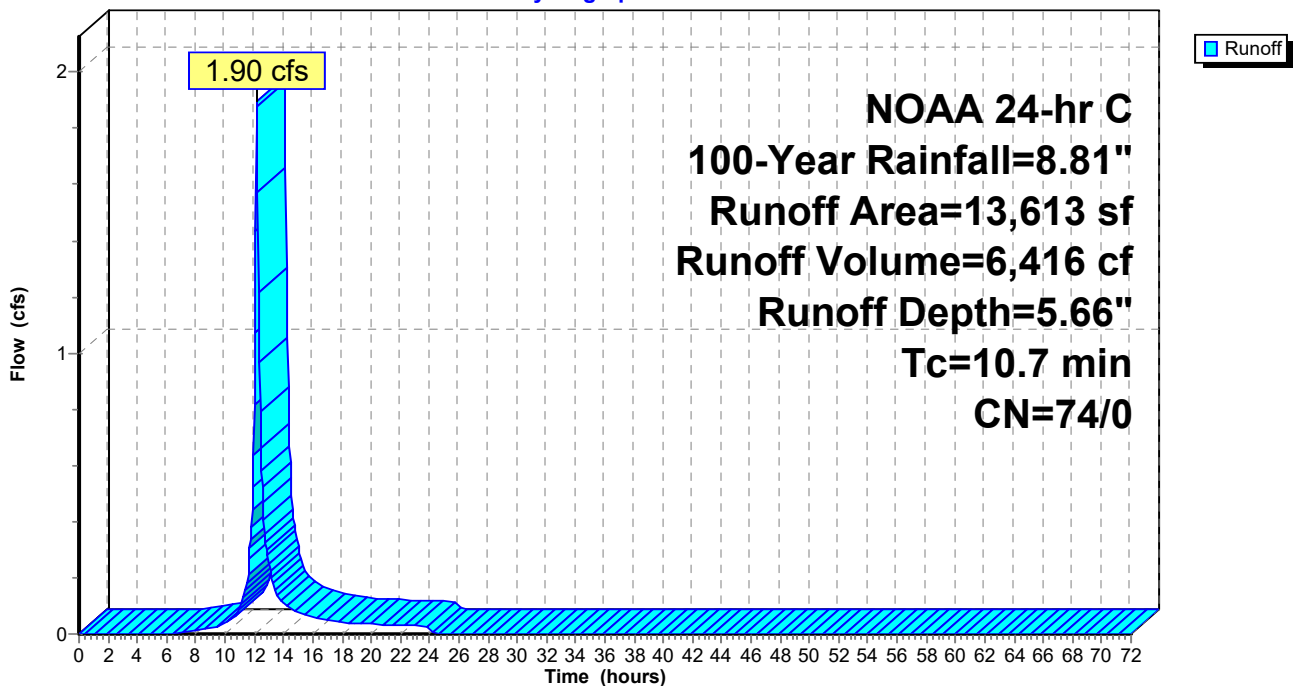
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 13,613 | 74 | >75% Grass cover, Good, HSG C |
| 13,613 | 74 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 10.7 | | | | | Direct Entry, Tc |

Subcatchment 4P: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 5P: Impervious

Runoff = 0.71 cfs @ 12.29 hrs, Volume= 3,583 cf, Depth= 8.56"

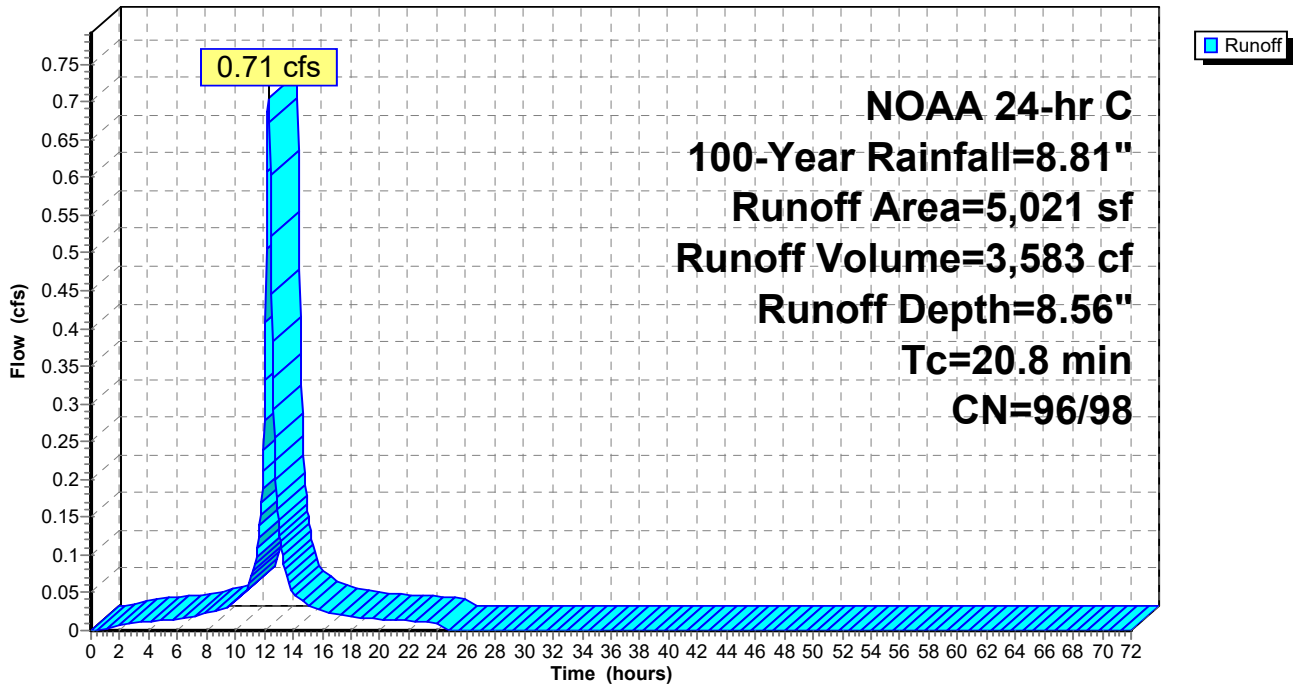
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|------------------------|
| 4,902 | 98 | Paved parking, HSG C |
| 119 | 96 | Gravel surface, HSG C |
| 5,021 | 98 | Weighted Average |
| 119 | 96 | 2.37% Pervious Area |
| 4,902 | 98 | 97.63% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 20.8 | | | | | Direct Entry, Tc |

Subcatchment 5P: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 6P: Pervious

Runoff = 0.70 cfs @ 12.30 hrs, Volume= 3,090 cf, Depth= 5.53"

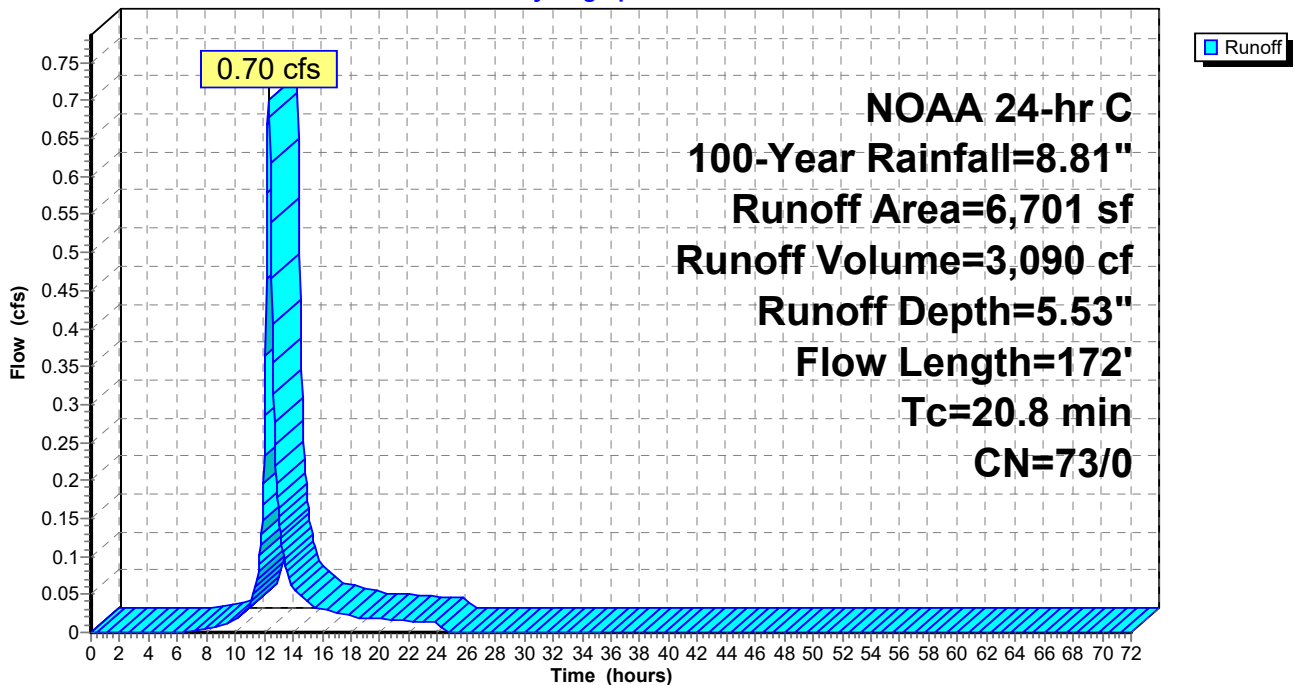
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 4,509 | 74 | >75% Grass cover, Good, HSG C |
| 2,192 | 70 | Woods, Good, HSG C |
| 6,701 | 73 | Weighted Average |
| 6,701 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|--|
| 20.4 | 104 | 0.0230 | 0.08 | | Sheet Flow, A-B Woods: Light underbrush n= 0.400 P2= 3.36" |
| 0.3 | 57 | 0.0230 | 3.08 | | Shallow Concentrated Flow, B-C Paved Kv= 20.3 fps |
| 0.1 | 11 | 0.0200 | 2.28 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 20.8 | 172 | Total | | | |

Subcatchment 6P: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 7P: Impervious

Runoff = 0.41 cfs @ 12.21 hrs, Volume= 1,780 cf, Depth= 8.57"

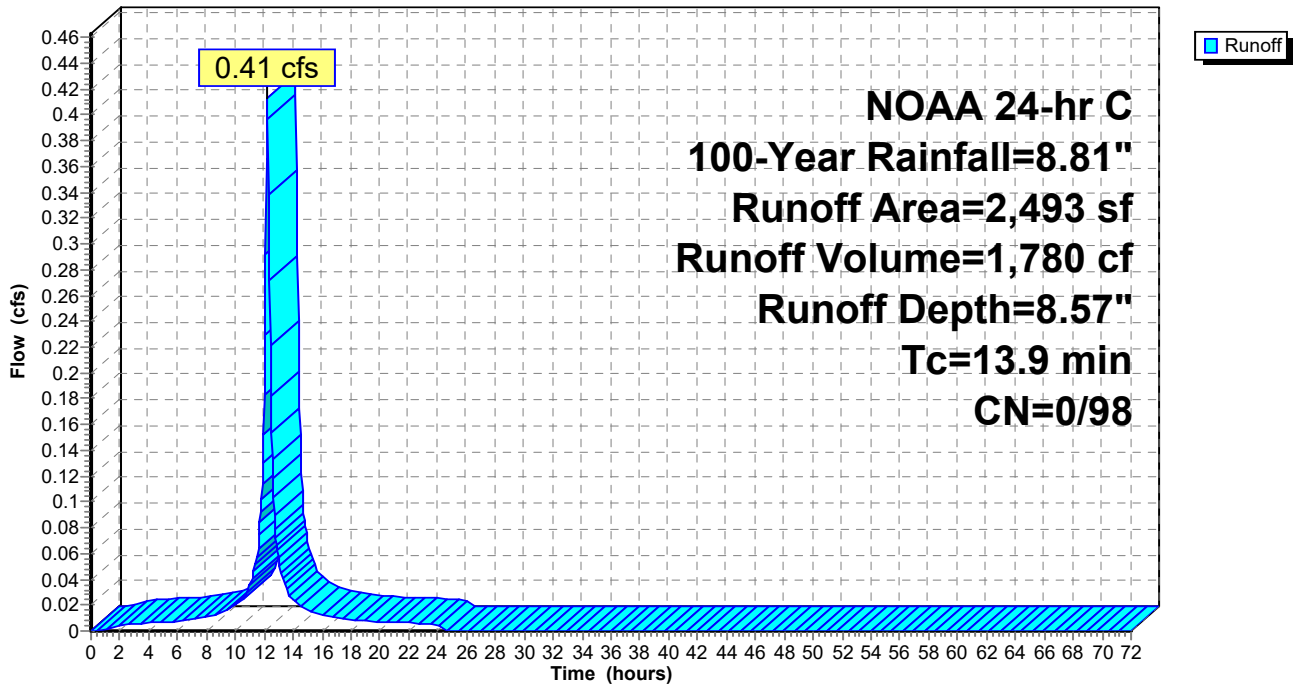
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|-------------------------|
| 2,493 | 98 | Paved parking, HSG C |
| 2,493 | 98 | 100.00% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|------------------|
| 13.9 | | | | | Direct Entry, Tc |

Subcatchment 7P: Impervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

Prepared by {enter your company name here}

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Summary for Subcatchment 8P: Pervious

Runoff = 7.54 cfs @ 12.22 hrs, Volume= 27,912 cf, Depth= 5.41"

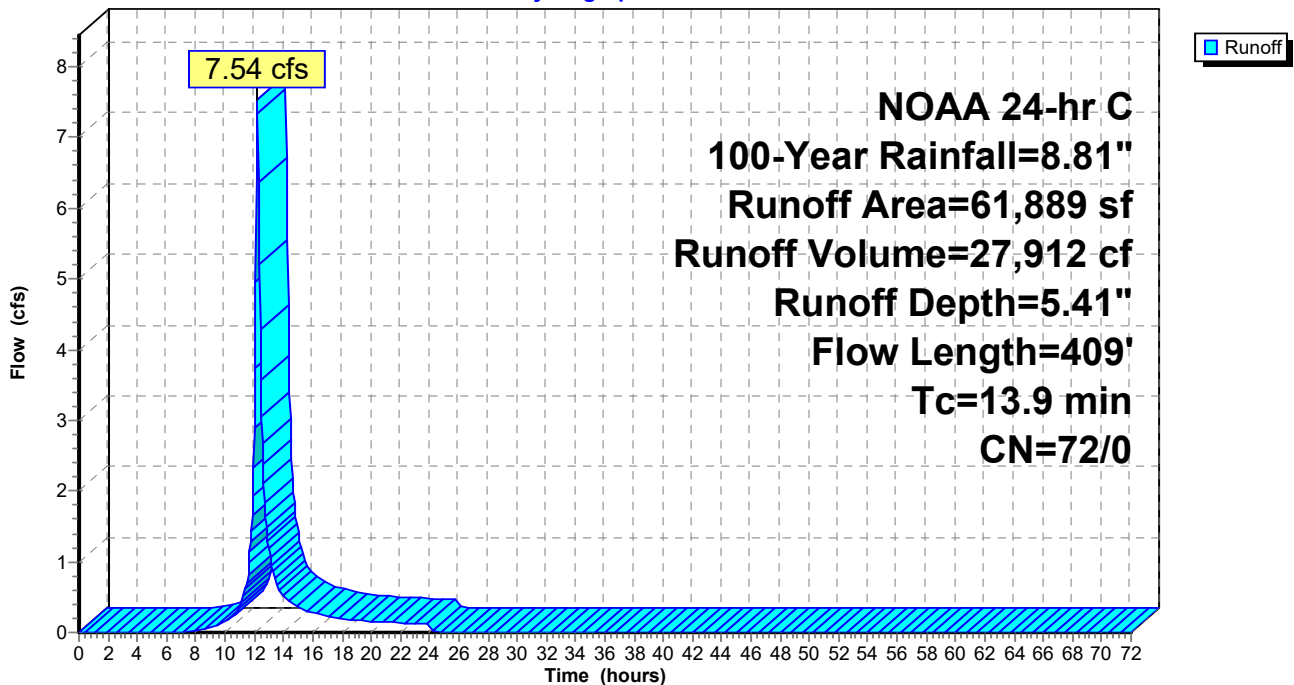
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 28,675 | 70 | Woods, Good, HSG C |
| 33,214 | 74 | >75% Grass cover, Good, HSG C |
| 61,889 | 72 | Weighted Average |
| 61,889 | 72 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 2.8 | 36 | 0.0560 | 0.21 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 4.3 | 51 | 0.0390 | 0.20 | | Sheet Flow, B-C Grass: Short n= 0.150 P2= 3.36" |
| 0.3 | 25 | 0.0800 | 1.41 | | Shallow Concentrated Flow, C-D Woodland Kv= 5.0 fps |
| 6.5 | 297 | 0.0230 | 0.76 | | Shallow Concentrated Flow, D-E Woodland Kv= 5.0 fps |
| 13.9 | 409 | Total | | | |

Subcatchment 8P: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Subcatchment 9P: Pervious

Runoff = 4.76 cfs @ 12.20 hrs, Volume= 16,785 cf, Depth= 5.53"

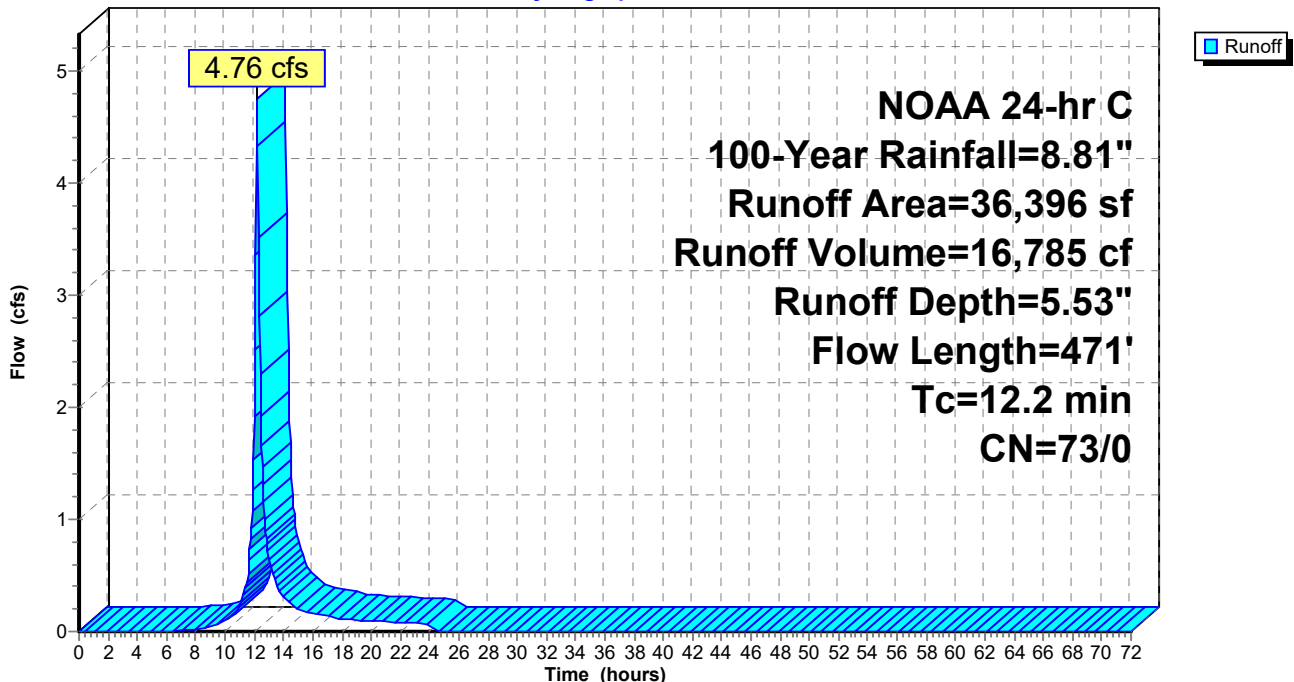
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 NOAA 24-hr C 100-Year Rainfall=8.81"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 5,369 | 70 | Woods, Good, HSG C |
| 31,027 | 74 | >75% Grass cover, Good, HSG C |
| 36,396 | 73 | Weighted Average |
| 36,396 | 73 | 100.00% Pervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|----------|---------------|---------------|-------------------|----------------|---|
| 9.8 | 100 | 0.0190 | 0.17 | | Sheet Flow, A-B Grass: Short n= 0.150 P2= 3.36" |
| 0.7 | 102 | 0.0240 | 2.49 | | Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps |
| 0.8 | 128 | 0.0310 | 2.83 | | Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps |
| 0.8 | 120 | 0.0250 | 2.55 | | Shallow Concentrated Flow, D-E Unpaved Kv= 16.1 fps |
| 0.1 | 21 | 0.0310 | 2.83 | | Shallow Concentrated Flow, E-F Unpaved Kv= 16.1 fps |
| 12.2 | 471 | Total | | | |

Subcatchment 9P: Pervious

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Pond B1: Bioretention Basin 1

[92] Warning: Device #2 is above defined storage

Inflow Area = 48,248 sf, 48.86% Impervious, Inflow Depth = 7.08" for 100-Year event
 Inflow = 7.70 cfs @ 12.18 hrs, Volume= 28,466 cf
 Outflow = 7.55 cfs @ 12.20 hrs, Volume= 24,571 cf, Atten= 2%, Lag= 1.4 min
 Primary = 7.55 cfs @ 12.20 hrs, Volume= 24,571 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 78.45' @ 12.20 hrs Surf.Area= 3,063 sf Storage= 4,786 cf

Plug-Flow detention time= 117.1 min calculated for 24,554 cf (86% of inflow)
 Center-of-Mass det. time= 52.5 min (828.0 - 775.5)

| Volume | Invert | Avail.Storage | Storage Description | |
|------------------|-------------------|------------------------|--|------------------|
| #1 | 76.50' | 4,938 cf | Custom Stage Data (Conic) Listed below (Recalc) | |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
| 76.50 | 1,883 | 0 | 0 | 1,883 |
| 77.50 | 2,461 | 2,166 | 2,166 | 2,484 |
| 78.50 | 3,096 | 2,772 | 4,938 | 3,146 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|---|
| #1 | Primary | 73.00' | 24.0" Round CMP_Round 24" L= 10.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.85' S= 0.0150 ' S Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf |
| #2 | Device 1 | 78.50' | 10.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 78.15' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=7.50 cfs @ 12.20 hrs HW=78.45' (Free Discharge)
 1=CMP_Round 24" (Passes 7.50 cfs of 25.19 cfs potential flow)
 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
 3=Orifice/Grate (Weir Controls 7.50 cfs @ 1.79 fps)

Pre vs Post

Prepared by {enter your company name here}

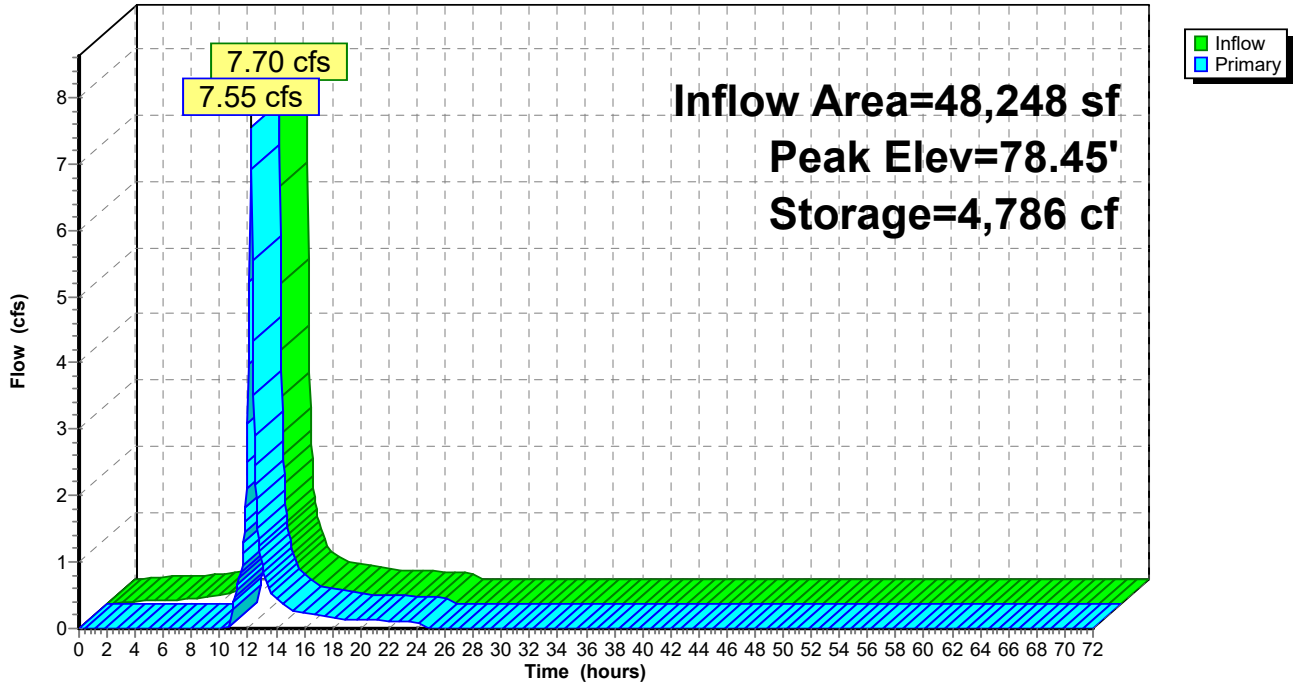
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NOAA 24-hr C 100-Year Rainfall=8.81"

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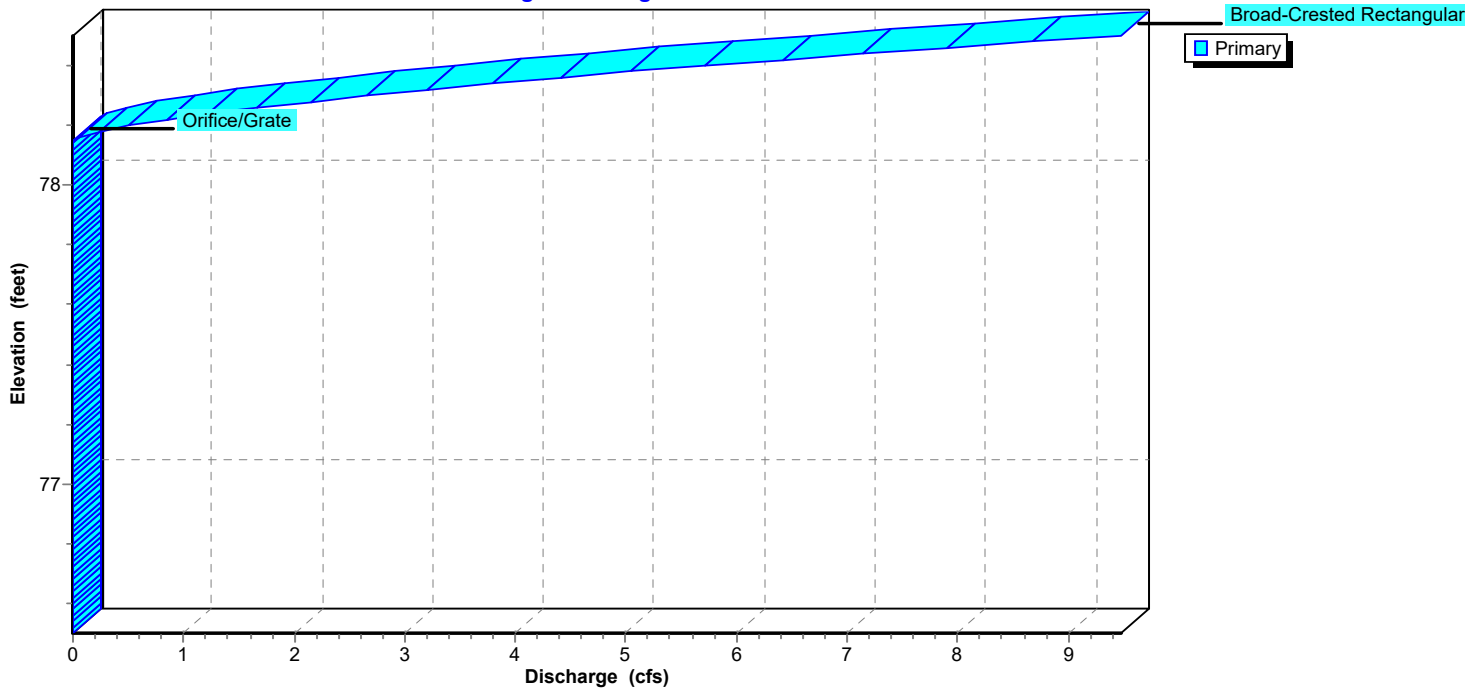
Pond B1: Bioretention Basin 1

Hydrograph



Pond B1: Bioretention Basin 1

Stage-Discharge



Pre vs Post

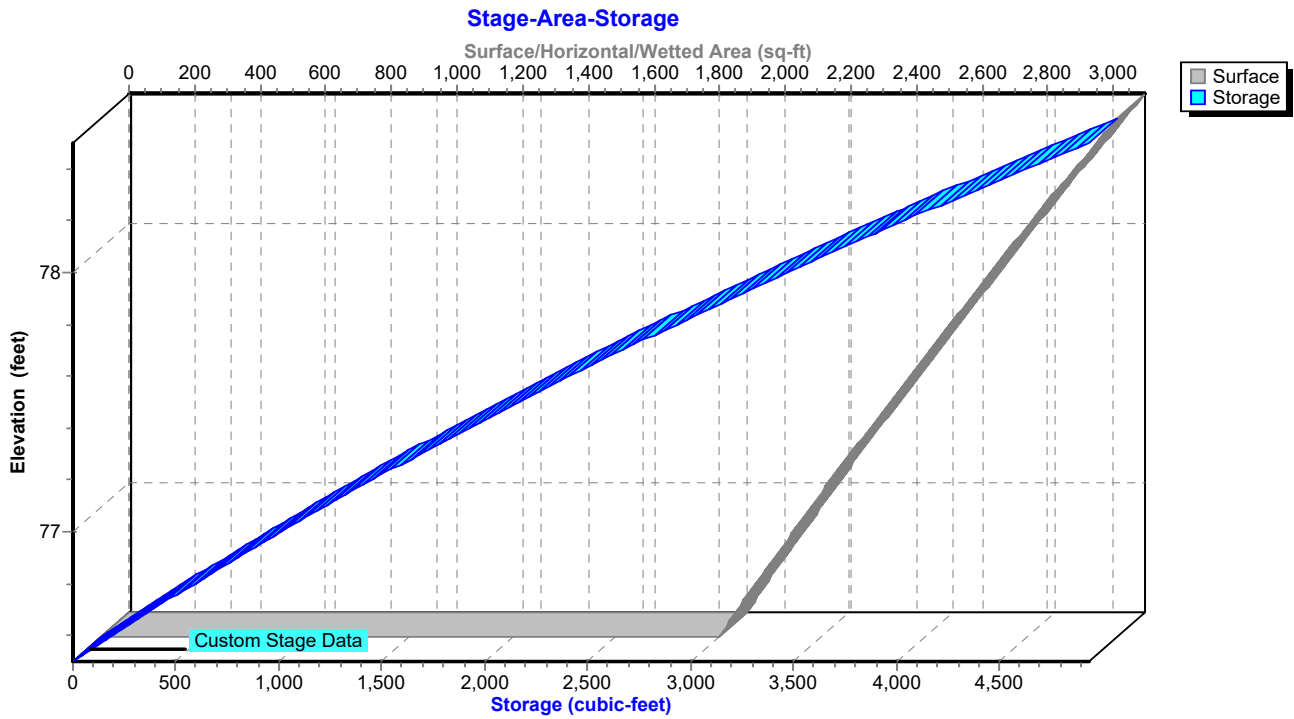
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Pond B1: Bioretention Basin 1



Pre vs Post

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Stage-Discharge for Pond B1: Bioretention Basin 1

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.03 | 0.00 | 77.56 | 0.00 | 78.09 | 0.00 |
| 76.51 | 0.00 | 77.04 | 0.00 | 77.57 | 0.00 | 78.10 | 0.00 |
| 76.52 | 0.00 | 77.05 | 0.00 | 77.58 | 0.00 | 78.11 | 0.00 |
| 76.53 | 0.00 | 77.06 | 0.00 | 77.59 | 0.00 | 78.12 | 0.00 |
| 76.54 | 0.00 | 77.07 | 0.00 | 77.60 | 0.00 | 78.13 | 0.00 |
| 76.55 | 0.00 | 77.08 | 0.00 | 77.61 | 0.00 | 78.14 | 0.00 |
| 76.56 | 0.00 | 77.09 | 0.00 | 77.62 | 0.00 | 78.15 | 0.00 |
| 76.57 | 0.00 | 77.10 | 0.00 | 77.63 | 0.00 | 78.16 | 0.05 |
| 76.58 | 0.00 | 77.11 | 0.00 | 77.64 | 0.00 | 78.17 | 0.13 |
| 76.59 | 0.00 | 77.12 | 0.00 | 77.65 | 0.00 | 78.18 | 0.24 |
| 76.60 | 0.00 | 77.13 | 0.00 | 77.66 | 0.00 | 78.19 | 0.37 |
| 76.61 | 0.00 | 77.14 | 0.00 | 77.67 | 0.00 | 78.20 | 0.51 |
| 76.62 | 0.00 | 77.15 | 0.00 | 77.68 | 0.00 | 78.21 | 0.67 |
| 76.63 | 0.00 | 77.16 | 0.00 | 77.69 | 0.00 | 78.22 | 0.85 |
| 76.64 | 0.00 | 77.17 | 0.00 | 77.70 | 0.00 | 78.23 | 1.04 |
| 76.65 | 0.00 | 77.18 | 0.00 | 77.71 | 0.00 | 78.24 | 1.24 |
| 76.66 | 0.00 | 77.19 | 0.00 | 77.72 | 0.00 | 78.25 | 1.45 |
| 76.67 | 0.00 | 77.20 | 0.00 | 77.73 | 0.00 | 78.26 | 1.67 |
| 76.68 | 0.00 | 77.21 | 0.00 | 77.74 | 0.00 | 78.27 | 1.90 |
| 76.69 | 0.00 | 77.22 | 0.00 | 77.75 | 0.00 | 78.28 | 2.15 |
| 76.70 | 0.00 | 77.23 | 0.00 | 77.76 | 0.00 | 78.29 | 2.40 |
| 76.71 | 0.00 | 77.24 | 0.00 | 77.77 | 0.00 | 78.30 | 2.66 |
| 76.72 | 0.00 | 77.25 | 0.00 | 77.78 | 0.00 | 78.31 | 2.93 |
| 76.73 | 0.00 | 77.26 | 0.00 | 77.79 | 0.00 | 78.32 | 3.21 |
| 76.74 | 0.00 | 77.27 | 0.00 | 77.80 | 0.00 | 78.33 | 3.50 |
| 76.75 | 0.00 | 77.28 | 0.00 | 77.81 | 0.00 | 78.34 | 3.79 |
| 76.76 | 0.00 | 77.29 | 0.00 | 77.82 | 0.00 | 78.35 | 4.09 |
| 76.77 | 0.00 | 77.30 | 0.00 | 77.83 | 0.00 | 78.36 | 4.41 |
| 76.78 | 0.00 | 77.31 | 0.00 | 77.84 | 0.00 | 78.37 | 4.72 |
| 76.79 | 0.00 | 77.32 | 0.00 | 77.85 | 0.00 | 78.38 | 5.05 |
| 76.80 | 0.00 | 77.33 | 0.00 | 77.86 | 0.00 | 78.39 | 5.38 |
| 76.81 | 0.00 | 77.34 | 0.00 | 77.87 | 0.00 | 78.40 | 5.72 |
| 76.82 | 0.00 | 77.35 | 0.00 | 77.88 | 0.00 | 78.41 | 6.07 |
| 76.83 | 0.00 | 77.36 | 0.00 | 77.89 | 0.00 | 78.42 | 6.42 |
| 76.84 | 0.00 | 77.37 | 0.00 | 77.90 | 0.00 | 78.43 | 6.78 |
| 76.85 | 0.00 | 77.38 | 0.00 | 77.91 | 0.00 | 78.44 | 7.15 |
| 76.86 | 0.00 | 77.39 | 0.00 | 77.92 | 0.00 | 78.45 | 7.52 |
| 76.87 | 0.00 | 77.40 | 0.00 | 77.93 | 0.00 | 78.46 | 7.90 |
| 76.88 | 0.00 | 77.41 | 0.00 | 77.94 | 0.00 | 78.47 | 8.29 |
| 76.89 | 0.00 | 77.42 | 0.00 | 77.95 | 0.00 | 78.48 | 8.68 |
| 76.90 | 0.00 | 77.43 | 0.00 | 77.96 | 0.00 | 78.49 | 9.08 |
| 76.91 | 0.00 | 77.44 | 0.00 | 77.97 | 0.00 | 78.50 | 9.48 |
| 76.92 | 0.00 | 77.45 | 0.00 | 77.98 | 0.00 | | |
| 76.93 | 0.00 | 77.46 | 0.00 | 77.99 | 0.00 | | |
| 76.94 | 0.00 | 77.47 | 0.00 | 78.00 | 0.00 | | |
| 76.95 | 0.00 | 77.48 | 0.00 | 78.01 | 0.00 | | |
| 76.96 | 0.00 | 77.49 | 0.00 | 78.02 | 0.00 | | |
| 76.97 | 0.00 | 77.50 | 0.00 | 78.03 | 0.00 | | |
| 76.98 | 0.00 | 77.51 | 0.00 | 78.04 | 0.00 | | |
| 76.99 | 0.00 | 77.52 | 0.00 | 78.05 | 0.00 | | |
| 77.00 | 0.00 | 77.53 | 0.00 | 78.06 | 0.00 | | |
| 77.01 | 0.00 | 77.54 | 0.00 | 78.07 | 0.00 | | |
| 77.02 | 0.00 | 77.55 | 0.00 | 78.08 | 0.00 | | |

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Stage-Area-Storage for Pond B1: Bioretention Basin 1

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 1,883 | 0 | 77.56 | 2,497 | 2,314 |
| 76.52 | 1,894 | 38 | 77.58 | 2,509 | 2,364 |
| 76.54 | 1,905 | 76 | 77.60 | 2,521 | 2,415 |
| 76.56 | 1,916 | 114 | 77.62 | 2,533 | 2,465 |
| 76.58 | 1,926 | 152 | 77.64 | 2,546 | 2,516 |
| 76.60 | 1,937 | 191 | 77.66 | 2,558 | 2,567 |
| 76.62 | 1,948 | 230 | 77.68 | 2,570 | 2,618 |
| 76.64 | 1,959 | 269 | 77.70 | 2,582 | 2,670 |
| 76.66 | 1,970 | 308 | 77.72 | 2,594 | 2,722 |
| 76.68 | 1,981 | 348 | 77.74 | 2,607 | 2,774 |
| 76.70 | 1,992 | 387 | 77.76 | 2,619 | 2,826 |
| 76.72 | 2,004 | 427 | 77.78 | 2,631 | 2,878 |
| 76.74 | 2,015 | 468 | 77.80 | 2,644 | 2,931 |
| 76.76 | 2,026 | 508 | 77.82 | 2,656 | 2,984 |
| 76.78 | 2,037 | 549 | 77.84 | 2,669 | 3,037 |
| 76.80 | 2,048 | 590 | 77.86 | 2,681 | 3,091 |
| 76.82 | 2,060 | 631 | 77.88 | 2,694 | 3,145 |
| 76.84 | 2,071 | 672 | 77.90 | 2,706 | 3,199 |
| 76.86 | 2,082 | 713 | 77.92 | 2,719 | 3,253 |
| 76.88 | 2,094 | 755 | 77.94 | 2,731 | 3,307 |
| 76.90 | 2,105 | 797 | 77.96 | 2,744 | 3,362 |
| 76.92 | 2,116 | 839 | 77.98 | 2,757 | 3,417 |
| 76.94 | 2,128 | 882 | 78.00 | 2,769 | 3,472 |
| 76.96 | 2,139 | 924 | 78.02 | 2,782 | 3,528 |
| 76.98 | 2,151 | 967 | 78.04 | 2,795 | 3,584 |
| 77.00 | 2,162 | 1,011 | 78.06 | 2,808 | 3,640 |
| 77.02 | 2,174 | 1,054 | 78.08 | 2,820 | 3,696 |
| 77.04 | 2,186 | 1,097 | 78.10 | 2,833 | 3,753 |
| 77.06 | 2,197 | 1,141 | 78.12 | 2,846 | 3,809 |
| 77.08 | 2,209 | 1,185 | 78.14 | 2,859 | 3,866 |
| 77.10 | 2,221 | 1,230 | 78.16 | 2,872 | 3,924 |
| 77.12 | 2,232 | 1,274 | 78.18 | 2,885 | 3,981 |
| 77.14 | 2,244 | 1,319 | 78.20 | 2,898 | 4,039 |
| 77.16 | 2,256 | 1,364 | 78.22 | 2,911 | 4,097 |
| 77.18 | 2,268 | 1,409 | 78.24 | 2,924 | 4,156 |
| 77.20 | 2,279 | 1,455 | 78.26 | 2,937 | 4,214 |
| 77.22 | 2,291 | 1,500 | 78.28 | 2,950 | 4,273 |
| 77.24 | 2,303 | 1,546 | 78.30 | 2,963 | 4,332 |
| 77.26 | 2,315 | 1,593 | 78.32 | 2,976 | 4,392 |
| 77.28 | 2,327 | 1,639 | 78.34 | 2,990 | 4,451 |
| 77.30 | 2,339 | 1,686 | 78.36 | 3,003 | 4,511 |
| 77.32 | 2,351 | 1,732 | 78.38 | 3,016 | 4,571 |
| 77.34 | 2,363 | 1,780 | 78.40 | 3,029 | 4,632 |
| 77.36 | 2,375 | 1,827 | 78.42 | 3,043 | 4,692 |
| 77.38 | 2,388 | 1,875 | 78.44 | 3,056 | 4,753 |
| 77.40 | 2,400 | 1,923 | 78.46 | 3,069 | 4,815 |
| 77.42 | 2,412 | 1,971 | 78.48 | 3,083 | 4,876 |
| 77.44 | 2,424 | 2,019 | 78.50 | 3,096 | 4,938 |
| 77.46 | 2,436 | 2,068 | | | |
| 77.48 | 2,449 | 2,116 | | | |
| 77.50 | 2,461 | 2,166 | | | |
| 77.52 | 2,473 | 2,215 | | | |
| 77.54 | 2,485 | 2,264 | | | |

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Pond B2: Bioretention Basin 2

[81] Warning: Exceeded Pond B1 by 0.12' @ 12.35 hrs

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 6.94" for 100-Year event
 Inflow = 15.77 cfs @ 12.19 hrs, Volume= 56,281 cf
 Outflow = 10.31 cfs @ 12.32 hrs, Volume= 53,114 cf, Atten= 35%, Lag= 7.8 min
 Primary = 10.31 cfs @ 12.32 hrs, Volume= 53,114 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 78.50' @ 12.31 hrs Surf.Area= 9,518 sf Storage= 16,324 cf

Plug-Flow detention time= 105.9 min calculated for 53,077 cf (94% of inflow)
 Center-of-Mass det. time= 75.0 min (864.8 - 789.8)

| Volume | Invert | Avail.Storage | Storage Description |
|------------------|-------------------|------------------------|--|
| #1 | 76.50' | 26,647 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
| 76.50 | 6,877 | 0 | 0 |
| 77.50 | 8,155 | 7,516 | 7,516 |
| 78.50 | 9,522 | 8,839 | 16,355 |
| 79.50 | 11,063 | 10,293 | 26,647 |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|--------|--|
| #1 | Primary | 73.00' | 15.0" Round Culvert L= 47.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.06' S= 0.0200 ' S= 0.0200 ' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf |
| #2 | Device 1 | 76.94' | 6.0" Vert. Orifice/Grate X 3.00 C= 0.600 |
| #3 | Device 1 | 77.78' | 4.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |
| #4 | Device 1 | 79.25' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=10.29 cfs @ 12.32 hrs HW=78.49' (Free Discharge)

- 1=Culvert (Inlet Controls 10.29 cfs @ 8.38 fps)
- 2=Orifice/Grate (Passes < 3.23 cfs potential flow)
- 3=Broad-Crested Rectangular Weir (Passes < 7.66 cfs potential flow)
- 4=Orifice/Grate (Controls 0.00 cfs)

Pre vs Post

Prepared by {enter your company name here}

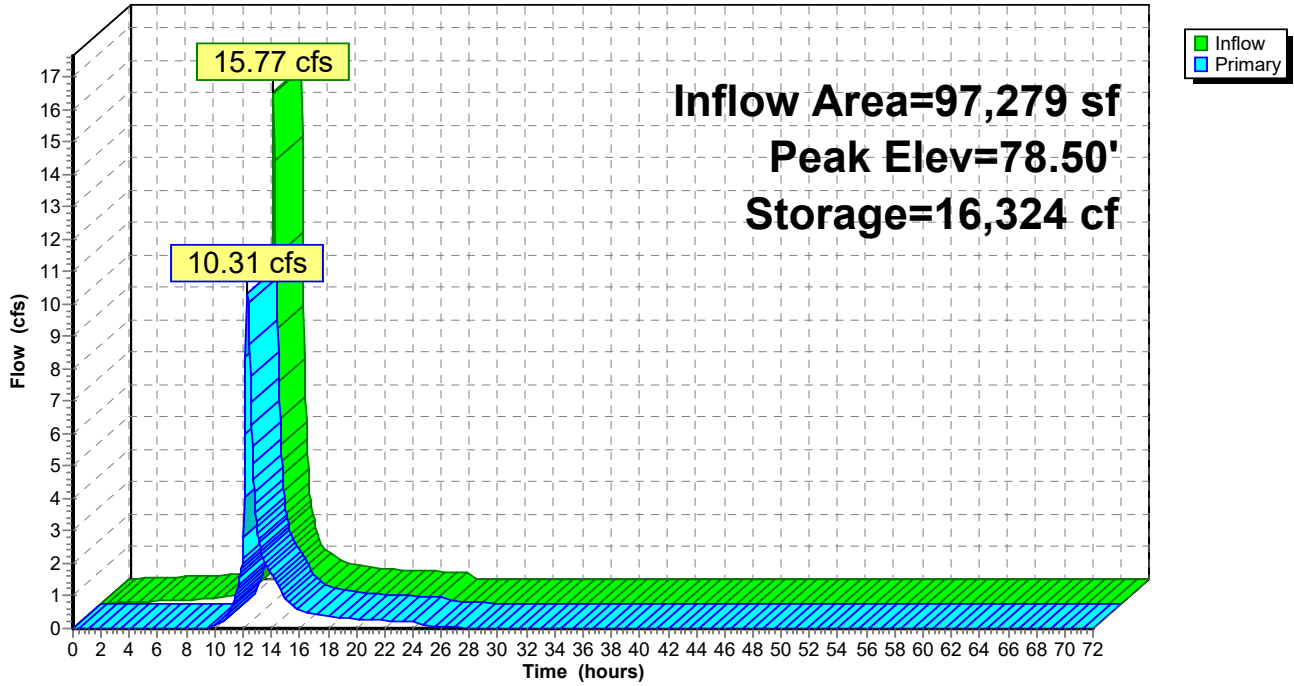
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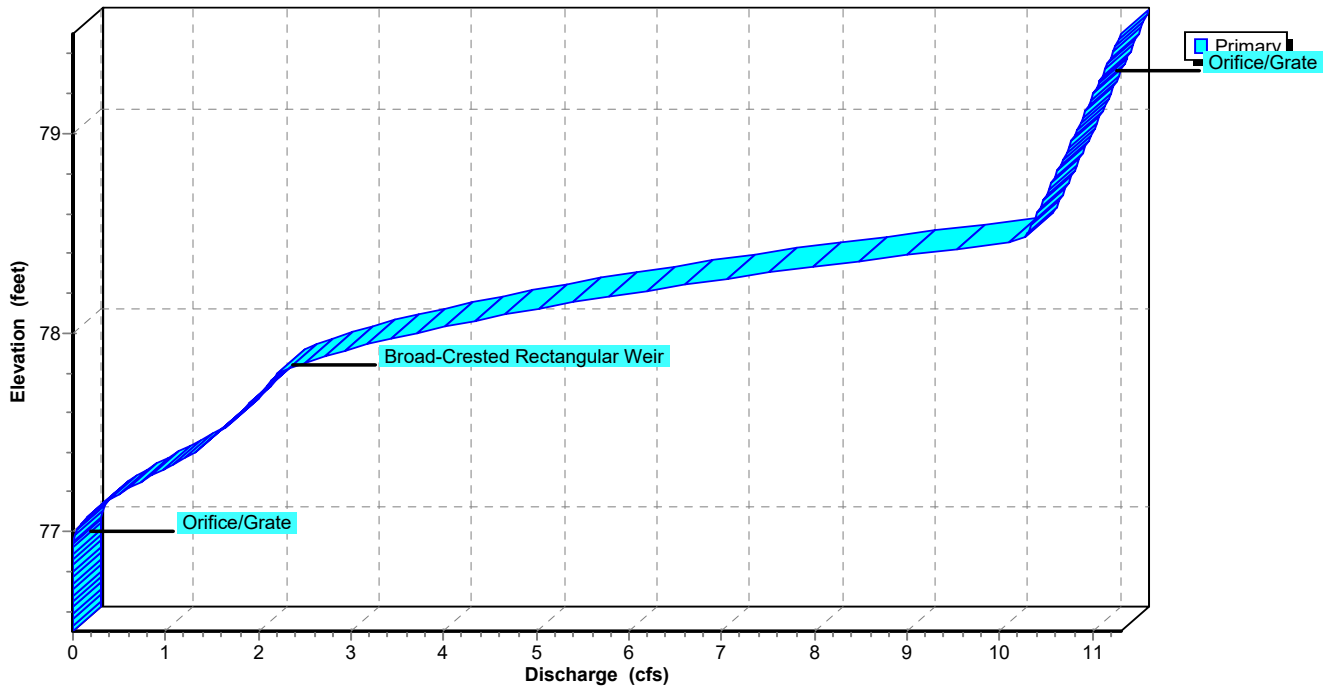
Pond B2: Bioretention Basin 2

Hydrograph



Pond B2: Bioretention Basin 2

Stage-Discharge



Pre vs Post

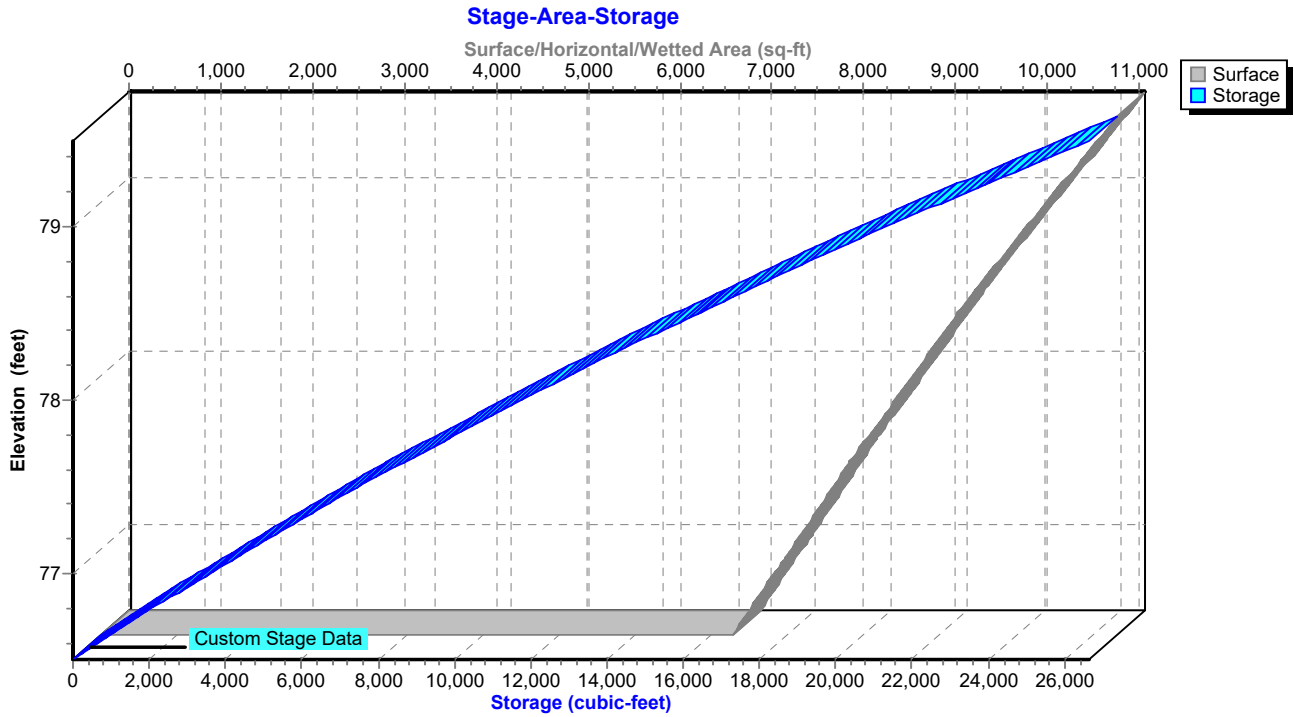
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Pond B2: Bioretention Basin 2



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Stage-Discharge for Pond B2: Bioretention Basin 2

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 76.50 | 0.00 | 77.56 | 1.73 | 78.62 | 10.43 |
| 76.52 | 0.00 | 77.58 | 1.77 | 78.64 | 10.45 |
| 76.54 | 0.00 | 77.60 | 1.82 | 78.66 | 10.47 |
| 76.56 | 0.00 | 77.62 | 1.86 | 78.68 | 10.49 |
| 76.58 | 0.00 | 77.64 | 1.90 | 78.70 | 10.51 |
| 76.60 | 0.00 | 77.66 | 1.94 | 78.72 | 10.53 |
| 76.62 | 0.00 | 77.68 | 1.99 | 78.74 | 10.55 |
| 76.64 | 0.00 | 77.70 | 2.03 | 78.76 | 10.57 |
| 76.66 | 0.00 | 77.72 | 2.06 | 78.78 | 10.59 |
| 76.68 | 0.00 | 77.74 | 2.10 | 78.80 | 10.61 |
| 76.70 | 0.00 | 77.76 | 2.14 | 78.82 | 10.63 |
| 76.72 | 0.00 | 77.78 | 2.18 | 78.84 | 10.65 |
| 76.74 | 0.00 | 77.80 | 2.25 | 78.86 | 10.67 |
| 76.76 | 0.00 | 77.82 | 2.34 | 78.88 | 10.69 |
| 76.78 | 0.00 | 77.84 | 2.45 | 78.90 | 10.71 |
| 76.80 | 0.00 | 77.86 | 2.58 | 78.92 | 10.73 |
| 76.82 | 0.00 | 77.88 | 2.71 | 78.94 | 10.75 |
| 76.84 | 0.00 | 77.90 | 2.86 | 78.96 | 10.77 |
| 76.86 | 0.00 | 77.92 | 3.01 | 78.98 | 10.79 |
| 76.88 | 0.00 | 77.94 | 3.17 | 79.00 | 10.82 |
| 76.90 | 0.00 | 77.96 | 3.34 | 79.02 | 10.84 |
| 76.92 | 0.00 | 77.98 | 3.52 | 79.04 | 10.86 |
| 76.94 | 0.00 | 78.00 | 3.71 | 79.06 | 10.88 |
| 76.96 | 0.00 | 78.02 | 3.91 | 79.08 | 10.90 |
| 76.98 | 0.02 | 78.04 | 4.12 | 79.10 | 10.92 |
| 77.00 | 0.03 | 78.06 | 4.33 | 79.12 | 10.94 |
| 77.02 | 0.06 | 78.08 | 4.56 | 79.14 | 10.96 |
| 77.04 | 0.09 | 78.10 | 4.79 | 79.16 | 10.97 |
| 77.06 | 0.13 | 78.12 | 5.02 | 79.18 | 10.99 |
| 77.08 | 0.17 | 78.14 | 5.27 | 79.20 | 11.01 |
| 77.10 | 0.22 | 78.16 | 5.52 | 79.22 | 11.03 |
| 77.12 | 0.28 | 78.18 | 5.78 | 79.24 | 11.05 |
| 77.14 | 0.34 | 78.20 | 6.05 | 79.26 | 11.07 |
| 77.16 | 0.40 | 78.22 | 6.32 | 79.28 | 11.09 |
| 77.18 | 0.47 | 78.24 | 6.61 | 79.30 | 11.11 |
| 77.20 | 0.54 | 78.26 | 6.90 | 79.32 | 11.13 |
| 77.22 | 0.61 | 78.28 | 7.20 | 79.34 | 11.15 |
| 77.24 | 0.69 | 78.30 | 7.51 | 79.36 | 11.17 |
| 77.26 | 0.77 | 78.32 | 7.83 | 79.38 | 11.19 |
| 77.28 | 0.85 | 78.34 | 8.15 | 79.40 | 11.21 |
| 77.30 | 0.93 | 78.36 | 8.48 | 79.42 | 11.23 |
| 77.32 | 1.01 | 78.38 | 8.82 | 79.44 | 11.25 |
| 77.34 | 1.09 | 78.40 | 9.18 | 79.46 | 11.27 |
| 77.36 | 1.17 | 78.42 | 9.54 | 79.48 | 11.29 |
| 77.38 | 1.24 | 78.44 | 9.92 | 79.50 | 11.31 |
| 77.40 | 1.31 | 78.46 | 10.26 | | |
| 77.42 | 1.37 | 78.48 | 10.28 | | |
| 77.44 | 1.42 | 78.50 | 10.30 | | |
| 77.46 | 1.47 | 78.52 | 10.32 | | |
| 77.48 | 1.53 | 78.54 | 10.34 | | |
| 77.50 | 1.58 | 78.56 | 10.36 | | |
| 77.52 | 1.63 | 78.58 | 10.38 | | |
| 77.54 | 1.68 | 78.60 | 10.40 | | |

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Stage-Area-Storage for Pond B2: Bioretention Basin 2

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 76.50 | 6,877 | 0 | 79.15 | 10,524 | 22,869 |
| 76.55 | 6,941 | 345 | 79.20 | 10,601 | 23,397 |
| 76.60 | 7,005 | 694 | 79.25 | 10,678 | 23,929 |
| 76.65 | 7,069 | 1,046 | 79.30 | 10,755 | 24,465 |
| 76.70 | 7,133 | 1,401 | 79.35 | 10,832 | 25,005 |
| 76.75 | 7,197 | 1,759 | 79.40 | 10,909 | 25,548 |
| 76.80 | 7,260 | 2,121 | 79.45 | 10,986 | 26,096 |
| 76.85 | 7,324 | 2,485 | 79.50 | 11,063 | 26,647 |
| 76.90 | 7,388 | 2,853 | | | |
| 76.95 | 7,452 | 3,224 | | | |
| 77.00 | 7,516 | 3,598 | | | |
| 77.05 | 7,580 | 3,976 | | | |
| 77.10 | 7,644 | 4,356 | | | |
| 77.15 | 7,708 | 4,740 | | | |
| 77.20 | 7,772 | 5,127 | | | |
| 77.25 | 7,836 | 5,517 | | | |
| 77.30 | 7,899 | 5,911 | | | |
| 77.35 | 7,963 | 6,307 | | | |
| 77.40 | 8,027 | 6,707 | | | |
| 77.45 | 8,091 | 7,110 | | | |
| 77.50 | 8,155 | 7,516 | | | |
| 77.55 | 8,223 | 7,925 | | | |
| 77.60 | 8,292 | 8,338 | | | |
| 77.65 | 8,360 | 8,755 | | | |
| 77.70 | 8,428 | 9,174 | | | |
| 77.75 | 8,497 | 9,597 | | | |
| 77.80 | 8,565 | 10,024 | | | |
| 77.85 | 8,633 | 10,454 | | | |
| 77.90 | 8,702 | 10,887 | | | |
| 77.95 | 8,770 | 11,324 | | | |
| 78.00 | 8,839 | 11,764 | | | |
| 78.05 | 8,907 | 12,208 | | | |
| 78.10 | 8,975 | 12,655 | | | |
| 78.15 | 9,044 | 13,106 | | | |
| 78.20 | 9,112 | 13,559 | | | |
| 78.25 | 9,180 | 14,017 | | | |
| 78.30 | 9,249 | 14,477 | | | |
| 78.35 | 9,317 | 14,942 | | | |
| 78.40 | 9,385 | 15,409 | | | |
| 78.45 | 9,454 | 15,880 | | | |
| 78.50 | 9,522 | 16,355 | | | |
| 78.55 | 9,599 | 16,833 | | | |
| 78.60 | 9,676 | 17,314 | | | |
| 78.65 | 9,753 | 17,800 | | | |
| 78.70 | 9,830 | 18,290 | | | |
| 78.75 | 9,907 | 18,783 | | | |
| 78.80 | 9,984 | 19,280 | | | |
| 78.85 | 10,061 | 19,782 | | | |
| 78.90 | 10,138 | 20,287 | | | |
| 78.95 | 10,215 | 20,795 | | | |
| 79.00 | 10,293 | 21,308 | | | |
| 79.05 | 10,370 | 21,825 | | | |
| 79.10 | 10,447 | 22,345 | | | |

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Pond B3: Bioretention Basin 3

[92] Warning: Device #2 is above defined storage

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 6.83" for 100-Year event
 Inflow = 1.41 cfs @ 12.30 hrs, Volume= 6,674 cf
 Outflow = 1.41 cfs @ 12.31 hrs, Volume= 6,199 cf, Atten= 0%, Lag= 0.7 min
 Primary = 1.41 cfs @ 12.31 hrs, Volume= 6,199 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 80.84' @ 12.31 hrs Surf.Area= 901 sf Storage= 560 cf

Plug-Flow detention time= 73.0 min calculated for 6,195 cf (93% of inflow)
 Center-of-Mass det. time= 33.5 min (823.5 - 790.1)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 79.98' | 694 cf | Custom Stage Data (Conic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
|------------------|-------------------|------------------------|------------------------|------------------|
| 79.98 | 432 | 0 | 0 | 432 |
| 80.98 | 995 | 694 | 694 | 1,003 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 77.48' | 15.0" Round CMP_Round 15" L= 96.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 77.48' / 77.00' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 1.23 sf |
| #2 | Secondary | 80.98' | 15.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 80.74' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=1.39 cfs @ 12.31 hrs HW=80.84' (Free Discharge)
 ↑1=CMP_Round 15" (Passes 1.39 cfs of 7.71 cfs potential flow)
 ↑3=Orifice/Grate (Weir Controls 1.39 cfs @ 1.02 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=79.98' (Free Discharge)
 ↑2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pre vs Post

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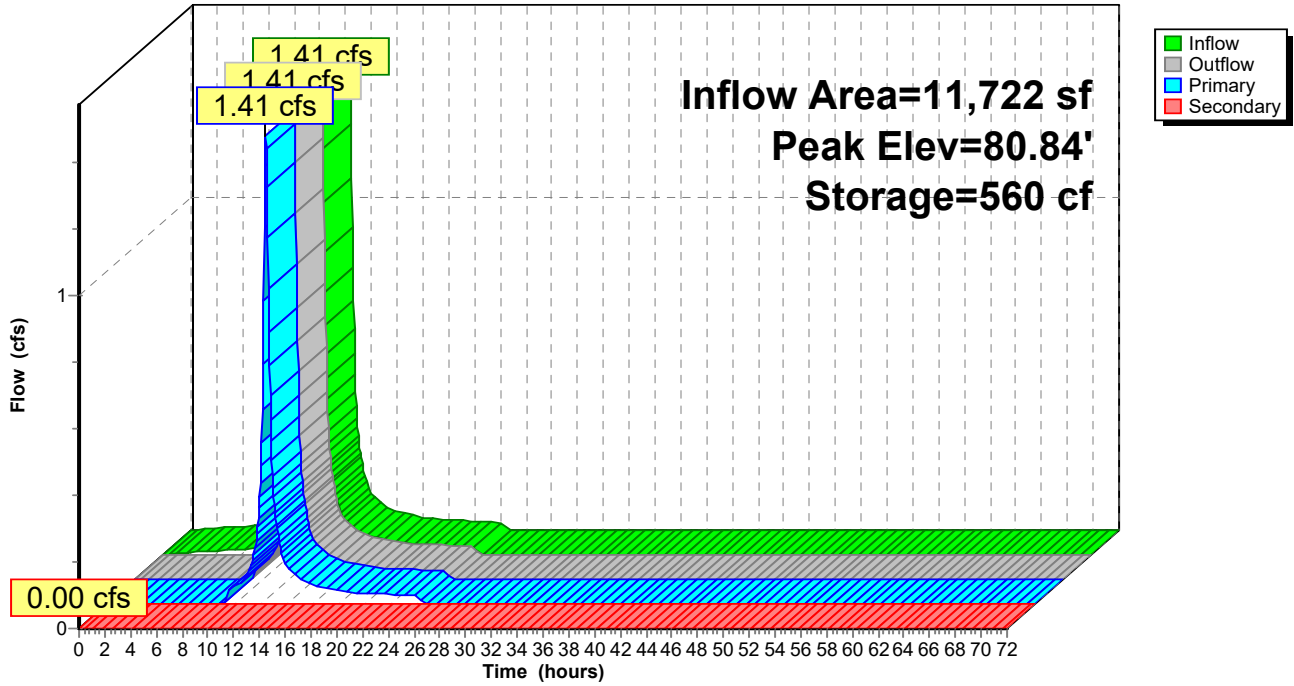
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NOAA 24-hr C 100-Year Rainfall=8.81"

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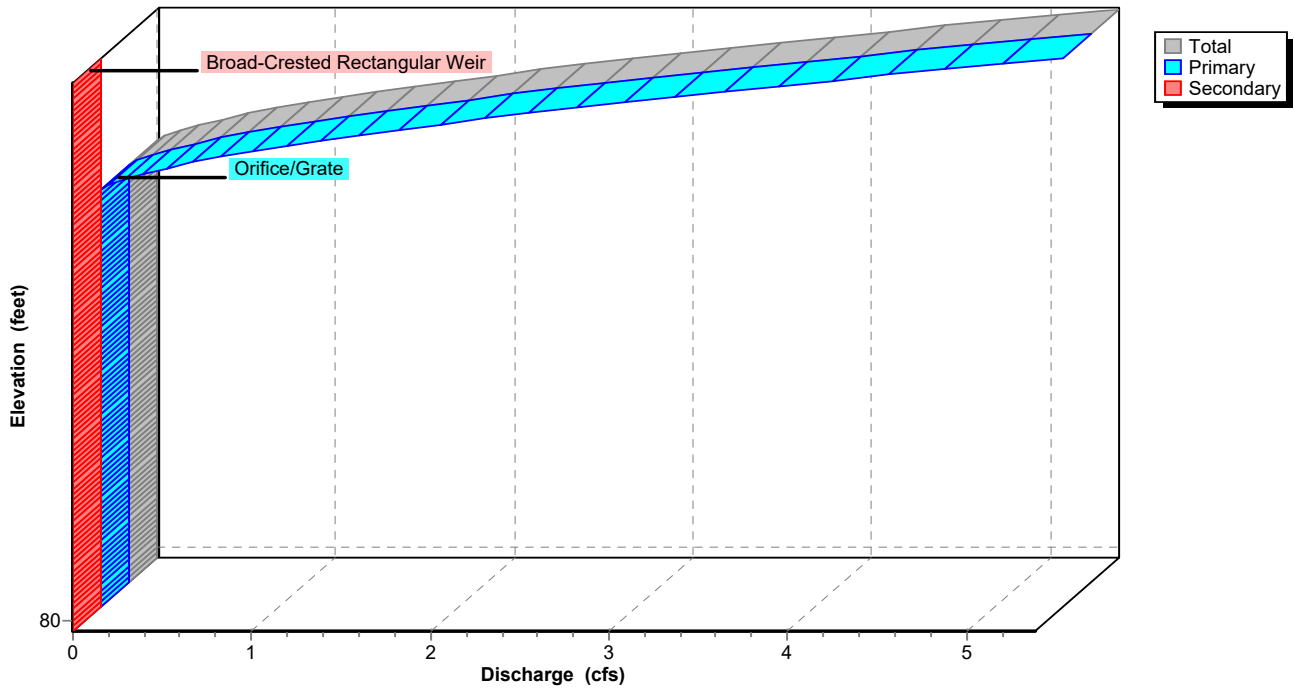
Pond B3: Bioretention Basin 3

Hydrograph



Pond B3: Bioretention Basin 3

Stage-Discharge



Pre vs Post

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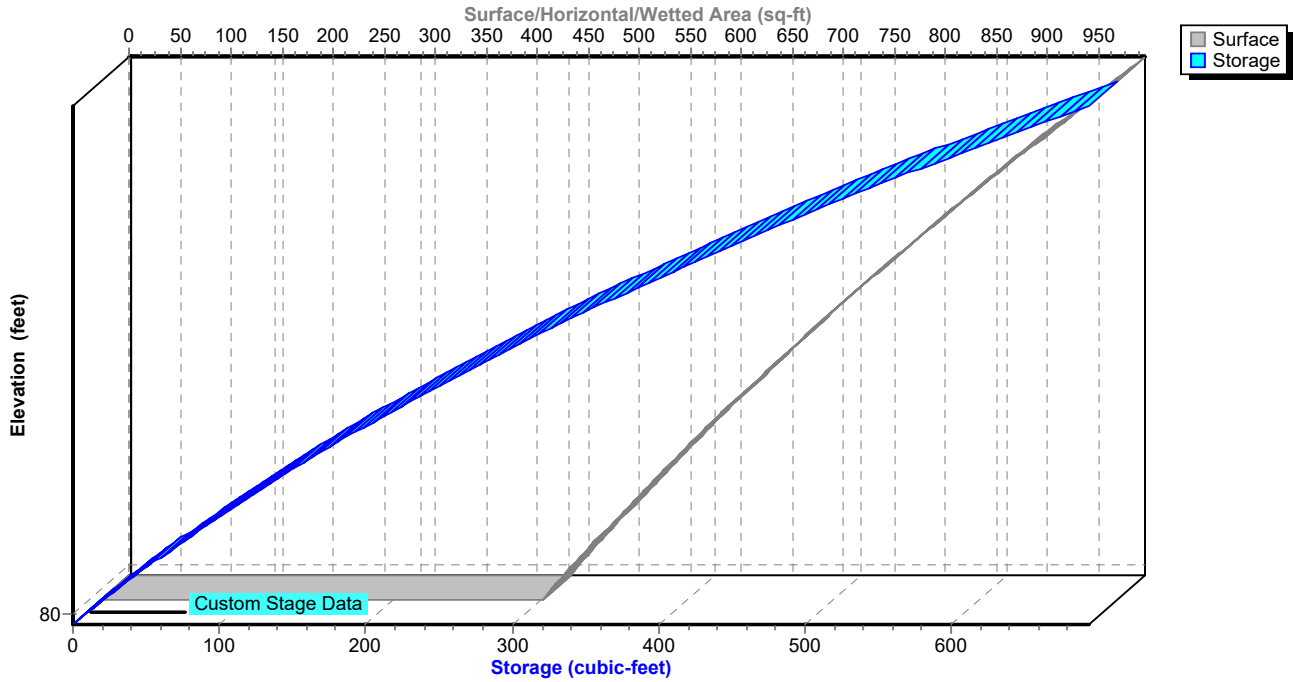
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Pond B3: Bioretention Basin 3

Stage-Area-Storage



Pre vs Post

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Stage-Discharge for Pond B3: Bioretention Basin 3

| Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) | Elevation (feet) | Discharge (cfs) | Primary (cfs) | Secondary (cfs) |
|---------------------|--------------------|------------------|--------------------|---------------------|--------------------|------------------|--------------------|
| 79.98 | 0.00 | 0.00 | 0.00 | 80.51 | 0.00 | 0.00 | 0.00 |
| 79.99 | 0.00 | 0.00 | 0.00 | 80.52 | 0.00 | 0.00 | 0.00 |
| 80.00 | 0.00 | 0.00 | 0.00 | 80.53 | 0.00 | 0.00 | 0.00 |
| 80.01 | 0.00 | 0.00 | 0.00 | 80.54 | 0.00 | 0.00 | 0.00 |
| 80.02 | 0.00 | 0.00 | 0.00 | 80.55 | 0.00 | 0.00 | 0.00 |
| 80.03 | 0.00 | 0.00 | 0.00 | 80.56 | 0.00 | 0.00 | 0.00 |
| 80.04 | 0.00 | 0.00 | 0.00 | 80.57 | 0.00 | 0.00 | 0.00 |
| 80.05 | 0.00 | 0.00 | 0.00 | 80.58 | 0.00 | 0.00 | 0.00 |
| 80.06 | 0.00 | 0.00 | 0.00 | 80.59 | 0.00 | 0.00 | 0.00 |
| 80.07 | 0.00 | 0.00 | 0.00 | 80.60 | 0.00 | 0.00 | 0.00 |
| 80.08 | 0.00 | 0.00 | 0.00 | 80.61 | 0.00 | 0.00 | 0.00 |
| 80.09 | 0.00 | 0.00 | 0.00 | 80.62 | 0.00 | 0.00 | 0.00 |
| 80.10 | 0.00 | 0.00 | 0.00 | 80.63 | 0.00 | 0.00 | 0.00 |
| 80.11 | 0.00 | 0.00 | 0.00 | 80.64 | 0.00 | 0.00 | 0.00 |
| 80.12 | 0.00 | 0.00 | 0.00 | 80.65 | 0.00 | 0.00 | 0.00 |
| 80.13 | 0.00 | 0.00 | 0.00 | 80.66 | 0.00 | 0.00 | 0.00 |
| 80.14 | 0.00 | 0.00 | 0.00 | 80.67 | 0.00 | 0.00 | 0.00 |
| 80.15 | 0.00 | 0.00 | 0.00 | 80.68 | 0.00 | 0.00 | 0.00 |
| 80.16 | 0.00 | 0.00 | 0.00 | 80.69 | 0.00 | 0.00 | 0.00 |
| 80.17 | 0.00 | 0.00 | 0.00 | 80.70 | 0.00 | 0.00 | 0.00 |
| 80.18 | 0.00 | 0.00 | 0.00 | 80.71 | 0.00 | 0.00 | 0.00 |
| 80.19 | 0.00 | 0.00 | 0.00 | 80.72 | 0.00 | 0.00 | 0.00 |
| 80.20 | 0.00 | 0.00 | 0.00 | 80.73 | 0.00 | 0.00 | 0.00 |
| 80.21 | 0.00 | 0.00 | 0.00 | 80.74 | 0.00 | 0.00 | 0.00 |
| 80.22 | 0.00 | 0.00 | 0.00 | 80.75 | 0.05 | 0.05 | 0.00 |
| 80.23 | 0.00 | 0.00 | 0.00 | 80.76 | 0.13 | 0.13 | 0.00 |
| 80.24 | 0.00 | 0.00 | 0.00 | 80.77 | 0.24 | 0.24 | 0.00 |
| 80.25 | 0.00 | 0.00 | 0.00 | 80.78 | 0.37 | 0.37 | 0.00 |
| 80.26 | 0.00 | 0.00 | 0.00 | 80.79 | 0.51 | 0.51 | 0.00 |
| 80.27 | 0.00 | 0.00 | 0.00 | 80.80 | 0.67 | 0.67 | 0.00 |
| 80.28 | 0.00 | 0.00 | 0.00 | 80.81 | 0.85 | 0.85 | 0.00 |
| 80.29 | 0.00 | 0.00 | 0.00 | 80.82 | 1.04 | 1.04 | 0.00 |
| 80.30 | 0.00 | 0.00 | 0.00 | 80.83 | 1.24 | 1.24 | 0.00 |
| 80.31 | 0.00 | 0.00 | 0.00 | 80.84 | 1.45 | 1.45 | 0.00 |
| 80.32 | 0.00 | 0.00 | 0.00 | 80.85 | 1.67 | 1.67 | 0.00 |
| 80.33 | 0.00 | 0.00 | 0.00 | 80.86 | 1.90 | 1.90 | 0.00 |
| 80.34 | 0.00 | 0.00 | 0.00 | 80.87 | 2.15 | 2.15 | 0.00 |
| 80.35 | 0.00 | 0.00 | 0.00 | 80.88 | 2.40 | 2.40 | 0.00 |
| 80.36 | 0.00 | 0.00 | 0.00 | 80.89 | 2.66 | 2.66 | 0.00 |
| 80.37 | 0.00 | 0.00 | 0.00 | 80.90 | 2.93 | 2.93 | 0.00 |
| 80.38 | 0.00 | 0.00 | 0.00 | 80.91 | 3.21 | 3.21 | 0.00 |
| 80.39 | 0.00 | 0.00 | 0.00 | 80.92 | 3.50 | 3.50 | 0.00 |
| 80.40 | 0.00 | 0.00 | 0.00 | 80.93 | 3.79 | 3.79 | 0.00 |
| 80.41 | 0.00 | 0.00 | 0.00 | 80.94 | 4.09 | 4.09 | 0.00 |
| 80.42 | 0.00 | 0.00 | 0.00 | 80.95 | 4.41 | 4.41 | 0.00 |
| 80.43 | 0.00 | 0.00 | 0.00 | 80.96 | 4.72 | 4.72 | 0.00 |
| 80.44 | 0.00 | 0.00 | 0.00 | 80.97 | 5.05 | 5.05 | 0.00 |
| 80.45 | 0.00 | 0.00 | 0.00 | 80.98 | 5.38 | 5.38 | 0.00 |
| 80.46 | 0.00 | 0.00 | 0.00 | | | | |
| 80.47 | 0.00 | 0.00 | 0.00 | | | | |
| 80.48 | 0.00 | 0.00 | 0.00 | | | | |
| 80.49 | 0.00 | 0.00 | 0.00 | | | | |
| 80.50 | 0.00 | 0.00 | 0.00 | | | | |

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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Stage-Area-Storage for Pond B3: Bioretention Basin 3

| Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) | Elevation (feet) | Surface (sq-ft) | Storage (cubic-feet) |
|---------------------|--------------------|-------------------------|---------------------|--------------------|-------------------------|
| 79.98 | 432 | 0 | 80.51 | 702 | 298 |
| 79.99 | 436 | 4 | 80.52 | 707 | 305 |
| 80.00 | 441 | 9 | 80.53 | 713 | 312 |
| 80.01 | 446 | 13 | 80.54 | 719 | 319 |
| 80.02 | 450 | 18 | 80.55 | 725 | 326 |
| 80.03 | 455 | 22 | 80.56 | 730 | 333 |
| 80.04 | 459 | 27 | 80.57 | 736 | 341 |
| 80.05 | 464 | 31 | 80.58 | 742 | 348 |
| 80.06 | 469 | 36 | 80.59 | 748 | 355 |
| 80.07 | 473 | 41 | 80.60 | 754 | 363 |
| 80.08 | 478 | 45 | 80.61 | 760 | 371 |
| 80.09 | 483 | 50 | 80.62 | 766 | 378 |
| 80.10 | 487 | 55 | 80.63 | 772 | 386 |
| 80.11 | 492 | 60 | 80.64 | 778 | 394 |
| 80.12 | 497 | 65 | 80.65 | 784 | 401 |
| 80.13 | 502 | 70 | 80.66 | 790 | 409 |
| 80.14 | 507 | 75 | 80.67 | 796 | 417 |
| 80.15 | 511 | 80 | 80.68 | 802 | 425 |
| 80.16 | 516 | 85 | 80.69 | 808 | 433 |
| 80.17 | 521 | 90 | 80.70 | 814 | 441 |
| 80.18 | 526 | 96 | 80.71 | 820 | 450 |
| 80.19 | 531 | 101 | 80.72 | 826 | 458 |
| 80.20 | 536 | 106 | 80.73 | 833 | 466 |
| 80.21 | 541 | 112 | 80.74 | 839 | 474 |
| 80.22 | 546 | 117 | 80.75 | 845 | 483 |
| 80.23 | 551 | 123 | 80.76 | 851 | 491 |
| 80.24 | 556 | 128 | 80.77 | 858 | 500 |
| 80.25 | 561 | 134 | 80.78 | 864 | 508 |
| 80.26 | 566 | 139 | 80.79 | 870 | 517 |
| 80.27 | 571 | 145 | 80.80 | 877 | 526 |
| 80.28 | 577 | 151 | 80.81 | 883 | 535 |
| 80.29 | 582 | 157 | 80.82 | 889 | 544 |
| 80.30 | 587 | 162 | 80.83 | 896 | 552 |
| 80.31 | 592 | 168 | 80.84 | 902 | 561 |
| 80.32 | 597 | 174 | 80.85 | 909 | 571 |
| 80.33 | 603 | 180 | 80.86 | 915 | 580 |
| 80.34 | 608 | 186 | 80.87 | 922 | 589 |
| 80.35 | 613 | 192 | 80.88 | 928 | 598 |
| 80.36 | 619 | 199 | 80.89 | 935 | 607 |
| 80.37 | 624 | 205 | 80.90 | 941 | 617 |
| 80.38 | 629 | 211 | 80.91 | 948 | 626 |
| 80.39 | 635 | 217 | 80.92 | 955 | 636 |
| 80.40 | 640 | 224 | 80.93 | 961 | 645 |
| 80.41 | 646 | 230 | 80.94 | 968 | 655 |
| 80.42 | 651 | 237 | 80.95 | 975 | 665 |
| 80.43 | 657 | 243 | 80.96 | 981 | 674 |
| 80.44 | 662 | 250 | 80.97 | 988 | 684 |
| 80.45 | 668 | 256 | 80.98 | 995 | 694 |
| 80.46 | 673 | 263 | | | |
| 80.47 | 679 | 270 | | | |
| 80.48 | 685 | 277 | | | |
| 80.49 | 690 | 284 | | | |
| 80.50 | 696 | 291 | | | |

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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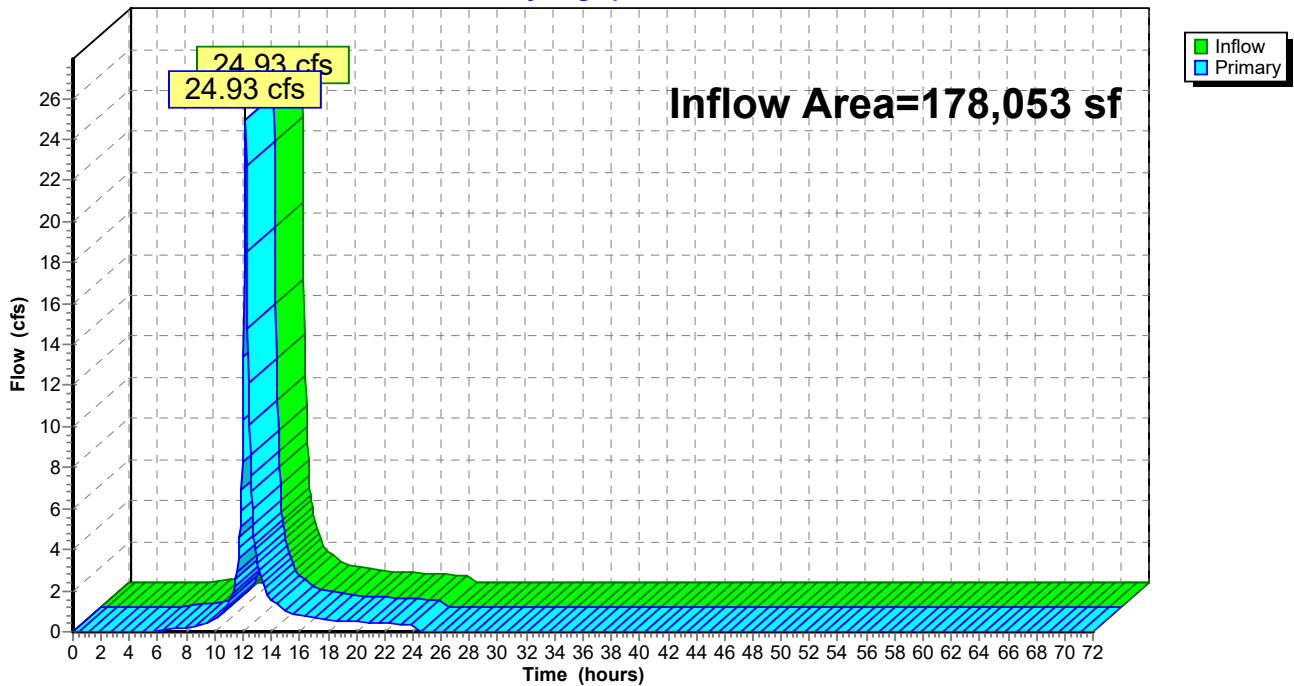
Summary for Link 5E: EDA 1

Inflow Area = 178,053 sf, 5.81% Impervious, Inflow Depth = 6.06" for 100-Year event
Inflow = 24.93 cfs @ 12.20 hrs, Volume= 89,848 cf
Primary = 24.93 cfs @ 12.20 hrs, Volume= 89,848 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 5E: EDA 1

Hydrograph



Pre vs Post

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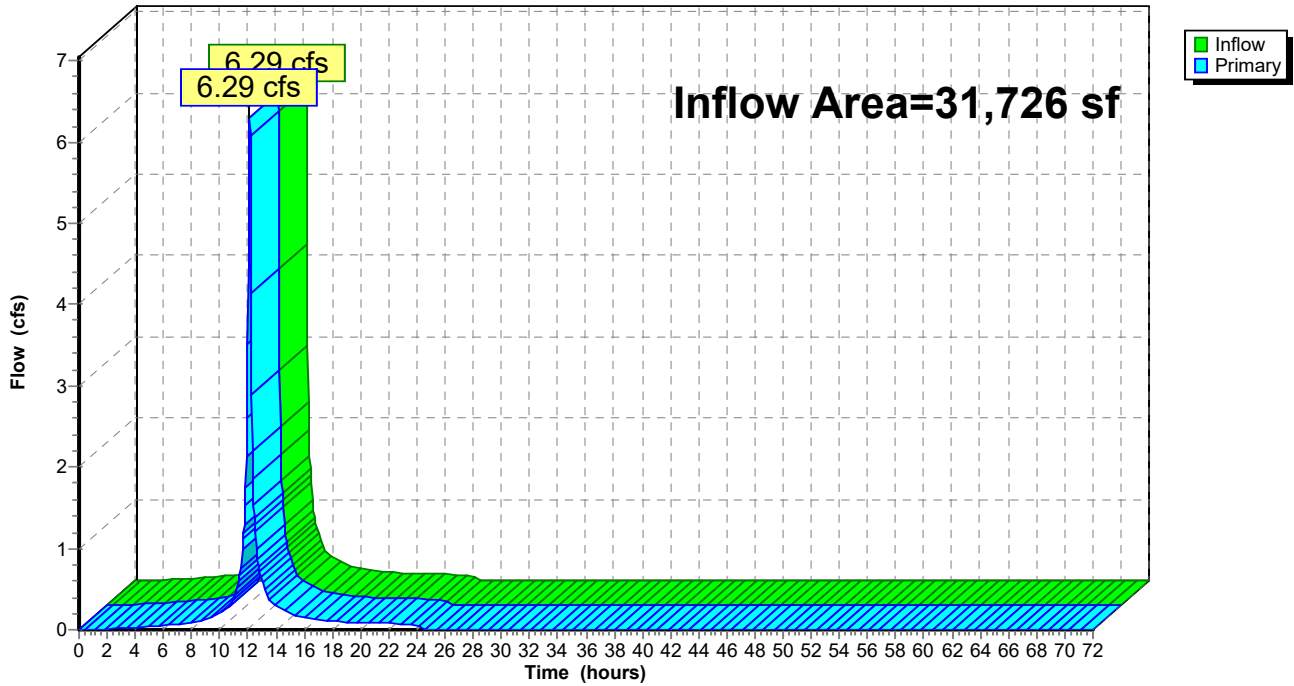
Summary for Link 6E: EDA 2

Inflow Area = 31,726 sf, 17.78% Impervious, Inflow Depth = 7.48" for 100-Year event
Inflow = 6.29 cfs @ 12.13 hrs, Volume= 19,767 cf
Primary = 6.29 cfs @ 12.13 hrs, Volume= 19,767 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 6E: EDA 2

Hydrograph



Pre vs Post

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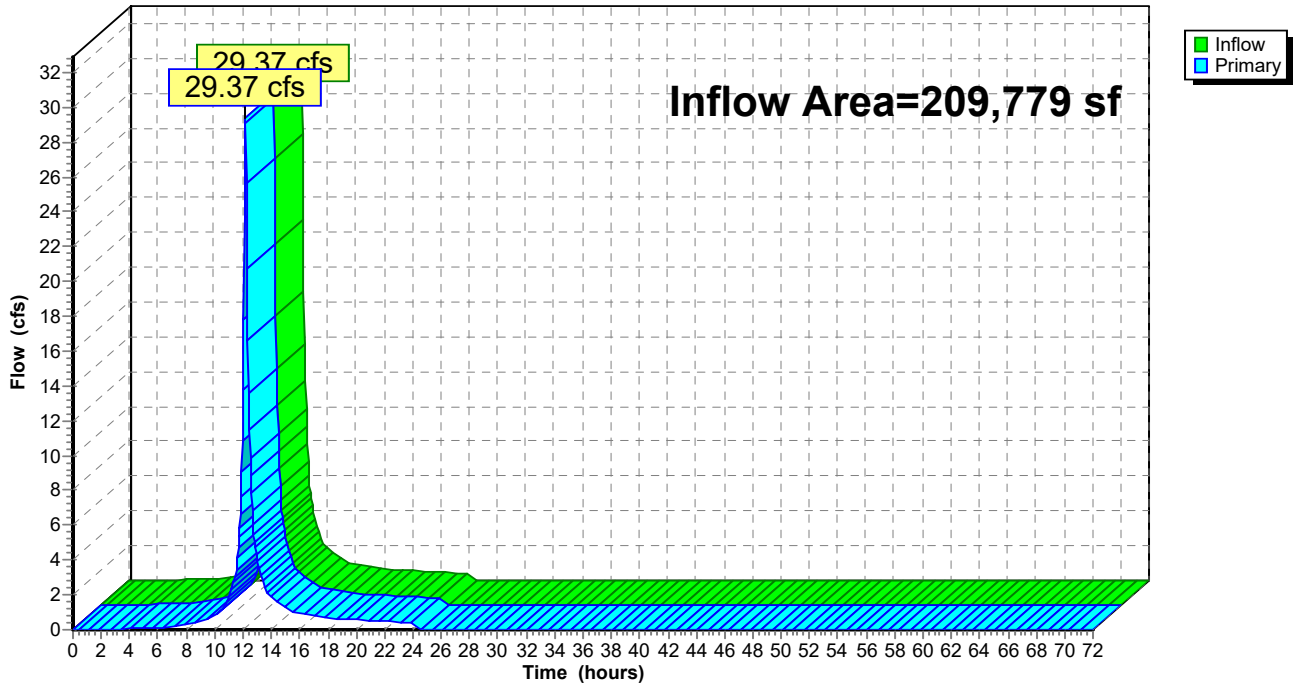
Summary for Link 7E: EDA

Inflow Area = 209,779 sf, 7.62% Impervious, Inflow Depth = 6.27" for 100-Year event
Inflow = 29.37 cfs @ 12.18 hrs, Volume= 109,615 cf
Primary = 29.37 cfs @ 12.18 hrs, Volume= 109,615 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 7E: EDA

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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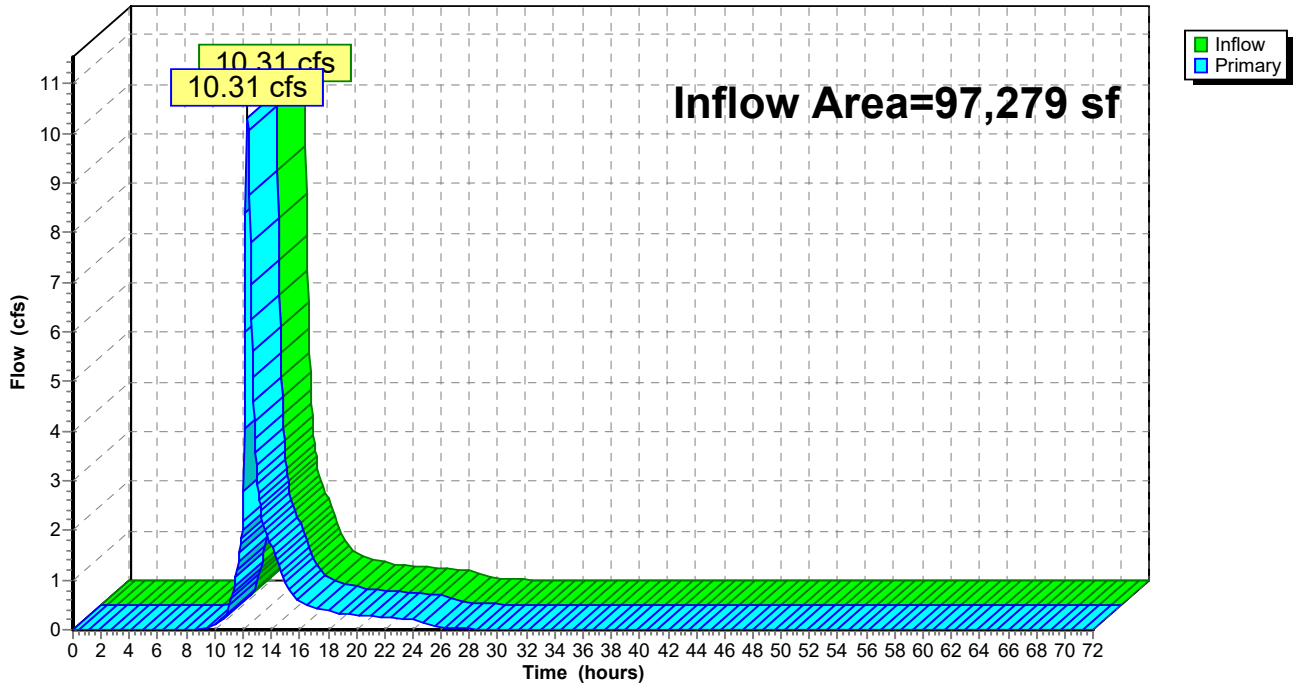
Summary for Link 10P: PDA 1A

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 6.55" for 100-Year event
Inflow = 10.31 cfs @ 12.32 hrs, Volume= 53,114 cf
Primary = 10.31 cfs @ 12.32 hrs, Volume= 53,114 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 10P: PDA 1A

Hydrograph



Pre vs Post

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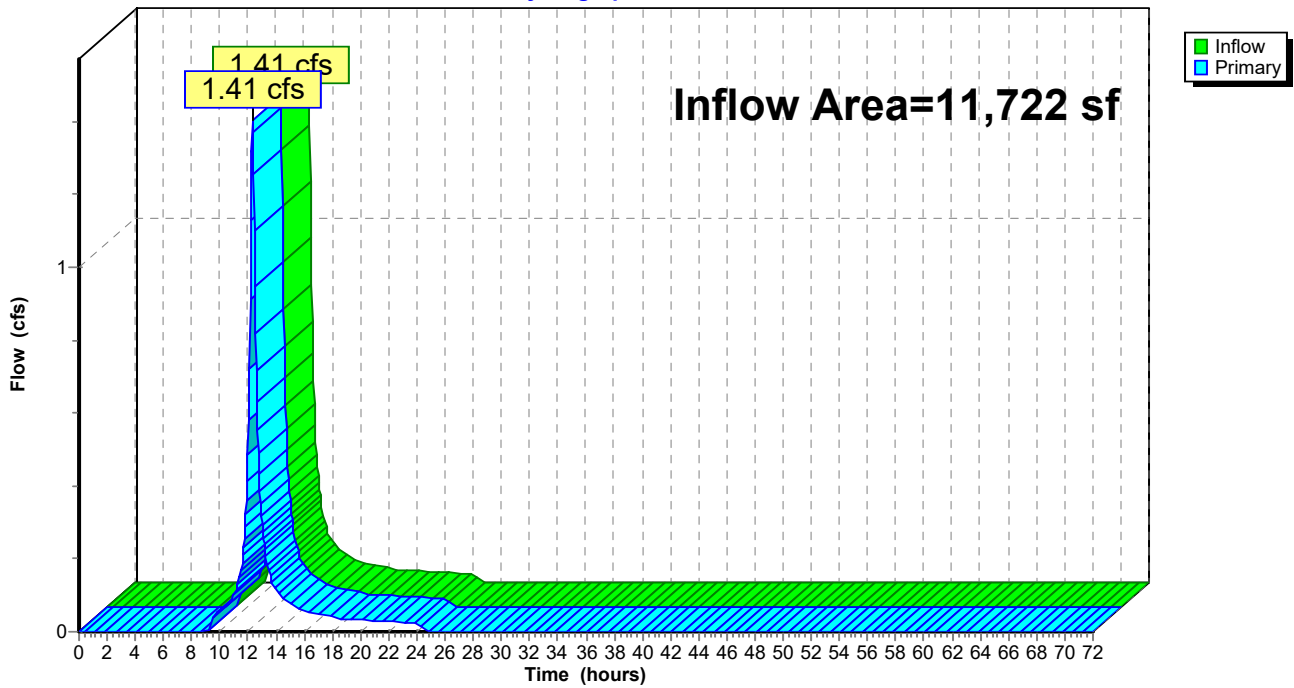
Summary for Link 11P: PDA 1B

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 6.35" for 100-Year event
Inflow = 1.41 cfs @ 12.31 hrs, Volume= 6,199 cf
Primary = 1.41 cfs @ 12.31 hrs, Volume= 6,199 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 11P: PDA 1B

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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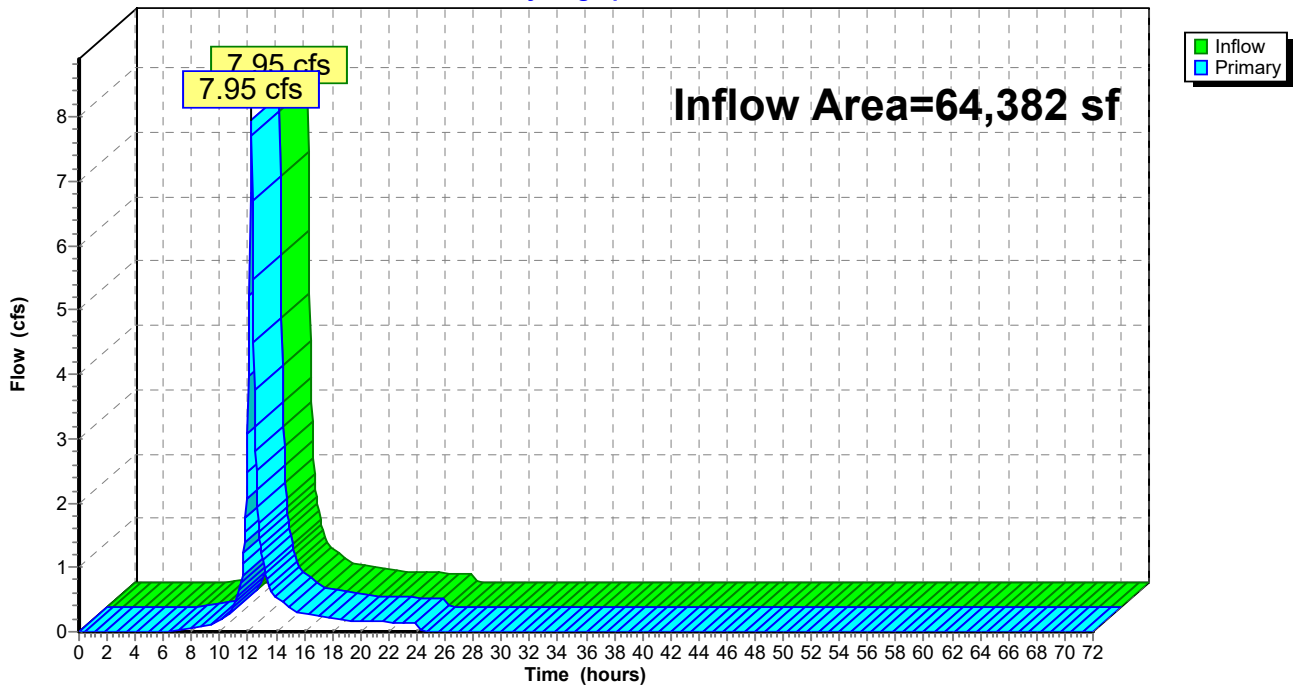
Summary for Link 12P: PDA 1C

Inflow Area = 64,382 sf, 3.87% Impervious, Inflow Depth = 5.53" for 100-Year event
Inflow = 7.95 cfs @ 12.22 hrs, Volume= 29,692 cf
Primary = 7.95 cfs @ 12.22 hrs, Volume= 29,692 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 12P: PDA 1C

Hydrograph



Pre vs Post

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NOAA 24-hr C 100-Year Rainfall=8.81"

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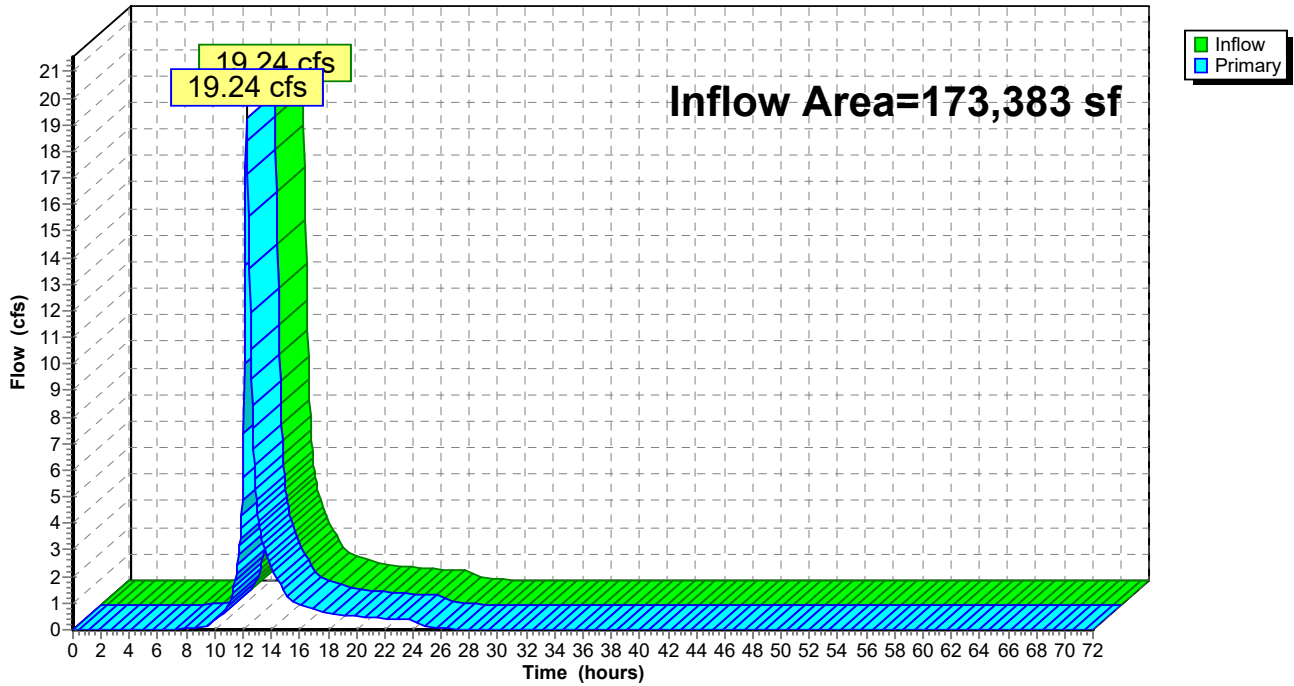
Summary for Link 13P: PDA 1

Inflow Area = 173,383 sf, 38.29% Impervious, Inflow Depth = 6.16" for 100-Year event
Inflow = 19.24 cfs @ 12.26 hrs, Volume= 89,005 cf
Primary = 19.24 cfs @ 12.26 hrs, Volume= 89,005 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 13P: PDA 1

Hydrograph



Pre vs Post

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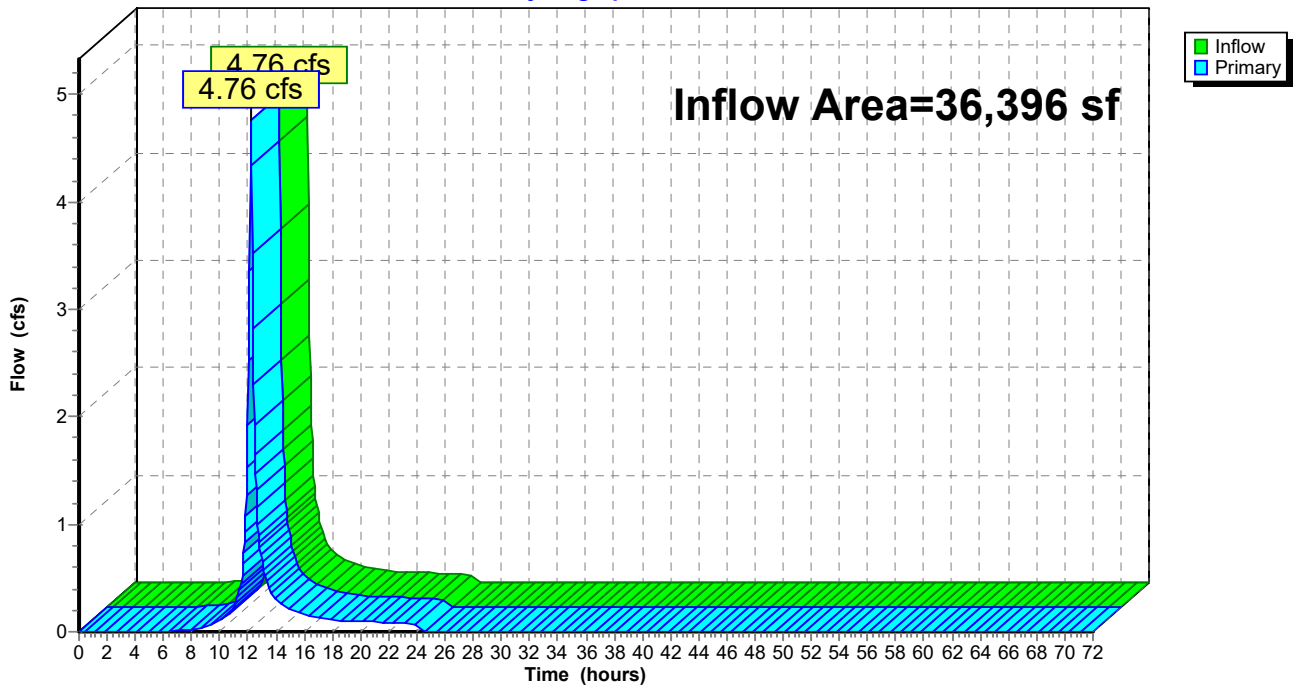
Summary for Link 14P: PDA 2

Inflow Area = 36,396 sf, 0.00% Impervious, Inflow Depth = 5.53" for 100-Year event
Inflow = 4.76 cfs @ 12.20 hrs, Volume= 16,785 cf
Primary = 4.76 cfs @ 12.20 hrs, Volume= 16,785 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Link 14P: PDA 2

Hydrograph



Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

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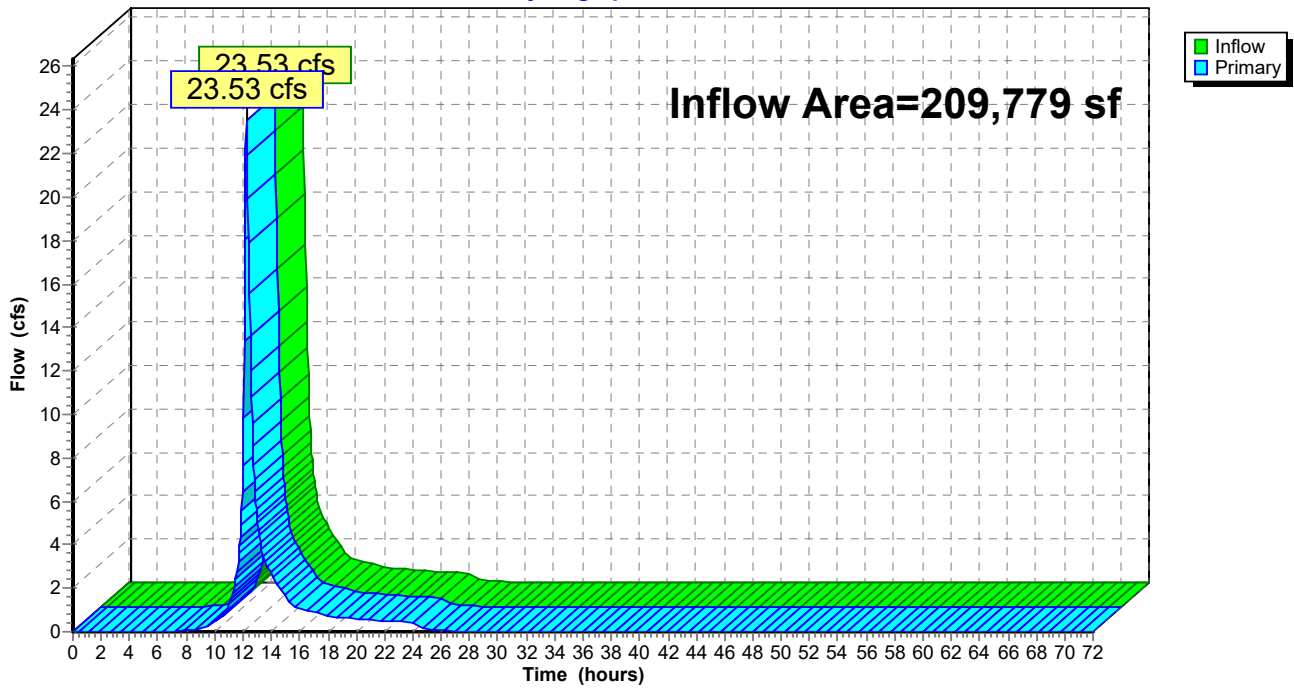
Summary for Link 15P: PDA

Inflow Area = 209,779 sf, 31.65% Impervious, Inflow Depth = 6.05" for 100-Year event
Inflow = 23.53 cfs @ 12.25 hrs, Volume= 105,790 cf
Primary = 23.53 cfs @ 12.25 hrs, Volume= 105,790 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

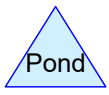
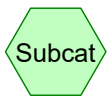
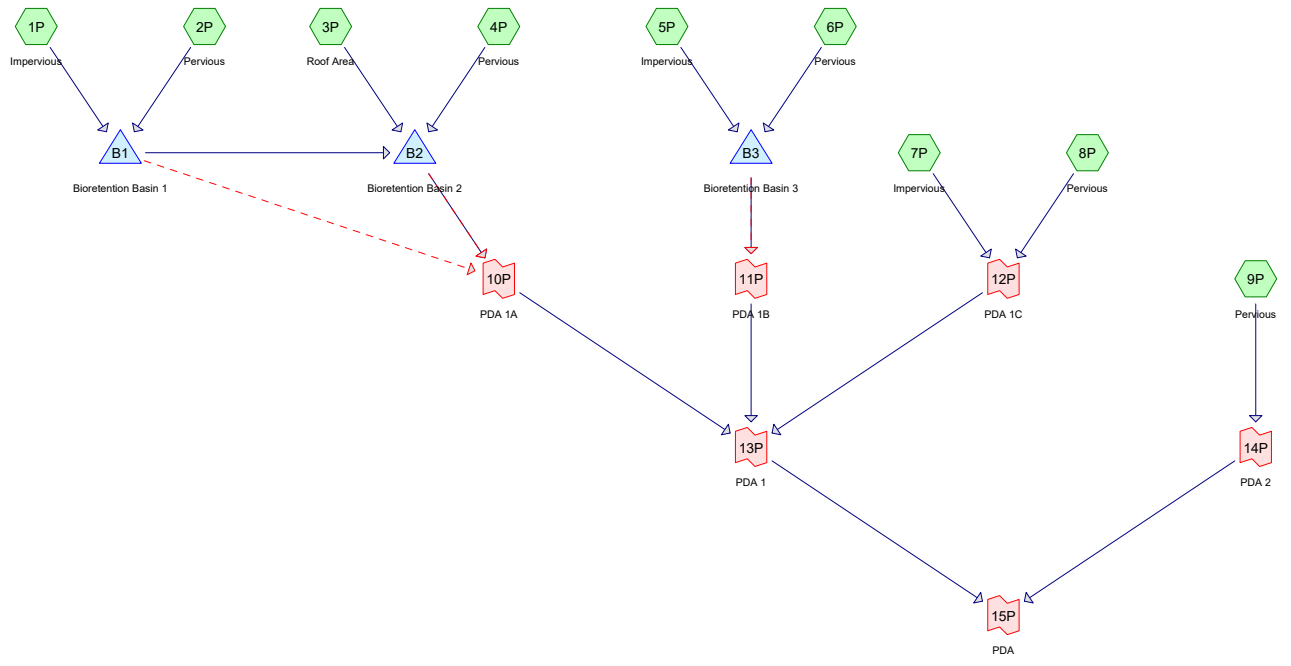
Link 15P: PDA

Hydrograph



B. DESIGN CALCULATIONS

- ◆ **Emergency Spillway**
- ◆ **Rip Rap**
 - **Rip Rap #100**
 - **Rip Rap #400**
- ◆ **Scour Hole**
- ◆ **Basin Drain Time**
- ◆ **Pipe Sizing**
- ◆ **NJDEP Nonstructural Strategies Points System (NSPS)**
- ◆ **Low Impact Development Checklist**
- ◆ **Geotechnical Report**



Routing Diagram for Emergency Spillway
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Emergency Spillway

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Pipe Listing (all nodes)

| Line# | Node Number | In-Invert (feet) | Out-Invert (feet) | Length (feet) | Slope (ft/ft) | n | Diam/Width (inches) | Height (inches) | Inside-Fill (inches) |
|-------|-------------|------------------|-------------------|---------------|---------------|-------|---------------------|-----------------|----------------------|
| 1 | 2P | 0.00 | 0.00 | 255.0 | 0.0050 | 0.013 | 15.0 | 0.0 | 0.0 |
| 2 | B1 | 73.00 | 72.85 | 10.0 | 0.0150 | 0.013 | 24.0 | 0.0 | 0.0 |
| 3 | B2 | 73.00 | 72.06 | 47.0 | 0.0200 | 0.011 | 15.0 | 0.0 | 0.0 |
| 4 | B3 | 77.48 | 77.00 | 96.0 | 0.0050 | 0.013 | 15.0 | 0.0 | 0.0 |

Emergency Spillway

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Pond B1: Bioretention Basin 1

[92] Warning: Device #2 is above defined storage

Inflow Area = 48,248 sf, 48.86% Impervious, Inflow Depth = 7.08" for 100-Year event
 Inflow = 7.70 cfs @ 12.18 hrs, Volume= 28,466 cf
 Outflow = 7.55 cfs @ 12.20 hrs, Volume= 24,571 cf, Atten= 2%, Lag= 1.4 min
 Primary = 7.55 cfs @ 12.20 hrs, Volume= 24,571 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 78.45' @ 12.20 hrs Surf.Area= 3,063 sf Storage= 4,786 cf

Plug-Flow detention time= 117.1 min calculated for 24,554 cf (86% of inflow)
 Center-of-Mass det. time= 52.5 min (828.0 - 775.5)

| Volume | Invert | Avail.Storage | Storage Description | |
|------------------|-------------------|------------------------|--|------------------|
| #1 | 76.50' | 4,938 cf | Custom Stage Data (Conic) Listed below (Recalc) | |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
| 76.50 | 1,883 | 0 | 0 | 1,883 |
| 77.50 | 2,461 | 2,166 | 2,166 | 2,484 |
| 78.50 | 3,096 | 2,772 | 4,938 | 3,146 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 73.00' | 24.0" Round CMP_Round 24" L= 10.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.85' S= 0.0150 ' S= 0.0150 ' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf |
| #2 | Secondary | 78.50' | 10.0' long x 5.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65 2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88 |
| #3 | Device 1 | 78.15' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=7.50 cfs @ 12.20 hrs HW=78.45' (Free Discharge)

↑ **1=CMP_Round 24"** (Passes 7.50 cfs of 25.19 cfs potential flow)

↑ **3=Orifice/Grate** (Weir Controls 7.50 cfs @ 1.79 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=76.50' (Free Discharge)

↑ **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Emergency Spillway

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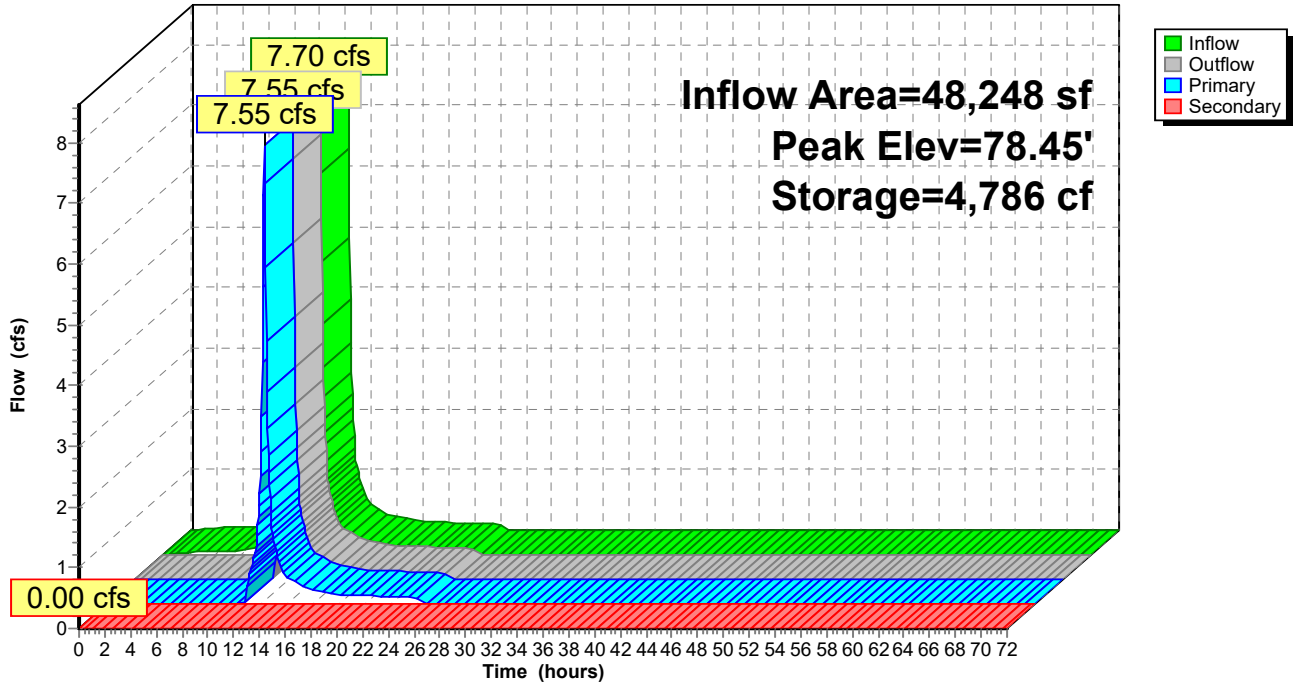
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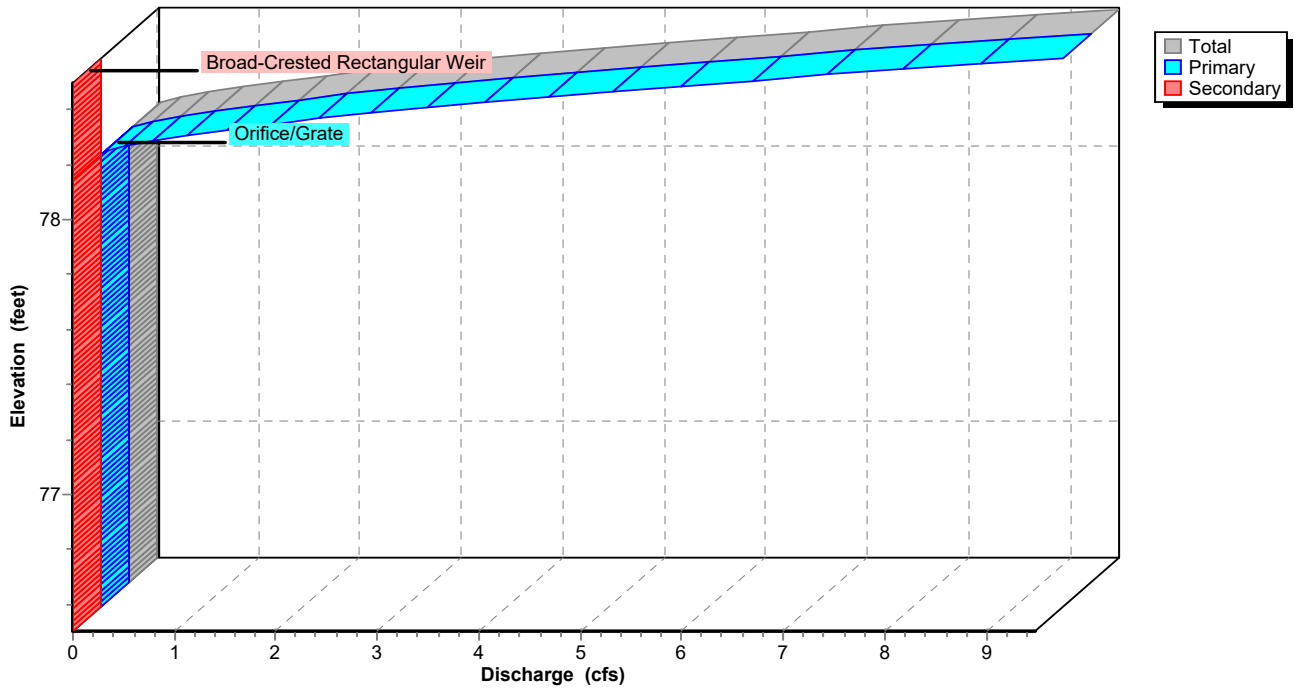
Pond B1: Bioretention Basin 1

Hydrograph



Pond B1: Bioretention Basin 1

Stage-Discharge



Emergency Spillway

NOAA 24-hr C 100-Year Rainfall=8.81"

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Summary for Pond B2: Bioretention Basin 2

[81] Warning: Exceeded Pond B1 by 0.12' @ 12.35 hrs

Inflow Area = 97,279 sf, 60.64% Impervious, Inflow Depth = 6.94" for 100-Year event
 Inflow = 15.77 cfs @ 12.19 hrs, Volume= 56,281 cf
 Outflow = 10.31 cfs @ 12.32 hrs, Volume= 53,114 cf, Atten= 35%, Lag= 7.8 min
 Primary = 10.31 cfs @ 12.32 hrs, Volume= 53,114 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 78.50' @ 12.31 hrs Surf.Area= 9,518 sf Storage= 16,324 cf

Plug-Flow detention time= 105.9 min calculated for 53,077 cf (94% of inflow)
 Center-of-Mass det. time= 75.0 min (864.8 - 789.8)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|--------|---------------|--|
| #1 | 76.50' | 26,647 cf | Custom Stage Data (Prismatic) Listed below (Recalc) |

| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) |
|------------------|-------------------|------------------------|------------------------|
| 76.50 | 6,877 | 0 | 0 |
| 77.50 | 8,155 | 7,516 | 7,516 |
| 78.50 | 9,522 | 8,839 | 16,355 |
| 79.50 | 11,063 | 10,293 | 26,647 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 73.00' | 15.0" Round Culvert L= 47.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 73.00' / 72.06' S= 0.0200 1' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.23 sf |
| #2 | Device 1 | 76.94' | 6.0" Vert. Orifice/Grate X 3.00 C= 0.600 |
| #3 | Device 1 | 77.78' | 4.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32 |
| #4 | Device 1 | 79.25' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |
| #5 | Secondary | 78.50' | 30.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 |

Primary OutFlow Max=10.29 cfs @ 12.32 hrs HW=78.49' (Free Discharge)

- ↑ 1=Culvert (Inlet Controls 10.29 cfs @ 8.38 fps)
- ↑ 2=Orifice/Grate (Passes < 3.23 cfs potential flow)
- ↑ 3=Broad-Crested Rectangular Weir (Passes < 7.66 cfs potential flow)
- ↑ 4=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=76.50' (Free Discharge)

- ↑ 5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Emergency Spillway

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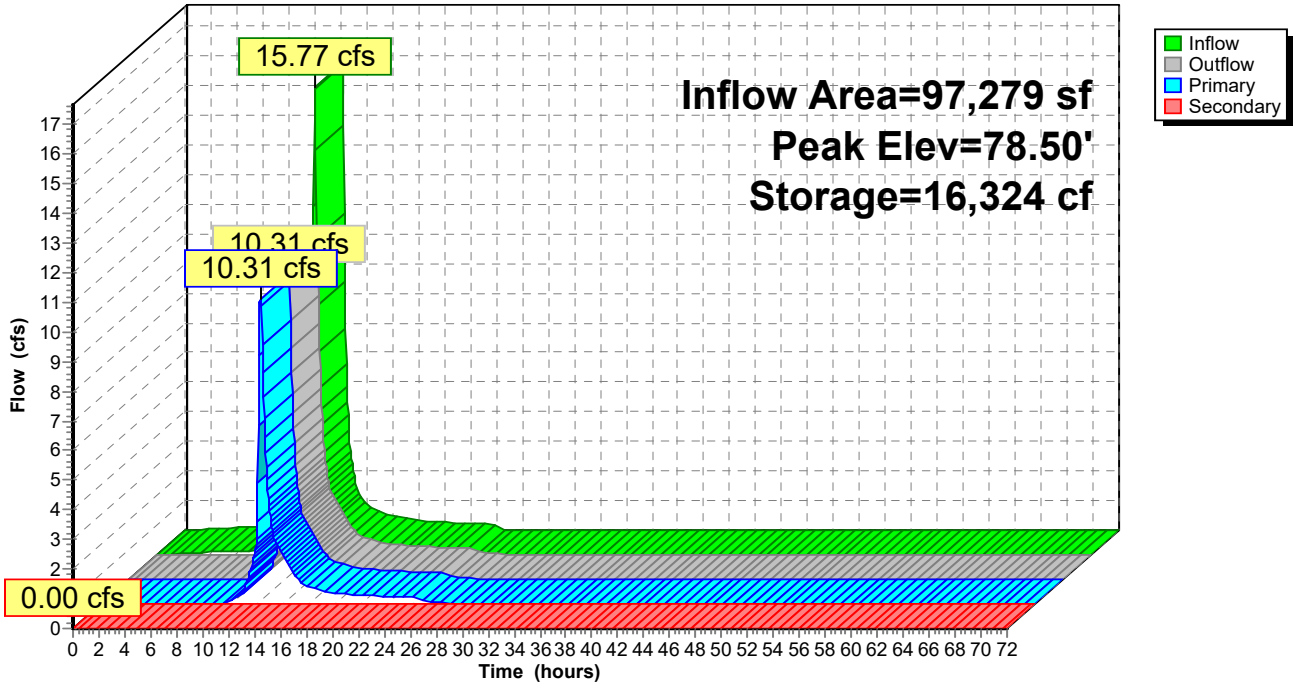
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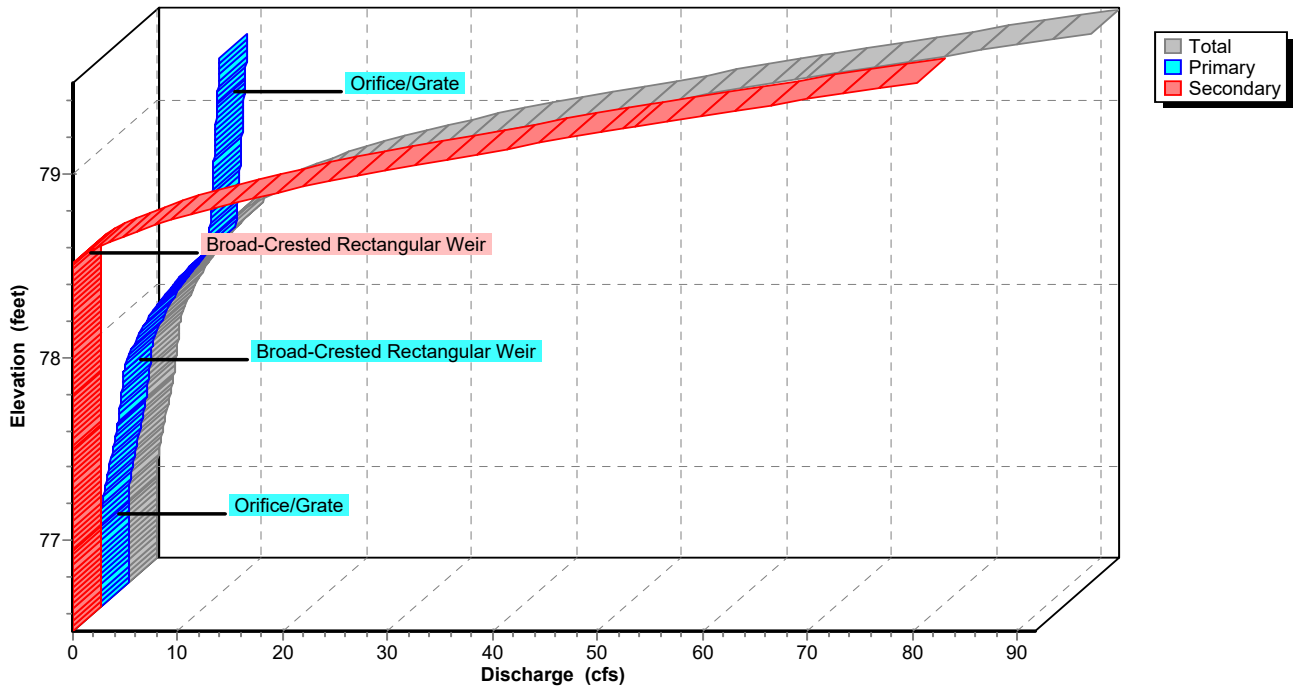
Pond B2: Bioretention Basin 2

Hydrograph



Pond B2: Bioretention Basin 2

Stage-Discharge



Emergency Spillway

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Summary for Pond B3: Bioretention Basin 3

[92] Warning: Device #2 is above defined storage

Inflow Area = 11,722 sf, 41.82% Impervious, Inflow Depth = 6.83" for 100-Year event
 Inflow = 1.41 cfs @ 12.30 hrs, Volume= 6,674 cf
 Outflow = 1.41 cfs @ 12.31 hrs, Volume= 6,199 cf, Atten= 0%, Lag= 0.7 min
 Primary = 1.41 cfs @ 12.31 hrs, Volume= 6,199 cf
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
 Peak Elev= 80.84' @ 12.31 hrs Surf.Area= 901 sf Storage= 560 cf

Plug-Flow detention time= 73.0 min calculated for 6,195 cf (93% of inflow)
 Center-of-Mass det. time= 33.5 min (823.5 - 790.1)

| Volume | Invert | Avail.Storage | Storage Description | |
|------------------|-------------------|------------------------|--|------------------|
| #1 | 79.98' | 694 cf | Custom Stage Data (Conic) Listed below (Recalc) | |
| Elevation (feet) | Surf.Area (sq-ft) | Inc.Store (cubic-feet) | Cum.Store (cubic-feet) | Wet.Area (sq-ft) |
| 79.98 | 432 | 0 | 0 | 432 |
| 80.98 | 995 | 694 | 694 | 1,003 |

| Device | Routing | Invert | Outlet Devices |
|--------|-----------|--------|---|
| #1 | Primary | 77.48' | 15.0" Round CMP_Round 15" L= 96.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 77.48' / 77.00' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.013 Concrete pipe, bends & connections, Flow Area= 1.23 sf |
| #2 | Secondary | 80.98' | 15.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32 |
| #3 | Device 1 | 80.74' | 42.0" x 42.0" Horiz. Orifice/Grate C= 0.600 in 42.0" x 42.0" Grate (100% open area) Limited to weir flow at low heads |

Primary OutFlow Max=1.39 cfs @ 12.31 hrs HW=80.84' (Free Discharge)

↑1=CMP_Round 15" (Passes 1.39 cfs of 7.71 cfs potential flow)

↑3=Orifice/Grate (Weir Controls 1.39 cfs @ 1.02 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=79.98' (Free Discharge)

↑2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Emergency Spillway

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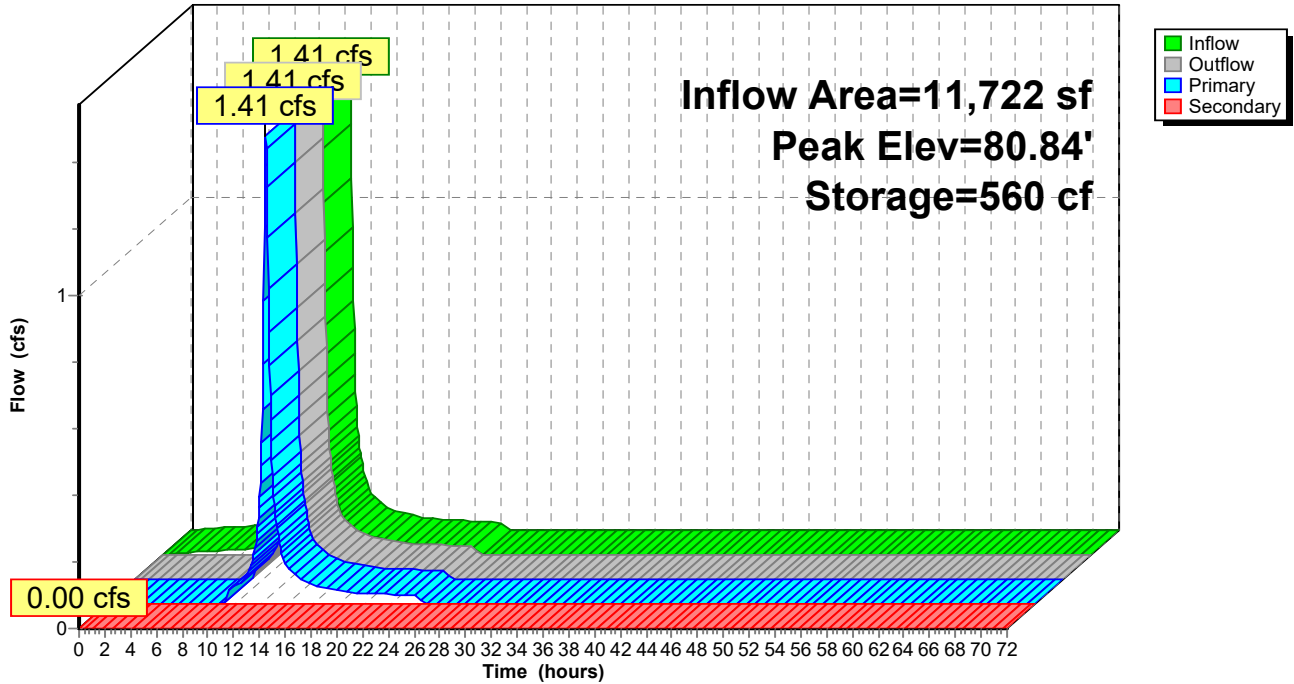
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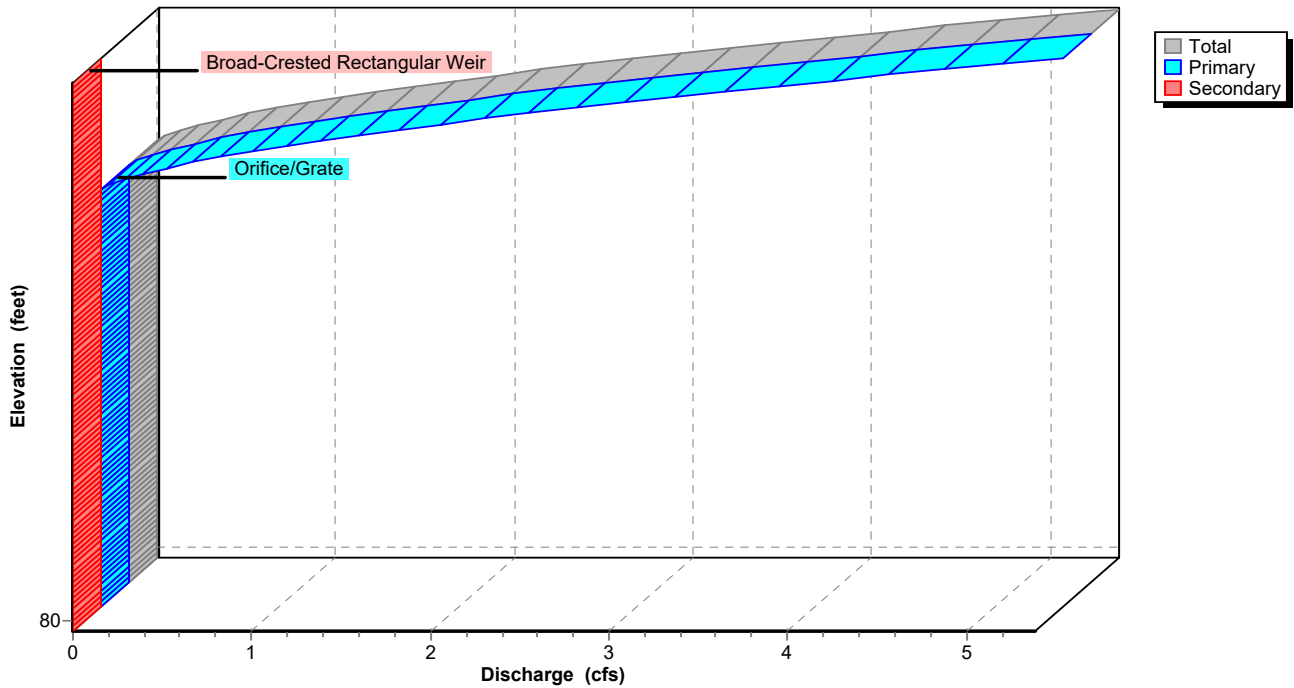
Pond B3: Bioretention Basin 3

Hydrograph



Pond B3: Bioretention Basin 3

Stage-Discharge



Conduit Outlet Protection Calculations

Rip Rap Pad # 1

Design Parameters:

| | |
|--|----------|
| Design Storm Flow for 25 Year, Q | 8.55 cfs |
| Vertical Dimension of Outlet Pipe, D_o | 15 in |
| Horizontal Dimension of Outlet Pipe, W_o | 15 in |
| Tailwater Depth, TW^1 | 0.87 ft |

Apron Dimension Calculations:

Unit Discharge, $q = Q/W_o = 6.84$ cfs per foot

• **Case I: $TW < 1/2 D_o$**

Apron Length, $L_a = \frac{1.8q}{D_o^{1/2}} + 7D_o =$

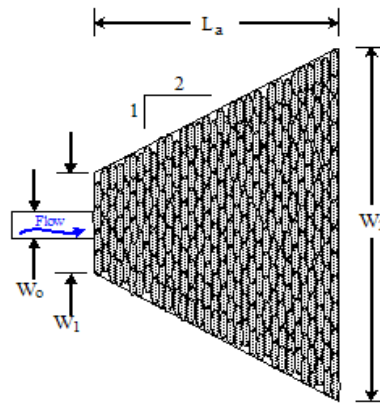
$L_a =$

Width, $W_1 = 3W_o =$

$W_1 =$

Width, $W_2 = 3W_o + L_a =$

$W_2 =$



• **Case II: $TW \geq 1/2 D_o$**

Apron Length, $L_a = \frac{3q}{D_o^{1/2}} = 18.35$ ft

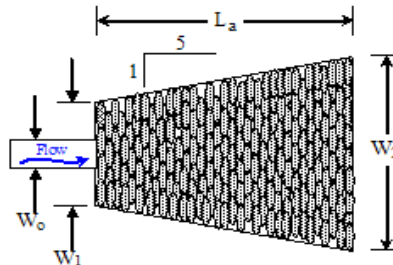
or $L_a = 19$ ft

Width, $W_1 = 3W_o = 3.75$ ft

or $W_1 = 6$ ft

Width, $W_2 = 3W_o + 0.4L_a = 11.09$ ft

or $W_2 = 12$ ft



Rip Rap Stone Size Calculations:

Median Stone, $d_{50} = \frac{0.02q^{1.33}}{TW} = 3.56$ in

$d_{50} = 6$ in

Notes:

1. Where there is a well-defined channel downstream of the apron, the bottom width of the apron shall be at least equal to the bottom width of the channel and the structural lining shall extend at least one foot above the tailwater elevation, but no lower than two-thirds of the vertical conduit dimension above the conduit invert.
2. The side slopes shall be 2:1 or flatter.
3. The bottom grade shall be 0.0% (level).
4. There shall be no overfall at the end of the apron or at the end of the culvert.
5. Fifty (50) percent by weight of the rip-rap mixture shall be smaller than the median size stone designated as d_{50} . The largest stone size in the mixture shall be 1.5 times the d_{50} size. The rip-rap shall be reasonably well graded.
6. The thickness of the rip-rap apron may be two (2) times the median stone diameter provided that the apron is constructed on a bedding of four (4) inches of 3/4 inch clean stone on approved filter fabric material.
7. Rip-rap and filter fabric shall meet the standards of the governing Soil Conservation District as well as the requirements of the local municipality.
8. No bends or curves at the intersection of the conduit and apron will be permitted.

Footnote:

1. Tailwater depth shall be the 2 year storm if discharging into a detention basin. For areas where tailwater cannot be computed, use $TW = 0.2D_o$.
2. For multiple pipes, increase rip-rap sizes by 25% when pipe spacing is greater than or equal to $1/4 W_o$.

Conduit Outlet Protection Calculations

Rip Rap Pad # 2

Design Parameters:

| | |
|--|----------|
| Design Storm Flow for 25 Year, Q | 4.95 cfs |
| Vertical Dimension of Outlet Pipe, D_o | 15 in |
| Horizontal Dimension of Outlet Pipe, W_o | 15 in |
| Tailwater Depth, TW^1 | 0.80 ft |

Apron Dimension Calculations:

Unit Discharge, $q = Q/W_o = 3.96$ cfs per foot

• **Case I: $TW < 1/2 D_o$**

Apron Length, $L_a = \frac{1.8q}{D_o^{1/2}} + 7D_o =$

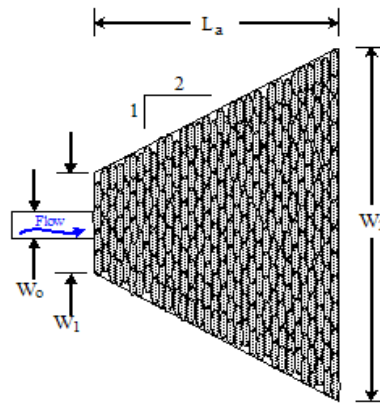
$L_a =$

Width, $W_1 = 3W_o =$

$W_1 =$

Width, $W_2 = 3W_o + L_a =$

$W_2 =$



• **Case II: $TW \geq 1/2 D_o$**

Apron Length, $L_a = \frac{3q}{D_o^{1/2}} = 10.63$ ft

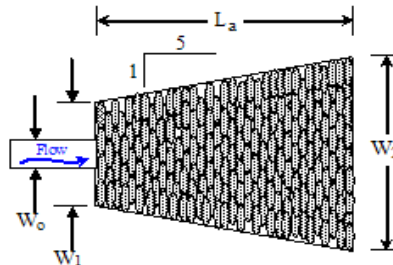
or $L_a = 11$ ft

Width, $W_1 = 3W_o = 3.75$ ft

or $W_1 = 6$ ft

Width, $W_2 = 3W_o + 0.4L_a = 8$ ft

or $W_2 = 9$ ft



Rip Rap Stone Size Calculations:

Median Stone, $d_{50} = \frac{0.02q^{1.33}}{TW} = 1.87$ in

$d_{50} = 6$ in

Notes:

1. Where there is a well-defined channel downstream of the apron, the bottom width of the apron shall be at least equal to the bottom width of the channel and the structural lining shall extend at least one foot above the tailwater elevation, but no lower than two-thirds of the vertical conduit dimension above the conduit invert.
2. The side slopes shall be 2:1 or flatter.
3. The bottom grade shall be 0.0% (level).
4. There shall be no overfall at the end of the apron or at the end of the culvert.
5. Fifty (50) percent by weight of the rip-rap mixture shall be smaller than the median size stone designated as d_{50} . The largest stone size in the mixture shall be 1.5 times the d_{50} size. The rip-rap shall be reasonably well graded.
6. The thickness of the rip-rap apron may be two (2) times the median stone diameter provided that the apron is constructed on a bedding of four (4) inches of 3/4 inch clean stone on approved filter fabric material.
7. Rip-rap and filter fabric shall meet the standards of the governing Soil Conservation District as well as the requirements of the local municipality.
8. No bends or curves at the intersection of the conduit and apron will be permitted.

Footnote:

1. Tailwater depth shall be the 2 year storm if discharging into a detention basin. For areas where tailwater cannot be computed, use $TW = 0.2D_o$.
2. For multiple pipes, increase rip-rap sizes by 25% when pipe spacing is greater than or equal to $1/4 W_o$.

Conduit Outlet Protection Calculations

Scour Hole # 200

Design Parameters:

| | |
|--|-----------|
| Design Storm Flow for 25 Year, Q | 11.38 cfs |
| Vertical Dimension of Outlet Pipe, D_o | 18 in |
| Horizontal Dimension of Outlet Pipe, W_o | 18 in |
| Tailwater Depth, TW^1 | 0.87 ft |
| Scour Hole Depth, y ($1/2 D_o$ or D_o) | 9 in |

Apron Dimension Calculations:

| | |
|---|-----------------|
| Minimum Bottom Width, $W_1 = 2W_o$ | $W_1 = 3.00$ ft |
| Minimum Bottom Length, $L_1 = 3D_o$ | $L_1 = 4.50$ ft |
| Minimum Top Width (max side slope of 3:1), W_2 | $W_2 = 7.50$ ft |
| Minimum Top Length (max side slope of 3:1), L_2 | $L_2 = 9.00$ ft |

Rip Rap Stone Size Calculations:

Unit Discharge, $q = Q/D_o = 7.59$ cfs per foot

• **Case I: $y = 1/2 D_o$**

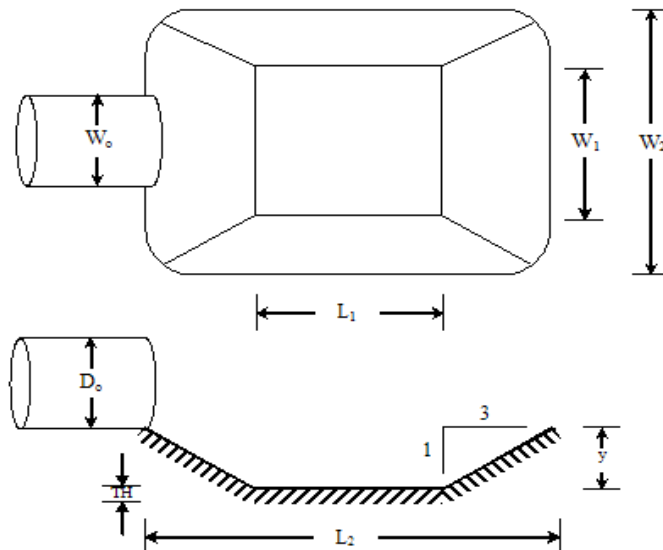
Median Stone, $d_{50} = \frac{0.0125 q^{1.33}}{TW} = 2.55$ in Therefore, use **$d_{50} = 6$ in**

Apron Thickness, $TH = 2 \times d_{50}$ with filter fabric **$TH = 12$ in**

• **Case II: $y = D_o$**

Median Stone, $d_{50} = \frac{0.0082 q^{1.33}}{TW} =$

Apron Thickness, $TH = 2 \times d_{50}$ with filter fabric



Notes:

1. The side slopes shall be 3:1 or flatter.
2. The bottom grade shall be 0.0% (level).
3. There shall be no overfall at the end of the apron or at the end of the culvert.
4. Fifty (50) percent by weight of the rip-rap mixture shall be smaller than the median size stone designated as d_{50} . The largest stone size in the mixture shall be 1.5 times the d_{50} size. The rip-rap shall be reasonably well graded.
5. The thickness of the rip-rap apron may be two (2) times the median stone diameter provided that the apron is constructed on a bedding of four (4) inches of 3/4 inch clean stone on approved filter fabric material.
6. Rip-rap and filter fabric shall meet the standards of the governing Soil Conservation District as well as the requirements of the local municipality.
7. Where the scour hole is to be placed within an existing or proposed waterway:
 - a. The scour hole sidewalls should be eliminated to maintain a smooth hydraulic line along the waterway bottom to avoid inviting turbulent flow from a sudden depression in the waterway.
 - b. If the flow in the waterway is greater than the flow from the proposed outlet, the rip-rap used to construct the scour hole should be sized based on the greater flow value according to the standard rip-rap.

Footnote:

1. Tailwater depth shall be the 2 year storm if discharging into a detention basin. For areas where tailwater cannot be computed, use $TW = 0.2D_o$.

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

Prepared by {enter your company name here}

Printed 5/17/2021

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Hydrograph for Pond B1: Bioretention Basin 1

| Time (hours) | Inflow (cfs) | Storage (cubic-feet) | Elevation (feet) | Primary (cfs) |
|--------------|--------------|----------------------|------------------|---------------|
| 0.00 | 0.00 | 0 | 76.50 | 0.00 |
| 2.50 | 0.04 | 187 | 76.60 | 0.00 |
| 5.00 | 0.07 | 693 | 76.85 | 0.00 |
| 7.50 | 0.11 | 1,431 | 77.19 | 0.00 |
| 10.00 | 0.27 | 2,937 | 77.80 | 0.00 |
| 12.50 | 2.24 | 4,310 | 78.29 | 2.47 |
| 15.00 | 0.29 | 3,994 | 78.18 | 0.30 |
| 17.50 | 0.18 | 3,964 | 78.17 | 0.18 |
| 20.00 | 0.13 | 3,950 | 78.17 | 0.13 |
| 22.50 | 0.11 | 3,943 | 78.17 | 0.11 |
| 25.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 27.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 30.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 32.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 35.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 37.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 40.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 42.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 45.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 47.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 50.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 52.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 55.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 57.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 60.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 62.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 65.00 | 0.00 | 3,895 | 78.15 | 0.00 |
| 67.50 | 0.00 | 3,895 | 78.15 | 0.00 |
| 70.00 | 0.00 | 3,895 | 78.15 | 0.00 |

Basin Drain Time = 25 -
12.50 = 12.5 hours

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

Prepared by {enter your company name here}

Printed 5/17/2021

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Hydrograph for Pond B2: Bioretention Basin 2

| Time (hours) | Inflow (cfs) | Storage (cubic-feet) | Elevation (feet) | Primary (cfs) |
|--------------|--------------|----------------------|------------------|---------------|
| 0.00 | 0.00 | 0 | 76.50 | 0.00 |
| 2.50 | 0.07 | 281 | 76.54 | 0.00 |
| 5.00 | 0.10 | 1,042 | 76.65 | 0.00 |
| 7.50 | 0.16 | 2,124 | 76.80 | 0.00 |
| 10.00 | 0.33 | 3,965 | 77.05 | 0.11 |
| 12.50 | 4.84 | 14,639 | 78.32 | 7.79 |
| 15.00 | 0.60 | 5,900 | 77.30 | 0.92 |
| 17.50 | 0.36 | 4,853 | 77.16 | 0.41 |
| 20.00 | 0.27 | 4,547 | 77.12 | 0.29 |
| 22.50 | 0.23 | 4,411 | 77.11 | 0.24 |
| 25.00 | 0.00 | 3,935 | 77.04 | 0.10 |
| 27.50 | 0.00 | 3,505 | 76.99 | 0.02 |
| 30.00 | 0.00 | 3,374 | 76.97 | 0.01 |
| 32.50 | 0.00 | 3,303 | 76.96 | 0.01 |
| 35.00 | 0.00 | 3,262 | 76.96 | 0.00 |
| 37.50 | 0.00 | 3,239 | 76.95 | 0.00 |
| 40.00 | 0.00 | 3,226 | 76.95 | 0.00 |
| 42.50 | 0.00 | 3,218 | 76.95 | 0.00 |
| 45.00 | 0.00 | 3,210 | 76.95 | 0.00 |
| 47.50 | 0.00 | 3,204 | 76.95 | 0.00 |
| 50.00 | 0.00 | 3,198 | 76.95 | 0.00 |
| 52.50 | 0.00 | 3,192 | 76.95 | 0.00 |
| 55.00 | 0.00 | 3,188 | 76.95 | 0.00 |
| 57.50 | 0.00 | 3,184 | 76.94 | 0.00 |
| 60.00 | 0.00 | 3,180 | 76.94 | 0.00 |
| 62.50 | 0.00 | 3,177 | 76.94 | 0.00 |
| 65.00 | 0.00 | 3,174 | 76.94 | 0.00 |
| 67.50 | 0.00 | 3,171 | 76.94 | 0.00 |
| 70.00 | 0.00 | 3,169 | 76.94 | 0.00 |

Basin Drain Time = 35 - 12.5
= 22.5 hours

Pre vs Post

NOAA 24-hr C 100-Year Rainfall=8.81"

Prepared by {enter your company name here}

Printed 5/17/2021

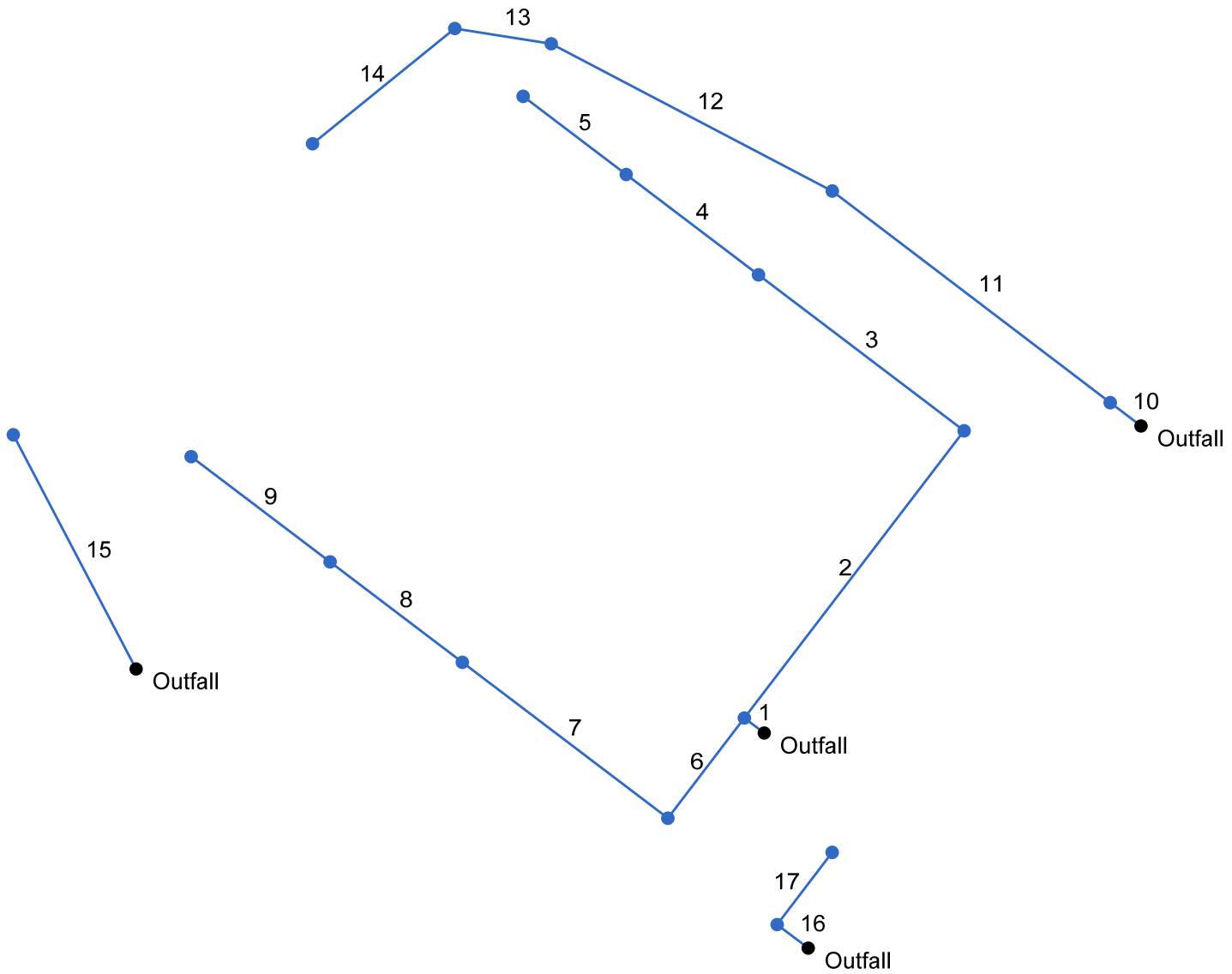
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Hydrograph for Pond B3: Bioretention Basin 3

| Time (hours) | Inflow (cfs) | Storage (cubic-feet) | Elevation (feet) | Outflow (cfs) | Primary (cfs) | Secondary (cfs) |
|--------------|--------------|----------------------|------------------|---------------|---------------|-----------------|
| 0.00 | 0.00 | 0 | 79.98 | 0.00 | 0.00 | 0.00 |
| 2.50 | 0.01 | 34 | 80.06 | 0.00 | 0.00 | 0.00 |
| 5.00 | 0.01 | 139 | 80.26 | 0.00 | 0.00 | 0.00 |
| 7.50 | 0.02 | 289 | 80.50 | 0.00 | 0.00 | 0.00 |
| 10.00 | 0.06 | 484 | 80.75 | 0.05 | 0.05 | 0.00 |
| 12.50 | 0.91 | 539 | 80.82 | 0.95 | 0.95 | 0.00 |
| 15.00 | 0.07 | 486 | 80.75 | 0.08 | 0.08 | 0.00 |
| 17.50 | 0.04 | 483 | 80.75 | 0.04 | 0.04 | 0.00 |
| 20.00 | 0.03 | 480 | 80.75 | 0.03 | 0.03 | 0.00 |
| 22.50 | 0.03 | 479 | 80.75 | 0.03 | 0.03 | 0.00 |
| 25.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 27.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 30.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 32.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 35.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 37.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 40.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 42.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 45.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 47.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 50.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 52.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 55.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 57.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 60.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 62.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 65.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 67.50 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |
| 70.00 | 0.00 | 474 | 80.74 | 0.00 | 0.00 | 0.00 |

Basin Drain Time = 25 - 12.5
= 12.5 hours

Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Project File: Pipe Calcs.stm

Number of lines: 17

Date: 5/14/2021

Storm Sewer Tabulation

| Station | | Len (ft) | Drng Area | | Rnoff coeff (C) | Area x C | | Tc | | Rain (l) (in/hr) | Total flow (cfs) | Cap full (cfs) | Vel (ft/s) | Pipe | | Invert Elev | | HGL Elev | | Grnd / Rim Elev | | Line ID |
|---------|------------|-------------|--------------|---------------|-----------------------|----------|-------|----------------|---------------|------------------------|------------------------|----------------------|---------------|--------------|--------------|-------------|------------|------------|------------|-----------------|------------|------------------|
| Line | To Line | | Incr (ac) | Total (ac) | | Incr | Total | Inlet (min) | Syst (min) | | | | | Size (in) | Slope (%) | Dn (ft) | Up (ft) | Dn (ft) | Up (ft) | Dn (ft) | Up (ft) | |
| 1 | End | 9.000 | 0.00 | 0.82 | 0.00 | 0.00 | 0.80 | 6.0 | 7.7 | 7.0 | 5.64 | 11.38 | 4.98 | 18 | 1.00 | 76.50 | 76.59 | 77.42 | 77.51 | 78.44 | 81.34 | HW 200 - MH 210 |
| 2 | 1 | 130.861 | 0.11 | 0.41 | 0.98 | 0.11 | 0.40 | 6.0 | 7.1 | 7.2 | 2.89 | 11.38 | 3.46 | 18 | 1.00 | 76.69 | 78.00 | 77.51 | 78.65 | 81.34 | 82.19 | MH 210 - MH 220 |
| 3 | 2 | 93.240 | 0.10 | 0.30 | 0.98 | 0.10 | 0.29 | 6.0 | 6.6 | 7.3 | 2.15 | 8.08 | 3.67 | 18 | 0.50 | 78.10 | 78.57 | 78.65 | 79.12 | 82.19 | 82.70 | MH 220 - CO 230 |
| 4 | 3 | 60.000 | 0.10 | 0.20 | 0.98 | 0.10 | 0.20 | 6.0 | 6.3 | 7.4 | 1.45 | 8.04 | 2.85 | 18 | 0.50 | 78.57 | 78.87 | 79.12 | 79.32 | 82.70 | 82.95 | CO 230 - MH 240 |
| 5 | 4 | 46.756 | 0.10 | 0.10 | 0.98 | 0.10 | 0.10 | 6.0 | 6.0 | 7.5 | 0.73 | 4.91 | 2.82 | 15 | 0.49 | 79.12 | 79.35 | 79.45 | 79.68 | 82.95 | 82.82 | MH 240 - MH 250 |
| 6 | 1 | 45.577 | 0.11 | 0.41 | 0.98 | 0.11 | 0.40 | 6.0 | 7.1 | 7.2 | 2.88 | 7.03 | 4.28 | 15 | 1.01 | 76.84 | 77.30 | 77.51 | 77.98 | 81.34 | 80.44 | MH 210 - MH 260 |
| 7 | 6 | 93.240 | 0.10 | 0.30 | 0.98 | 0.10 | 0.29 | 6.0 | 6.7 | 7.3 | 2.14 | 6.99 | 3.82 | 15 | 1.00 | 77.40 | 78.33 | 77.98 | 78.91 | 80.44 | 82.01 | MH 260 - CO 270 |
| 8 | 7 | 60.000 | 0.10 | 0.20 | 0.98 | 0.10 | 0.20 | 6.0 | 6.4 | 7.4 | 1.44 | 7.00 | 3.34 | 15 | 1.00 | 78.43 | 79.03 | 78.91 | 79.51 | 82.01 | 82.22 | CO 270 - CO 280 |
| 9 | 8 | 62.997 | 0.10 | 0.10 | 0.98 | 0.10 | 0.10 | 6.0 | 6.0 | 7.5 | 0.73 | 7.00 | 2.57 | 15 | 1.00 | 79.13 | 79.76 | 79.51 | 80.09 | 82.22 | 82.57 | CO 280 - MH 290 |
| 10 | End | 13.939 | 0.19 | 1.02 | 0.93 | 0.18 | 0.88 | 6.0 | 7.4 | 7.1 | 6.26 | 8.06 | 4.99 | 18 | 0.50 | 76.50 | 76.57 | 77.51 | 77.56 | 78.44 | 80.28 | HW 300 - IN 310 |
| 11 | 10 | 126.269 | 0.18 | 0.83 | 0.90 | 0.16 | 0.70 | 6.0 | 6.9 | 7.2 | 5.09 | 8.04 | 4.55 | 18 | 0.50 | 76.67 | 77.30 | 77.62 | 78.17 | 80.28 | 81.24 | IN 310 - IN 320 |
| 12 | 11 | 114.634 | 0.29 | 0.65 | 0.80 | 0.23 | 0.54 | 6.0 | 6.5 | 7.4 | 3.98 | 4.93 | 4.47 | 15 | 0.50 | 77.55 | 78.12 | 78.40 | 78.97 | 81.24 | 81.90 | IN 320 - IN 330 |
| 13 | 12 | 35.240 | 0.00 | 0.36 | 0.98 | 0.00 | 0.31 | 6.0 | 6.3 | 7.4 | 2.29 | 5.00 | 3.21 | 15 | 0.51 | 78.22 | 78.40 | 79.09 | 79.00 | 81.90 | 82.86 | IN 330 - MH 340 |
| 14 | 13 | 66.170 | 0.36 | 0.36 | 0.86 | 0.31 | 0.31 | 6.0 | 6.0 | 7.5 | 2.32 | 4.94 | 3.94 | 15 | 0.50 | 78.50 | 78.83 | 79.10 | 79.44 | 82.86 | 81.76 | MH 340 - IN 350 |
| 15 | End | 95.713 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.0 | 6.0 | 0.0 | 0.96 | 4.95 | 3.02 | 15 | 0.50 | 77.00 | 77.48 | 77.38 | 77.86 | 78.39 | 80.41 | FES 400 - OS 410 |
| 16 | End | 14.058 | 0.00 | 0.00 | 0.98 | 0.00 | 0.00 | 6.0 | 6.1 | 0.0 | 5.74 | 8.55 | 6.04 | 15 | 1.49 | 72.20 | 72.41 | 73.05 | 73.38 | 74.48 | 76.57 | HW 100 - MH 110 |
| 17 | 16 | 32.859 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.0 | 6.0 | 0.0 | 5.74 | 8.54 | 5.96 | 15 | 1.49 | 72.51 | 73.00 | 73.38 | 73.97 | 76.57 | 77.00 | MH 110 - OS 120 |

Project File: Pipe Calcs.stm

Number of lines: 17

Run Date: 5/14/2021

NOTES: Intensity = 182.59 / (Inlet time + 19.10) ^ 0.99; Return period = Yrs. 25 ; c = cir e = ellip b = box

NJDEP Nonstructural Strategies Points System (NSPS)

Version: January 31, 2006

Note: Input Values in Yellow Cells Only

Project:

Date:

User:

Notes:

| |
|--|
| |
| |
| |
| |

Step 1 - Provide Basic Major Development Site Information

A. Specify Total Area in Acres of Development Site Described in Steps 2 and 3 = Acres

B. Specify by Percent the Various Planning Areas Located within the Development Site:

| State Plan Planning Area: | PA-1 | PA-2 | PA-3 | PA-4 | PA-4B | PA-5 | Total % Area |
|--|----------------------|-------------------------------------|----------------------|----------------------|----------------------|----------------------|-------------------------------------|
| Percent of Each Planning Area within Site: | <input type="text"/> | <input type="text" value="100.0%"/> | <input type="text"/> | <input type="text"/> | <input type="text"/> | <input type="text"/> | <input type="text" value="100.0%"/> |

Note: See User's Guide for Equivalent Zones within Designated Centers and the NJ Meadowlands, Pinelands, and Highlands Districts

Step 2 - Describe Existing or Pre-Developed Site Conditions

A. Specify Existing Land Use/Land Cover Descriptions and Areas:

| Site Segment | Land Use/Land Cover Description | Specify Land Use/Land Cover in Acres for Each HSG | | | | Use/Cover | Points |
|-------------------------------|--|---|-------|--------|-------|-----------|--|
| | | HSG A | HSG B | HSG C | HSG D | Subtotals | |
| 1 | Wetlands and Undisturbed Stream Buffers | | | 0.2 | | 0.2 | 13 |
| 2 | Lawn and Open Space | | | 1.6 | | 1.6 | 78 |
| 3 | Brush and Shrub | | | | | 0.0 | 0 |
| 4 | Meadow, Pasture, Grassland, or Range | | | | | 0.0 | 0 |
| 5 | Row Crop | | | | | 0.0 | 0 |
| 6 | Small Grain and Legumes | | | | | 0.0 | 0 |
| 7 | Woods - Indigenous | | | 1.7 | | 1.7 | 115 |
| 8 | Woods - Planted | | | | | 0.0 | 0 |
| 9 | Woods and Grass Combination | | | | | 0.0 | 0 |
| 10 | Ponds, Lakes, and Other Open Water | | | | | 0.0 | 0 |
| 11 | Gravel and Dirt | | | 0.9 | | 0.9 | 27 |
| 12 | Porous and Permeable Paving | | | | | 0.0 | 0 |
| 13 | Directly Connected Impervious | | | 0.4 | | 0.4 | 0 |
| 14 | Unconnected Impervious with Small D/S Pervious | | | | | 0.0 | 0 |
| 15 | Unconnected Impervious with Large D/S Pervious | | | | | 0.0 | 0 |
| HSG Subtotals (Acres): | | 0.0 | 0.0 | 4.8 | 0.0 | | Total Area: 4.8 |
| HSG Subtotals (%): | | 0.0% | 0.0% | 100.0% | 0.0% | | Total % Area: 100.0% |
| | | | | | | | Points Subtotal: 234 |
| | | | | | | | Total Existing Site Points: 234 |

Step 3 - Describe Proposed or Post-Developed Site Conditions

A. Specify Proposed Land Use/Land Cover Descriptions and Areas:

| Site Segment | Land Use/Land Cover Description | Specify Land Use/Land Cover in Acres for Each HSG | | | | Use/Cover | Points |
|-------------------------------|--|---|-------|--------|-------|-----------|-----------------------------|
| | | HSG A | HSG B | HSG C | HSG D | Subtotals | |
| 1 | Wetlands and Undisturbed Stream Buffers | | | 0.2 | | 0.2 | 13 |
| 2 | Lawn and Open Space | | | 2.3 | | 2.3 | 109 |
| 3 | Brush and Shrub | | | | | 0.0 | 0 |
| 4 | Meadow, Pasture, Grassland, or Range | | | | | 0.0 | 0 |
| 5 | Row Crop | | | | | 0.0 | 0 |
| 6 | Small Grain and Legumes | | | | | 0.0 | 0 |
| 7 | Woods - Indigenous | | | 0.9 | | 0.9 | 58 |
| 8 | Woods - Planted | | | | | 0.0 | 0 |
| 9 | Woods and Grass Combination | | | | | 0.0 | 0 |
| 10 | Ponds, Lakes, and Other Open Water | | | | | 0.0 | 0 |
| 11 | Gravel and Dirt | | | | | 0.0 | 0 |
| 12 | Porous and Permeable Paving | | | | | 0.0 | 0 |
| 13 | Directly Connected Impervious | | | 1.5 | | 1.5 | 0 |
| 14 | Unconnected Impervious with Small D/S Pervious | | | | | 0.0 | 0 |
| 15 | Unconnected Impervious with Large D/S Pervious | | | | | 0.0 | 0 |
| HSG Subtotals (Acres): | | 0.0 | 0.0 | 4.8 | 0.0 | | Total Area: 4.8 |
| HSG Subtotals (%): | | 0.0% | 0.0% | 100.0% | 0.0% | | Total % Area: 100.0% |
| | | | | | | | Points Subtotal: 180 |

B. Compare Proposed Impervious Coverage with Maximum Allowable Impervious Coverage:

| | | |
|---|-----|-----------|
| Total Directly Connected Impervious Coverage = | 32% | % of Site |
| Total Unconnected Impervious Coverage with Small D/S Pervious = | 0% | % of Site |
| Total Unconnected Impervious Coverage with Large D/S Pervious = | 0% | % of Site |
| Total Site Impervious Coverage = | 32% | % of Site |
| Effective Site Impervious Coverage = | 32% | % of Site |

Specify Source of Maximum Allowable Impervious Coverage: None (None or Table)

Points Subtotal: 0

C. Compare Proposed Site Disturbance with Maximum Allowable Site Disturbance:

| | | |
|---|-----|-----------|
| Total Proposed Site Disturbance = | 30% | % of Site |
| Maximum Allowable Site Disturbance by Municipal Ordinance = | 60% | % of Site |

Points Subtotal: 23

D. Describe Proposed Runoff Conveyance System:

| | | |
|---|----|------|
| Total Length of Runoff Conveyance System = | | Feet |
| Length of Vegetated Runoff Conveyance System = | | Feet |
| % of Total Runoff Conveyance System That is Vegetated = | 0% | |

Points Subtotal: 0

E. Residential Lot Clustering:

| | | |
|--|--|-----------------------------|
| Percent of Total Site Area that will be Clustered = | | % of Site |
| Minimum Standard Lot Size as Per Zoning (Note: 1/2 Acre or Greater) = | | Acres |
| Maximum Proposed Cluster Lot Size (Note: 1/4 Acre or Less) = | | Acres |
| Percent of Clustered Portion of Site to be Preserved as Vegetated Open Space = | | % of Clustered Site Portion |

Points Subtotal: 0

F. Will the Following be Utilized to Minimize Soil Compaction?

Proposed Lawn Areas will be Graded with Lightweight Construction Equipment:
Percent of Proposed Lawn Areas to be Graded with Such Equipment:

| | |
|------|-----------------|
| Yes | (Yes or No) |
| 100% | % of Lawn Areas |

Points Subtotal: **23**

G. Are Any of the Following Stormwater Management Standards Met Using Only Nonstructural Strategies and Measures?

Groundwater Recharge Standards (NJAC 7:8-5.4-a-2):
Stormwater Runoff Quality Standards (NJAC 7:8-5.5):
Stormwater Runoff Quantity Standards (NJAC 7:8-5.4-a-3):

| | |
|-----|-------------|
| No | (Yes or No) |
| Yes | (Yes or No) |
| No | (Yes or No) |

Points Subtotal: **68**

Note: If the Answers to All Three Questions at G Above are "Yes", Adequate Nonstructural Measures have been Utilized.

Total Proposed Site Points: 294

Ratio of Proposed to Existing Site Points: 126%

Required Site Points Ratio: 88%

Nonstructural Point System Results:

Proposed Nonstructural Measures are Adequate

New Jersey Stormwater Best Management Practices Manual

February 2004

A P P E N D I X A

Low Impact Development Checklist

A checklist for identifying nonstructural stormwater management strategies incorporated into proposed land development

According to the NJDEP Stormwater Management Rules at N.J.A.C. 7:8, the groundwater recharge, stormwater quality, and stormwater quantity standards established by the Rules for major land development projects must be met by incorporating nine specific nonstructural stormwater management strategies into the project's design to the maximum extent practicable.

To accomplish this, the Rules require an applicant seeking land development approval from a regulatory board or agency to identify those nonstructural strategies that have been incorporated into the project's design. In addition, if an applicant contends that it is not feasible to incorporate any of the specific strategies into the project's design, particularly for engineering, environmental, or safety reasons, the Rules further require that the applicant provide a basis for that contention.

This checklist has been prepared to assist applicants, site designers, and regulatory boards and agencies in ensuring that the nonstructural stormwater management requirements of the Rules are met. It provides an applicant with a means to identify both the nonstructural strategies incorporated into the development's design and the specific low impact development BMPs (LID-BMPs) that have been used to do so. It can also help an applicant explain the engineering, environmental, and/or safety reasons that a specific nonstructural strategy could not be incorporated into the development's design.

The checklist can also assist municipalities and other land development review agencies in the development of specific requirements for both nonstructural strategies and LID-BMPs in zoning and/or land use ordinances and regulations. As such, where requirements consistent with the Rules have been adopted, they may supersede this checklist.

Finally, the checklist can be used during a pre-design meeting between an applicant and pertinent review personnel to discuss local nonstructural strategies and LID-BMPs requirements in order to optimize the development's nonstructural stormwater management design.

Since this checklist is intended to promote the use of nonstructural stormwater management strategies and provide guidance in their incorporation in land development projects, municipalities are permitted to revise it as necessary to meet the goals and objectives of their specific stormwater management program and plan within the limits of N.J.A.C. 7:8.

Low Impact Development Checklist

A checklist for identifying nonstructural stormwater management strategies incorporated into proposed land development

Municipality: _____

County: _____ Date: _____

Review board or agency: _____

Proposed land development name: _____

Lot(s): _____ Block(s): _____

Project or application number: _____

Applicant's name: _____

Applicant's address: _____

Telephone: _____ Fax: _____

Email address: _____

Designer's name: _____

Designer's address: _____

Telephone: _____ Fax: _____

Email address: _____

Part 1: Description of Nonstructural Approach to Site Design

In narrative form, provide an overall description of the nonstructural stormwater management approach and strategies incorporated into the proposed site's design. Attach additional pages as necessary. Details of each nonstructural strategy are provided in Part 3 below.

Part 2: Review of Local Stormwater Management Regulations

Title and date of stormwater management regulations used in development design:

Do regulations include nonstructural requirements? Yes: _____ No: _____

If yes, briefly describe: _____

List LID-BMPs prohibited by local regulations: _____

Pre-design meeting held? Yes: _____ Date: _____ No: _____

Meeting held with: _____

Pre-design site walk held? Yes: _____ Date: _____ No: _____

Site walk held with: _____

Other agencies with stormwater review jurisdiction:

Name: _____

Required approval: _____

Name: _____

Required approval: _____

Name: _____

Required approval: _____

Part 3: Nonstructural Strategies and LID-BMPs in Design

3.1 Vegetation and Landscaping

Effective management of both existing and proposed site vegetation can reduce a development's adverse impacts on groundwater recharges and runoff quality and quantity. This section of the checklist helps identify the vegetation and landscaping strategies and nonstructural LID-BMPs that have been incorporated into the proposed development's design to help maintain existing recharge rates and/or minimize or prevent increases in runoff quantity and pollutant loading.

A. Has an inventory of existing site vegetation been performed? Yes: _____ No: _____

If yes, was this inventory a factor in the site's layout and design? Yes: _____ No: _____

B. Does the site design utilize any of the following nonstructural LID-BMPs?

Preservation of natural areas? Yes: _____ No: _____ If yes, specify % of site: _____

Native ground cover? Yes: _____ No: _____ If yes, specify % of site: _____

Vegetated buffers? Yes: _____ No: _____ If yes, specify % of site: _____

C. Do the land development regulations require these nonstructural LID-BMPs?

Preservation of natural areas? Yes: _____ No: _____ If yes, specify % of site: _____

Native ground cover? Yes: _____ No: _____ If yes, specify % of site: _____

Vegetated buffers? Yes: _____ No: _____ If yes, specify % of site: _____

D. If vegetated filter strips or buffers are utilized, specify their functions:

Reduce runoff volume increases through lower runoff coefficient: Yes: _____ No: _____

Reduce runoff pollutant loads through runoff treatment: Yes: _____ No: _____

Maintain groundwater recharge by preserving natural areas: Yes: _____ No: _____

3.2 Minimize Land Disturbance

Minimizing land disturbance is a nonstructural LID-BMP that can be applied during both the development's construction and post-construction phases. This section of the checklist helps identify those land disturbance strategies and nonstructural LID-BMPs that have been incorporated into the proposed development's design to minimize land disturbance and the resultant change in the site's hydrologic character.

A. Have inventories of existing site soils and slopes been performed? Yes: _____ No: _____

If yes, were these inventories factors in the site's layout and design? Yes: _____ No: _____

B. Does the development's design utilize any of the following nonstructural LID-BMPs?

Restrict permanent site disturbance by land owners? Yes: _____ No: _____

If yes, how: _____

Restrict temporary site disturbance during construction? Yes: _____ No: _____

If yes, how: _____

Consider soils and slopes in selecting disturbance limits? Yes: _____ No: _____

If yes, how: _____

C. Specify percentage of site to be cleared: _____ Regraded: _____

D. Specify percentage of cleared areas done so for buildings: _____

For driveways and parking: _____ For roadways: _____

E. What design criteria and/or site changes would be required to reduce the percentages in C and D above?

F. Specify site's hydrologic soil group (HSG) percentages:

HSG A: _____ HSG B: _____ HSG C: _____ HSG D: _____

G. Specify percentage of each HSG that will be permanently disturbed:

HSG A: _____ HSG B: _____ HSG C: _____ HSG D: _____

H. Locating site disturbance within areas with less permeable soils (HSG C and D) and minimizing disturbance within areas with greater permeable soils (HSG A and B) can help maintain groundwater recharge rates and reduce runoff volume increases. In light of the HSG percentages in F and G above, what other practical measures if any can be taken to achieve this?

I. Does the site include Karst topography? Yes: _____ No: _____

If yes, discuss measures taken to limit Karst impacts:

3.3 Impervious Area Management

New impervious surfaces at a development site can have the greatest adverse effect on groundwater recharge and stormwater quality and quantity. This section of the checklist helps identify those nonstructural strategies and LID-BMPs that have been incorporated into a proposed development's design to comprehensively manage the extent and impacts of new impervious surfaces.

A. Specify impervious cover at site: Existing: _____ Proposed: _____

B. Specify maximum site impervious coverage allowed by regulations: _____

C. Compare proposed street cartway widths with those required by regulations:

| Type of Street | Proposed Cartway Width (feet) | Required Cartway Width (feet) |
|---|-------------------------------|-------------------------------|
| Residential access – low intensity | | |
| Residential access – medium intensity | | |
| Residential access – high intensity with parking | | |
| Residential access – high intensity without parking | | |
| Neighborhood | | |
| Minor collector – low intensity without parking | | |
| Minor collector – with one parking lane | | |
| Minor collector – with two parking lanes | | |
| Minor collector – without parking | | |
| Major collector | | |

D. Compare proposed parking space dimensions with those required by regulations:

Proposed: _____ Regulations: _____

E. Compare proposed number of parking spaces with those required by regulations:

Proposed: _____ Regulations: _____

F. Specify percentage of total site impervious cover created by buildings:

By driveways and parking: _____ By roadways: _____

G. What design criteria and/or site changes would be required to reduce the percentages in F above?

H. Specify percentage of total impervious area that will be unconnected:

Total site: _____ Buildings: _____ Driveways and parking: _____ Roads: _____

I. Specify percentage of total impervious area that will be porous:

Total site: _____ Buildings: _____ Driveways and parking: _____ Roads: _____

J. Specify percentage of total building roof area that will be vegetated: _____

K. Specify percentage of total parking area located beneath buildings: _____

L. Specify percentage of total parking located within multi-level parking deck: _____

3.4 Time of Concentration Modifications

Decreasing a site's time of concentration (Tc) can lead directly to increased site runoff rates which, in turn, can create new and/or aggravate existing erosion and flooding problems downstream. This section of the checklist helps identify those nonstructural strategies and LID-BMPs that have been incorporated into the proposed development's design to effectively minimize such Tc decreases.

When reviewing Tc modification strategies, it is important to remember that a drainage area's Tc should reflect the general conditions throughout the area. As a result, Tc modifications must generally be applied throughout a drainage area, not just along a specific Tc route.

A. Specify percentage of site's total stormwater conveyance system length that will be:

Storm sewer: _____ Vegetated swale: _____ Natural channel: _____

Stormwater management facility: _____ Other: _____

Note: the total length of the stormwater conveyance system should be measured from the site's downstream property line to the downstream limit of sheet flow at the system's headwaters.

B. What design criteria and/or site changes would be required to reduce the storm sewer percentages and increase the vegetated swale and natural channel percentages in A above?

C. In conveyance system subareas that have overland or sheet flow over impervious surfaces or turf grass, what practical and effective site changes can be made to:

Decrease overland flow slope: _____

Increase overland flow roughness: _____

3.5 Preventative Source Controls

The most effective way to address water quality concerns is by pollution prevention. This section of the checklist helps identify those nonstructural strategies and LID-BMPs that have been incorporated into the proposed development's design to reduce the exposure of pollutants to prevent their release into the stormwater runoff.

A. Trash Receptacles

Specify the number of trash receptacles provided: _____

Specify the spacing between the trash receptacles: _____

Compare trash receptacles proposed with those required by regulations:

Proposed: _____ Regulations: _____

B. Pet Waste Stations

Specify the number of pet waste stations provided: _____

Specify the spacing between the pet waste stations: _____

Compare pet waste stations proposed with those required by regulations:

Proposed: _____ Regulations: _____

C. Inlets, Trash Racks, and Other Devices that Prevent Discharge of Large Trash and Debris

Specify percentage of total inlets that comply with the NJPDES storm drain inlet criteria: _____

D. Maintenance

Specify the frequency of the following maintenance activities:

Street sweeping: Proposed: _____ Regulations: _____

Litter collection: Proposed: _____ Regulations: _____

Identify other stormwater management measures on the site that prevent discharge of large trash and debris:

E. Prevention and Containment of Spills

Identify locations where pollutants are located on the site, and the features that prevent these pollutants from being exposed to stormwater runoff:

Pollutant: _____ Location: _____

Feature utilized to prevent pollutant exposure, harmful accumulation, or contain spills:

Pollutant: _____ Location: _____

Feature utilized to prevent pollutant exposure, harmful accumulation, or contain spills:

Pollutant: _____ Location: _____

Feature utilized to prevent pollutant exposure, harmful accumulation, or contain spills:

Pollutant: _____ Location: _____

Feature utilized to prevent pollutant exposure, harmful accumulation, or contain spills:

Pollutant: _____ Location: _____

Part 4: Compliance with Nonstructural Requirements of NJDEP Stormwater Management Rules

1. Based upon the checklist responses above, indicate which nonstructural strategies have been incorporated into the proposed development's design in accordance with N.J.A.C. 7:8-5.3(b):

| No. | Nonstructural Strategy | Yes | No |
|-----|--|-----|----|
| 1. | Protect areas that provide water quality benefits or areas particularly susceptible to erosion and sediment loss. | | |
| 2. | Minimize impervious surfaces and break up or disconnect the flow of runoff over impervious surfaces. | | |
| 3. | Maximize the protection of natural drainage features and vegetation. | | |
| 4. | Minimize the decrease in the pre-construction time of concentration. | | |
| 5. | Minimize land disturbance including clearing and grading. | | |
| 6. | Minimize soil compaction. | | |
| 7. | Provide low maintenance landscaping that encourages retention and planting of native vegetation and minimizes the use of lawns, fertilizers, and pesticides. | | |
| 8. | Provide vegetated open-channel conveyance systems discharge into and through stable vegetated areas. | | |
| 9. | Provide preventative source controls. | | |

2. For those strategies that have not been incorporated into the proposed development's design, provide engineering, environmental, and/or safety reasons. Attached additional pages as necessary.



30 INDEPENDENCE BOULEVARD
SUITE 250
WARREN, NJ 07059
908.668.7777
whitestoneassoc.com

March 4, 2021

via email

SAFSTOR REAL ESTATE CO, LLC
c/o W&A ENGINEERING
355 Oneta Street
Suite D100
Athens, Georgia 30601

Attention: Mr. Jim Burtt
Project Manager

**Regarding: SWM AREA EVALUATION & ON-SITE WASTEWATER
MANAGEMENT EVALUATION SERVICES
PROPOSED SELF-STORAGE FACILITY
471 ELIZABETH AVENUE
FRANKLIN TOWNSHIP, SOMERSET COUNTY, NEW JERSEY
WHITESTONE PROJECT NO.: GJ2117698.000**

Dear Mr. Burtt:

Whitestone Associates, Inc. (Whitestone) has completed a stormwater management (SWM) area evaluation and on-site wastewater management evaluation services at the above-referenced site. The results of the evaluation presented below are based on the soil conditions disclosed by the profile pits performed during Whitestone's February 2021 field investigation.

1.0 PROJECT DESCRIPTION

The subject property located at 471 Elizabeth Avenue in Franklin Township, Somerset County, New Jersey currently consists of an undeveloped lot. Based on the January 18, 2021 *Conceptual Grading, Drainage & Utility Plan* prepared by Bohler Engineering NJ, LLC (Bohler), the proposed development will include construction of a three-story, self-storage facility with new pavements, landscaping, SWM area, septic area, and utilities. The SWM facility will be located within the southern portion of the site. The septic area preliminarily is anticipated to be located within the eastern portion of the site. Final details regarding the type, bottom elevation, and size of the proposed SWM/septic facilities have not been established at the time of this report.

2.0 FIELD EXPLORATION

Whitestone's scope of services consisted of conducting an engineering evaluation of the subsurface conditions disclosed by nine profile pits (identified as SPP-1A, SPP-2A, SPP-3 through SPP-6, and offsets SPP-3A, SPP-4A, and SPP-5A). The subsurface tests extended to depths ranging from approximately five feet below ground surface (fbgs) to 8.5 fbgs. The subsurface tests were located in the field using normal taping procedures and estimated right angles from existing features and are presumed

Other Office Locations:

CHALFONT, PA
215.712.2700

SOUTHBOROUGH, MA
508.485.0755

ROCKY HILL, CT
860.726.7889

WALL, NJ
732.592.2101

PHILADELPHIA, PA
215.848.2323

to be accurate within a few feet. Upon completion, the test locations were backfilled to existing surface levels using soils generated during excavation of the test pits. Soil profile pits and associated infiltration testing performed for the proposed septic system were witnessed by a representative of the Franklin Township Health Department.

3.0 SWM AREA TEST RESULTS

General: The SWM area investigation included four profile pits (identified as SPP-4, SPP-5, and associated offsets SPP-4A and SPP-5A for basin flood testing) performed within the anticipated location of the SWM area. The test locations are shown on the *Test Location Plan* included as Figure 1. Details of the subsurface materials encountered are presented on the *Records of Subsurface Exploration* presented in Appendix A.

Estimated Seasonal High Groundwater Levels: The methods used in determining the estimated seasonal high groundwater (ESHGW) level include evaluating the soil morphology within a test location and identifying irregular spots or blotches of different colors or minerals unlike that of the surrounding soils (mottles). Mottling is the result of the oxidation of minerals within a soil structure as a water level slowly fluctuates.

Groundwater and indications of seasonal high groundwater levels were encountered within the profile pits performed at the depths/elevations indicated in the *Records of Subsurface Exploration*. Groundwater conditions likely will fluctuate seasonally and following periods of precipitation.

Infiltration Testing: Basin flood tests were conducted within the weathered rock/bedrock strata encountered at profile pits SPP-4A and SPP-5A. The basin flood tests performed within the profile pits were conducted in general accordance with the *New Jersey Stormwater Best Management Practices Manual* (BMP Manual). The results of the in-situ testing indicated that basin flood tests did not drain the required 12 inches within 24 hours of filling. Therefore, per the BMP Manual, the limiting zone is considered to be a massive rock substratum and a infiltration rate cannot be assigned. Detailed in-situ infiltration test results are available in Appendix C.

Additionally, representative samples within profile pits SPP-4 and SPP-5 were subjected to tube permeameter analysis as detailed in *New Jersey Stormwater Best Practices Manual*. Laboratory tube permeameter testing resulted in a infiltration rate of less than 0.2 iph. Individual tube permeameter test results are provided in Appendix B.

4.0 SEPTIC AREA TEST RESULTS

General: The septic area investigation included four profile pits (identified as SPP-1A, SPP-2A, SPP-3 and associated offset SPP-3A for basin flood testing) performed within the potential locations of the septic disposal bed areas. The test locations are shown on the *Test Location Plan* included as Figure 1. Details of the subsurface materials encountered are presented on the *Records of Subsurface Exploration* presented in Appendix A.

Estimated Seasonal High Groundwater Levels: Groundwater and indications of seasonal high groundwater levels were encountered within the profile pits performed at the depths/elevations indicated in the *Records of Subsurface Exploration*. Groundwater conditions likely will fluctuate seasonally and following periods of precipitation.

Infiltration Testing: A pit-bailing test was conducted within the weathered rock strata encountered at profile pit SPP-2A at a depth of approximately eight fbg. The pit-bailing test was conducted in general accordance with the *Standards for Individual Subsurface Sewage Disposal Systems (N.J.A.C. 7:9A)* and was witnessed by a Township of Franklin Health Department representative. The results of the pit-bailing test indicated a permeability rate (K) of approximately 3.4 inches per hour.

Additionally, a basin flood test was conducted at profile pit SPP-3A and tube permeameter testing was conducted at profile pit SPP-3. The basin flood test was conducted within the weathered rock strata encountered within SPP-3A. The basin flood test was conducted in general accordance with the *Standards for Individual Subsurface Sewage Disposal Systems (N.J.A.C. 7:9A)*. The results of the in-situ testing indicated that basin flood test did not drain the required 12 inches within 24 hours of filling. Therefore, the limiting zone is considered to be a massive rock substratum and a permeability rate cannot be assigned. Detailed in-situ permeability test results are available in Appendix C. The laboratory tube permeameter testing conducted for SPP-3 resulted in a permeability rate of less than 0.2 iph. Individual tube permeameter test results are provided in Appendix B.

5.0 CLOSING

Whitestone appreciates the opportunity to be of service to SAFStor Real Estate Co, LLC and W&A Engineering and trusts that this information will be helpful for evaluating the proposed development of this property. Please contact us at (908) 668-7777 to further discuss these findings.

Sincerely,

WHITESTONE ASSOCIATES, INC.



Mudar Khantamr, P.E.
Project Manager



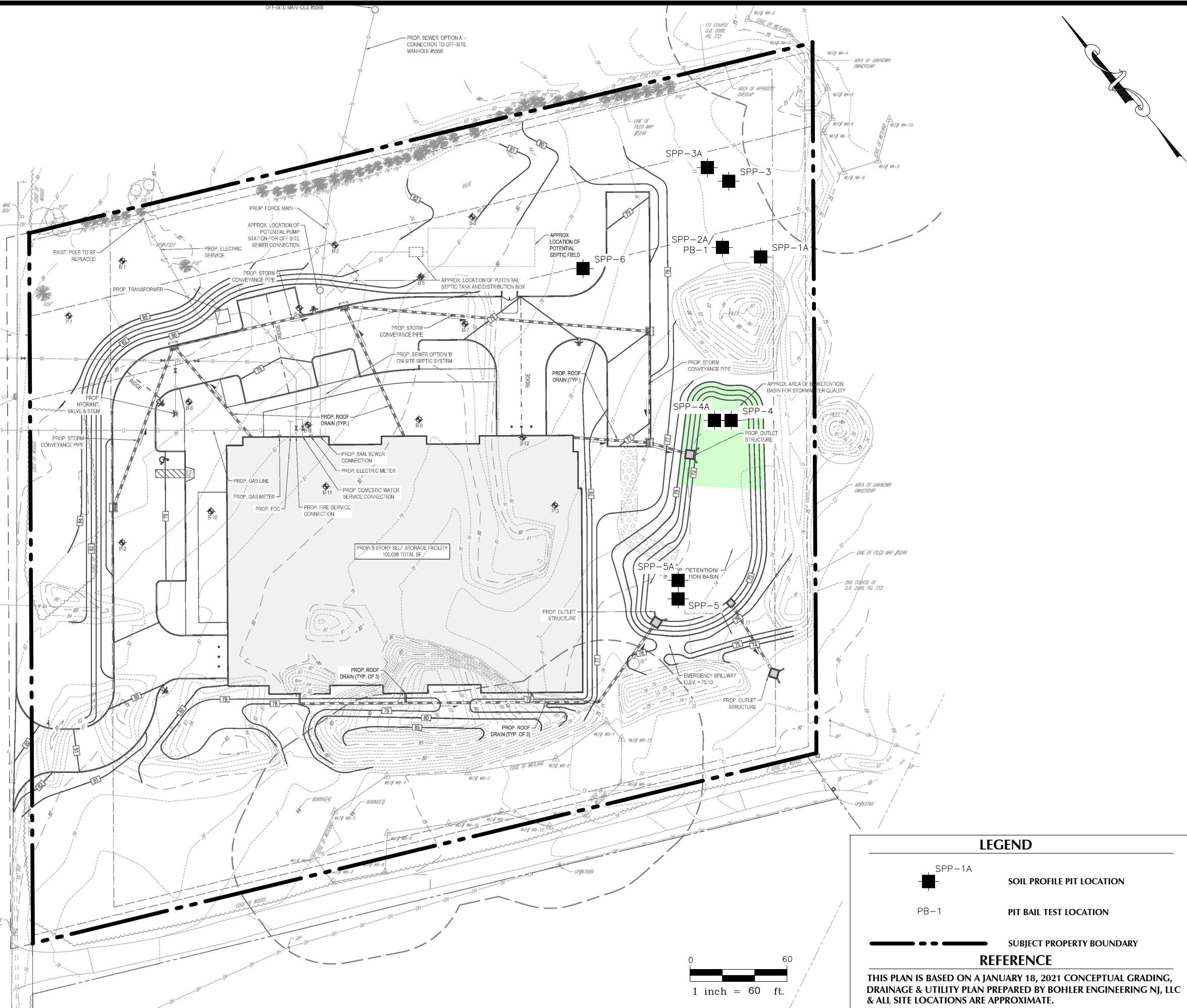
Kevin A. Feath, P.E.
Associate

MK/pwd L:\Job Folders\2021\2117698GJ\Reports and Submittals\17698 SWM&Septic.docx
Enclosures
Copy: Kyle McKenna, P.E., Bohler Engineering NJ, LLC
Laurence W. Keller, P.E., Whitestone Associates, Inc.

FIGURE 1
Test Location Plan

I:\Job_Folders\2021\2117698G\Drawings and Plans\GJ2117698.000_BLP.dwg

ELIZABETH AVENUE
(70' WIDE R.O.W.)
(ASPHALT ROADWAY)
(TWO WAY TRAFFIC)

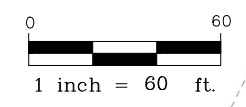


LEGEND

- SPP-1A SOIL PROFILE PIT LOCATION
- PB-1 PIT BAIL TEST LOCATION
- SUBJECT PROPERTY BOUNDARY

REFERENCE

THIS PLAN IS BASED ON A JANUARY 18, 2021 CONCEPTUAL GRADING, DRAINAGE & UTILITY PLAN PREPARED BY BOHLER ENGINEERING NJ, LLC & ALL SITE LOCATIONS ARE APPROXIMATE.



WHITESTONE ASSOCIATES, INC.
Environmental & Geotechnical Engineers & Consultants

30 INDEPENDENCE BOULEVARD, SUITE 250, WARREN, NJ 07059
908.668.7777 WHITESTONEASSOC.COM

DRAWING TITLE:
TEST LOCATION PLAN

CLIENT:
SAFSTOR REAL ESTATE CO, LLC

PROJECT:
PROPOSED SELF-STORAGE FACILITY
471 ELIZABETH AVENUE
FRANKLIN TOWNSHIP, SOMERSET COUNTY, NJ

PROJECT #:
GJ2117698.000

| | |
|---------------------------|---------------------------|
| DESIGNED BY: GR | PROJ. MGR.: KAF |
| DATE: 3/3/21 | FIGURE: 1 |
| SCALE: 1" = 60' | |

APPENDIX A
Records of Subsurface Exploration

RECORD OF SUBSURFACE EXPLORATION

| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | | | | | | | | | | | |
|---|---------------------------------|--|--|-------------------------|--|-------------------------------|--|---------------------|--------------|----------------|-------------|-----------|-------------|
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | | | | | | | | | | | |
| Surface Elevation: ± 77.0 feet | Date Started: 2/8/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2">Water Depth Elevation</th> </tr> <tr> <th>(feet bgs) (feet)</th> <th></th> </tr> <tr> <td>During:</td> <td style="text-align: center;">6.0 71.0 ▼</td> </tr> <tr> <td>At Completion:</td> <td style="text-align: center;">--- --- ▼</td> </tr> <tr> <td>24 Hours:</td> <td style="text-align: center;">--- --- ▼</td> </tr> </table> | | Water Depth Elevation | | (feet bgs) (feet) | | During: | 6.0 71.0 ▼ | At Completion: | --- --- ▼ | 24 Hours: | --- --- ▼ |
| Water Depth Elevation | | | | | | | | | | | | | |
| (feet bgs) (feet) | | | | | | | | | | | | | |
| During: | 6.0 71.0 ▼ | | | | | | | | | | | | |
| At Completion: | --- --- ▼ | | | | | | | | | | | | |
| 24 Hours: | --- --- ▼ | | | | | | | | | | | | |
| Termination Depth: 8.5 feet bgs | Date Completed: 2/8/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2">Estimated Seasonal High</th> </tr> <tr> <th>Groundwater Depth Elevation</th> <th></th> </tr> <tr> <td>(feet bgs) (feet)</td> <td></td> </tr> <tr> <td>At Completion:</td> <td style="text-align: center;">4.0 73.0</td> </tr> </table> | | Estimated Seasonal High | | Groundwater Depth Elevation | | (feet bgs) (feet) | | At Completion: | 4.0 73.0 | | |
| Estimated Seasonal High | | | | | | | | | | | | | |
| Groundwater Depth Elevation | | | | | | | | | | | | | |
| (feet bgs) (feet) | | | | | | | | | | | | | |
| At Completion: | 4.0 73.0 | | | | | | | | | | | | |
| Proposed Location: Septic | Logged By: CN | | | | | | | | | | | | |
| Excavating Method: Test Pit Excavation | Contractor: LNR | | | | | | | | | | | | |
| Test Method: Visual Observation | Rig Type: PC88MR | | | | | | | | | | | | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|---------|----------------|---|--|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 3 | | | 0 - 3 | FILL | 30" Asphalt Millings | Water Seeping in All Sidewalls 2"/10 Minutes |
| 3 - 6 | | | 3 - 6 | RESIDUAL | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Moist to Wet; Friable; No Roots; >15MM Mottling Starting at 4.0 fbg; Clear Boundary | Mottling @ 4.0 fbg to 8.5 fbg Water Sitting on Weathered Rock |
| 6 - 8.5 | | | 6 - 8.5 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling; Clear Boundary | |
| | | | 9.0 | | Soil Profile Pit SPP-1A Terminated at a Depth of 8.5 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| | | | |
|---|---------------------------------|---|---|
| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | |
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | |
| Surface Elevation: ± 77.0 feet | Date Started: 2/6/2021 | Water Depth Elevation (feet bgs) (feet) | |
| Termination Depth: 8.0 feet bgs | Date Completed: 2/6/2021 | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) | |
| Proposed Location: Septic | Logged By: CN | During: 5.5 71.5 | ▼ |
| Excavating Method: Test Pit Excavation | Contractor: LNR | At Completion: --- --- | ▼ |
| Test Method: Visual Observation | Rig Type: PC88MR | 24 Hours: --- --- | ▼ |
| | | At Completion: 4.0 73.0 | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|---------|----------------|--|--|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 2 | | | 0 - 2 | FILL | 24" Asphalt Millings | Water Seeping in All Sidewalls 2"/10 Minutes 0.0 fbg to 5.0 fbg |
| 2 - 5.5 | | | 2 - 5.5 | RESIDUAL | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Moist to Wet; Friable; No Roots; >15MM Mottling at 4.0 fbg; Clear Boundary | Mottling @ 4.0 fbg |
| 5.5 - 8 | | | 5.5 - 8 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; No Mottling; Clear Boundary | Water Sitting on Weathered Rock |
| | | | 8.0 | | Soil Profile Pit SPP-2A Terminated at a Depth of 8.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | SPP-2A Used for Pit Bail Test (PB-1) |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | | | | | | | | | | | |
|---|---------------------------------|--|--|-------------------------|-------------------|------------|------------|--------------------|--------|---------------------------|------|----------------------|-----|
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | | | | | | | | | | | |
| Surface Elevation: ± 77.0 feet | Date Started: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="text-align: left;">Water Depth</th> <th style="text-align: left;">Elevation</th> </tr> <tr> <td style="text-align: center;">(feet bgs)</td> <td style="text-align: center;">(feet)</td> </tr> <tr> <td>During: 4.0</td> <td>73.0</td> </tr> <tr> <td>At Completion: ---</td> <td>---</td> </tr> <tr> <td>24 Hours: ---</td> <td>---</td> </tr> </table> | | Water Depth | Elevation | (feet bgs) | (feet) | During: 4.0 | 73.0 | At Completion: --- | --- | 24 Hours: --- | --- |
| Water Depth | Elevation | | | | | | | | | | | | |
| (feet bgs) | (feet) | | | | | | | | | | | | |
| During: 4.0 | 73.0 | | | | | | | | | | | | |
| At Completion: --- | --- | | | | | | | | | | | | |
| 24 Hours: --- | --- | | | | | | | | | | | | |
| Termination Depth: 6.0 feet bgs | Date Completed: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="text-align: left;">Estimated Seasonal High</th> <th style="text-align: left;">Groundwater Depth</th> <th style="text-align: left;">Elevation</th> </tr> <tr> <td style="text-align: center;">(feet bgs)</td> <td style="text-align: center;">(feet)</td> <td style="text-align: center;">(feet)</td> </tr> <tr> <td>At Completion: 3.8</td> <td>73.2</td> <td></td> </tr> </table> | | Estimated Seasonal High | Groundwater Depth | Elevation | (feet bgs) | (feet) | (feet) | At Completion: 3.8 | 73.2 | | |
| Estimated Seasonal High | Groundwater Depth | | | Elevation | | | | | | | | | |
| (feet bgs) | (feet) | (feet) | | | | | | | | | | | |
| At Completion: 3.8 | 73.2 | | | | | | | | | | | | |
| Proposed Location: Septic | Logged By: CN | | | | | | | | | | | | |
| Excavating Method: Test Pit Excavation | Contractor: LNR | | | | | | | | | | | | |
| Test Method: Visual Observation | Rig Type: PC88MR | | | | | | | | | | | | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|---------|----------------|--|---------------------------------|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 2.5 | | | 0 - 2.5 | FILL | 30" Asphalt Millings | |
| 2.5 - 4 | S-1 | BAG | 2.5 - 4 | RESIDUAL | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Wet; Friable; No Roots; >15MM Mottling at 3.8 fbgs; Clear Boundary | Bag/Tubes Taken @ 3.0 fbgs |
| 4 - 6 | | | 4 - 7 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling; Clear Boundary | Water Sitting on Weathered Rock |
| | | | 6.0 | | Soil Profile Pit SPP-3 Terminated at a Depth of 6.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 7.0 | | | |
| | | | 8.0 | | | |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | | | | | | | | | |
|---|---|--|--|--|---|----------------------|--|----------------------------|--|-----------------------|--|
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | | | | | | | | | |
| Surface Elevation: ± 77.0 feet | Date Started: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="text-align: center;">Water Depth Elevation (feet bgs) (feet)</th> <th style="text-align: center;">Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet)</th> </tr> <tr> <td style="text-align: center;">During: 4.0 73.0 ▼</td> <td></td> </tr> <tr> <td style="text-align: center;">At Completion: --- --- ▼</td> <td></td> </tr> <tr> <td style="text-align: center;">24 Hours: --- --- ▼</td> <td></td> </tr> </table> | | Water Depth Elevation (feet bgs) (feet) | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) | During: 4.0 73.0 ▼ | | At Completion: --- --- ▼ | | 24 Hours: --- --- ▼ | |
| Water Depth Elevation (feet bgs) (feet) | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) | | | | | | | | | | |
| During: 4.0 73.0 ▼ | | | | | | | | | | | |
| At Completion: --- --- ▼ | | | | | | | | | | | |
| 24 Hours: --- --- ▼ | | | | | | | | | | | |
| Termination Depth: 6.0 feet bgs | Date Completed: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="text-align: center;">At Completion: 3.8 73.2</td> </tr> </table> | | At Completion: 3.8 73.2 | | | | | | | |
| At Completion: 3.8 73.2 | | | | | | | | | | | |
| Proposed Location: Septic | Logged By: CN | | | | | | | | | | |
| Excavating Method: Test Pit Excavation | Contractor: LNR | | | | | | | | | | |
| Test Method: Visual Observation | Rig Type: PC88MR | | | | | | | | | | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|---------|----------------|--|---------------------------------|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 2.5 | | | 0 - 2.5 | FILL | 30" Asphalt Millings | |
| 2.5 - 4 | S-1 | BAG | 2.5 - 4 | RESIDUAL | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Wet; Friable; No Roots; >15MM Mottling at 3.8 fbgs; Clear Boundary | Bag/Tubes Taken @ 3.0 fbgs |
| 4 - 6 | | | 4 - 7 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling; Clear Boundary | Water Sitting on Weathered Rock |
| | | | 6.0 | | Soil Profile Pit SPP-3A Terminated at a Depth of 6.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 7.0 | | | |
| | | | 8.0 | | | |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | | | | | | | | | | | |
|---|---------------------------------|--|--|-------------------------|--|-------------------------------|--|---------------------|------------|----------------|-------------|-----------|-------------|
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | | | | | | | | | | | |
| Surface Elevation: ± 75.0 feet | Date Started: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2">Water Depth Elevation</th> </tr> <tr> <th>(feet bgs) (feet)</th> <th></th> </tr> <tr> <td>During:</td> <td>NE --- ▼</td> </tr> <tr> <td>At Completion:</td> <td>--- --- ▼</td> </tr> <tr> <td>24 Hours:</td> <td>--- --- ▼</td> </tr> </table> | | Water Depth Elevation | | (feet bgs) (feet) | | During: | NE --- ▼ | At Completion: | --- --- ▼ | 24 Hours: | --- --- ▼ |
| Water Depth Elevation | | | | | | | | | | | | | |
| (feet bgs) (feet) | | | | | | | | | | | | | |
| During: | NE --- ▼ | | | | | | | | | | | | |
| At Completion: | --- --- ▼ | | | | | | | | | | | | |
| 24 Hours: | --- --- ▼ | | | | | | | | | | | | |
| Termination Depth: 6.0 feet bgs | Date Completed: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2">Estimated Seasonal High</th> </tr> <tr> <th>Groundwater Depth Elevation</th> <th></th> </tr> <tr> <td>(feet bgs) (feet)</td> <td></td> </tr> <tr> <td>At Completion:</td> <td>3.0 72.0</td> </tr> </table> | | Estimated Seasonal High | | Groundwater Depth Elevation | | (feet bgs) (feet) | | At Completion: | 3.0 72.0 | | |
| Estimated Seasonal High | | | | | | | | | | | | | |
| Groundwater Depth Elevation | | | | | | | | | | | | | |
| (feet bgs) (feet) | | | | | | | | | | | | | |
| At Completion: | 3.0 72.0 | | | | | | | | | | | | |
| Proposed Location: Proposed SWM | Logged By: CN | | | | | | | | | | | | |
| Excavating Method: Test Pit Excavation | Contractor: LNR | | | | | | | | | | | | |
| Test Method: Visual Observation | Rig Type: PC88MR | | | | | | | | | | | | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|-------|------------------|--|--|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 1 | | | 0 - 1 | FILL | 12" to 18" Asphalt Millings | |
| 1 - 2 | | | 1 - 2 | TOPSOIL | 6" to 12" Topsoil | |
| 2 - 4 | S-1 | BAG | 2 - 4 | GLACIAL DEPOSITS | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Wet; Friable; Sticky; No Roots; >15MM Mottling at 3.0 fbgs; Clear Boundary | Tubes/Bags Taken @ 2.0 fbgs >15MM Mottling 3.0 fbgs to 6.0 fbgs |
| 4 - 6 | | | 4 - 6 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling | |
| | | | 6.0 | | Soil Profile Pit SPP-4 Terminated at a Depth of 6.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 7.0 | | | |
| | | | 8.0 | | | |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| | | | |
|---|---------------------------------|---|---|
| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | |
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | |
| Surface Elevation: ± 75.0 feet | Date Started: 2/6/2021 | Water Depth Elevation (feet bgs) (feet) | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) |
| Termination Depth: 6.0 feet bgs | Date Completed: 2/6/2021 | | |
| Proposed Location: Proposed SWM | Logged By: CN | During: NE --- ▼ | At Completion: 3.0 72.0 |
| Excavating Method: Test Pit Excavation | Contractor: LNR | At Completion: --- --- ▼ | |
| Test Method: Visual Observation | Rig Type: PC88MR | 24 Hours: --- --- ▼ | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|-------|------------------|--|--|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 1 | | | 0 - 1 | FILL | 12" to 18" Asphalt Millings | |
| 1 - 2 | | | 1 - 2 | TOPSOIL | 6" to 12" Topsoil | |
| 2 - 4 | S-1 | BAG | 2 - 4 | GLACIAL DEPOSITS | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Wet; Friable; Sticky; No Roots; >15MM Mottling at 3.0 fbgs; Clear Boundary | Tubes/Bags Taken @ 2.0 fbgs >15MM Mottling 3.0 fbgs to 6.0 fbgs |
| 4 - 6 | | | 4 - 6 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling | |
| | | | 6.0 | | Soil Profile Pit SPP-4A Terminated at a Depth of 6.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 7.0 | | | |
| | | | 8.0 | | | |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | | | | | | | | | | | | | |
|---|---|--|--|--|---|--|----------------------|--|--|------------------------------|--|--|-------------------------|--|--|
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | | | | | | | | | | | | | |
| Surface Elevation: ± 74.5 feet | Date Started: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="text-align: center;">Water Depth Elevation (feet bgs) (feet)</th> <th colspan="2" style="text-align: center;">Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet)</th> </tr> <tr> <td style="text-align: center;">During: NE --- ▼</td> <td colspan="2"></td> </tr> <tr> <td style="text-align: center;">At Completion: --- --- ▼</td> <td colspan="2"></td> </tr> <tr> <td style="text-align: center;">24 Hours: --- --- ▼</td> <td colspan="2"></td> </tr> </table> | | Water Depth Elevation (feet bgs) (feet) | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) | | During: NE --- ▼ | | | At Completion: --- --- ▼ | | | 24 Hours: --- --- ▼ | | |
| Water Depth Elevation (feet bgs) (feet) | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) | | | | | | | | | | | | | | |
| During: NE --- ▼ | | | | | | | | | | | | | | | |
| At Completion: --- --- ▼ | | | | | | | | | | | | | | | |
| 24 Hours: --- --- ▼ | | | | | | | | | | | | | | | |
| Termination Depth: 5.0 feet bgs | Date Completed: 2/6/2021 | At Completion: 2.5 72.0 | | | | | | | | | | | | | |
| Proposed Location: SWM | Logged By: CN | | | | | | | | | | | | | | |
| Excavating Method: Test Pit Excavation | Contractor: LNR | | | | | | | | | | | | | | |
| Test Method: Visual Observation | Rig Type: PC88MR | | | | | | | | | | | | | | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|---------|----------------|--|---|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 1.5 | | | 0 - 1.5 | FILL | 18" Asphalt Millings | |
| 1.5 - 3 | S-1 | BAG | 1.5 - 3 | RESIDUAL | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Moist; Friable; Sticky; No Roots; >15MM Mottling @ 2.5 fbg; Clear Boundary | Tubes/Bag Taken @ 2.0 fbg Mottling from 2.5 fbg to 5.0 fbg |
| 3 - 5 | | | 3 - 5 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling | |
| | | | 5.0 | | Soil Profile Pit SPP-5 Terminated at a Depth of 5.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 6.0 | | | |
| | | | 7.0 | | | |
| | | | 8.0 | | | |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | | | | | | | | | | | | | |
|---|---|--|--|--|---|--|----------------------|--|--|------------------------------|--|--|-------------------------|--|--|
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | | | | | | | | | | | | | |
| Surface Elevation: ± 74.5 feet | Date Started: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="text-align: center;">Water Depth Elevation (feet bgs) (feet)</th> <th colspan="2" style="text-align: center;">Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet)</th> </tr> <tr> <td style="text-align: center;">During: NE --- ▼</td> <td colspan="2"></td> </tr> <tr> <td style="text-align: center;">At Completion: --- --- ▼</td> <td colspan="2"></td> </tr> <tr> <td style="text-align: center;">24 Hours: --- --- ▼</td> <td colspan="2"></td> </tr> </table> | | Water Depth Elevation (feet bgs) (feet) | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) | | During: NE --- ▼ | | | At Completion: --- --- ▼ | | | 24 Hours: --- --- ▼ | | |
| Water Depth Elevation (feet bgs) (feet) | Estimated Seasonal High Groundwater Depth Elevation (feet bgs) (feet) | | | | | | | | | | | | | | |
| During: NE --- ▼ | | | | | | | | | | | | | | | |
| At Completion: --- --- ▼ | | | | | | | | | | | | | | | |
| 24 Hours: --- --- ▼ | | | | | | | | | | | | | | | |
| Termination Depth: 5.0 feet bgs | Date Completed: 2/6/2021 | At Completion: 2.5 72.0 | | | | | | | | | | | | | |
| Proposed Location: SWM | Logged By: CN | | | | | | | | | | | | | | |
| Excavating Method: Test Pit Excavation | Contractor: LNR | | | | | | | | | | | | | | |
| Test Method: Visual Observation | Rig Type: PC88MR | | | | | | | | | | | | | | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|---------|-------------------|--|---|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 1.5 | | | 0 - 1.5 | FILL | 18" Asphalt Millings | |
| 1.5 - 3 | S-1 | BAG | 1.5 - 3 | RESIDUAL | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Moist; Friable; Sticky; No Roots; >15MM Mottling @ 2.5 fbg; Clear Boundary | Tubes/Bag Taken @ 2.0 fbg Mottling from 2.5 fbg to 5.0 fbg |
| 3 - 5 | | | 3 - 5 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling | |
| | | | 5.0 | | Soil Profile Pit SPP-5A Terminated at a Depth of 5.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 6.0 | | | |
| | | | 7.0 | | | |
| | | | 8.0 | | | |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

RECORD OF SUBSURFACE EXPLORATION

| Project: Proposed Self-Storage Facility | | WAI Project No.: GJ2117698.000 | | | | | | | | | | | |
|---|---------------------------------|---|--|-------------------------|--|-------------------------------|--|---------------------------|---|--------------------------|---|---------------------|---|
| Location: 471 Elizabeth Avenue; Franklin Township, Somerset County, New Jersey | | Client: SAFStor Real Estate Co, LLC | | | | | | | | | | | |
| Surface Elevation: ± 78.5 feet | Date Started: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2">Water Depth Elevation</th> </tr> <tr> <th>(feet bgs) (feet)</th> <th></th> </tr> <tr> <td>During: 3.0 75.5</td> <td style="text-align: right;">▼</td> </tr> <tr> <td>At Completion: --- ---</td> <td style="text-align: right;">▼</td> </tr> <tr> <td>24 Hours: --- ---</td> <td style="text-align: right;">▼</td> </tr> </table> | | Water Depth Elevation | | (feet bgs) (feet) | | During: 3.0 75.5 | ▼ | At Completion: --- --- | ▼ | 24 Hours: --- --- | ▼ |
| Water Depth Elevation | | | | | | | | | | | | | |
| (feet bgs) (feet) | | | | | | | | | | | | | |
| During: 3.0 75.5 | ▼ | | | | | | | | | | | | |
| At Completion: --- --- | ▼ | | | | | | | | | | | | |
| 24 Hours: --- --- | ▼ | | | | | | | | | | | | |
| Termination Depth: 5.0 feet bgs | Date Completed: 2/6/2021 | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2">Estimated Seasonal High</th> </tr> <tr> <th>Groundwater Depth Elevation</th> <th></th> </tr> <tr> <td>At Completion: 3.0 75.5</td> <td></td> </tr> </table> | | Estimated Seasonal High | | Groundwater Depth Elevation | | At Completion: 3.0 75.5 | | | | | |
| Estimated Seasonal High | | | | | | | | | | | | | |
| Groundwater Depth Elevation | | | | | | | | | | | | | |
| At Completion: 3.0 75.5 | | | | | | | | | | | | | |
| Proposed Location: Septic | Logged By: CN | | | | | | | | | | | | |
| Excavating Method: Test Pit Excavation | Contractor: LNR | | | | | | | | | | | | |
| Test Method: Visual Observation | Rig Type: PC88MR | | | | | | | | | | | | |

| SAMPLE INFORMATION | | | DEPTH | HORIZON | DESCRIPTION OF MATERIALS (Classification) | REMARKS |
|--------------------|--------|------|-----------|----------------|---|------------------------------------|
| Depth (feet) | Number | Type | feet | | | |
| | | | 0.0 | | | |
| 0 - 1.5 | | | 0 - 1.5 | FILL | 18" Asphalt Millings | |
| 1.5 - 2.2 | | | 1.5 - 2.2 | TOPSOIL | 8" Topsoil | |
| 2.2 - 3 | S-1 | BAG | 2.2 - 3 | RESIDUAL | Reddish-Brown (5YR 5/4) CLAY LOAM; 10% Gravel; Moderate, Medium Blocky Structure; Wet; Friable; No Roots; No Mottling; Clear Boundary | Tubes/Bags Taken @ 2.5 fbgs |
| 3 - 5 | | | 3 - 5 | WEATHERED ROCK | Dark Reddish-Brown (5YR 4/3) Fractured WEATHERED SHALE; Strong, Coarse Structure; Moist; Very Hard; No Roots; Mottling | Mottling from 3.0 fbgs to 5.0 fbgs |
| | | | 5.0 | | Soil Profile Pit SPP-6 Terminated at a Depth of 5.0 Feet Below Ground Surface Due to Refusal on Weathered Rock/Bedrock | |
| | | | 6.0 | | | |
| | | | 7.0 | | | |
| | | | 8.0 | | | |
| | | | 9.0 | | | |
| | | | 10.0 | | | |
| | | | 11.0 | | | |
| | | | 12.0 | | | |
| | | | 13.0 | | | |
| | | | 14.0 | | | |
| | | | 15.0 | | | |

APPENDIX B

Laboratory Test Results

Tube Permeameter Test Data

Job Number: GJ2117698.000
Project: Proposed Self-Storage Facility
Client: Safstor Real Estate Co, LLC
Lab Tech: T. Jovanov

Sample ID: _____ **Profile Pit No.:** SPP-3 **Sample No.:** T-1 **Depth:** 3.0'

COUNTY/MUNICIPALITY Franklin Twp, Somerset Co BLOCK _____ LOT _____

1. Test Number 1 Replicate (letter) A Date Collected 2/6/2021

2. Material Tested: _____ Fill _____ Test in Native Soil

3. Type of Sample: X Undisturbed _____ Disturbed

4. Sample Dimensions: Inside Radius of Sample Tube, R, in cm 1.91
 Length of Sample, L, in inches 3.50

5. Bulk Density Determination (Disturbed Samples Only): N/A

6. Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams 0.00

Wt. of Tube Containing Sample _____
 Wt. of Empty Tube _____

7. Sample Volume (L x 2.54 cm./inch x 3.14R²), cc. 101.30

8. Bulk Density (Sample Wt./Sample Volume), grams/cc. 0 > 1.2

9. Standpipe Used: X No _____ Yes, Indicate Internal Radius, cm. N/A

10. Height of Water Level Above Rim of Test Basin, in inches:

At the Beginning of Each Test Interval, H1 5.00
 At the End of Each Test Interval, H2 4.75

11. Rate of Water Level Drop (Add additional lines if needed):

| Time, Start of Test Interval, T1 | Time End of Test Interval T2 | Length of Test Interval, T, Minutes |
|----------------------------------|------------------------------|-------------------------------------|
| | | 92.00 |
| | | 96.00 |
| | | 92.00 |
| | | |

12. Calculation of Permeability: $K, (in/hr) = 60 \text{ min/hr} \times r^2/R^2 \times L(in)/T(\text{min}) \times \ln (H1/H2)$ T= 93.33

K (in/hr) = 0.12 **Classification:** **K0**

13. Defects in the Sample (Check appropriate items):

_____ None
 _____ Soil/Tube Contact _____ Large Gravel _____ Large Roots
 _____ Dry Soil _____ Smearing _____ Compaction
 _____ Other - Specify _____

Tube Permeameter Test Data

Job Number: GJ2117698.000
Project: Proposed Self-Storage Facility
Client: Safstor Real Estate Co, LLC
Lab Tech: T. Jovanov

Sample ID: _____ **Profile Pit No.:** SPP-3 **Sample No.:** T-1 **Depth:** 3.0'

COUNTY/MUNICIPALITY Franklin Twp, Somerset Co **BLOCK** _____ **LOT** _____

1. **Test Number** 1 **Replicate (letter)** B **Date Collected** 2/6/2021

2. **Material Tested:** _____ **Fill** _____ **Test in Native Soil** _____

3. **Type of Sample:** X **Undisturbed** _____ **Disturbed** _____

4. **Sample Dimensions:** **Inside Radius of Sample Tube, R, in cm** 1.91
Length of Sample, L, in inches 3.25

5. **Bulk Density Determination (Disturbed Samples Only):** N/A

6. **Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams** 0.00

Wt. of Tube Containing Sample _____
Wt. of Empty Tube _____

7. **Sample Volume (L x 2.54 cm./inch x 3.14R²), cc.** 94.07

8. **Bulk Density (Sample Wt./Sample Volume), grams/cc.** 0 > 1.2

9. **Standpipe Used:** X **No** _____ **Yes, Indicate Internal Radius, cm.** N/A

10. **Height of Water Level Above Rim of Test Basin, in inches:**
 At the Beginning of Each Test Interval, H1 5.00
 At the End of Each Test Interval, H2 4.99

11. **Rate of Water Level Drop (Add additional lines if needed):**

| Time, Start of Test Interval, T1 | Time End of Test Interval T2 | Length of Test Interval, T, Minutes |
|----------------------------------|------------------------------|-------------------------------------|
| | | 240.00 |
| | | |
| | | |
| | | |

12. **Calculation of Permeability:** $K, (in/hr) = 60 \text{ min/hr} \times r^2/R^2 \times L(in)/T(\text{min}) \times \ln (H1/H2)$ **T=** 240.00

K (in/hr) = 0.00 **Classification:** **K0**

13. **Defects in the Sample (Check appropriate items):**
 _____ **None**
 _____ **Soil/Tube Contact** _____ **Large Gravel** _____ **Large Roots**
 _____ **Dry Soil** _____ **Smearing** _____ **Compaction**
 _____ **Other - Specify** _____

Tube Permeameter Test Data

Job Number: GJ2117698.000
Project: Proposed Self-Storage Facility
Client: Safstor Real Estate Co, LLC
Lab Tech: T. Jovanov

Sample ID: _____ **Profile Pit No.:** SPP-4 **Sample No.:** T-1 **Depth:** 2.0'

COUNTY/MUNICIPALITY Franklin Twp, Somerset Co BLOCK _____ LOT _____

1. Test Number 1 Replicate (letter) A Date Collected 2/6/2021

2. Material Tested: _____ Fill _____ Test in Native Soil

3. Type of Sample: X Undisturbed _____ Disturbed

4. Sample Dimensions: Inside Radius of Sample Tube, R, in cm 1.91
 Length of Sample, L, in inches 3.50

5. Bulk Density Determination (Disturbed Samples Only): N/A

6. Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams 0.00

Wt. of Tube Containing Sample _____
 Wt. of Empty Tube _____

7. Sample Volume (L x 2.54 cm./inch x 3.14R²), cc. 101.30

8. Bulk Density (Sample Wt./Sample Volume), grams/cc. 0 > 1.2

9. Standpipe Used: X No _____ Yes, Indicate Internal Radius, cm. N/A

10. Height of Water Level Above Rim of Test Basin, in inches:

At the Beginning of Each Test Interval, H1 5.00
 At the End of Each Test Interval, H2 4.75

11. Rate of Water Level Drop (Add additional lines if needed):

| Time, Start of Test Interval, T1 | Time End of Test Interval T2 | Length of Test Interval, T, Minutes |
|----------------------------------|------------------------------|-------------------------------------|
| | | 72.00 |
| | | 73.00 |
| | | 69.00 |
| | | |

12. Calculation of Permeability: $K, (in/hr) = 60 \text{ min/hr} \times r^2/R^2 \times L(in)/T(\text{min}) \times \ln (H1/H2)$ T= 71.33

K (in/hr) = 0.15 **Classification:** **K0**

13. Defects in the Sample (Check appropriate items):

_____ None
 _____ Soil/Tube Contact _____ Large Gravel _____ Large Roots
 _____ Dry Soil _____ Smearing _____ Compaction
 _____ Other - Specify _____

Tube Permeameter Test Data

Job Number: GJ2117698.000
Project: Proposed Self-Storage Facility
Client: Safstor Real Estate Co, LLC
Lab Tech: T. Jovanov

Sample ID: _____ **Profile Pit No.:** SPP-4 **Sample No.:** T-1 **Depth:** 2.0'

COUNTY/MUNICIPALITY Franklin Twp, Somerset Co **BLOCK** _____ **LOT** _____

1. **Test Number** 1 **Replicate (letter)** B **Date Collected** 2/6/2021

2. **Material Tested:** _____ **Fill** _____ **Test in Native Soil** _____

3. **Type of Sample:** X **Undisturbed** _____ **Disturbed** _____

4. **Sample Dimensions:** **Inside Radius of Sample Tube, R, in cm** 1.91
Length of Sample, L, in inches 3.25

5. **Bulk Density Determination (Disturbed Samples Only):** N/A

6. **Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams** 0.00

Wt. of Tube Containing Sample _____
Wt. of Empty Tube _____

7. **Sample Volume (L x 2.54 cm./inch x 3.14R²), cc.** 94.07

8. **Bulk Density (Sample Wt./Sample Volume), grams/cc.** 0 > 1.2

9. **Standpipe Used:** X **No** _____ **Yes, Indicate Internal Radius, cm.** N/A

10. **Height of Water Level Above Rim of Test Basin, in inches:**

At the Beginning of Each Test Interval, H1 4.50
At the End of Each Test Interval, H2 4.49

11. **Rate of Water Level Drop (Add additional lines if needed):**

| Time, Start of Test Interval, T1 | Time End of Test Interval T2 | Length of Test Interval, T, Minutes |
|----------------------------------|------------------------------|-------------------------------------|
| | | 240.00 |
| | | |
| | | |
| | | |

12. **Calculation of Permeability:** $K, (in/hr) = 60 \text{ min/hr} \times r^2/R^2 \times L(in)/T(\text{min}) \times \ln (H1/H2)$ **T=** 240.00

K (in/hr) = 0.00 **Classification:** **K0**

13. **Defects in the Sample (Check appropriate items):**

_____ **None**
 _____ **Soil/Tube Contact** _____ **Large Gravel** _____ **Large Roots**
 _____ **Dry Soil** _____ **Smearing** _____ **Compaction**
 _____ **Other - Specify** _____

Tube Permeameter Test Data

Job Number: GJ2117698.000
Project: Proposed Self-Storage Facility
Client: Safstor Real Estate Co, LLC
Lab Tech: T. Jovanov

Sample ID: _____ **Profile Pit No.:** SPP-5 **Sample No.:** T-1 **Depth:** 3.0'

COUNTY/MUNICIPALITY Franklin Twp, Somerset Co **BLOCK** _____ **LOT** _____

1. **Test Number** 1 **Replicate (letter)** A **Date Collected** 2/6/2021

2. **Material Tested:** _____ **Fill** _____ **Test in Native Soil** _____

3. **Type of Sample:** X **Undisturbed** _____ **Disturbed** _____

4. **Sample Dimensions:** **Inside Radius of Sample Tube, R, in cm** 1.91
Length of Sample, L, in inches 3.50

5. **Bulk Density Determination (Disturbed Samples Only):** N/A

6. **Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams** 0.00

Wt. of Tube Containing Sample _____
Wt. of Empty Tube _____

7. **Sample Volume (L x 2.54 cm./inch x 3.14R²), cc.** 101.30

8. **Bulk Density (Sample Wt./Sample Volume), grams/cc.** 0 > 1.2

9. **Standpipe Used:** X **No** _____ **Yes, Indicate Internal Radius, cm.** N/A

10. **Height of Water Level Above Rim of Test Basin, in inches:**

At the Beginning of Each Test Interval, H1 5.00
At the End of Each Test Interval, H2 4.99

11. **Rate of Water Level Drop (Add additional lines if needed):**

| Time, Start of Test Interval, T1 | Time End of Test Interval T2 | Length of Test Interval, T, Minutes |
|----------------------------------|------------------------------|-------------------------------------|
| | | 240.00 |
| | | |
| | | |
| | | |

12. **Calculation of Permeability:** $K, (in/hr) = 60 \text{ min/hr} \times r^2/R^2 \times L(in)/T(\text{min}) \times \ln (H1/H2)$ **T=** 240.00

K (in/hr) = 0.00 **Classification:** **K0**

13. **Defects in the Sample (Check appropriate items):**

- _____ **None**
 _____ **Soil/Tube Contact** _____ **Large Gravel** _____ **Large Roots**
 _____ **Dry Soil** _____ **Smearing** _____ **Compaction**
 _____ **Other - Specify** _____

Tube Permeameter Test Data

Job Number: GJ2117698.000
Project: Proposed Self-Storage Facility
Client: Safstor Real Estate Co, LLC
Lab Tech: T. Jovanov

Sample ID: _____ **Profile Pit No.:** SPP-5 **Sample No.:** T-1 **Depth:** 3.0'

COUNTY/MUNICIPALITY Franklin Twp, Somerset Co **BLOCK** _____ **LOT** _____

1. **Test Number** 1 **Replicate (letter)** B **Date Collected** 2/6/2021

2. **Material Tested:** _____ **Fill** _____ **Test in Native Soil** _____

3. **Type of Sample:** X **Undisturbed** _____ **Disturbed** _____

4. **Sample Dimensions:**
 Inside Radius of Sample Tube, R, in cm 1.91
 Length of Sample, L, in inches 2.25

5. **Bulk Density Determination (Disturbed Samples Only):** N/A

6. **Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams** 0.00

Wt. of Tube Containing Sample _____
Wt. of Empty Tube _____

7. **Sample Volume (L x 2.54 cm./inch x 3.14R²), cc.** 65.12

8. **Bulk Density (Sample Wt./Sample Volume), grams/cc.** 0 > 1.2

9. **Standpipe Used:** X **No** _____ **Yes, Indicate Internal Radius, cm.** N/A

10. **Height of Water Level Above Rim of Test Basin, in inches:**

At the Beginning of Each Test Interval, H1 5.00
 At the End of Each Test Interval, H2 4.99

11. **Rate of Water Level Drop (Add additional lines if needed):**

| Time, Start of Test Interval, T1 | Time End of Test Interval T2 | Length of Test Interval, T, Minutes |
|----------------------------------|------------------------------|-------------------------------------|
| | | 240.00 |
| | | |
| | | |
| | | |

12. **Calculation of Permeability:** $K, (in/hr) = 60 \text{ min/hr} \times r^2/R^2 \times L(in)/T(\text{min}) \times \ln (H1/H2)$ **T=** 240.00

K (in/hr) = 0.00 **Classification:** **K0**

13. **Defects in the Sample (Check appropriate items):**

_____ **None**
 _____ **Soil/Tube Contact** _____ **Large Gravel** _____ **Large Roots**
 _____ **Dry Soil** _____ **Smearing** _____ **Compaction**
 _____ **Other - Specify** _____

APPENDIX C
Basin Flood Test Data



BASIN FLOOD TEST DATA

Client: SAFStor Real Estate Co, LLC
Project: Proposed Self-Storage Facility
Location: 471 Elizabeth Ave., Franklin Twp., NJ
File No. GJ2117698.000
Surf. Elev. ± 77.0

Basin No.: SPP-3A
Date: 2/8/21 - 2/10/21
Weather: Overcast, Light Snow, 20-35°F
Field Engineer: C. Naugle
Test Depth/Elev.: 5.0 72.0

| Reading No. | Date | Time | Water Level Reading | | Water Level Fall (Inches) | Time Interval (Hours) | Rate of Flow (Inches/Hour) |
|-------------|----------|----------|---------------------|----------------------|---------------------------|-----------------------|----------------------------|
| | | | Depth (inches) | Water Surface (IBGS) | | | |
| 1 | 2/8/2021 | 1:15 PM | 12.0 | 42.0 | --- | --- | --- |
| 2 | 2/8/2021 | 3:15 PM | 13.0 | 41.0 | 1.0 | 2.0 | --- |
| 3 | 2/9/2021 | 8:15 AM | 14.0 | 40.0 | 2.0 | 19.0 | --- |
| 4 | 2/9/2021 | 10:15 AM | 14.0 | 40.0 | 2.0 | 21.0 | --- |
| 5 | 2/9/2021 | 12:15 PM | 15.0 | 39.0 | 3.0 | 23.0 | --- |
| 6 | 2/9/2021 | 1:15 PM | 15.0 | 39.0 | 3.0 | 24.0 | --- |
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BFT: basin flood test
 IBGS: inches below ground surface



BASIN FLOOD TEST DATA

Client: SAFStor Real Estate Co, LLC
Project: Proposed Self-Storage Facility
Location: 471 Elizabeth Ave., Franklin Twp., NJ
File No. GJ2117698.000
Surf. Elev. ± 75.0

Basin No.: SPP-4A
Date: 2/8/21 - 2/10/21
Weather: Overcast, Light Snow, 20-35°F
Field Engineer: C. Naugle
Test Depth/Elev.: 4.0 71.0

| Reading No. | Date | Time | Water Level Reading | | Water Level Fall (Inches) | Time Interval (Hours) | Rate of Flow (Inches/Hour) |
|-------------|----------|----------|---------------------|----------------------|---------------------------|-----------------------|----------------------------|
| | | | Depth (inches) | Water Surface (IBGS) | | | |
| 1 | 2/8/2021 | 1:15 PM | 12.0 | 32.0 | --- | --- | --- |
| 2 | 2/8/2021 | 3:15 PM | 12.0 | 32.0 | 0.0 | 2.0 | --- |
| 3 | 2/9/2021 | 8:15 AM | 15.5 | 28.5 | 3.5 | 19.0 | --- |
| 4 | 2/9/2021 | 10:15 AM | 15.5 | 28.5 | 3.5 | 21.0 | --- |
| 5 | 2/9/2021 | 12:15 PM | 15.5 | 28.5 | 3.5 | 23.0 | --- |
| 6 | 2/9/2021 | 1:15 PM | 15.5 | 28.5 | 3.5 | 24.0 | --- |
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BFT: basin flood test
 IBGS: inches below ground surface



BASIN FLOOD TEST DATA

Client: SAFStor Real Estate Co, LLC
Project: Proposed Self-Storage Facility
Location: 471 Elizabeth Ave., Franklin Twp., NJ
File No. GJ2117698.000
Surf. Elev. ± 75.0

Basin No.: SPP-5A
Date: 2/8/21 - 2/10/21
Weather: Overcast, Light Snow, 20-35°F
Field Engineer: C. Naugle
Test Depth/Elev.: 4.0 71.0

| Reading No. | Date | Time | Water Level Reading | | Water Level Fall (Inches) | Time Interval (Hours) | Rate of Flow (Inches/Hour) |
|-------------|----------|----------|---------------------|----------------------|---------------------------|-----------------------|----------------------------|
| | | | Depth (inches) | Water Surface (IBGS) | | | |
| 1 | 2/8/2021 | 1:15 PM | 12.0 | 35.0 | --- | --- | --- |
| 2 | 2/8/2021 | 3:15 PM | 12.0 | 35.0 | 0.0 | 2.0 | --- |
| 3 | 2/9/2021 | 8:15 AM | 17.0 | 30.0 | 5.0 | 19.0 | --- |
| 4 | 2/9/2021 | 10:15 AM | 17.0 | 30.0 | 5.0 | 21.0 | --- |
| 5 | 2/9/2021 | 12:15 PM | 17.5 | 29.5 | 5.5 | 23.0 | --- |
| 6 | 2/9/2021 | 1:15 PM | 18.0 | 29.0 | 6.0 | 24.0 | --- |
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BFT: basin flood test
 IBGS: inches below ground surface

APPENDIX D
Supplemental Information
(USCS, Terms & Symbols)



UNIFIED SOIL CLASSIFICATION SYSTEM

SOIL CLASSIFICATION CHART

| MAJOR DIVISIONS | | | LETTER SYMBOL | TYPICAL DESCRIPTIONS |
|---|---|--|---------------|--|
| COARSE GRAINED SOILS | GRAVEL AND GRAVELLY SOILS | CLEAN GRAVELS (LITTLE OR NO FINES) | GW | WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES |
| | | GRAVELS WITH FINES (APPRECIABLE AMOUNT OF FINES) | GP | POORLY-GRADED GRAVELS, GRAVEL-SAND MIXTURES, LITTLE OR NO FINES |
| | SAND AND SANDY SOILS | CLEAN SAND (LITTLE OR NO FINES) | GM | SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES |
| | | SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES) | GC | CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES |
| MORE THAN 50% OF MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE | MORE THAN 50% OF COARSE FRACTION <u>RETAINED</u> ON NO. 4 SIEVE | CLEAN SAND (LITTLE OR NO FINES) | SW | WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES |
| | | SANDS WITH FINES (APPRECIABLE AMOUNT OF FINES) | SP | POORLY-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES |
| FINE GRAINED SOILS | SILTS AND CLAYS | LIQUID LIMITS <u>LESS</u> THAN 50 | SM | SILTY SANDS, SAND-SILT MIXTURES |
| | | | SC | CLAYEY SANDS, SAND-CLAY MIXTURES |
| MORE THAN 50% OF MATERIAL IS <u>SMALLER</u> THAN NO. 200 SIEVE SIZE | SILTS AND CLAYS | LIQUID LIMITS <u>GREATER</u> THAN 50 | ML | INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY |
| | | | CL | INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS |
| HIGHLY ORGANIC SOILS | SILTS AND CLAYS | LIQUID LIMITS <u>GREATER</u> THAN 50 | OL | ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY |
| | | | MH | INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS |
| HIGHLY ORGANIC SOILS | SILTS AND CLAYS | LIQUID LIMITS <u>GREATER</u> THAN 50 | CH | INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS |
| | | | OH | ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS |
| HIGHLY ORGANIC SOILS | | | PT | PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS |

NOTE: DUAL SYMBOLS ARE USED TO INDICATE BORDERLINE SOIL CLASSIFICATIONS FOR SAMPLES WITH 5% TO 12% FINES

GRADATION*

% FINER BY WEIGHT

TRACE..... 1% TO 10%
LITTLE..... 10% TO 20%
SOME..... 20% TO 35%
AND..... 35% TO 50%

COMPACTNESS*
Sand and/or Gravel

RELATIVE DENSITY

LOOSE..... 0% TO 40%
MEDIUM DENSE.... 40% TO 70%
DENSE..... 70% TO 90%
VERY DENSE..... 90% TO 100%

CONSISTENCY*
Clay and/or Silt

RANGE OF SHEARING STRENGTH IN POUNDS PER SQUARE FOOT

VERY SOFT..... LESS THAN 250
SOFT..... 250 TO 500
MEDIUM..... 500 TO 1000
STIFF..... 1000 TO 2000
VERY STIFF..... 2000 TO 4000
HARD..... GREATER THAN 4000

* VALUES ARE FROM LABORATORY OR FIELD TEST DATA, WHERE APPLICABLE. WHEN NO TESTING WAS PERFORMED, VALUES ARE ESTIMATED.

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Other Office Locations:

CHALFONT, PA
215.712.2700

SOUTHBOROUGH, MA
508.485.0755

ROCKY HILL, CT
860.726.7889

WALL, NJ
732.592.2101

PHILADELPHIA, PA
215.848.2323

GEOTECHNICAL TERMS AND SYMBOLS

SAMPLE IDENTIFICATION

The Unified Soil Classification System is used to identify the soil unless otherwise noted.

SOIL PROPERTY SYMBOLS

- N: Standard Penetration Value: Blows per ft. of a 140 lb. hammer falling 30" on a 2" O.D. split-spoon.
 Qu: Unconfined compressive strength, TSF.
 Qp: Penetrometer value, unconfined compressive strength, TSF.
 Mc: Moisture content, %.
 LL: Liquid limit, %.
 PI: Plasticity index, %.
 δd: Natural dry density, PCF.
 ▽: Apparent groundwater level at time noted after completion of boring.

DRILLING AND SAMPLING SYMBOLS

- NE: Not Encountered (Groundwater was not encountered).
 SS: Split-Spoon - 1 3/8" I.D., 2" O.D., except where noted.
 ST: Shelby Tube - 3" O.D., except where noted.
 AU: Auger Sample.
 OB: Diamond Bit.
 CB: Carbide Bit
 WS: Washed Sample.

RELATIVE DENSITY AND CONSISTENCY CLASSIFICATION

| <u>Term (Non-Cohesive Soils)</u> | <u>Standard Penetration Resistance</u> |
|----------------------------------|--|
| Very Loose | 0-4 |
| Loose | 4-10 |
| Medium Dense | 10-30 |
| Dense | 30-50 |
| Very Dense | Over 50 |

| <u>Term (Cohesive Soils)</u> | <u>Qu (TSF)</u> |
|------------------------------|-----------------|
| Very Soft | 0 - 0.25 |
| Soft | 0.25 - 0.50 |
| Firm (Medium) | 0.50 - 1.00 |
| Stiff | 1.00 - 2.00 |
| Very Stiff | 2.00 - 4.00 |
| Hard | 4.00+ |

PARTICLE SIZE

| | | | | | |
|----------|-------------|-------------|---------------|------|-----------------|
| Boulders | 8 in.+ | Coarse Sand | 5mm-0.6mm | Silt | 0.074mm-0.005mm |
| Cobbles | 8 in.-3 in. | Medium Sand | 0.6mm-0.2mm | Clay | -0.005mm |
| Gravel | 3 in.-5mm | Fine Sand | 0.2mm-0.074mm | | |

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Other Office Locations:

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215.712.2700

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ROCKY HILL, CT
860.726.7889

WALL, NJ
732.592.2101

PHILADELPHIA, PA
215.848.2323

C. MAPS

- ◆ **Aerial Map**
- ◆ **Soil Map**
- ◆ **USGS**
- ◆ **HUC14 Location Map**
- ◆ **Flood Map**
- ◆ **Drainage Area Maps**
 - **Existing Drainage Area Map**
 - **Proposed Drainage Area Map**
 - **Inlet Drainage Area Map**



Aerial Map

Source: NearMaps

Date Access: 05/17/2021

SafStor Real Estate CO, LLC

471 Elizabeth Avenue
Block 507.14; Lot 65.01

Township of Franklin, Somerset County, New Jersey

BENJ# J200933

Prepared by: CR

Date: 4/13/2021

Checked by: KM

Scale: NTS

BOHLER //



| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|---------------------------------------|--------|--------------|----------------|
| PenB | Penn silt loam, 2 to 6 percent slopes | C | 4.8 | 100.0% |
| Totals for Area of Interest | | | 4.8 | 100.0% |

Soils Map

Source: NRCS Web Soil Survey, 2012

Date Access: 05/17/2021

SafStor Real Estate CO, LLC

471 Elizabeth Avenue
Block 507.14; Lot 65.01

Township of Franklin, Somerset County, New Jersey

BENJ# J200933

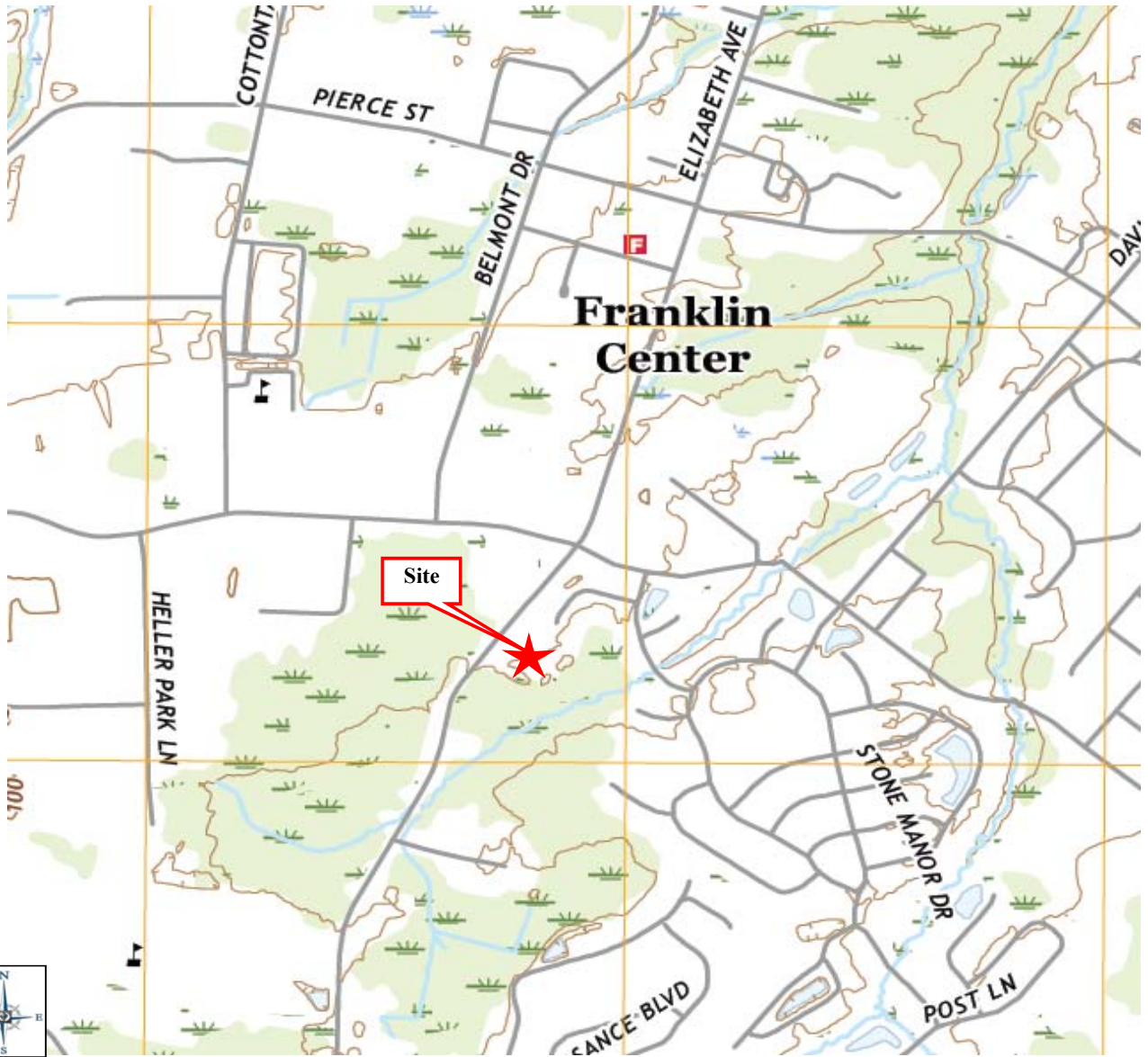
Prepared by: CR

Date: 4/13/2021

Checked by: KM

Scale: NTS

BOHLER //



USGS Map
479,828-ft. E; 619,071-ft. N
Bound Brook Quadrangle

Source: USGS, 2019

Date Access: 05/17/2021

SafStor Real Estate CO, LLC

471 Elizabeth Avenue
 Block 507.14; Lot 65.01

Township of Franklin, Somerset County, New Jersey

BENJ# J200933

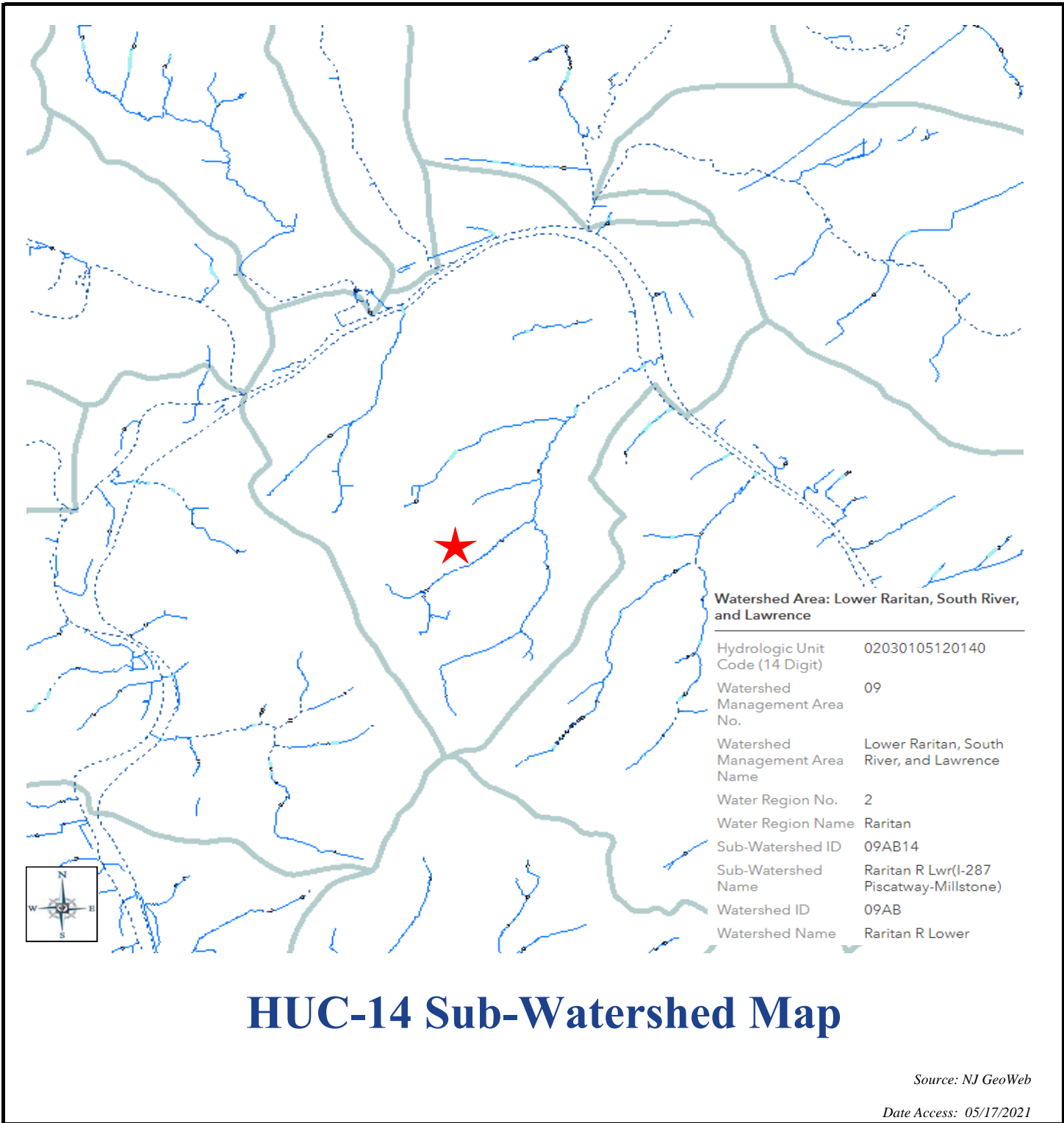
Prepared by: CR

Date: 4/13/2021

Checked by: KM

Scale: NTS

BOHLER //

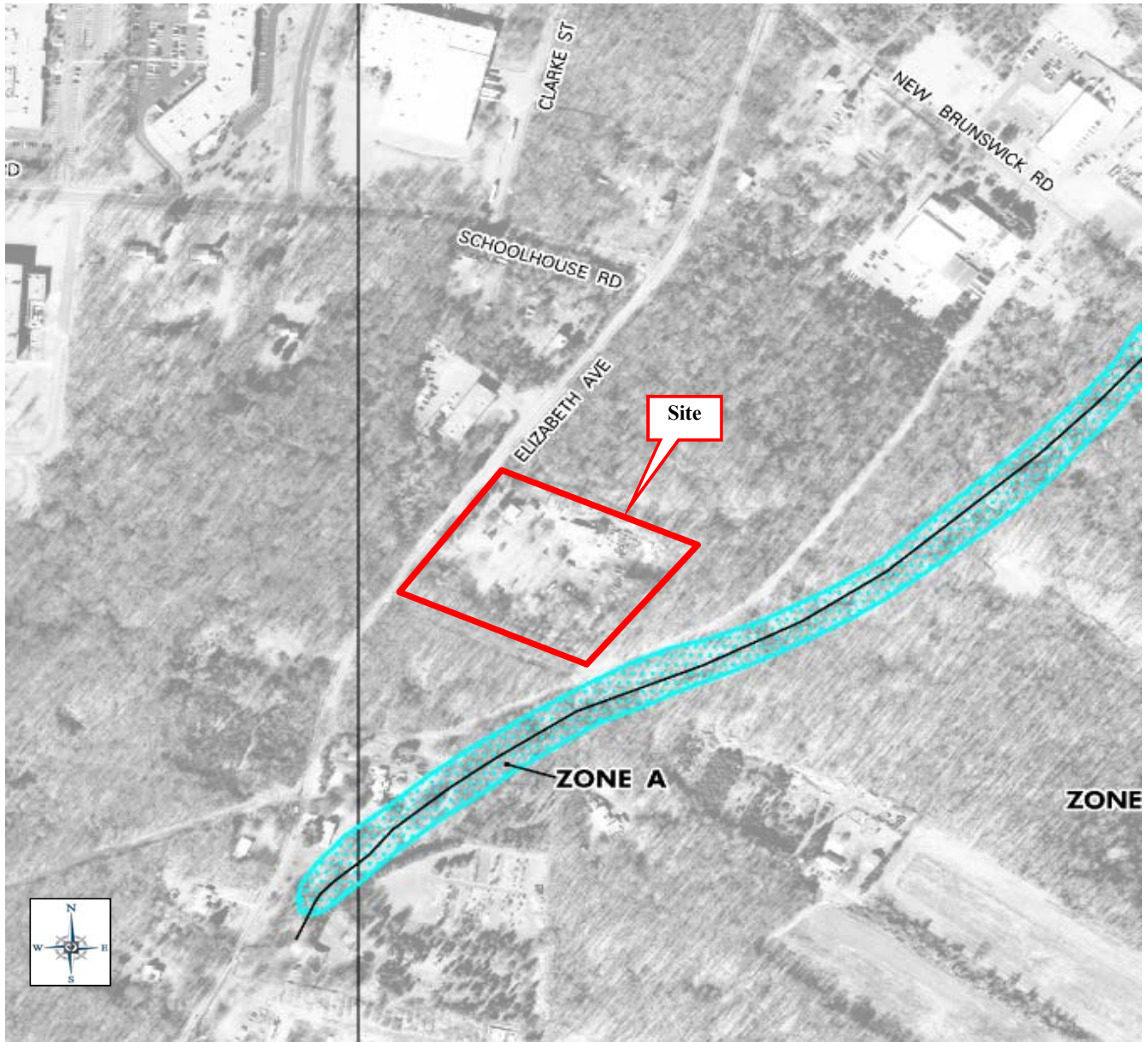


HUC-14 Sub-Watershed Map

Source: NJ GeoWeb

Date Access: 05/17/2021

| | |
|---|---|
| SafStor Real Estate CO, LLC | |
| 471 Elizabeth Avenue Block 507.14; Lot 65.01 | Township of Franklin, Somerset County, New Jersey |
| BENJ# J200933 | |
| Prepared by: CR | Date: 4/13/2021 |
| Checked by: KM | Scale: NTS |
| BOHLER // | |



FEMA Flood Map

Source: FEMA FIRM Map #34023C0043F, Date July 6, 2010

Date Access: 05/17/2021

SafStor Real Estate CO, LLC

471 Elizabeth Avenue
Block 507.14; Lot 65.01

Township of Franklin, Somerset County, New Jersey

BENJ# J200933

Prepared by: CR

Date: 4/13/2021

Checked by: KM

Scale: NTS

BOHLER //