## **Stormwater Management Report**

for:

# **Cosmopolitan at Somerset Town Center**

Block 385, Lot 2.07 Township of Franklin Somerset County, New Jersey

#### **Prepared By:**

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**Under the Immediate Supervision of:** 

Scott H. Turner NJ PE# 43811

ST/MAD/hc MEA # 2021.019

Dated: August 16, 2021



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#### INTRODUCTION

The following Stormwater Management Report details the design of the stormwater management plan for a proposed development located in the Township of Franklin, Somerset County, New Jersey and has been prepared by Menlo Engineering Associates, Inc. in accordance with the standards of the Township of Franklin, the County of Somerset, the New Jersey Soil Conservation Service, and the New Jersey Department of Environmental Protection. This report supplements, and should be reviewed in conjunction with, the project development plans prepared by Menlo Engineering Associates, Inc.

The purpose of this report is to demonstrate that the proposed stormwater management system adequately convey stormwater runoff, and to assist Engineers at the Municipal, County, and State levels in evaluating the drainage calculations and considerations incorporated in the design as shown on the plans submitted. The report supplements, and should be reviewed in conjunction with, the project development plans prepared by Menlo Engineering Associates, Inc. This office will readily respond to questions and requests for additional calculations or verification of the proposed design by Municipal, County, or State Engineers, and will be responsive to their suggestions and modifications to the design in conformance to the applicable codes in the interest of land use control consistent with environmental protection.

#### STORMWATER MANAGEMENT PLAN & DESIGN

The guidelines for hydraulic design, as prepared by the Soil Conservation District, the Township of Franklin, Somerset County, and the New Jersey Department of Environmental Protection have been utilized for the drainage design of this project. The purpose of the drainage design is to safely convey the stormwater runoff and attenuate the discharges in accordance with regulations promulgated by the above cited agencies.

The stormwater management plan for the site is to provide for conveyance of stormwater runoff from the proposed 4-story apartment building and parking lot retrofit to the existing stormwater collection system. The stormwater collection system will consist of inlets and pipe networks. The stormwater conveyance system has been designed for the 25-year storm and the inlet grates have been designed to comply with the most current regulations.

The proposed redevelopment results in a net decrease in impervious coverage of 1.46 acres. Moreover, the proposed redevelopment does not increase the peak runoff rates for the pre-construction condition leaving the site for the two-, ten-, and 100-year storm events, on the contrary, it decreases the peak runoff rates for the post construction conditions.

#### **Summary Tables:**

The following tables summarize the reduction of runoff for the 2, 10, 25, and 100-year storm events as analyzed utilizing the Rational method:

STORM	EXISTING RUNOFF FROM SITE (CFS)	PROPOSED RUNOFF FROM SITE (CFS)	FLOW REDUCTION (CFS)
100	201.8	197.4	4.4
25	169.0	165.3	3.7
10	146.3	143.1	3.2
2	106.0	103.6	2.4

#### **Environmental Site Analysis.**

In accordance with the township ordinance 330-27.A(2), the 27.42 acres parcel is currently developed and consists of 21.60 acres of impervious coverage. Most of the site is classified as Klinesville soils which belongs to the hydraulic group D. The existing runoff is collected by an underground pipe network that discharges into Seeley's Brook which is maintain in the proposed conditions. Also, the existing drainage patterns are maintained in the proposed condition. Moreover, in the proposed conditions the impervious coverage is decreased to 20.14 acres which will generate lower peak runoff flows than in the existing condition. The site does not contain any environmental sensitive features nor any unique conditions.

#### Land Use Planning and Source Control Plan.

In accordance with the township ordinance 330-27.A(4), as mentioned in this report the proposed redevelopment proposes a 1.46 acres of impervious reduction from the existing conditions. Therefore, water quality, quantity and ground water recharge are meet by increasing the pervious areas. The existing peak runoff flows for the two-, ten- and 100-year storm are decreased in the proposed conditions. Since there is no increase in volume for the two-year storm the groundwater recharge standards are met. By providing two Water Quality Structures with a Removal TSS rate of 50% the stormwater runoff quality standards are met (see Appendix D for Water Quality Structure Sizing Calculations).

#### CONCLUSION

The proposed stormwater management system for the proposed redevelopment has been designed with provisions for safe and efficient control of stormwater runoff in a manner which will not adversely affect the existing drainage patterns found in the surrounding areas. It is the opinion of this office that the proposed development will not have any negative impacts on the drainage characteristics of the site, or the immediately surrounding areas. Further, it is the opinion of this office, that the proposed development will be in compliance with all applicable stormwater management regulations as established by the NJDEP and the Township of Franklin Standards.

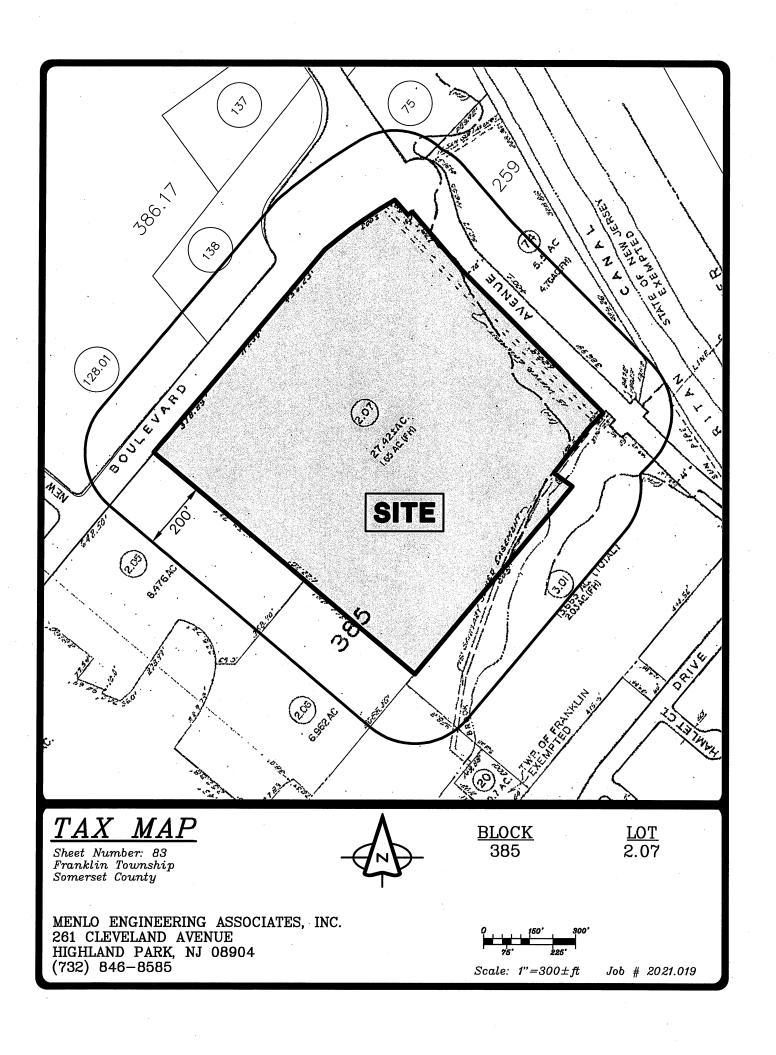
### **APPENDIX A: PRE-DEVELOPMENT CONDITION**

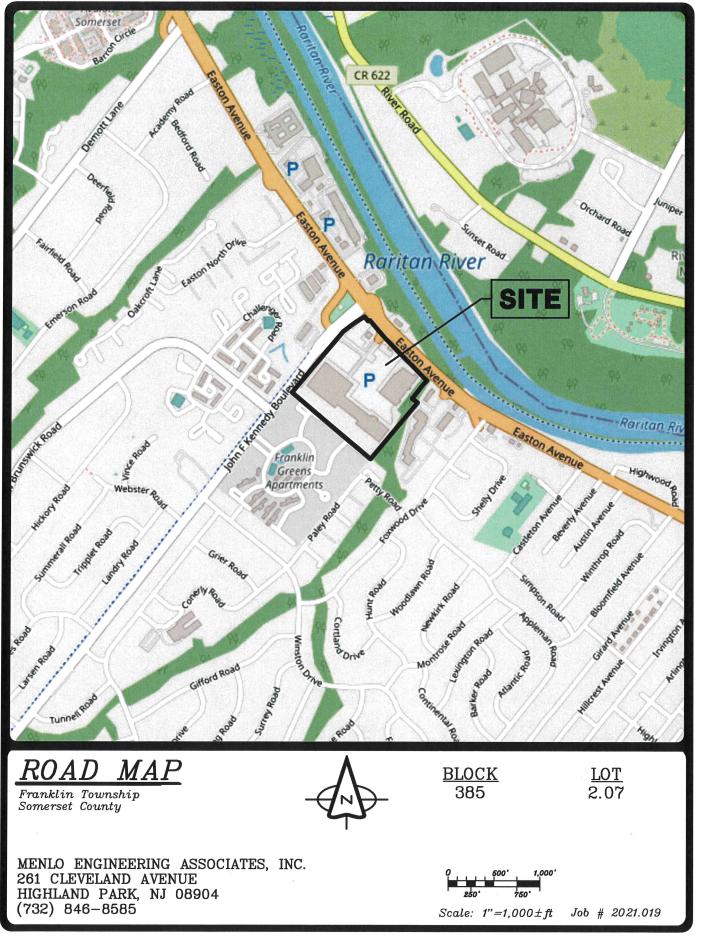
## **APPENDIX B: POST-DEVELOPMENT CONDITION**

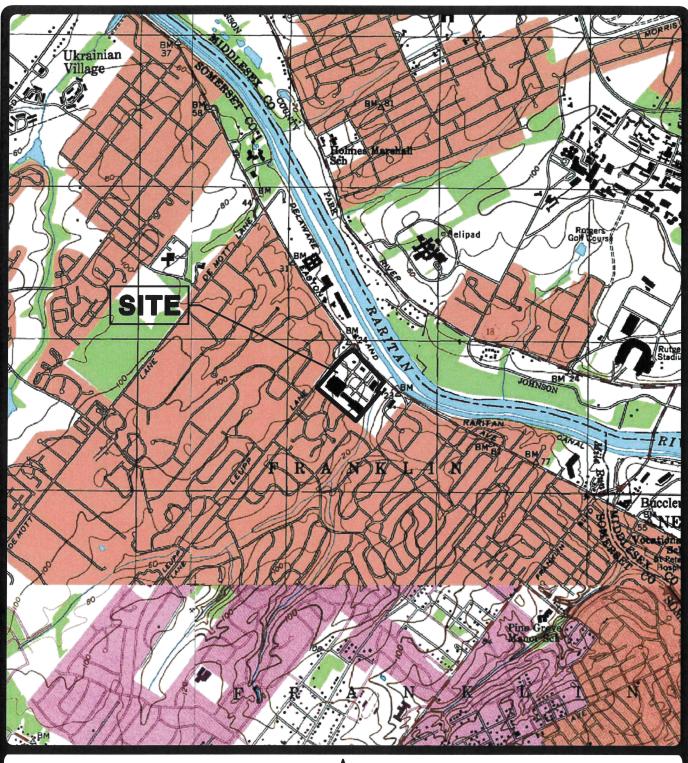
## **APPENDIX C: PIPE CALCULATIONS**

## **APPENDIX D: WATER QUALITY CALCULATIONS**

## **APPENDIX E: DRAINAGE AREA MAPS**







U.S.G.S. MAP

Quad Name: Plainfield Franklin Township Somerset County



BLOCK 385 <u>LOT</u> 2.07

MENLO ENGINEERING ASSOCIATES, INC.

261 CLEVELAND AVENUE HIGHLAND PARK, NJ 08904 (732) 846-8585

<u>State Plane Coordinates:</u>
N: 611,406.76 ft.
E: 495,678.94 ft.

0 1,000' 2,000'

Scale:  $1''=2,000\pm ft$  Job # 2021.019

## **APPENDIX A: PRE-DEVELOPMENT CONDITION**

## PRE-DEVELOPMENT DRAINAGE CONDITION

I. Total Drainage Area:

27.42 Acres

II. Soil Groups/Types:

KkoC -Klinesville

Type

III. Time of Concentration:

10 Minutes

IV Rainfall Intensity:

<u>Storm</u>	<u>Rainfall(in/hr)</u>
100-YR	8.00
25-YR	6.70
10-YR	5.80
2-YR	4.20
1-YR	3.20

#### V. Weighted 'c' Calulation:

Land Use	<u>Area</u>	% of Cover	C Value	<u>Total</u>
Impervious	21.60 Acres	0.79	0.99	0.78
Gravel	0.00 Acres	0.00	0.84	0.00
Grass	5.82 Acres	0.21	0.65	0.14
Woods	0.00 Acres	0.00	0.59	0.00
			Weighted 'c':	0.92

#### VI. Q=ciA

Q=	<u>c</u>	<u> 1</u>	<u>A</u>	=	Q .
$Q_{100} =$	0.92	8.00	27.42	=	201.8
Q <sub>25</sub> =	0.92	6.70	27.42	=	169.0
$Q_{10} =$	0.92	5.80	27.42	=	146.3
$Q_2 =$	0.92	4.20	27.42	=	106.0

## **APPENDIX B: POST-DEVELOPMENT CONDITION**

## POST DEVELOPMENT RUNOFF CONDITION

I. Total Drainage Area:

27.42 Acres

II. Soil Groups/Types:

KkoC -Klinesville

Type D

III. Time of Concentration:

10 Minutes

IV Rainfall Intensity:

<u>Storm</u>	Rainfall(in/hr)
100-YR	8.00
25-YR	6.70
10-YR	5.80
2-YR	4.20
1-YR	3.20

V. Weighted 'c' Calulation:

Land Use	<u>Area</u>	% of Cover	<u>C Value</u>	<u>Total</u>
Impervious	20.14 Acres	0.73	0.99	0.73
Gravel	0.00 Acres	0.00	0.84	0.00
Grass	7.28 Acres	0.27	0.65	0.17
Woods	0.00 Acres	0.00	0.59	0.00
•			Weighted 'c'	0.90

VI. Q=ciA

Q=	<u>c</u>	<u>1</u>	<u>A</u>	=	Q
Q <sub>100</sub> =	0.90	8.00	27.42	=	197.4
Q <sub>25</sub> =	0.90	6.70	27.42	=	165.3
Q <sub>10</sub> =	0.90	5.80	27.42	=	143.1
$Q_2 =$	0.90	4.20	27.42	=	103.6

## **APPENDIX C: PIPE CALCULATIONS**

		20	2021.019-RI	9-RUT	GERS	PLA	UTGERS PLAZA - WEIGHTED 'C' VALUES	EIGH	TED '	C' VA	LUES			
	-			SOIL	TYPE(S	): (Kko(	OIL TYPE(S): (KkoC) KLINESVILLE (TYPE 'D')	SVILLE	(TYPE	D')				
	TOTAL	TOTAL IMPERVIOUS	VIOUS	-,C,=	0.99	GR.	GRASS	ار' =	0.65	WOODS	SQ	-,C,=	0.59	TOTAL
STRUCTURE AREA (acres)	AREA (acres)	AREA (acres)	%	,D,	IMPERV AREA 'C' (acres)	AREA (acres)	%	,C,	GRASS AREA 'C' (acres)	AREA (acres)	%	,C,	WOODS 'C'	WEIGHTED 'C' (F+T+N)
A2	0.41	0.33	%08	0.99	0.80	80.0	20%	0.65	0.13		%0	0.59	0.00	0.92
TOTALS	0.41	0.33	%08	0.99	08.0	80.0	70%	9.65	0.13	0.00	%0	0.59	0.00	

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	n-val Pipe		0.0013	
	+	£	0 44.10	
	+	Œ	4.50	2021
		(£t/s)	4	Date: 8/12/2021
	Φ.	(%)	68.0	Dat
		(in)	5	
_		(cfs)	10.4	-
		(cfs)	2.54	ines: 1
		(cts)	0.00	Number of lines: 1
	al Kno			Ž
1		ır) (cfs)	2.54	
	- Sys	(in/hr)	0 6.73	
_		(min)	10.0	
-	-	(ac)	14.0	
		r) (cfs)	2.5	
	- Inet	) (in/hr)	6.73	
-		(min)	10.0	
	~ U	<u>0</u>	0.92	
	Drng Area	(ac)	0.41	
	Line Length	Œ)	103.471	
	Gnd/Rim El Up	E)	47.00	Project File: 2021.019-LINE A.stm
	Line D		4	.010.020
	nlet D		Y2	t File: 2(
	No.			Projec

Storm Sewers

NOTES: Intensity = 42.39 / (Inlet time + 5.10) ^ 0.68 -- Return period = 25 Yrs.; \*\* Critical depth

	202	2021.019-RUTGERS PLAZA - WEIGHTED 'C' VALUES	IUT.	GE	RS PL	AZA	_ W	EIG	HTE	C'V	AI	'UES		
		- 1	SOIL '	TYP	E(S): (K	SOIL TYPE(S): (KkoC) KLINESVILLE (TYPE 'D')	INE	SVIL	LE (TYF	E'D')				
		IMPERVIOUS 'C' = 0.99	SOOS	_,C,=	0.99	GRAS	SS	رر = ارر =	GRASS $'C' = 0.65$	WOODS $^{1}$ C' = 0.59		] = 0.	.59	TOTAL
STRUCTURE	AREA (acres)	AREA (acres)	%	رز	IMPERV 'C'	'C' IMPERV AREA % 'C'	%	Ç	GRASS 'C'	$\begin{array}{c c} AREA & \% & C' & V \\ (acres) & \% & C' & V \end{array}$	%	'C' WO	WOODS 'C'	(F+I+N)
B2	0.05	0.05 100% 0.99 0.99	100%	0.99	0.99		%0	0% 0.65	0.00		0% 0.59	0.00	8	0.99
B3	0.38	0.30	79% 0.99	0.99	0.78	0.08 21% 0.65	21%	9.02	0.14		0% 0.59	0 65.0	0.00	0.92
TOTALS	0.43	0.35	81%	66.0	0.35 81% 0.99 0.81	80.0	19%	0.65	0.08   19%   0.65   0.12	0.00   0%   0.59   0.00	%	0.59 0.	00	

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				Т
				-
n-val Pipe		0.013		
Invert	( <del>L</del>	41.60		
Invert	(£)	43.00		2/2021
Vel	(ft/s)	3.25		Date: 8/12/2021
Line Slope	(%)	0.99		
Line	(in)	र्ह र		
Capac	(cfs)	6.44		2
Flow	(cfs)	2.63		Number of lines: 2
Known	(cfs)	0.00		Number
Total Runoff	(cfs)	2.63		
i. Sys	(in/hr)	6.58		-
2	(min)	10.5		
Total Area	(ac)	0.43	·	
D Q	(cfs)	0.33		
i lilet	(in/hr)	6.73		
Inlet	(min)	10.0		
Runoff	<u>(</u> )	0.99		
Drng Area	(ac)	0.05		
Line Length	(£)	140.777		
Gnd/Rim El Up	(H)	47.20		Project File: 2021.019-LINE B.stm
Line O		P27		1.019-LI
D let		B3 B3		File: 202
Line No.		- 2		Project F

Storm Sewers

NOTES: Intensity = 42.39 / (Inlet time + 5.10) ^ 0.68 -- Return period = 25 Yrs.; \*\* Critical depth

ĭ		2021.01	9-RI	JTG	.019-RUTGERS PLAZA - WEIGHTED 'C' VALUES	LAZA	<b>W</b> -	EIC	HITED	,C, V		UES	70	
			SC	IL T	SOIL TYPE(S): (KkoC) KLINESVILLE (TYPE 'D')	KkoC) KI	,INE	SVII	LE (TYP)	E 'D')				
	TOTAL	IMPERV	ERVIOUS	_ ,C,	0.99	GRASS		,C,=	0.65	WOODS	S	,C,=	0.59	TOTAL
TRUCTUR	AREA	AREA	%	ı.Jı	IMPERV	AREA	70	<u>-</u>	יטי ממע מבי	AREA	è		WOODS	WEIGHTE
	(acres)	(acres)	0/	ر	, C,	(acres)	0/		UKASS C	(acres)	%	ز	رَ	D'C'
C2.1	0.22	0.22	100% 0.99	66.0	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C2.2	0.23	0.23	100% 0.99	66.0	0.99		0% 0.65	9.02	0.00		%0	0% 0.59	0.00	0.99
C2.3	0.04	0.04	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C2.4	0.07	0.07	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C2.5	0.05	0.05	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C2.6	0.05	0.05	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C4	0.26	0.26	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C4.1	0.26	0.26	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
CS	0.03	0.03	100% 0.99	0.99	0.99		0% 0.65	9.02	0.00		%0	0% 0.59	0.00	0.99
9) C	0.02	0.02	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C7	0.03	0.03	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
<b>8</b> 0	0.05	0.05	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
60	0.05	0.05	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C10	0.04	0.04	100% 0.99	0.99	0.99		0% 0.65	9.65	0.00		%0	0% 0.59	0.00	0.99
C11	90.0	90.0	100% 0.99	0.99	0.99		0% 0.65	0.65	0.00		%0	0% 0.59	0.00	0.99
TOTALS	1.46	1.46	100% 0.99	66.0	66.0	00.0	0% 0.65	9.65	0.00	0.00	%0	0% 0.59	0.00	

# Pipe Calc

																											Ī
	n-val Pipe		0.013	0.013	0.013	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.013	0.013	0.013	0.013	0.010	0.010	0.010								
	Invert	£	39.00	41.00	42.00	42.85	43.45	43.80	44.15	44.60	45.00	45.45	44.80	42.20	42.80	43.20	43.85	44.30	44.85		-		1				
	Invert Up	Œ	39.75	41.90	42.75	43.35	43.70	44.05	44.50	44.90	45.35	45.70	45.25	42.70	43.10	43.75	44.20	44.75	45.25							8/12/2021	
	Vel Ave	(ft/s)	5.20	5.52	5.56	3.25	5.25	5.03	4.61	3.87	3.26	2.77	4.08	5.18	3.93	2.90	4.45	3.09	2.48	,						Date: 8/1	
	Line	(%)	0.50	1.00	1.02	1.02	1.20	1.20	1.00	1.15	1.09	1.20	1.08	1.03	1.13	1.04	1.04	1.05	1.06						1		
·	Line Size	(in)	24	15	15	12	ω	ω	. ω	ω	ω		15	15	15	15	ω	∞	∞								
	Capac Full	(cfs)	15.94	6.47	6.51	4.67	1.72	1.72	1.57	1.69	1.64	1.72	6.71	6.54	6.87	6.58	1.60	1.61	1.61							17	
	Flow	(cfs)	8.79	4.96	5.02	1.78	1.60	1.47	1.29	0.97	99.0	0.40	1.73	4.01	2.69	1.33	1.08	0.65	0.33							Number of lines: 17	
	Known	(cfs)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							Number	
	Total   Runoff	(cfs)	8.79	4.96	5.02	1.78	1.60	1.47	1.29	76.0	99.0	0.40	1.73	4.01	2.69	1.33	1.08	0.65	0.33								
	Sys	(in/hr)	80.9	6.26	6.34	6.43	6.45	6.47	6.52	6.56	6.64	6.73	6.73	6.14	6.18	6.39	6.43	6.54	6.73								
	ဦ	(min)	12.4	11.7	4.11	11.1	11.0	10.9	10.7	10.6	10.3	10.0	10.0	12.2	12.0	11.2	11.0	10.7	10.0								
•	Total Area	(ac)	1.46	0.80	0.80	0.28	0.25	0.23	0.20	0.15	0.10	90.0	0.26	99.0	0.44	0.21	0.17	0.10	90.0								
	o luc	(cfs)	0.00	0.00	1.73	0.20	0.13	0.20	0.33	0.33	0.27	0.40	1.73	1.47	1.53	0.27	0.47	0.33	0.33								
	i Inlet	(in/hr)	00.0	0.00	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73	6.73		,						
	Inlet	(min)	0.0	0.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0								
	Runoff Coeff	<u>(</u> )	0.00	0.00	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99								
	Drng Area	(ac)	0.00	0.00	0.26	0.03	0.02	0.03	0.05	0.05	0.04	90:0	0.26	0.22	0.23	0.04	0.07	0.05	0.05								
	Line Length	(£	150.973	89.646	73.686	49.168	20.813	20.813	35.128	26.000	32.170	20.813	41.625	48.742	26.513	53.000	33.697	42.725	37.882	****					-		
	Gnd/Rim El Up	(#)	47.50	48.10	48.25	48.70	48.70	48.70	48.80	48.80	48.70	48.70	48.25	48.25	48.25	48.25	48.25	48.25	48.25						•	2021.019-LINE C.stm	
2	Line D		P30	P39	P38	P37	P36	P35	P34	P33	P32	P31	P40	P24	P23	. P22	P21	P20	P19			•				21.019-L	
3	Inlet		22	ឌ	2	CS	90	C7	<del></del> 8	<u>ව</u>	C10	5	2.	C2.1	C2.2	C2.3	C2.4	C2.5	C2.6					-		File: 20	
2	Line No.		-	7	ო	4	.c	9	7	00	6	10	7	12	13	4	15	16	17							Project File:	
2	Line No.		<u></u>	7	က	4	5	9	7	ω	6	10	7	12	13	4	15	16	17								Projec

NOTES: Intensity = 42.39 / (Inlet time + 5.10) ^ 0.68 -- Return period = 25 Yrs.; \*\* Critical depth

	202	21.019	RUJ		RS P	LAZA	- WE	IGE	ITED	2021.019-RUTGERS PLAZA - WEIGHTED 'C' VALUES	T	ES	,
			SOII	LY	PE(S):(	SOIL TYPE(S): (KkoC) KLINESVILLE (TYPE 'D')	LINESV	TLE	(TYPE	( D.)			
	TOTAL	IMPERVIOUS 'C' = 0.99	SOOI	ار <u>.</u> =	0.99	GR/	GRASS	_'C' =	'C' = 0.65	WOODS $'C' = 0.59$	Ď	'= 0.59	TOTAL
STRUCTURE	AREA (acres)	AREA (acres)	%	Ç	% 'C'   IMPERV AREA 'C' (acres)	AREA (acres)	%	Ĺ,	GRASS 'C'	C, GRASS AREA 9	, C. N	WOODS 'C'	WEIGHIED 'C'
D4	0.08	0.08   100%   0.99   0.99	100%	66.0	0.99		0% 0.65 0.00	0.65	0.00		0% 0.59	90.00	0.99
TOTALS	0.08	0.08	100%	66.0	0.08   100%   0.99   0.99	0.00	%0	0.65	00.0 59.0 %0	0.00	% 0.	0.00 0% 0.59 0.00	

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•	n-val Pipe		0.013	0.013	0.013	0.013	
	Invert	£	38.80	39.00	39.15	42.10	
	Invert Up	Œ	38.90	39.15	39.30	43.70	Date: 8/12/2021
	Vel Ave	(ft/s)	2.20	2.51	2.34	3.48	Date: 8
	Line Slope	(%)	0.50	0.96	0.92	2.55	
	Line	(in)	24	24	24	15	
	Capac Full	(cfs)	16.04	22.11	21.72	10.32	4 ::
	Flow Rate	(cfs)	0.43	0.45	0.48	0.53	Number of lines: 4
	Known Q	(cfs)	0.00	0.00	0.00	0.00	Numbe
	Total Runoff	(cfs)	0.43	0.45	0.48	0.53	
	i Sys	(in/hr)	5.44	5.73	6.09	6.73	
	2	(min)	15.6	14.0	12.4	10.0	
	Total Area	(ac)	0.08	0.08	0.08	0.08	
	o Inc	(cfs)	0.00	0.00	0.00	0.53	
	i	(in/hr)	0.00	0.00	0.00	6.73	
	Inlet	(min)	0.0	0:0	0.0	10.0	
	Runoff	<u>(</u> )	0.00	0.00	0.00	0.99	
. [	Drng Area	(ac)	00.00	00:00	00.00	0.08	
	Line Length	(#)	19.876	15.704	16.272	62.663	
	Gnd/Rim El Up	(ft)	47.30	47.00	45.54	47.70	Project File: 2021.019-LINE D.stm
ا د	Line		P43	P42	P41	P25	21.019-1
ב של ב	inlet D		5	D2	23	D4	File: 20
2	Line No.		Ψ-	7	ო	4	Project

NOTES: Intensity = 42.39 / (Inlet time + 5.10) ^ 0.68 - Return period = 25 Yrs.; \*\* Critical depth

	2	2021.01	9-R	UT	GERS P	LAZA	- W	EIC	HTED	1.019-RUTGERS PLAZA - WEIGHTED 'C' VALUES	LUE	S	
			S	OIL	SOIL TYPE(S): (KkoC) KLINESVILLE (TYPE 'D')	(KkoC) K	LINE	SVIL	LE (TYP)	E 'D')			
	TOTAL	IMPERVI	SOC	= , <b>C</b> ,=	PERVIOUS $'C' = 0.99$	GRAS		C' =	GRASS $'C' = 0.65$	WOODS	_,C,	WOODS $'C' = 0.59$	TOTAL
TRUCTUR	AREA	AREA	70	رَ	IMPERV	AREA	/0	15.	וטו שטיי פט	AREA	2	WOODS	WOODS WEIGHTE
	(acres)	(acres)	0/	70 C	,C,	(acres)	0/	<u>ر</u> د	% C UKASS C		ن چ	نِ	D'C'
E1	0.19	0.09	47%	47% 0.99	0.47	0.10   53%   0.65   0.34	23% (	9.65	0.34		0% 0.59	0.00	0.81
TOTALS	0.19	60.0	47%	66.0	47% 0.99 0.47	0.10	53% (	3.65	53% 0.65 0.34	0.00 0% 0.59	0.59	0.00	

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Line Inlet No. ID	Line O	Gnd/Rim El Up	Line Length	Drng Area	Runoff Coeff	Inlet	in et	ဉ် ဝ	Total	ဥ	Sys	Total Runoff	Known	Flow Rate	Capac Full	Line Size	Line Slope	Vel	Invert	Invert	n-val Pipe	
		(#)	(£)	(ac)	(C)	(min)	(in/hr)	(cfs)	(ac)	(min)	(in/hr)	(cfs)	(cfs)	(cfs)	(cfs)	(in)	(%)	(ft/s)	<b>(#</b>	(#)		
Project File: 2	202 P1	Project File: 2021.019-LINE E.stm	32.822	0.10	0. 8.	10.0		1.04		10.0	6.73	10,0	Number	0.00 1.04 Number of lines: 1	1:	5	1	3.06 39.50 Date: 8/5/2021	39.50	39.20	0.013	
NO IES: INF	ensity = 4	NOTES: Intensity = 42.39 / (Inlet time + 5.10) ^ 0.68 - Return period = 25 Yrs.;	ne + 5.10)	~ 0.68	Return pe.	riod = 25		" Critical depth	depth													

	2	2021.01	9-RL	TLC	ERS P	.019-RUTGERS PLAZA - WEIGHTED 'C' VALUES	M	EIG	HTED	C'VA	LUE		
			SO	II T	YPE(S):(	SOIL TYPE(S): (KkoC) KLINESVILLE (TYPE 'D')	NE	SVIL	LE (TYPI	3 'D')			
	TOTAL	IMPERVI	ERVIOUS 'C' =	'C' =	0.99	GRASS $C' = 0.65$	_	C =	0.65	WOODS	WOODS $'C' =$	0.59	TOTAL
TRUCTUR	AREA	AREA	70	ز	IMPERV	AREA	  - 		יטו טט ע פר	AREA	2	WOODS	WEIGHTE
	(acres)	(acres)	0	ر	,C,	(acres)	0/	<u>-</u> د	C UKASS C	(acres)	ز — چ	Ç	D'C'
F2.1	0.63	69.0	100% 0.99	0.99	66.0		69.0   %0	3.65	0.00		0% 0.59	00.0	0.99
F2.1	0.39	0.39	100% 0.99	0.99	0.99		0% 0.65	3.65	0.00		0% 0.59	0.00	0.99
F3	0.74	0.74	100% 0.99	0.99	0.99		0% 0.65	3.65	0.00		0% 0.59	0.00	66.0
TOTALS	1.76	1.76	100% 0.99	66.0	66.0	0.00	0% 0.65	3.65	0.00	0.00	0% 0.59	0.00	

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	n-val Pipe		0.013	0.013	0.013		
	Invert	£	35.40	35.65	35.65		
	Invert	<b>£</b>	35.65	35.95	36.55	•	2021
	Vel Ave	(£/t/s)	7.12	3.56	4.62	·	Date: 8/5/2021
	Line	(%)	1.95	0.94	1.00		
	Line	(in)	18	15	15		
	Capac	(cfs)	14.67	6.27	6.45		8
	Flow	(cfs)	11.54	4.20	4.93		Number of lines: 3
	Known	(cfs)	00:00	0.00	0.00		Number
	Total K Runoff	(cfs)	11.54	4.20	4.93		
	Sys R	(in/hr)	6.62	6.73	6.73		
	2	(min)	10.4	10.0	10.0		
	Total	(ac)	1.76	0.63	0.74		
	D O	(cfs)	2.60	4.20	4.93		
	i	(in/hr)	6.73	6.73	6.73		
	Inlet Time	(min)	10.0	10.0	10.0		
	Runoff	(C)	0.99	66.0	0.99		
i	Drng Area	(ac)	0.39	0.63	0.74		
	Line Length	(#)	12.811	31.807	90.193		stm
	Gnd/Rim El Up	(#)	39.50	39.50	40.75		Project File: 2021.019-LINE F.stm
	Line		23	P5	P2		721.019-
۱ ا	nlet D		F2	F2.1	£3		t File: 20
	Line No.		_		က		Projec
		_					

NOTES: Intensity = 42.39 / (Inlet time + 5.10) ^ 0.68 -- Return period = 25 Yrs.; \*\* Critical depth

## **APPENDIX D: WATER QUALITY CALCULATIONS**



WQ DEVICE #1



WQ DEVICE #2









Routing Diagram for 2021.019-Rutgers Plaza-WQ
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#### 2021.019-Rutgers Plaza-WQ

Prepared by Menlo Engineering Associates, Inc HydroCAD® 10.10-4b s/n 01129 © 2020 HydroCAD Software Solutions LLC

#### **Summary for Subcatchment 1S: WQ DEVICE #1**

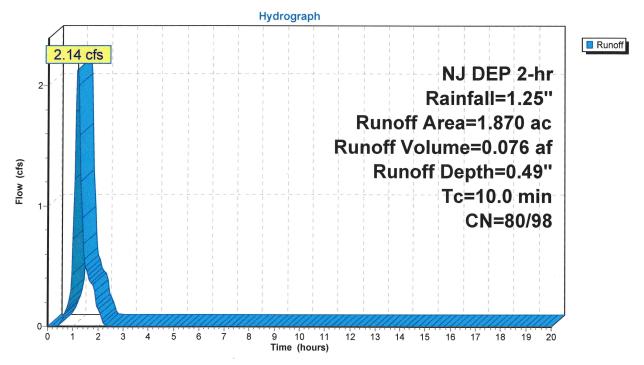
Runoff = 2.14 cfs @ 1.16 hrs, Volume=

0.076 af, Depth= 0.49"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-20.00 hrs, dt= 0.05 hrs NJ DEP 2-hr Rainfall=1.25"

-	Area	(ac)	CN	Desc	cription			
	0.600 98 Paved parking, HSG D					, HSG D		
	1.190		80	>75%	>75% Grass cover, Good, HSG D			
*	0.	080	98	Cond	crete			
	1.870 87 Weighted Average				hted Aver	age		
	1.190 80 63.64% Pervious Area				4% Pervio	us Area		
	0.680 98 36.36% Impervious Area				3% Imperv	ious Area		
	_					_		
	Тс	Lengt		Slope	Velocity	Capacity	Description	
-	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)		
	10.0						Direct Entry,	

#### Subcatchment 1S: WQ DEVICE #1



Page 7

#### 2021.019-Rutgers Plaza-WQ

Prepared by Menlo Engineering Associates, Inc HydroCAD® 10.10-4b s/n 01129 © 2020 HydroCAD Software Solutions LLC

#### **Summary for Subcatchment 2S: WQ DEVICE #2**

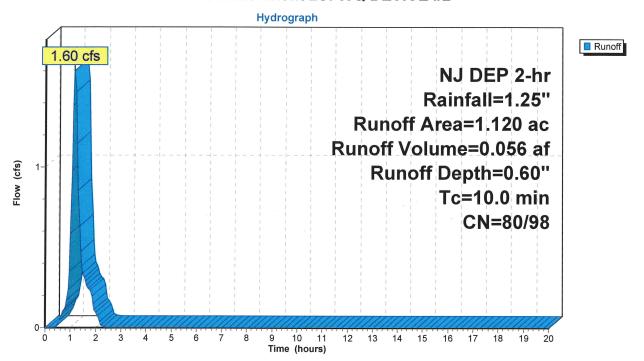
Runoff = 1.60 cfs @ 1.16 hrs, Volume=

0.056 af, Depth= 0.60"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-20.00 hrs, dt= 0.05 hrs NJ DEP 2-hr Rainfall=1.25"

	Area (	(ac)	CN	Description					
	0.9	500	98	Pave	Paved parking, HSG D				
	0.9	570	80	>75%	√ Grass co √	over, Good	, HSG D		
*	0.0	050	98	Cond	rete				
	1.120 89 Weighted Average					age			
	0.570 80 50.89% Pervious Area					us Area			
	0.550 98 49.11% Impervious Area				1% Imperv	ious Area			
	_		_					•	
		Lengt		Slope	Velocity	Capacity	Description		
-	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)			
	10.0						Direct Entry,		

#### Subcatchment 2S: WQ DEVICE #2





## State of New Jersey

PHILIP D. MURPHY Governor

SHEILA Y. OLIVER Lt. Governor DEPARTMENT OF ENVIRONMENTAL PROTECTION
Bureau of Nonpoint Pollution Control
Division of Water Quality
401-02B
Post Office Box 420
Trenton, New Jersey 08625-0420
609-633-7021 Fax: 609-777-0432
http://www.state.nj.us/dep/dwg/bnpc home.htm

CATHERINE R. McCABE

Commissioner

May 18, 2020

Derek M. Berg Director – Stormwater Regulatory Management - East Contech Engineered Solutions LLC 71 US Route 1, Suite F Scarborough, ME 04074

Re:

MTD Lab Certification Cascade Separator<sup>TM</sup> On-line Installation

TSS Removal Rate 50%

Dear Mr. Berg:

This revised certification letter supersedes the Department's prior certification dated October 1, 2019. This revision was completed to reflect Contech's enhanced fabrication capability to manufacture a smaller-size unit of its the Cascade Separator<sup>TM</sup> Manufactured Treatment Device (MTD), while still meeting the scaling methodology as agreed upon by the manufacturers' working group on September 19, 2016. Based on this modification, Table A-1 of the New Jersey Corporation for Advanced Technology (NJCAT) Verification report located at <a href="http://www.njcat.org/uploads/newDocs/NJCATTechnologyVerificationFinal.pdf">http://www.njcat.org/uploads/newDocs/NJCATTechnologyVerificationFinal.pdf</a> has been revised to reflect this same updated model size and flow rate.

The Stormwater Management rules under N.J.A.C. 7:8-5.5(b) and 5.7(c) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Contech Engineered Solutions, LLC (Contech) has requested an MTD Laboratory Certification for the Cascade Separator<sup>TM</sup> stormwater treatment system.

The project falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advance Technology" dated January 25,

2013. The applicable protocol is the "New Jersey Laboratory Testing Protocol to Assess Total Suspended Solids Removal by a Hydrodynamic Sedimentation Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated September 2019) for this device is published online at <a href="http://www.njcat.org/verification-process/technology-verification-database.html">http://www.njcat.org/verification-process/technology-verification-database.html</a>.

The NJDEP certifies the use of the Cascade Separator<sup>TM</sup> stormwater treatment system at a TSS removal rate of 50% when designed, operated, and maintained in accordance with the information provided in the Verification Appendix and the following conditions:

- 1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-5.5.
- 2. The Cascade Separator<sup>TM</sup> shall be installed using the same configuration reviewed by NJCAT and shall be sized in accordance with the criteria specified in item 6 below.
- 3. This Cascade Separator<sup>TM</sup> cannot be used in series with another MTD or a media filter (such as a sand filter) to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
- 4. Additional design criteria for MTDs can be found in Chapter 9.6 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual, which can be found online at <a href="https://www.njstormwater.org">www.njstormwater.org</a>.
- 5. The maintenance plan for a site using this device shall incorporate, at a minimum, the maintenance requirements for the Cascade Separator<sup>TM</sup>. A copy of the maintenance plan is attached to this certification. However, it is recommended to review the maintenance website at <a href="https://www.conteches.com/Portals/0/Documents/Maintenance%20Guides/Cascade-Maintenance%20Guide.pdf?ver=2018-11-05-093254-300">https://www.conteches.com/Portals/0/Documents/Maintenance%20Guides/Cascade-Maintenance%20Guide.pdf?ver=2018-11-05-093254-300</a>. for any changes to the maintenance requirements.

#### 6. Sizing Requirement:

The example below demonstrates the sizing procedure for the Cascade Separator<sup>TM</sup>:

Example:

A 0.25-acre impervious site is to be treated to 50% TSS removal using a Cascade Separator<sup>TM</sup>. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs.

#### Maximum Treatment Flow Rate (MTFR) Evaluation:

The site runoff (O) was based on the following:

time of concentration = 10 minutes i = 3.2 in/hr (page 5-8, Fig. 5-3 of the NJ Stormwater BMP Manual) c = 0.99 (runoff coefficient for impervious)  $Q = ciA = 0.99 \times 3.2 \times 0.25 = 0.79$  cfs

Given the site runoff is 0.79 cfs and based on Table A-1 below, the Cascade Separator™ Model CS-3 with an MTFR of 1.02 cfs would be the smallest model approved that could be used for this site to remove 50% of the TSS from the impervious area without exceeding the MTFR.

The sizing table corresponding to the available system models is noted below. Additional specifications regarding each model can be found in the Verification Appendix under Table A-1.

Table A-1 Cascade Separator<sup>TM</sup> Models and Associated MTFRs

Model	Manhole Diameter (ft)	MTFR (cfs)	50% Maximum Sediment Storage Area Volume (ft <sup>3</sup> )
CS-3	3	1.02	5.3
CS-4	4	1.80	9.4
CS-5	5	2.81	14.7
CS-6	6	4.05	21.2
CS-8	8	7.20	37.7
CS-10	10	11.3	58.9
CS-12	12	16.2	84.8

A detailed maintenance plan is mandatory for any project with a stormwater BMP subject to the Stormwater Management rules under N.J.A.C. 7:8. The plan must include all of the items identified in the Maintenance requirements section of the Stormwater Management rules under N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of inspection and maintenance equipment and tools, specific corrective and preventative maintenance tasks, indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance and Retrofit of Stormwater Management Measures.

If you have any questions regarding the above information, please contact Brian Salvo of my office at (609) 633-7021.

Sincerely,

Gabriel Mahon, Chief

Bureau of Nonpoint Pollution Control

Attachment: Maintenance Plan

cc: Chron File

Richard Magee, NJCAT Jim Murphy, NJDEP-BNPC Vince Mazzei, NJDEP-DLUR Brian Salvo, NJDEP-BNPC

## **APPENDIX E: DRAINAGE AREA MAPS**