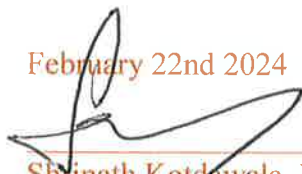


STORMWATER MANAGEMENT REPORT

FOR

**OFFICE AND RETAIL BUILDINGS AT 390 DAVIDSON AVENUE
(BLOCK 502.01, TAX LOT 57.01)
IN TOWNSHIP OF FRANKLIN,
SOMERSET COUNTY, NEW JERSEY**

February 22nd 2024



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TABLE OF CONTENTS

1.0 INTRODUCTION

Figure 1 : Site Mapped Over a 2020 NJGIN Aerial Map

Figure 2 : Site Mapped Over a Bound Brook USGS Quadrangle

Figure 3 : Site Mapped Over a Web Soil Survey Map (A NRCS Publication)

2.0 STORMWATER QUALITY CRITERIA

3.0 GROUNDWATER RECHARGE ANALYSIS

4.0 CONCLUSIONS

5.0 ATTACHMENTS AS REFERENCED IN THE REPORT

APPENDIX A:

PRE AND POST DEVELOPMENT RUNOFF CURVE NUMBER, TIME OF CONCENTRATION COMPUTATIONS AND STORM HYDROGRAPHS

APPENDIX B:

CONVEYANCE CAPACITY OF UNDERGROUND STORMWATER PIPES AND SCOUR HOLE SIZING COMPUTATIONS

APPENDIX C:

ANNUAL GROUND WATER RECHARGE ANALYSIS WORKSHEETS AND MOUNDING ANALYSIS

APPENDIX D:

WATER QUALITY STORM HYDROGRAPHS AND DETAILS OF MTD DEVICES TO REMOVED 80% TOTAL SUSPENDED SOLIDS

APPENDIX E:

SOIL PROFILES AND SOIL PERMEABILITY TEST DATA

APPENDIX F:

PRE AND POST DEVELOPMENT DRAINAGE AREA MAP

SOIL EROSION AND SEDIMENT CONTROL PLAN

SOIL EROSIONS AND SEDIMENT CONTROL NOTES

1.0 INTRODUCTION:

This report is prepared to support a Site Plan approval for two commercial buildings on land parcel known as lot 57.01 in block 502.01 in Township of Franklin, Somerset County. The site measures 2.456 acres and is located at the intersection of Davidson Avenue and New Brunswick Road. Figure 1 show the site mapped over a 2020 NJGIN aerial photograph. The following definitions are utilized for this report:

Where “MTD” means Mechanical Treatment Devices, which are certified to remove 80% of TSS from the parking lot stormwater runoff;

Where the “Rules” means Storm water Management Rules, which is known as N.J.A.C. 7:8;

Where “Site” means Land Parcel in Township of Franklin known as Lot 57.01 in Block 502.01;

Where “TSS” means Total Suspended Solids; and

Where “UG” means Underground Stormwater Storage System.



Figure 1: Site Mapped over a 2020 NJGIN Aerial Image

Figure 2 shows a Bound Brook USGS Quadrangle with site boundaries. Figure 3 shows the site mapped over a USDA Web Soil Survey along with the extent of the soil series. The site has three types of soil; Penn silt loam (PenB) with hydrologic soil group “C,” The second one is Penn Channery silt loam (PeoC) with hydrologic soil group “C,” and the third one is Rowland silt loam (RorAt) with hydrologic soil group “C.” Appendix E shows the soil profiles and permeability results, which are used in determining infiltration rates and ground water mounding analysis. Appendix F shows the Pre and Post development Drainage Area Map and locations of all the structures of proposed stormwater management system.

2.0 PRE DEVELOPMENT HYDROLOGY:

The site currently drains westerly to Raritan River Tributary. The rainfall amounts for 2, 10 and 100-year storm events are computed as:

2.1 Peak Stormwater Runoff is computed for the site based on following parameters:

2, 10, and 100 year storm event precipitation frequency is obtained from NOAA atlas 14-point precipitation frequency (a publication of Hydro meteorological design study center):

2 Year	- 3.3 inches
10 year	- 5.01 inches
100 year	-8.35 inches

2.2 Factors for Somerset County under Table 5.5 of Stormwater Rules are described below:

2 Year	3.3 inches x 1.00 = 3.3 inches
10 year	5.01 inches x 1.03 = 5.16 inches
100 year	8.35 inches x 1.09 = 9.10 inches

2.3 Further as required under table 5.6 of the stormwater rules the precipitation amount is computed below:

2 Year	3.3 inches x 1.19 = 3.72 inches
10 year	5.16 inches x 1.24 = 6.40 inches
100 year	9.10 inches x 1.48 = 13.47 inches

Table 1 shows the pre development parameters that are used to compute peak flows:

TABLE 1: SUMMARY OF HYDROLOGIC PARAMETERS

Sub-Area	Area (Ac.)	Runoff Coeff. (C)	Tc (Min.)
Pre to North-West	1.35	74 (Hydrology Group C)	12 As computed

Appendix A shows the hydrographs for pre and post development land use for 2, 10 and 100-year storm events. Table 1A and 1B provide the compliances with the peak flow reductions in post development conditions.

3.0 POST-DEVELOPMENT HYDROLOGY:

Applicant is proposing two commercial buildings on the site and a parking lot. As the land use change is classified as major development under the rules peak flows are reduced by 50%, 25% and 20% for 2, 10 and 100-year storm events.

Proposed site improvements include construction of an Office and Retail Buildings with a parking lot. A quantitative hydrologic analysis for the disturbed areas of the site has been performed utilizing the same methodology as for the pre-development conditions. The hydrologic parameters were derived from the

same sources as the pre-development parameters. In post development conditions, the disturbed area of the site will continue to drain via the same general drainage areas as described in the pre-development hydrology.

To reduce peak flows from the site two underground (UG) storage systems are proposed. These systems include underground slotted ADS pipes and outlet structures. The outlet structures control the release of stormwater runoff to the stream. Appendix A shows the peak flow hydrographs for the post development conditions. It also shows the UG system routing and outflow volume for 2, 10 and 100-year storm event.

The pipe utilized to carry stormwater to the UG systems has capacity to handle 25-year storm event. Appendix B shows the pipe capacity computations for the all of the conveyance pipes used for the project. In addition Somerset Union County Soil Conservation District (SCD) requires the erosion protection at the stormwater discharge points. Appendix B shows the scour hole sizing computations for the anticipated stormwater runoff from the UG system.

4.0 GROUNDWATER RECHARGE AND GROUND WATER MOUNDING ANALYSIS:

In accordance with Chapter 6 of the BMP manual, compliance with one of the following two groundwater recharge standards is required:

1. "That 100% of the site's average annual pre-developed groundwater recharge volume be maintained after development;" or
2. "That 100% of the difference between the site's pre- and post-development 2-year runoff volumes be infiltrated."

The BMP areas of the site are the bottom areas of the UG systems. The Annual Groundwater Recharge Analysis (Based on GSR-32) computed the required BMP areas for the proposed development. The required BMP area is 2,155 sf while proposed BMP area for recharge is 3,795 sf. Attachment c shows the Recharge Analysis for the pre and post development conditions.

This appendix also shows the groundwater mounding analysis for proposed UG systems. Based on the results mounding due to infiltration is not negatively influencing neighboring sites. This analysis was conducted based on Hantush (1967) equation.

5. WATER QUALITY IMPROVEMENTS:

Subject project requires that the pavement area stormwater runoff is collected and filtered such that an 80% of TSS is removed prior to groundwater recharge and discharge to the stream. Two mechanical treatment devices that are certified by NJDEP are utilized to remove TSS. These device details and capacity computations are shown at appendix D. The stormwater runoff, which needs to be treated, is computed based on 1.25" rainfall in 2 hours with hydrograph distribution mentioned at the BMP manual.

6.0 NONSTRUCTURAL STRATEGIES

In addition, the stormwater management system complies with the New Jersey Stormwater Best Management Practices Manual (BMPM), dated April 2004. The site is designed in accordance with the nonstructural stormwater management strategies, to the maximum extent practical. More precisely, to achieve the required design and performance standards, the following nonstructural strategies are being applied to the design of the site:

- 6.1 Minimize impervious surfaces and break up or disconnect the flow of runoff over impervious surfaces.

- The impervious surfaces on the site are disconnected by the provision of the proposed stormwater management basin that receives and treats the runoff from the site. The basin has been designed without a low flow channel and with a flat sand bottom to break up the flow of stormwater runoff over impervious surfaces prior to discharging to the existing drainage system within Tax Lot 57.01
- 6.2 Maximize the protection of natural drainage features and vegetation.
The site grading and stormwater management system have been designed to maintain the existing drainage patterns of the site. This manner of development protects the natural drainage features and vegetation.
 - 6.3 Minimize the decrease in the time of concentration from pre- to post-construction.
To the maximum extent practical, the site was designed to minimize the decrease in pre-construction "time of concentration".
 - 6.4 Minimize land disturbance including clearing and grading.
The site has been designed to utilize a majority of the cleared site, as well as minimize the fill material needed for construction, to reduce the amount of disturbance to the site.
 - 6.5 Minimize soil compaction.
After rough grading of the site, heavy construction machinery on-site will be minimal.
 - 6.6 Provide low-maintenance landscaping that encourages retention and planting of native vegetation and minimizes the use of lawns, fertilizers and pesticides.
The site has been designed to utilize a majority of the cleared site to maintain the natural vegetation. In addition, a detailed landscape plan has been provided to supplement the existing vegetation.
 - 6.7 Provide other source controls to prevent or minimize the release of pollutants into stormwater runoff.

The site is subject to and has been designed in accordance with the standards established under the Soil Erosion and Sediment Control Act.

7.0 CONCLUSIONS:

The proposed Stormwater management systems has been designed to meet the BMPM water quality, groundwater recharge standards, nonstructural Stormwater management strategy requirements, and reductions to the peak Stormwater flow rates from this development.



Figure 1: Site Mapped Over a 2020 Aerial Map Published By NJGIN

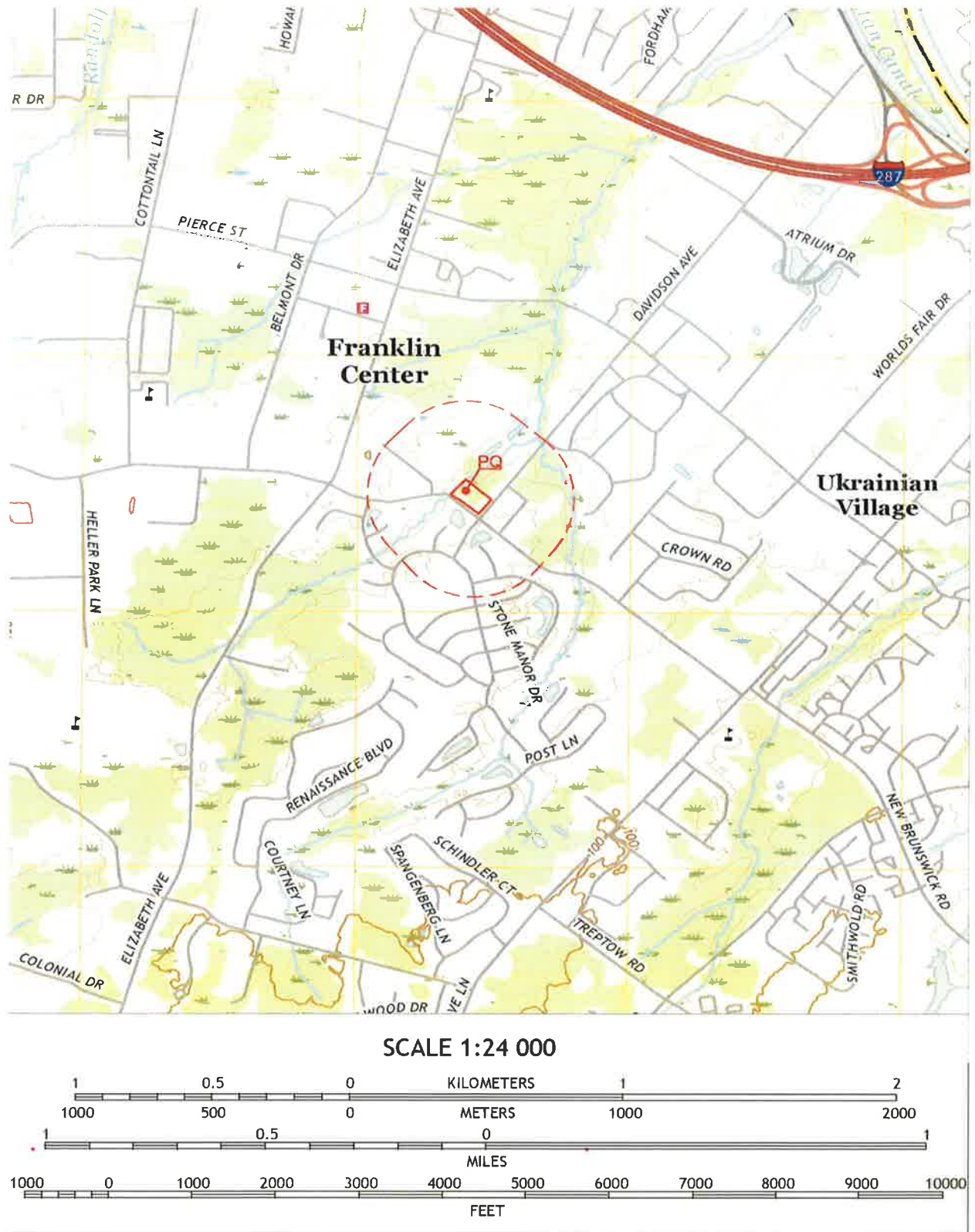


Figure 2: Site Mapped Over a Portion of the Bound Brook USGS Quadrangle - A USGS Publication

Custom Soil Resource Report
Soil Map

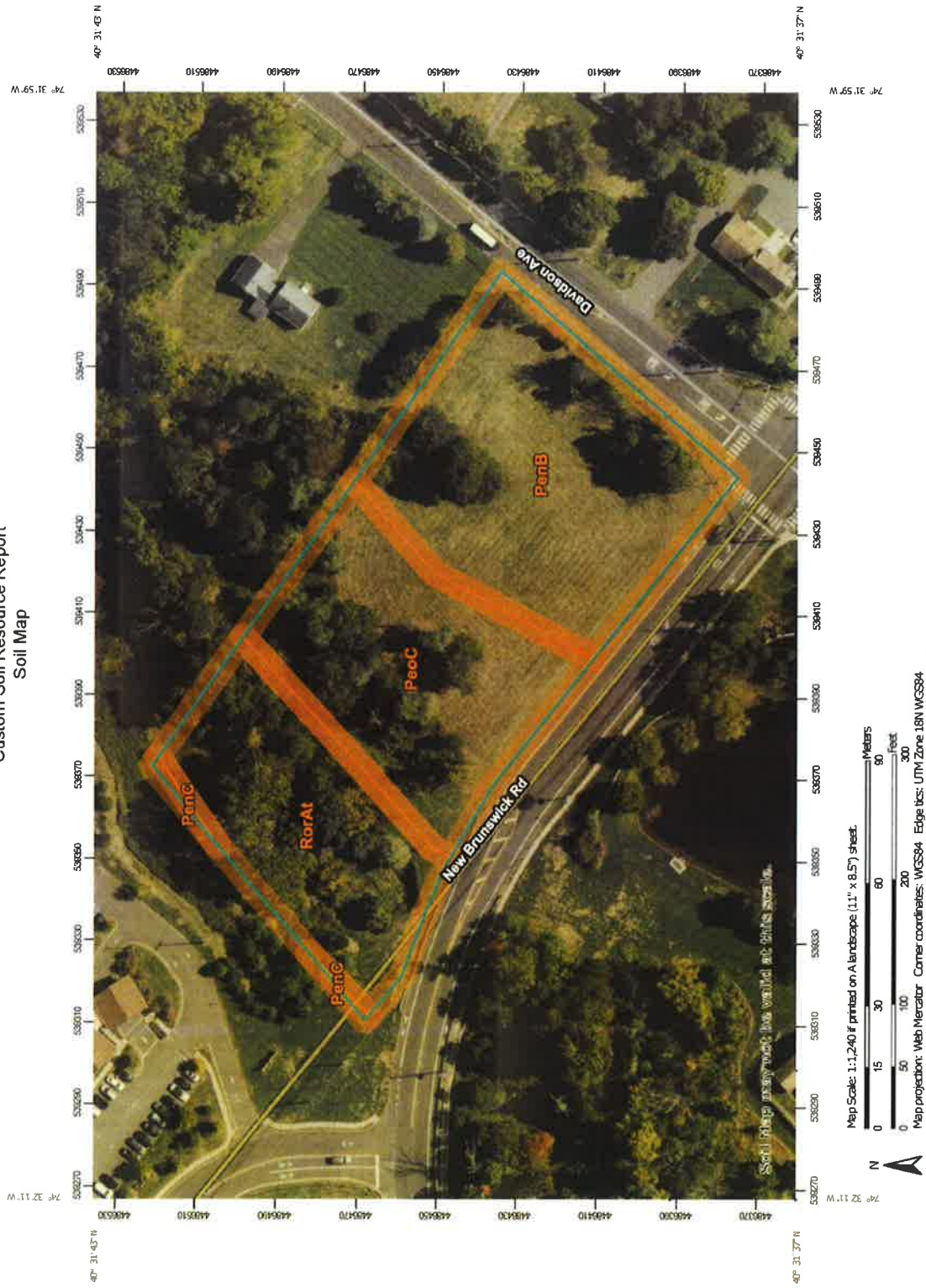


Table 1A- PRE DEVELOPMENT PEAK FLOW COMPUTATIONS AND DETERMINATION OF ALLOWED PEAK FLOW UPON NEW DEVELOPMENT ON THE SITE (WHERE CFS MEANS CUBIC FEET PER SECOND)

Storm Frequency - Years	(B) Peak Flow (Pre Development) - CFS		% of Peak Flow Reduction For Rule Compliance	Maximum Peak Flow Allowed - CFS (B - C) + D
2	1.1		50.00%	0.6
10	2.8		75.00%	2.1
100	8		80.00%	6.4

Table 1B -POST DEVELOPMENT PEAK FLOW COMPUTATIONS FROM THE DEVELOPMENT ON SITE (WHERE CFS MEANS CUBIC FEET PER SECOND)

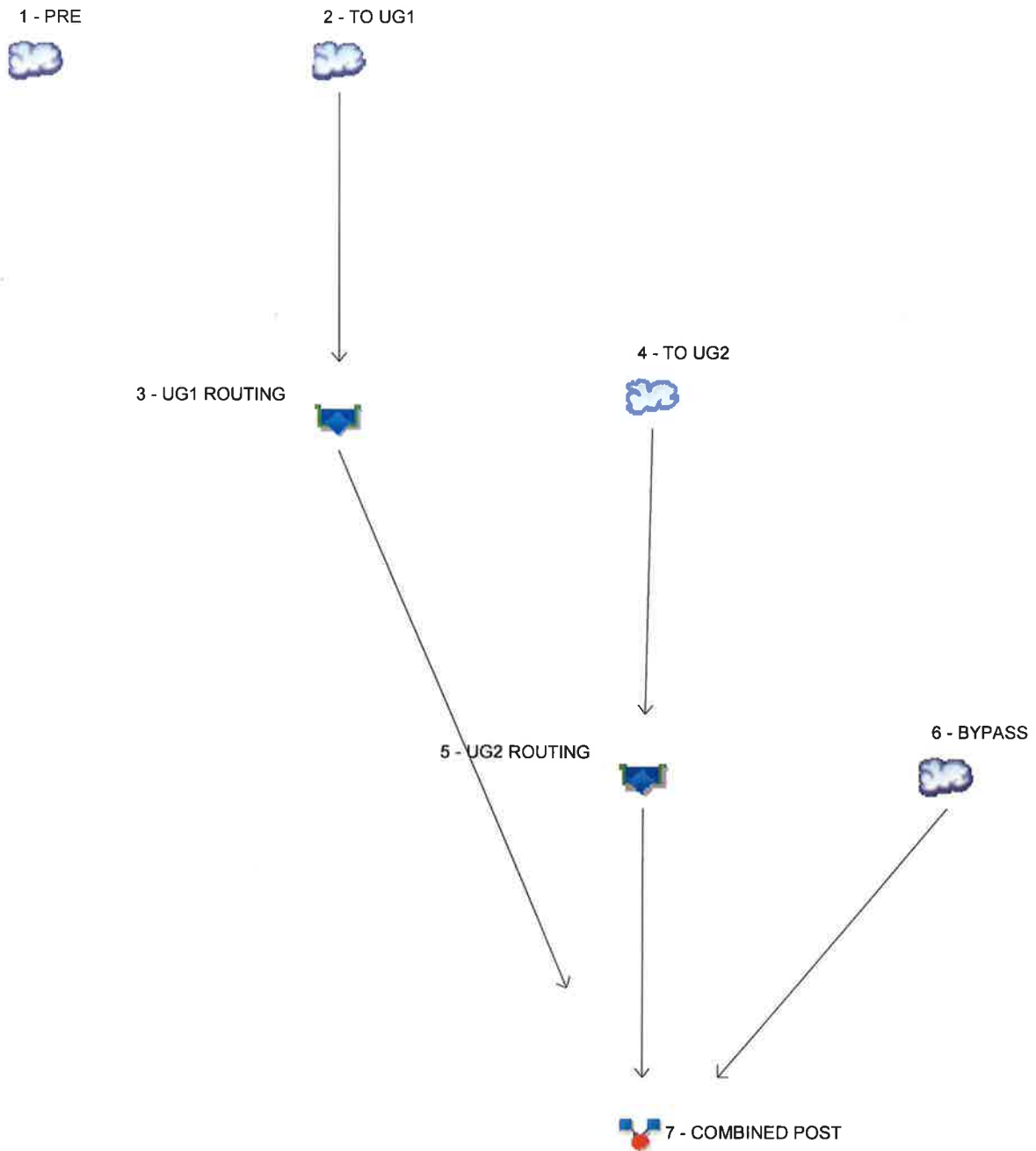
Storm Frequency - Years	Post Development Peak Flows - CFS	Maximum Peak Flow Allowed - CFS	Peak Flow Reduction Criteria Complied
2	0.5	0.6	YES
10	1.9	2.1	YES
100	6.4	6.4	YES

APPENDIX A:

**PRE AND POST DEVELOPMENT RUNOFF CURVE NUMBER, TIME OF CONCENTRATION
COMPUTATIONS AND STORM HYDROGRAPHS**

Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024



Legend

Hyd. Origin	Description
1	SCS Runoff PRE
2	SCS Runoff TO UG1
3	Reservoir UG1 ROUTING
4	SCS Runoff TO UG2
5	Reservoir UG2 ROUTING
6	SCS Runoff BYPASS
7	Combine COMBINED POST

Hydrograph Return Period Recap

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Hyd. No.	Hydrograph type (origin)	Inflow hyd(s)	Peak Outflow (cfs)								Hydrograph Description
			1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	
1	SCS Runoff	-----	-----	1.076	-----	-----	2.835	2.687	-----	7.993	PRE
2	SCS Runoff	-----	-----	1.247	-----	-----	2.228	2.151	-----	4.775	TO UG1
3	Reservoir	2	-----	0.184	-----	-----	1.185	1.123	-----	4.481	UG1 ROUTING
4	SCS Runoff	-----	-----	0.806	-----	-----	1.409	1.362	-----	2.988	TO UG2
5	Reservoir	4	-----	0.146	-----	-----	0.208	0.204	-----	1.366	UG2 ROUTING
6	SCS Runoff	-----	-----	0.273	-----	-----	0.659	0.628	-----	1.736	BYPASS
7	Combine	3, 5, 6	-----	0.533	-----	-----	1.878	1.781	-----	6.426	COMBINED POST

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

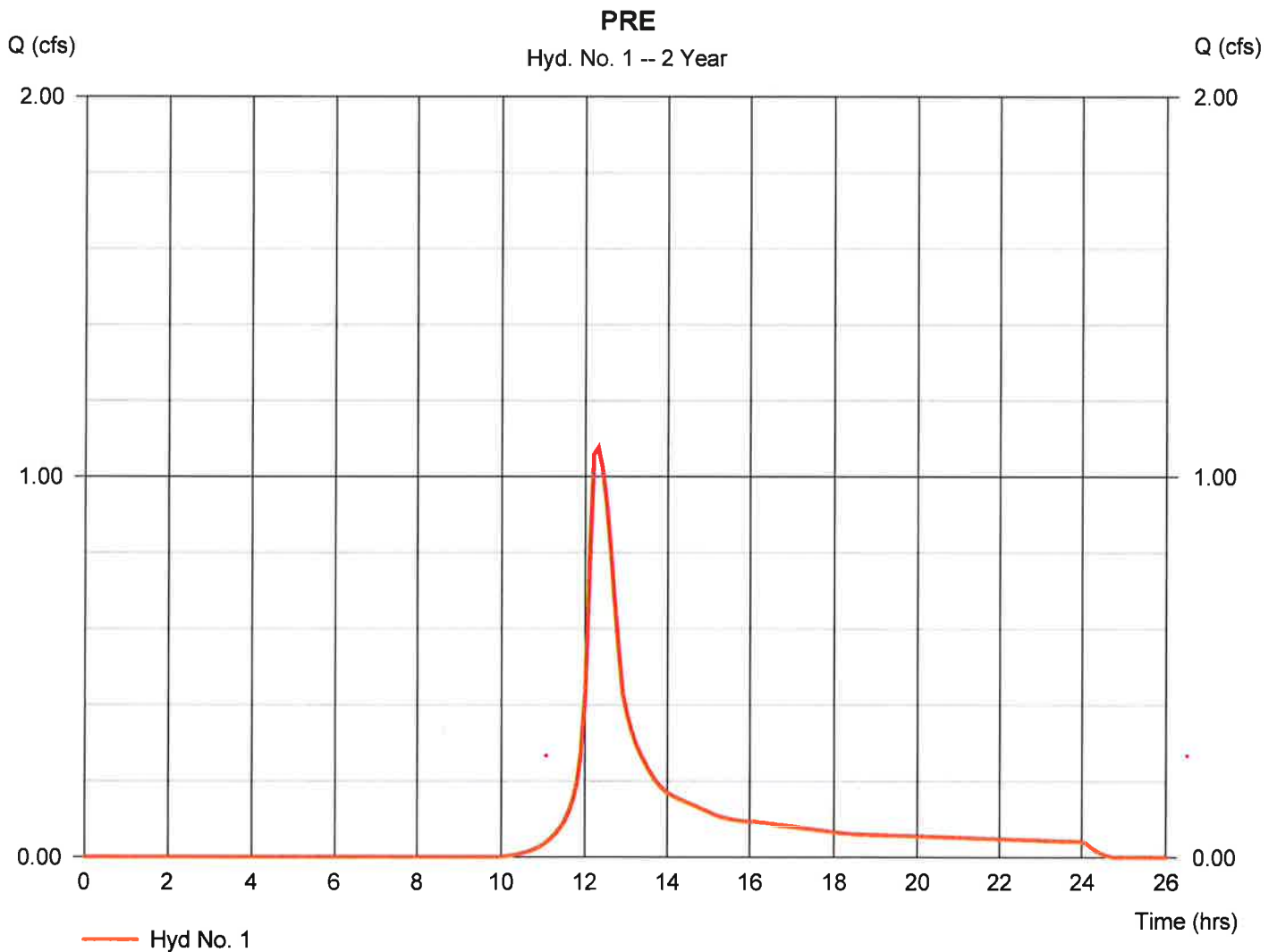
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.076	6	738	6,788	----	----	----	PRE
2	SCS Runoff	1.247	6	732	7,853	----	----	----	TO UG1
3	Reservoir	0.184	6	774	1,557	2	68.86	2,380	UG1 ROUTING
4	SCS Runoff	0.806	6	732	5,232	----	----	----	TO UG2
5	Reservoir	0.146	6	768	1,027	4	65.39	1,023	UG2 ROUTING
6	SCS Runoff	0.273	6	738	1,683	----	----	----	BYPASS
7	Combine	0.533	6	744	4,268	3, 5, 6	----	----	COMBINED POST
FRANK.gpw					Return Period: 2 Year			Thursday, 02 / 22 / 2024	

Hydrograph Report

Hyd. No. 1

PRE

Hydrograph type	= SCS Runoff	Peak discharge	= 1.076 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.30 hrs
Time interval	= 6 min	Hyd. volume	= 6,788 cuft
Drainage area	= 1.350 ac	Curve number	= 74
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 11.50 min
Total precip.	= 3.72 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285



TR55 Tc Worksheet

Hyd. No. 1

PRE

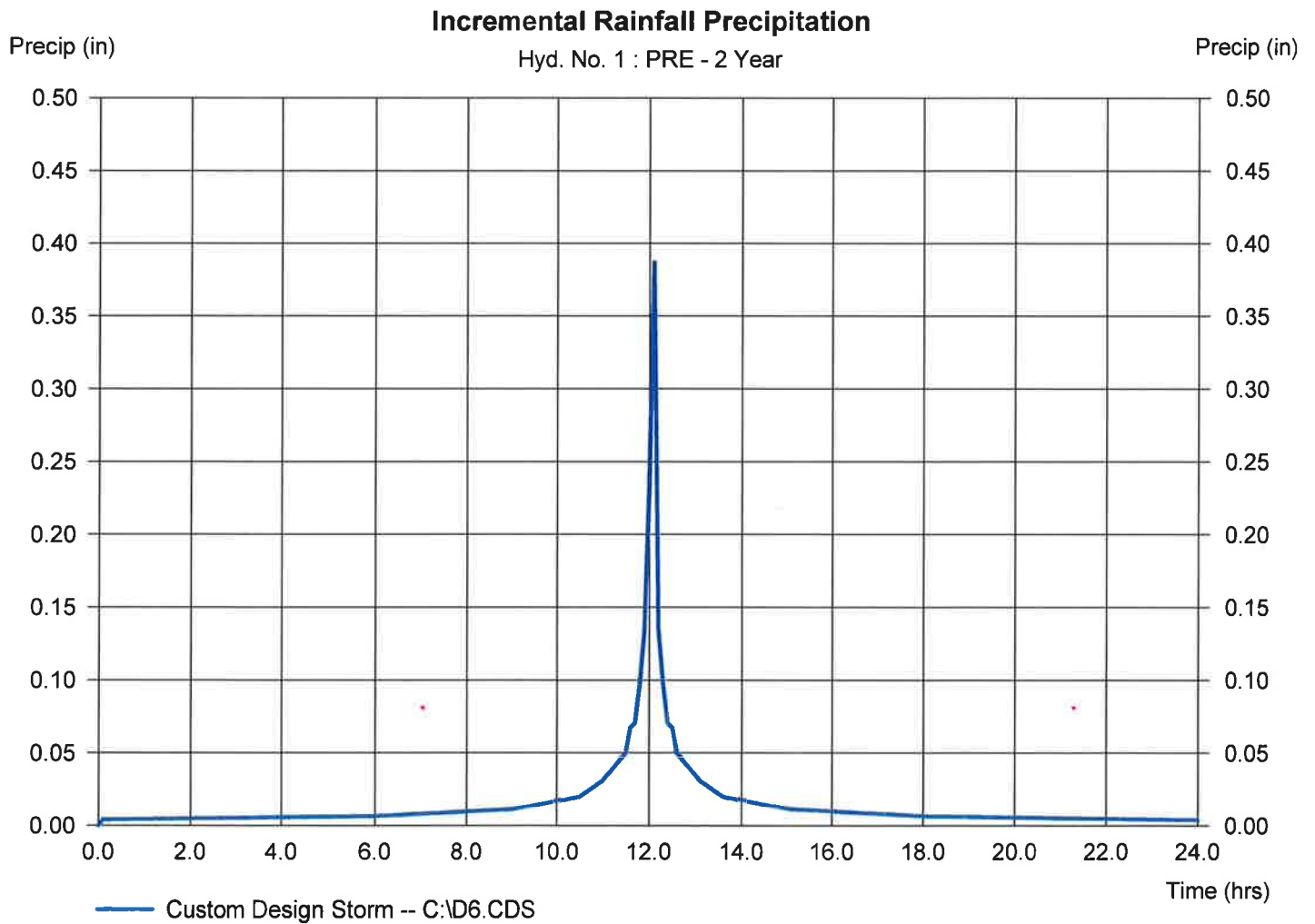
<u>Description</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>Totals</u>
Sheet Flow				
Manning's n-value	= 0.240	0.011	0.011	
Flow length (ft)	= 100.0	0.0	0.0	
Two-year 24-hr precip. (in)	= 3.35	0.00	0.00	
Land slope (%)	= 4.00	0.00	0.00	
Travel Time (min)	= 10.57	+ 0.00	+ 0.00	= 10.57
Shallow Concentrated Flow				
Flow length (ft)	= 200.00	0.00	0.00	
Watercourse slope (%)	= 5.10	0.00	0.00	
Surface description	= Unpaved	Paved	Paved	
Average velocity (ft/s)	=3.64	0.00	0.00	
Travel Time (min)	= 0.91	+ 0.00	+ 0.00	= 0.91
Channel Flow				
X sectional flow area (sqft)	= 0.00	0.00	0.00	
Wetted perimeter (ft)	= 0.00	0.00	0.00	
Channel slope (%)	= 0.00	0.00	0.00	
Manning's n-value	= 0.015	0.015	0.015	
Velocity (ft/s)	=0.00	0.00	0.00	
Flow length (ft)	({0})0.0	0.0	0.0	
Travel Time (min)	= 0.00	+ 0.00	+ 0.00	= 0.00
Total Travel Time, Tc				11.50 min

Precipitation Report

Hyd. No. 1

PRE

Storm Frequency	= 2 yrs	Time interval	= 6 min
Total precip.	= 3.7200 in	Distribution	= Custom
Storm duration	= C:\D6.CDS		



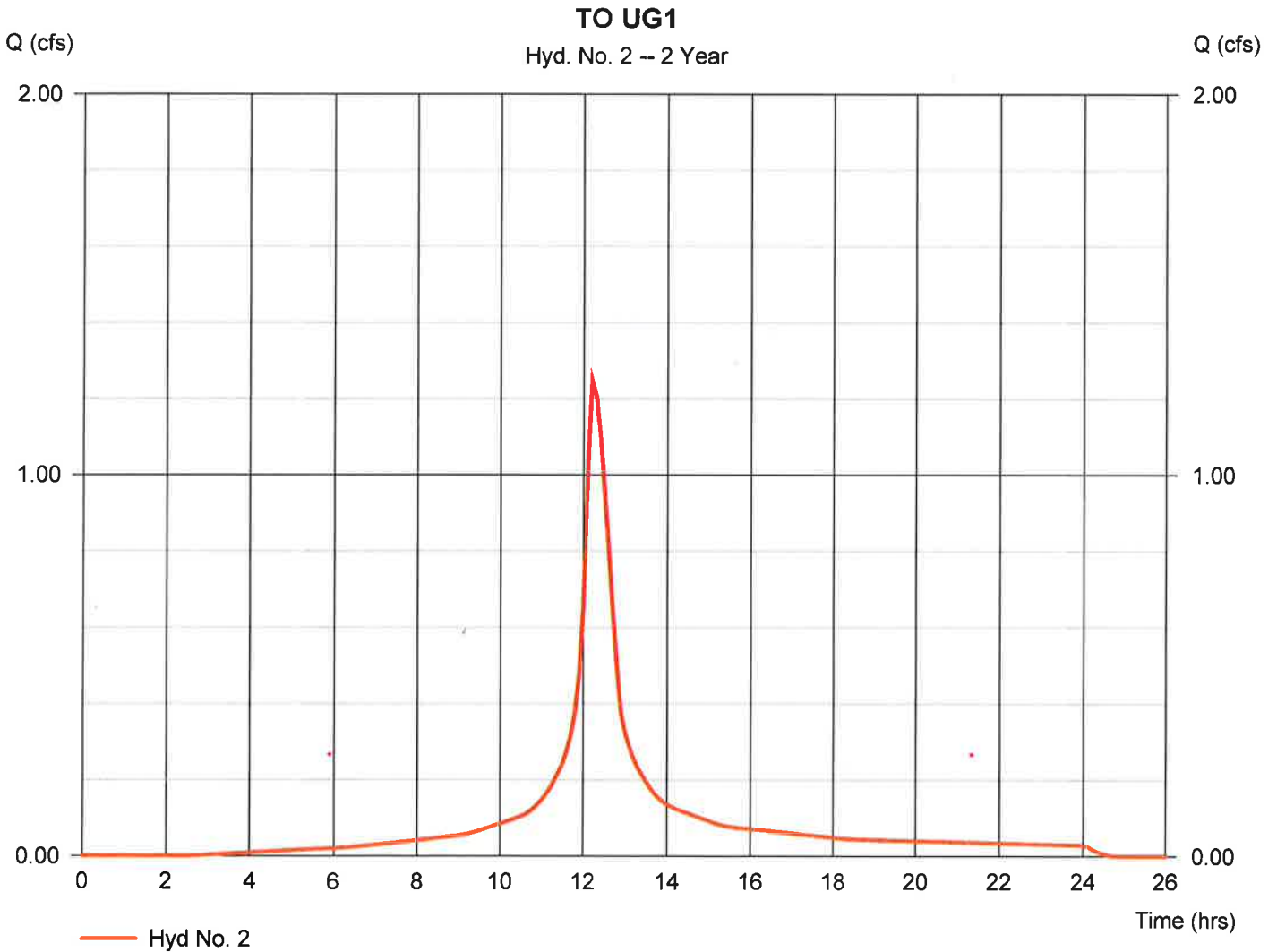
Hydrograph Report

Hyd. No. 2

TO UG1

Hydrograph type	= SCS Runoff	Peak discharge	= 1.247 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 7,853 cuft
Drainage area	= 0.690 ac	Curve number	= 95*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 3.72 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = [(0.100 x 74) + (0.590 x 98)] / 0.690

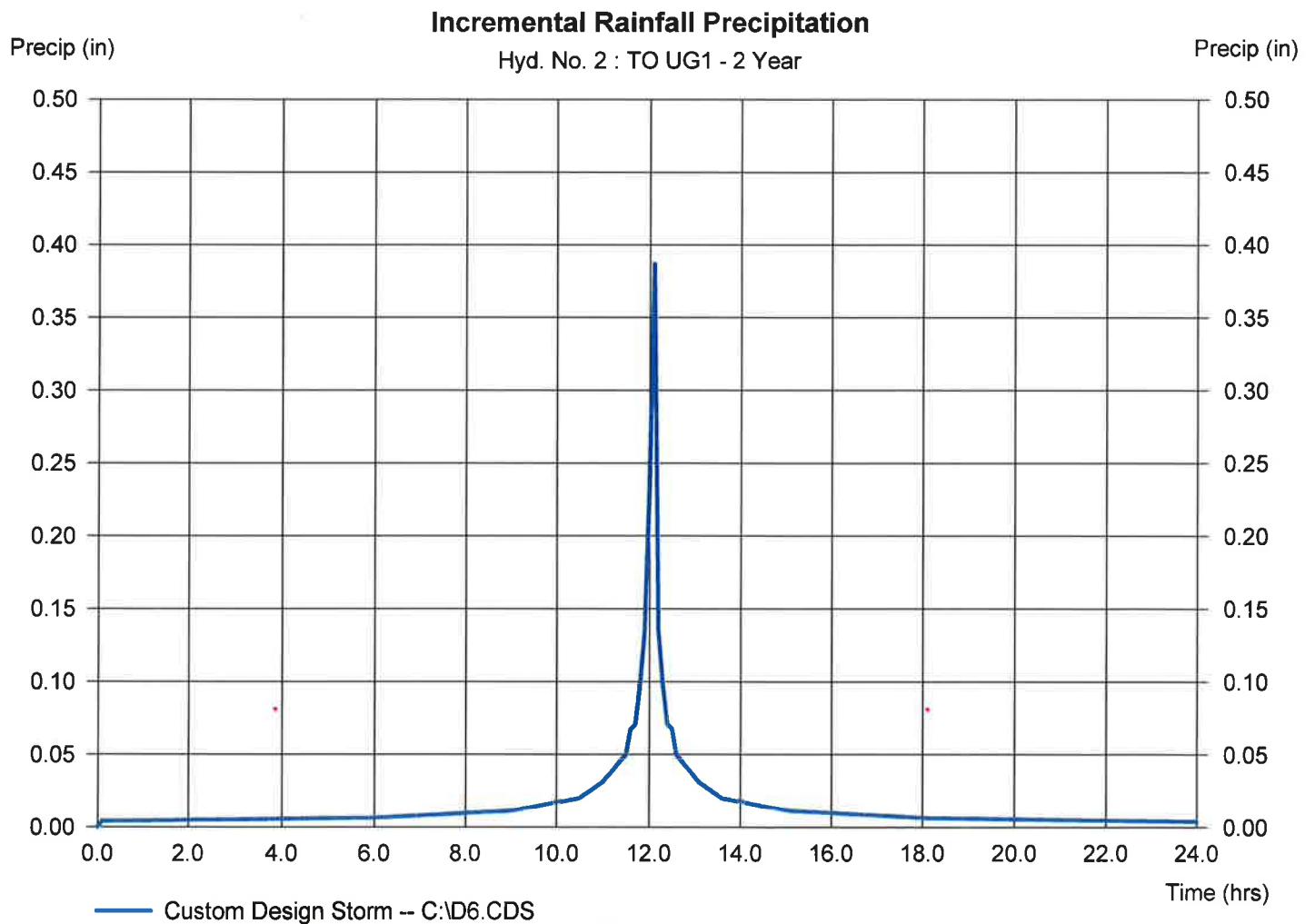


Precipitation Report

Hyd. No. 2

TO UG1

Storm Frequency	= 2 yrs	Time interval	= 6 min
Total precip.	= 3.7200 in	Distribution	= Custom
Storm duration	= C:\D6.CDS		



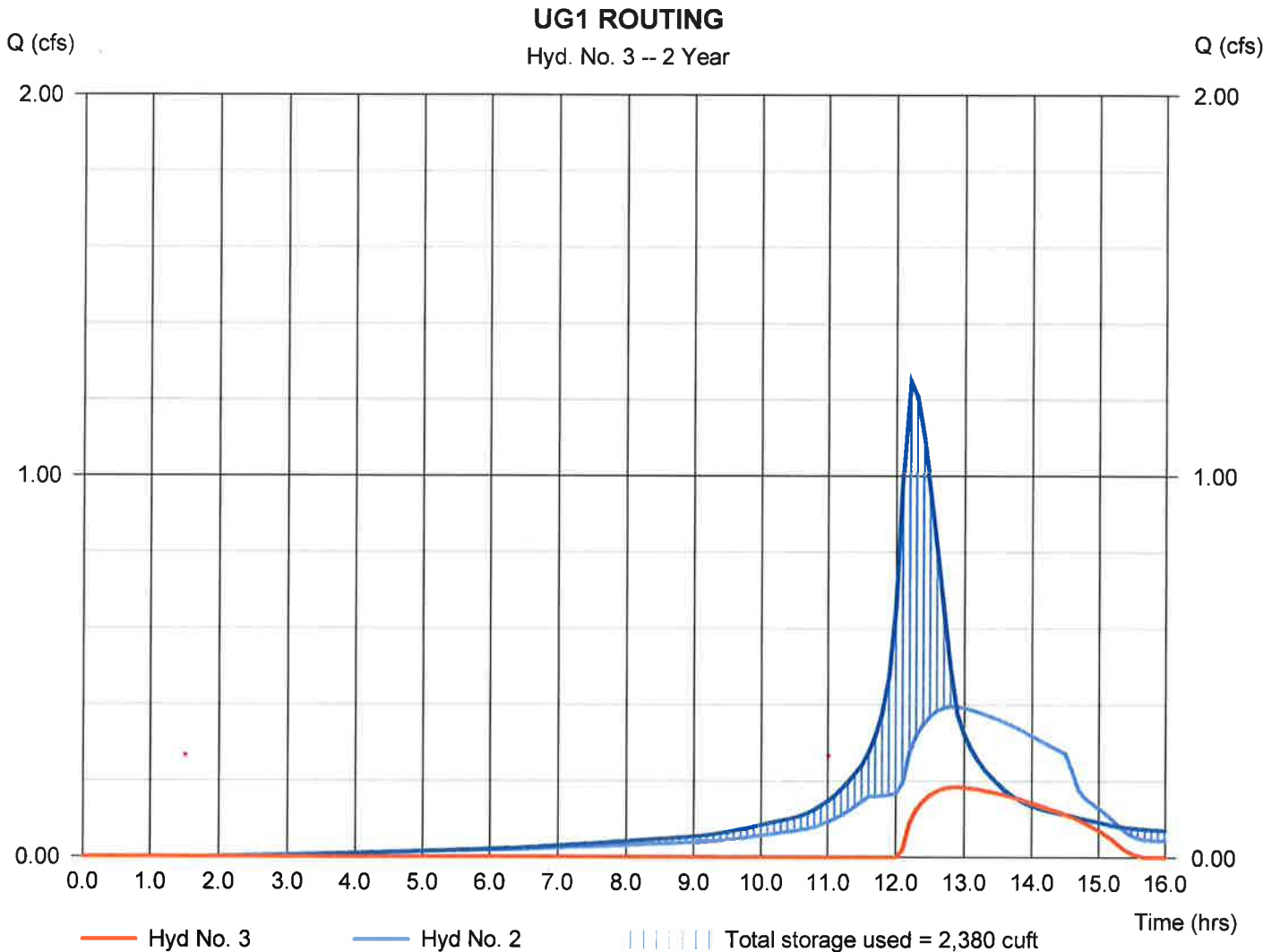
Hydrograph Report

Hyd. No. 3

UG1 ROUTING

Hydrograph type	= Reservoir	Peak discharge	= 0.184 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.90 hrs
Time interval	= 6 min	Hyd. volume	= 1,557 cuft
Inflow hyd. No.	= 2 - TO UG1	Max. Elevation	= 68.86 ft
Reservoir name	= UG1	Max. Storage	= 2,380 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Pond No. 1 - UG1

Pond Data

UG Chambers -Invert elev. = 67.50 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 80.00 ft, No. Barrels = 4, Slope = 0.00%, Headers = Yes

Encasement -Invert elev. = 66.50 ft, Width = 5.00 ft, Height = 5.00 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	66.50	n/a	0	0
0.50	67.00	n/a	360	360
1.00	67.50	n/a	360	720
1.50	68.00	n/a	527	1,247
2.00	68.50	n/a	639	1,886
2.50	69.00	n/a	678	2,564
3.00	69.50	n/a	678	3,242
3.50	70.00	n/a	638	3,881
4.00	70.50	n/a	527	4,408
4.50	71.00	n/a	360	4,768
5.00	71.50	n/a	360	5,128

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 2.50	7.00	0.00	0.00
Span (in)	= 2.50	7.00	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 67.50	69.00	0.00	0.00
Length (ft)	= 0.00	0.00	0.00	0.00
Slope (%)	= 0.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 3.50	0.00	0.00	0.00
Crest El. (ft)	= 70.50	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= Rect	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 3.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Civ A cfs	Civ B cfs	Civ C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	66.50	0.00	0.00	---	---	0.00	---	---	---	0.000	---	0.000
0.50	360	67.00	0.00	0.00	---	---	0.00	---	---	---	0.142	---	0.142
1.00	720	67.50	0.00 ic	0.00	---	---	0.00	---	---	---	0.165	---	0.165
1.50	1,247	68.00	0.10 ic	0.00	---	---	0.00	---	---	---	0.189	---	0.292
2.00	1,886	68.50	0.16 ic	0.00	---	---	0.00	---	---	---	0.212	---	0.368
2.50	2,564	69.00	0.19 ic	0.00 ic	---	---	0.00	---	---	---	0.236	---	0.430
3.00	3,242	69.50	0.23 ic	0.59 ic	---	---	0.00	---	---	---	0.260	---	1.074
3.50	3,881	70.00	0.25 ic	1.08 ic	---	---	0.00	---	---	---	0.283	---	1.621
4.00	4,408	70.50	0.28 ic	1.41 ic	---	---	0.00	---	---	---	0.307	---	2.001
4.50	4,768	71.00	0.30 ic	1.68 ic	---	---	4.13	---	---	---	0.331	---	6.445
5.00	5,128	71.50	0.32 ic	1.91 ic	---	---	11.67	---	---	---	0.354	---	14.26

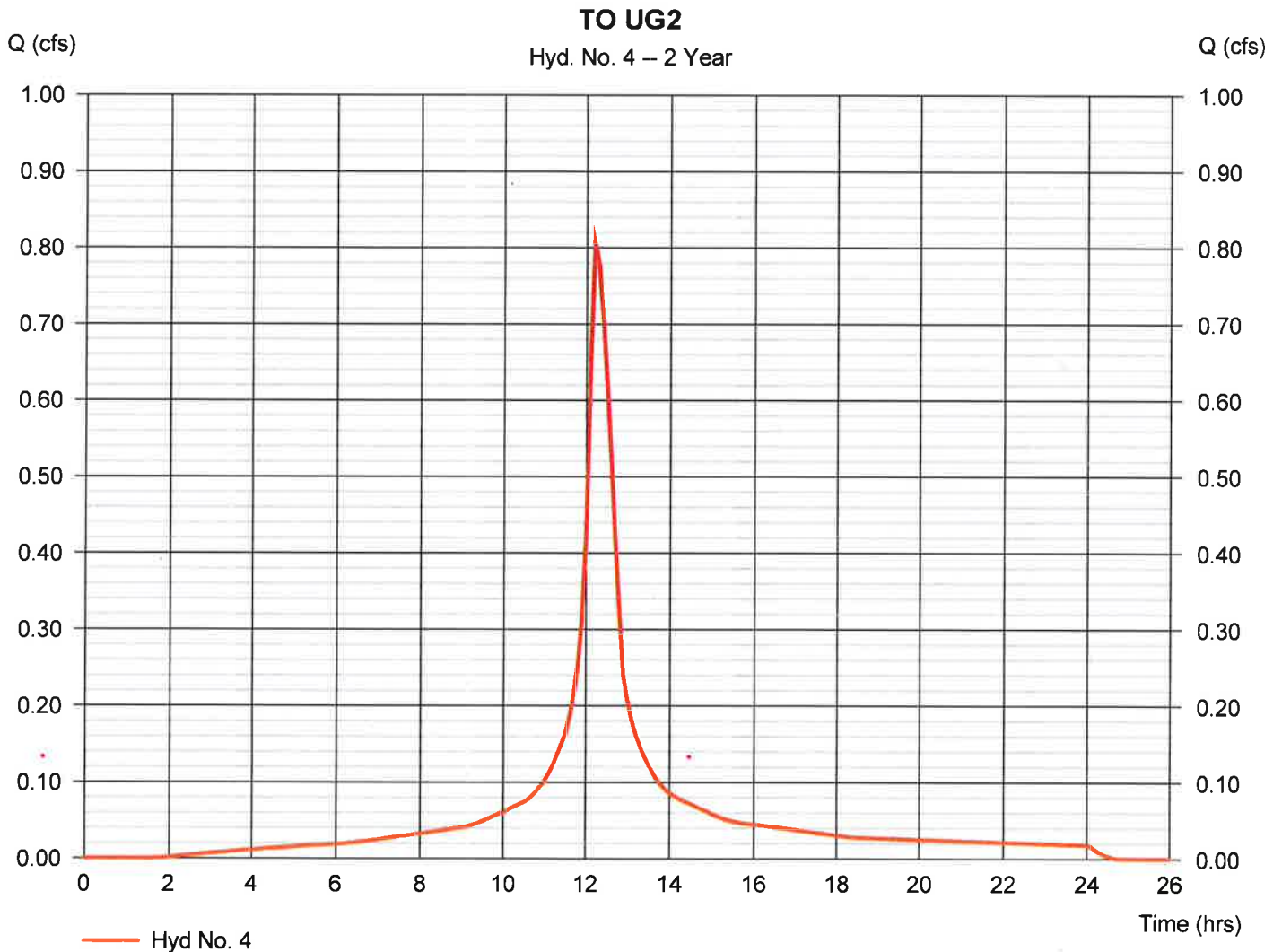
Hydrograph Report

Hyd. No. 4

TO UG2

Hydrograph type	= SCS Runoff	Peak discharge	= 0.806 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 5,232 cuft
Drainage area	= 0.430 ac	Curve number	= 97*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 3.72 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = $[(0.010 \times 74) + (0.420 \times 98)] / 0.430$

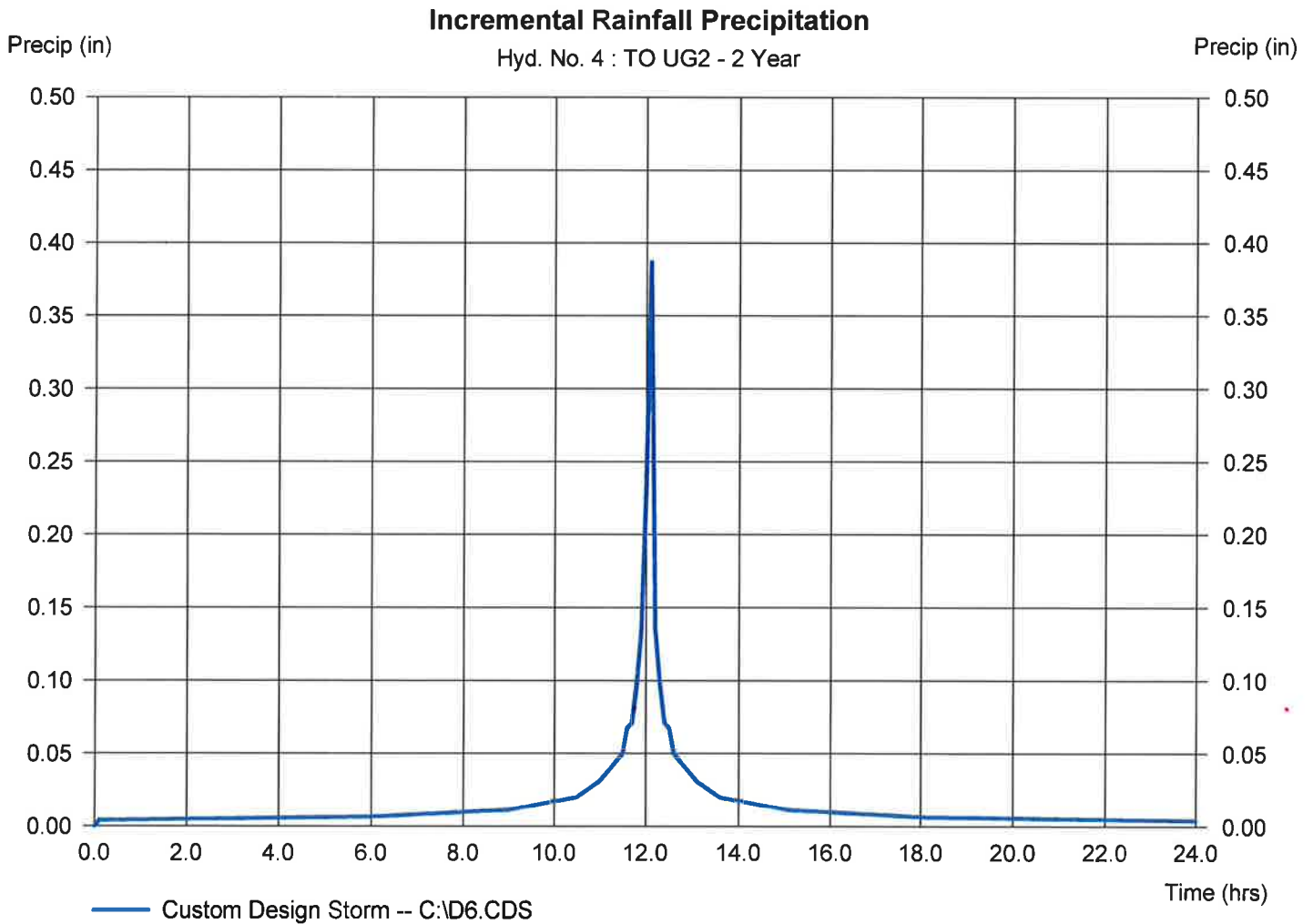


Precipitation Report

Hyd. No. 4

TO UG2

Storm Frequency	= 2 yrs	Time interval	= 6 min
Total precip.	= 3.7200 in	Distribution	= Custom
Storm duration	= C:\D6.CDS		



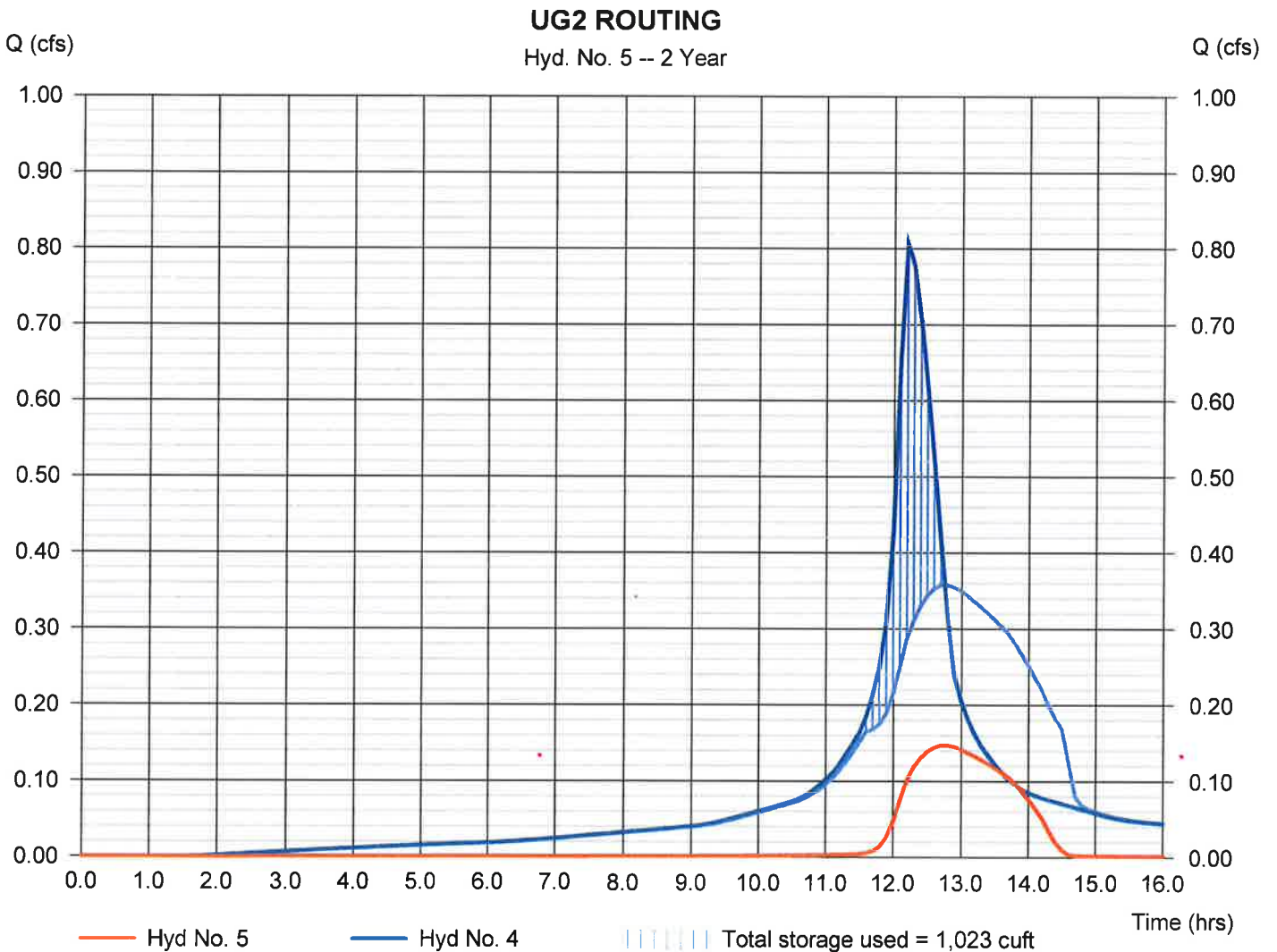
Hydrograph Report

Hyd. No. 5

UG2 ROUTING

Hydrograph type	= Reservoir	Peak discharge	= 0.146 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.80 hrs
Time interval	= 6 min	Hyd. volume	= 1,027 cuft
Inflow hyd. No.	= 4 - TO UG2	Max. Elevation	= 65.39 ft
Reservoir name	= UG2	Max. Storage	= 1,023 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Pond Report

Pond No. 3 - UG2

Pond Data

UG Chambers -Invert elev. = 65.00 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 85.00 ft, No. Barrels = 5, Slope = 0.00%, Headers = Yes
Encasement -Invert elev. = 64.50 ft, Width = 5.00 ft, Height = 5.00 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	64.50	n/a	0	0
0.50	65.00	n/a	475	475
1.00	65.50	n/a	696	1,171
1.50	66.00	n/a	843	2,013
2.00	66.50	n/a	895	2,908
2.50	67.00	n/a	895	3,803
3.00	67.50	n/a	842	4,645
3.50	68.00	n/a	696	5,341
4.00	68.50	n/a	475	5,816
4.50	69.00	n/a	475	6,291
5.00	69.50	n/a	475	6,766

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 2.50	0.00	0.00	0.00
Span (in)	= 2.50	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 64.50	0.00	0.00	0.00
Length (ft)	= 0.00	0.00	0.00	0.00
Slope (%)	= 0.00	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 3.50	0.00	0.00	0.00
Crest El. (ft)	= 68.50	0.00	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= Rect	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 3.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Civ A cfs	Civ B cfs	Civ C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	64.50	0.00	---	---	---	0.00	---	---	---	0.000	---	0.000
0.50	475	65.00	0.10 ic	---	---	---	0.00	---	---	---	0.187	---	0.291
1.00	1,171	65.50	0.16 ic	---	---	---	0.00	---	---	---	0.219	---	0.374
1.50	2,013	66.00	0.19 ic	---	---	---	0.00	---	---	---	0.250	---	0.444
2.00	2,908	66.50	0.23 ic	---	---	---	0.00	---	---	---	0.281	---	0.507
2.50	3,803	67.00	0.25 ic	---	---	---	0.00	---	---	---	0.312	---	0.567
3.00	4,645	67.50	0.28 ic	---	---	---	0.00	---	---	---	0.344	---	0.623
3.50	5,341	68.00	0.30 ic	---	---	---	0.00	---	---	---	0.375	---	0.677
4.00	5,816	68.50	0.32 ic	---	---	---	0.00	---	---	---	0.406	---	0.730
4.50	6,291	69.00	0.34 ic	---	---	---	4.13	---	---	---	0.438	---	4.912
5.00	6,766	69.50	0.36 ic	---	---	---	11.67	---	---	---	0.469	---	12.50

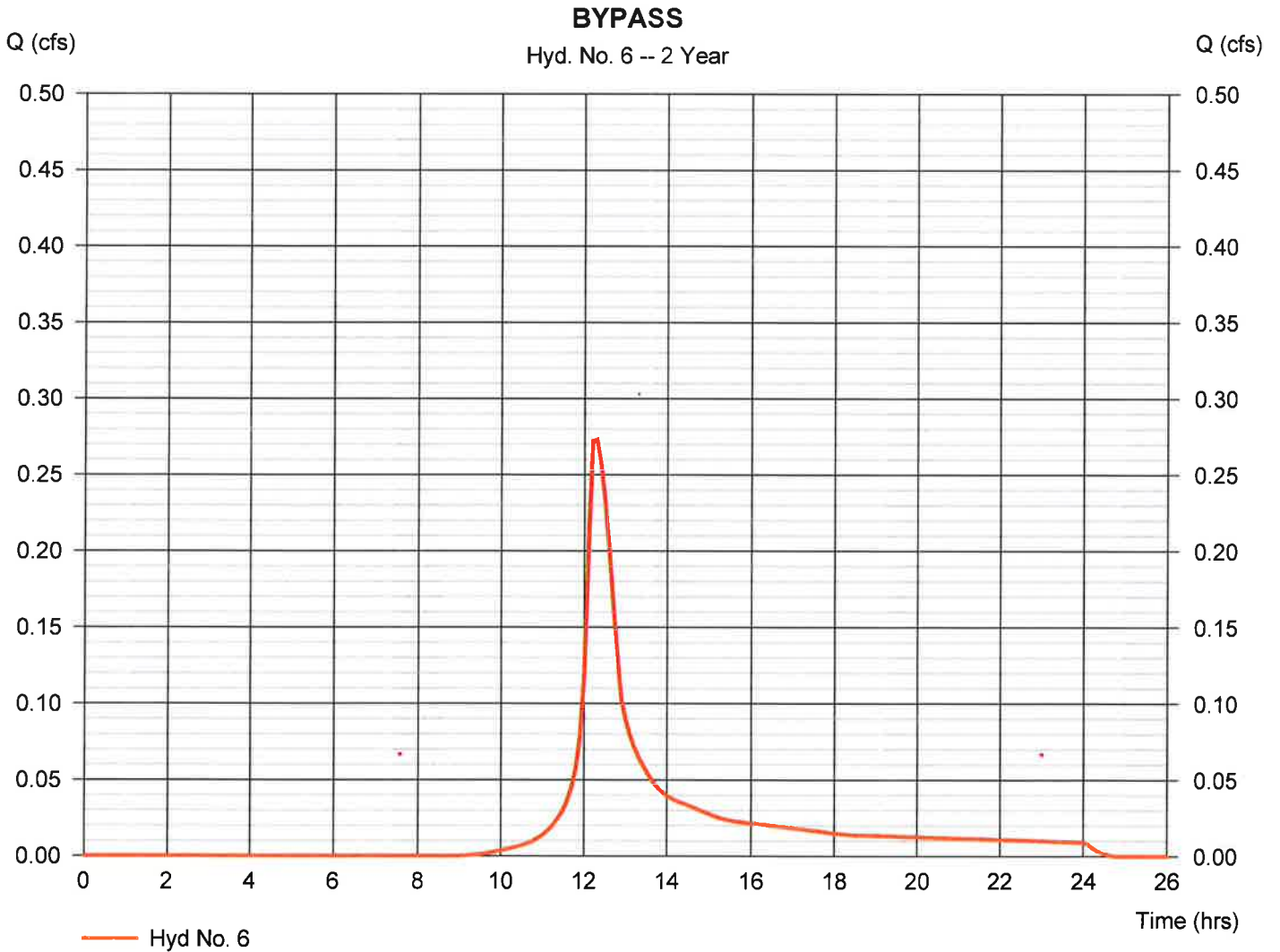
Hydrograph Report

Hyd. No. 6

BYPASS

Hydrograph type	= SCS Runoff	Peak discharge	= 0.273 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.30 hrs
Time interval	= 6 min	Hyd. volume	= 1,683 cuft
Drainage area	= 0.280 ac	Curve number	= 78*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 3.72 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = [(0.050 x 98) + (0.230 x 74)] / 0.280

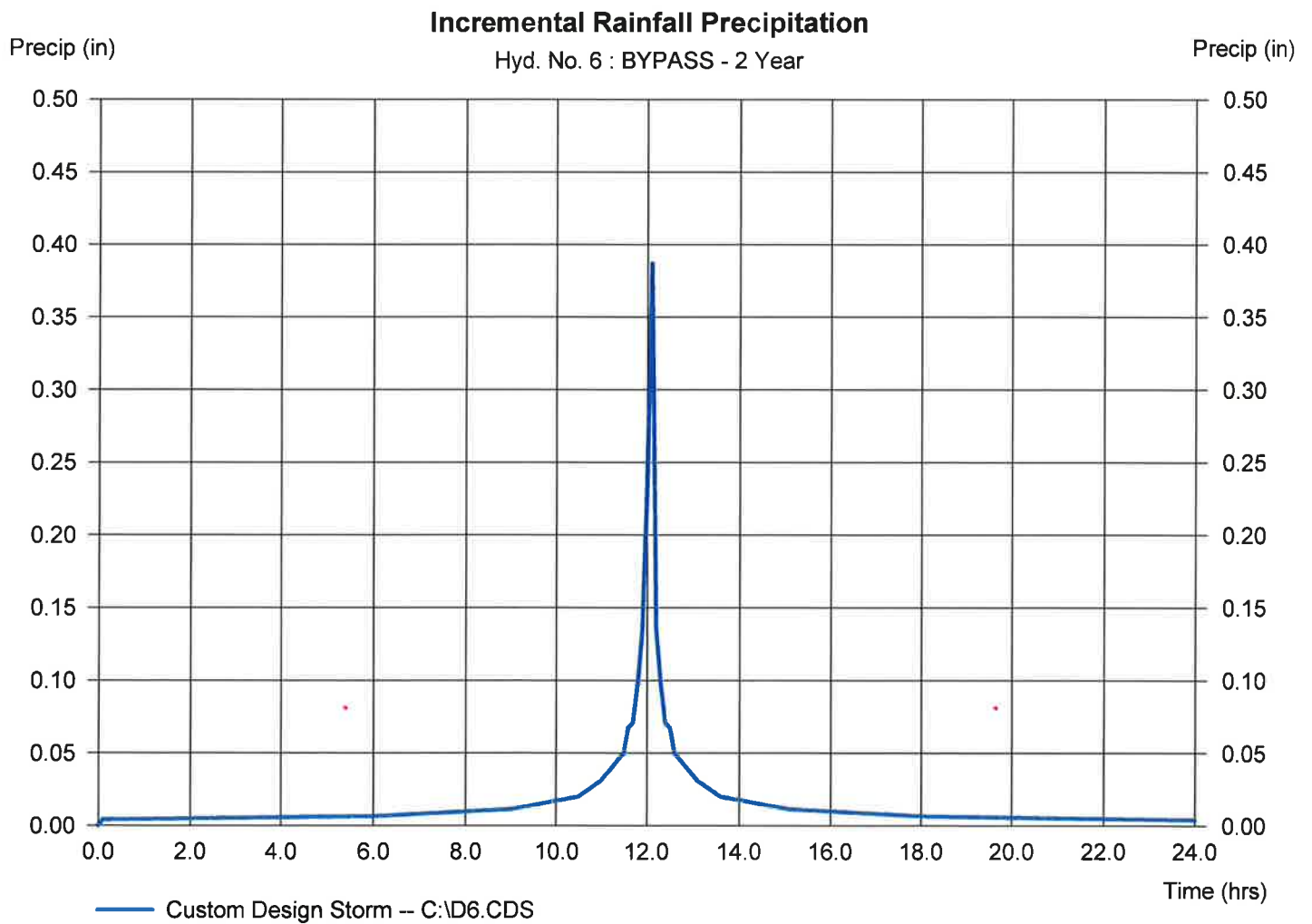


Precipitation Report

Hyd. No. 6

BYPASS

Storm Frequency	= 2 yrs	Time interval	= 6 min
Total precip.	= 3.7200 in	Distribution	= Custom
Storm duration	= C:\D6.CDS		



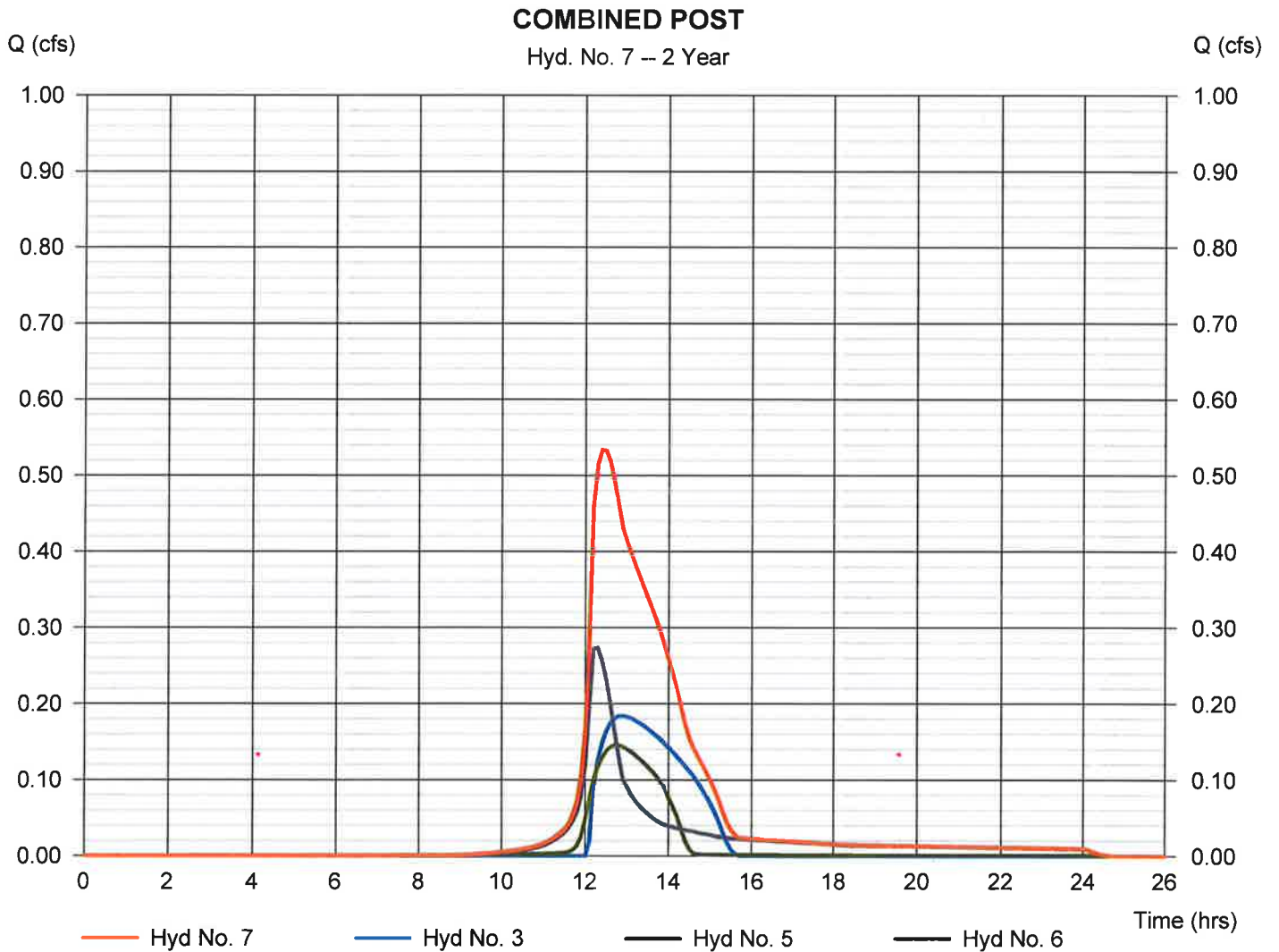
Hydrograph Report

Hyd. No. 7

COMBINED POST

Hydrograph type = Combine
Storm frequency = 2 yrs
Time interval = 6 min
Inflow hyds. = 3, 5, 6

Peak discharge = 0.533 cfs
Time to peak = 12.40 hrs
Hyd. volume = 4,268 cuft
Contrib. drain. area = 0.280 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

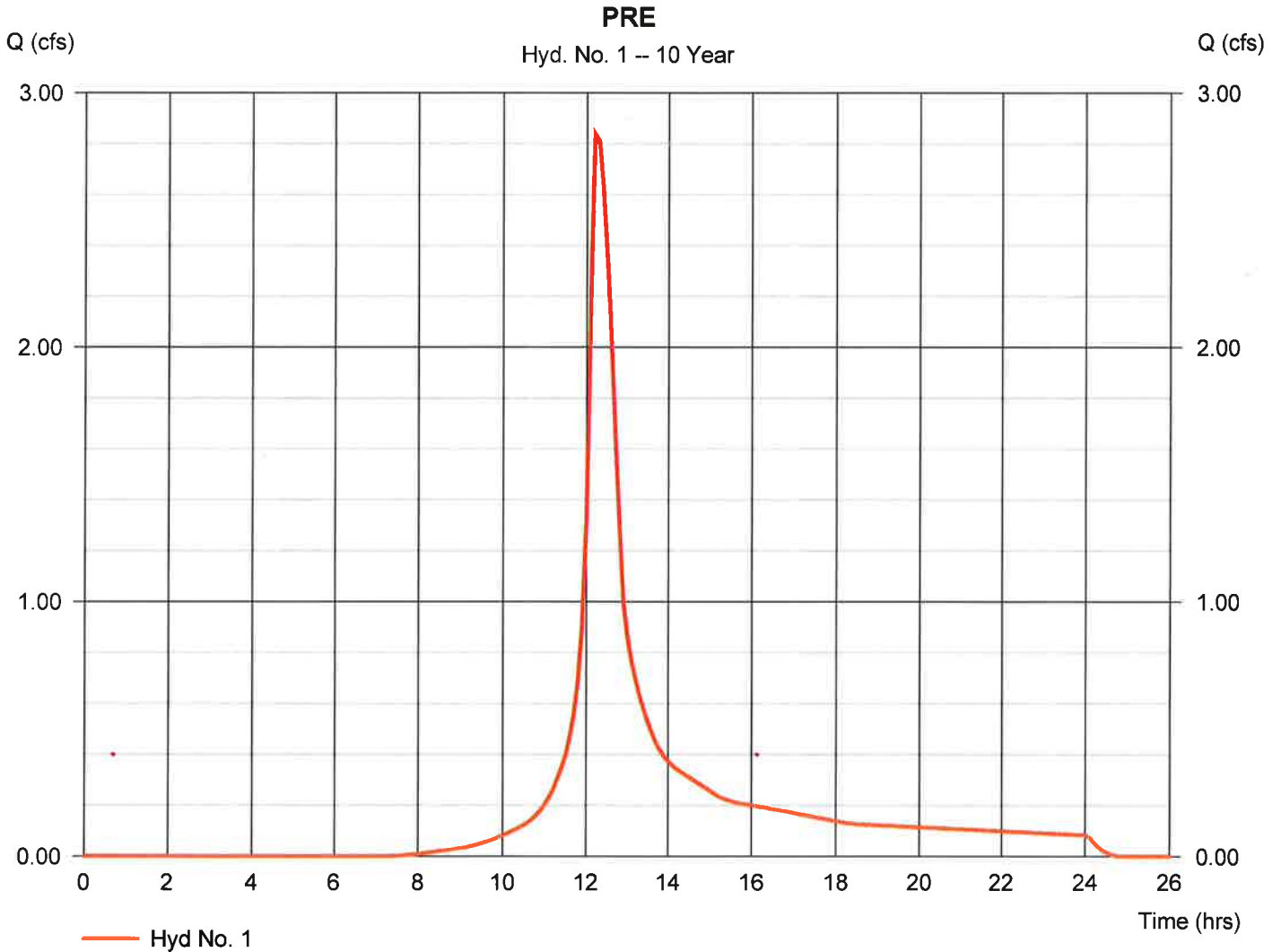
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	2.835	6	732	17,160	-----	-----	-----	PRE	
2	SCS Runoff	2.228	6	732	14,458	-----	-----	-----	TO UG1	
3	Reservoir	1.185	6	756	5,236	2	69.83	3,658	UG1 ROUTING	
4	SCS Runoff	1.409	6	732	9,373	-----	-----	-----	TO UG2	
5	Reservoir	0.208	6	774	2,416	4	66.21	2,396	UG2 ROUTING	
6	SCS Runoff	0.659	6	732	3,974	-----	-----	-----	BYPASS	
7	Combine	1.878	6	750	11,626	3, 5, 6	-----	-----	COMBINED POST	
FRANK.gpw					Return Period: 10 Year			Thursday, 02 / 22 / 2024		

Hydrograph Report

Hyd. No. 1

PRE

Hydrograph type	= SCS Runoff	Peak discharge	= 2.835 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 17,160 cuft
Drainage area	= 1.350 ac	Curve number	= 74
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 11.50 min
Total precip.	= 6.40 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285



Precipitation Report

Hyd. No. 1

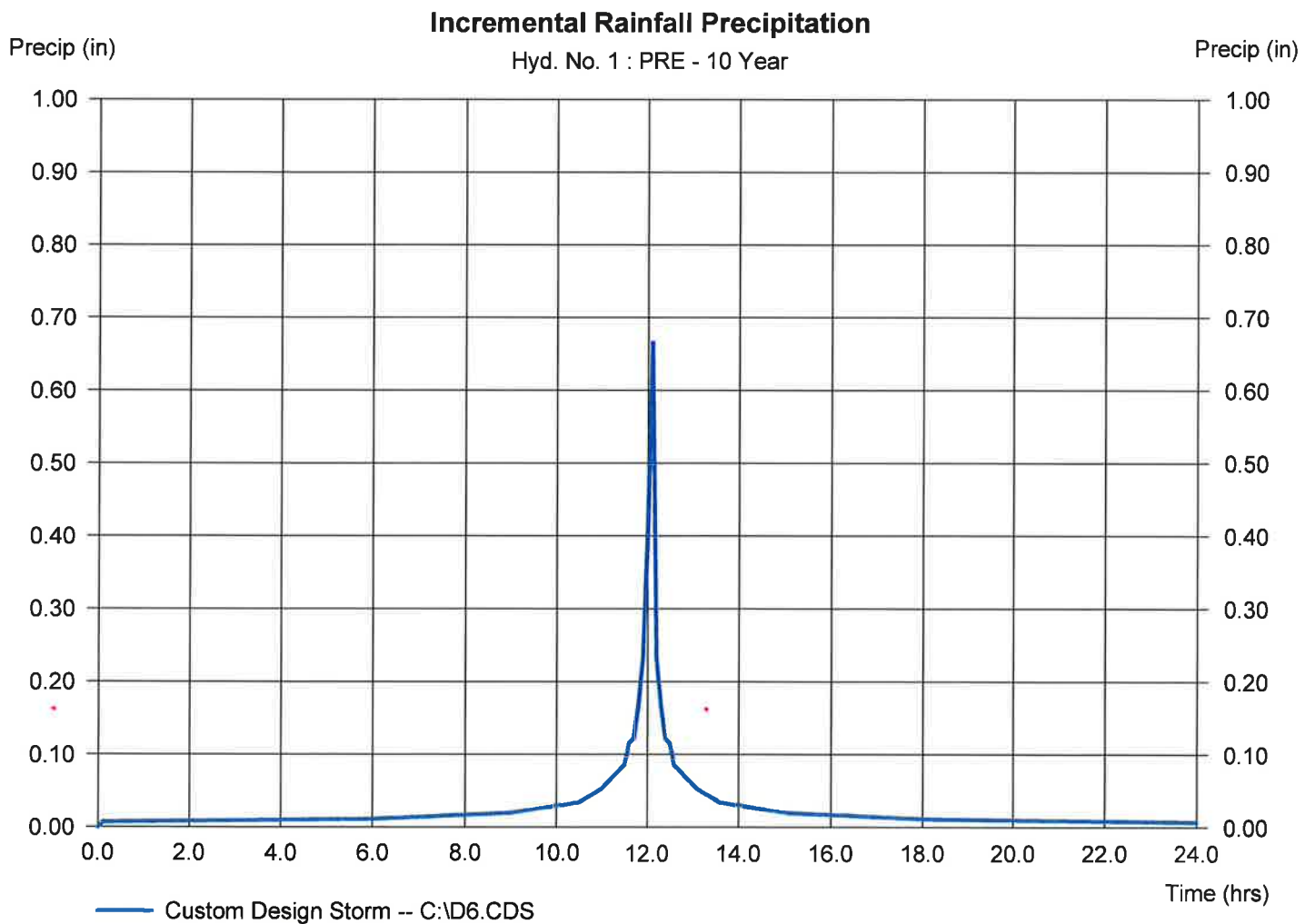
PRE

Storm Frequency
Total precip.
Storm duration

= 10 yrs
= 6.4000 in
= C:\D6.CDS

Time interval
Distribution

= 6 min
= Custom



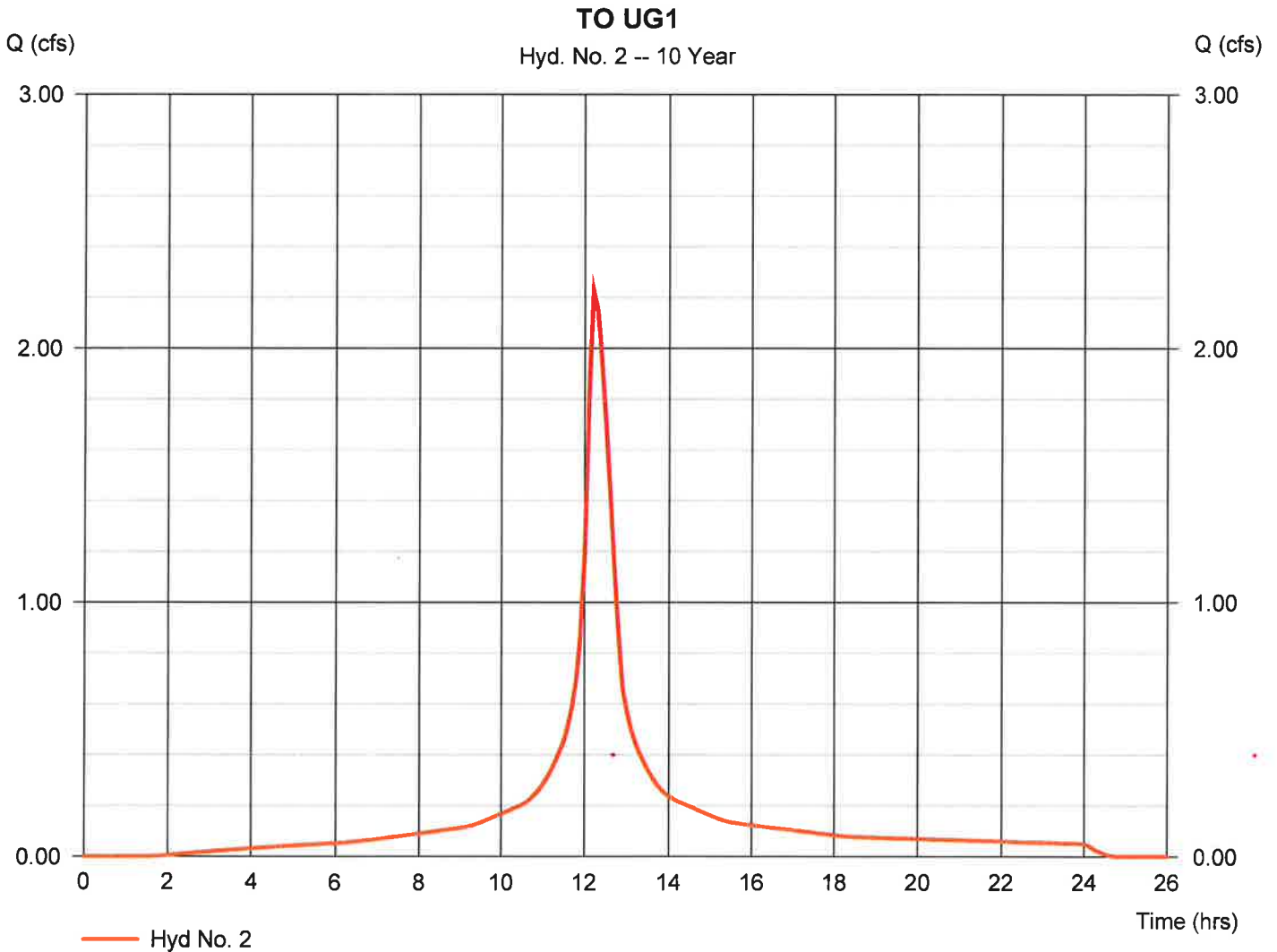
Hydrograph Report

Hyd. No. 2

TO UG1

Hydrograph type	= SCS Runoff	Peak discharge	= 2.228 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 14,458 cuft
Drainage area	= 0.690 ac	Curve number	= 95*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 6.40 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = $[(0.100 \times 74) + (0.590 \times 98)] / 0.690$



Precipitation Report

Hyd. No. 2

TO UG1

Storm Frequency
Total precip.
Storm duration

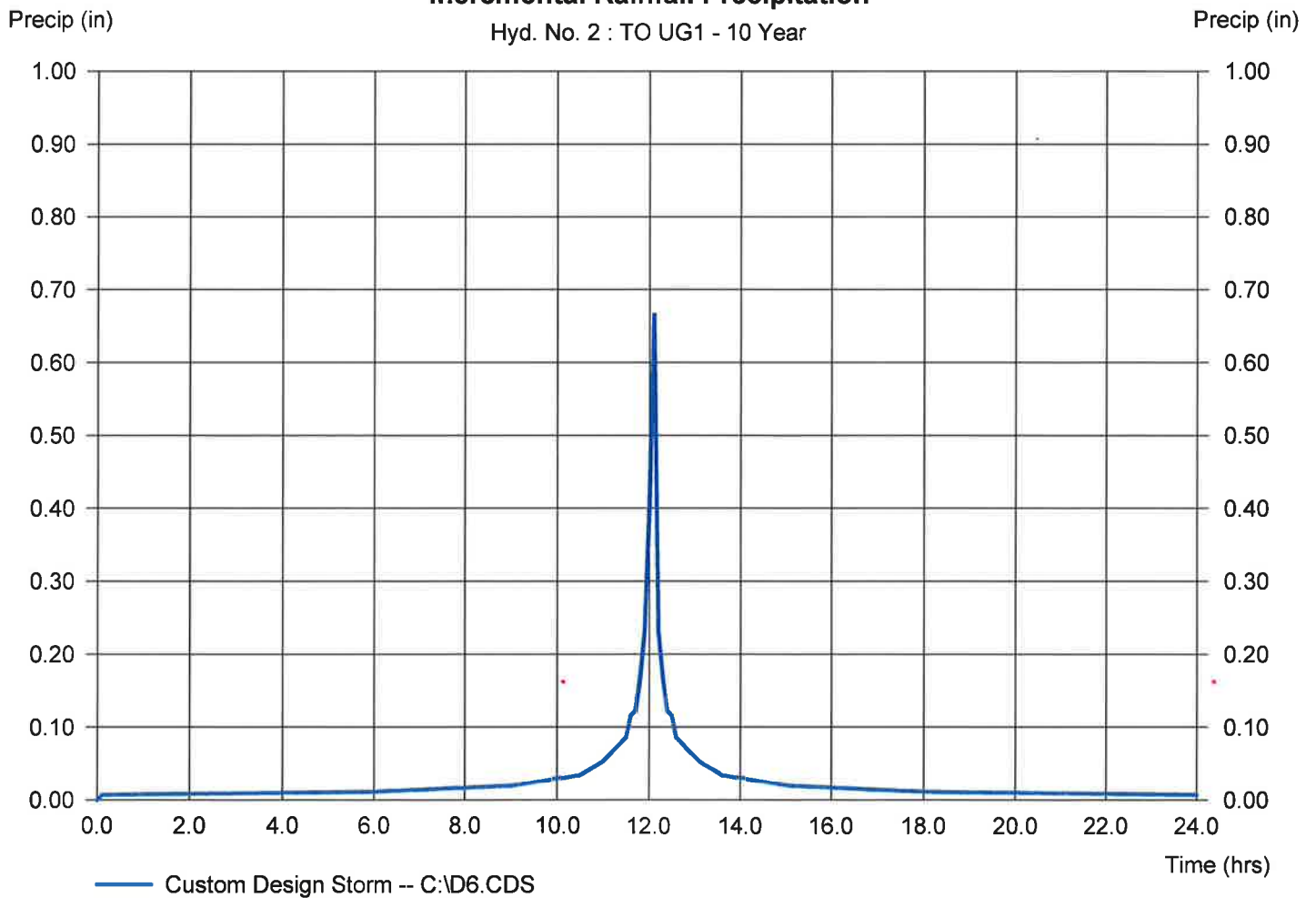
= 10 yrs
= 6.4000 in
= C:\D6.CDS

Time interval
Distribution

= 6 min
= Custom

Incremental Rainfall Precipitation

Hyd. No. 2 : TO UG1 - 10 Year



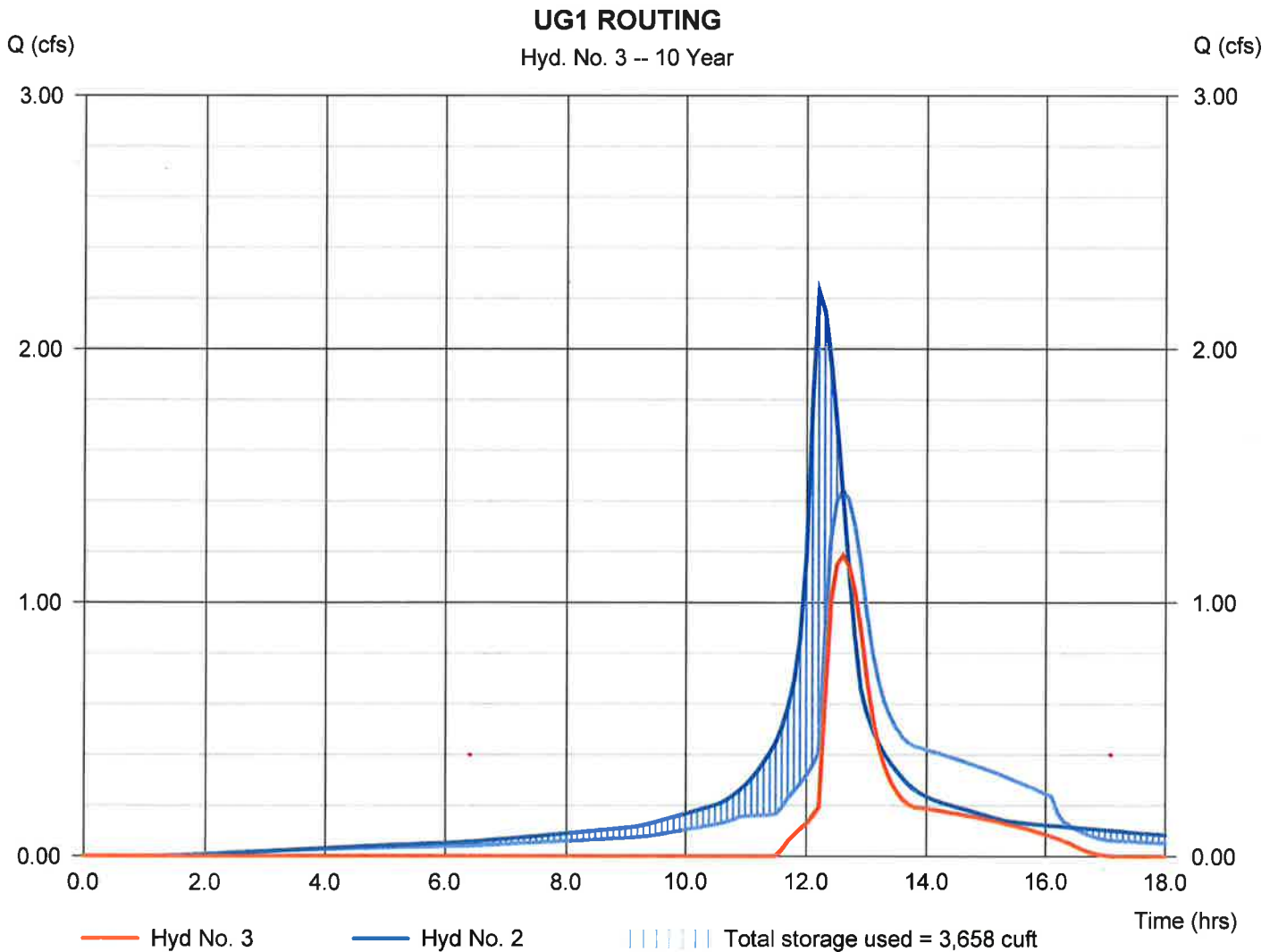
Hydrograph Report

Hyd. No. 3

UG1 ROUTING

Hydrograph type	= Reservoir	Peak discharge	= 1.185 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.60 hrs
Time interval	= 6 min	Hyd. volume	= 5,236 cuft
Inflow hyd. No.	= 2 - TO UG1	Max. Elevation	= 69.83 ft
Reservoir name	= UG1	Max. Storage	= 3,658 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



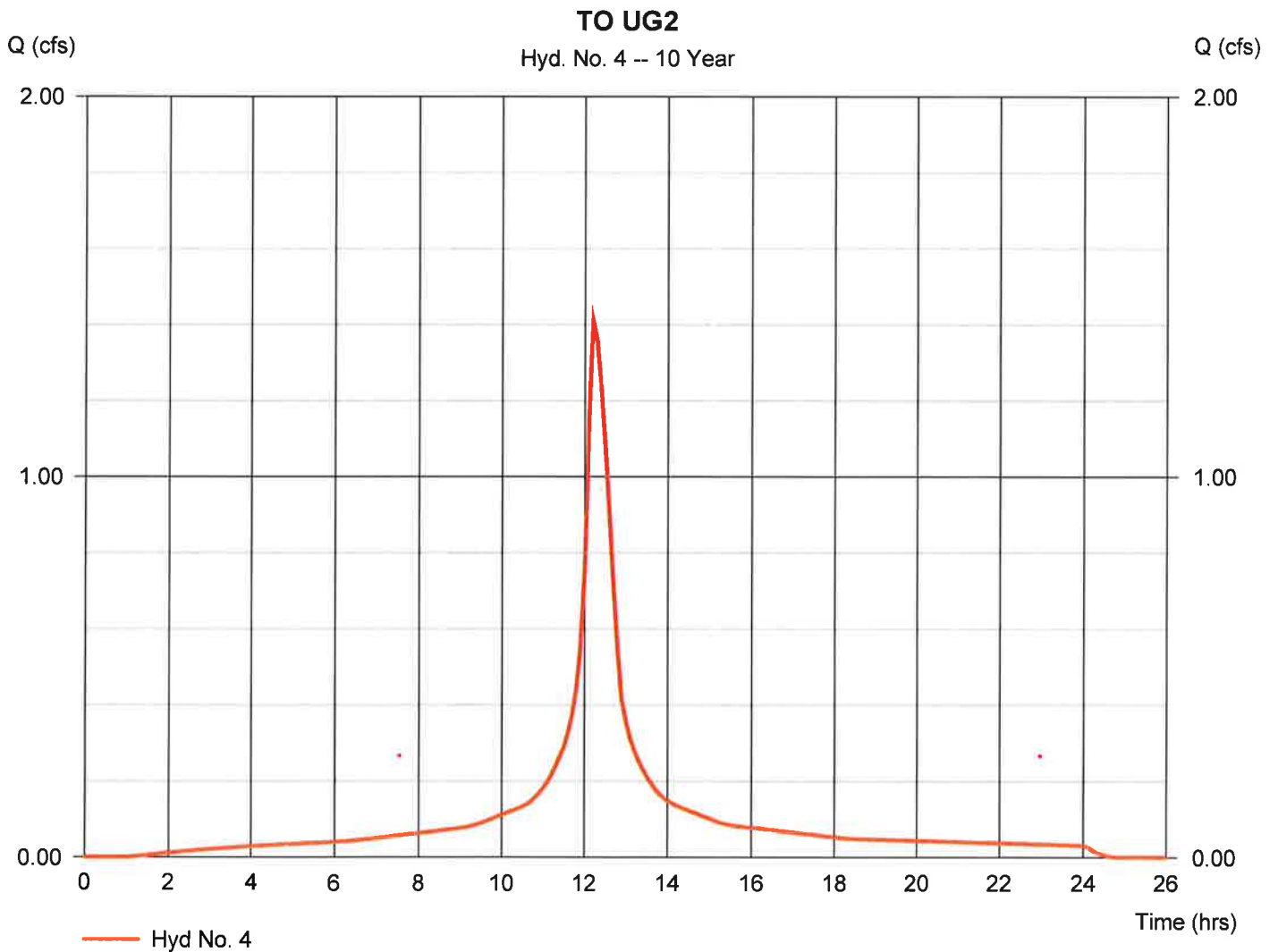
Hydrograph Report

Hyd. No. 4

TO UG2

Hydrograph type	= SCS Runoff	Peak discharge	= 1.409 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 9,373 cuft
Drainage area	= 0.430 ac	Curve number	= 97*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 6.40 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = $[(0.010 \times 74) + (0.420 \times 98)] / 0.430$

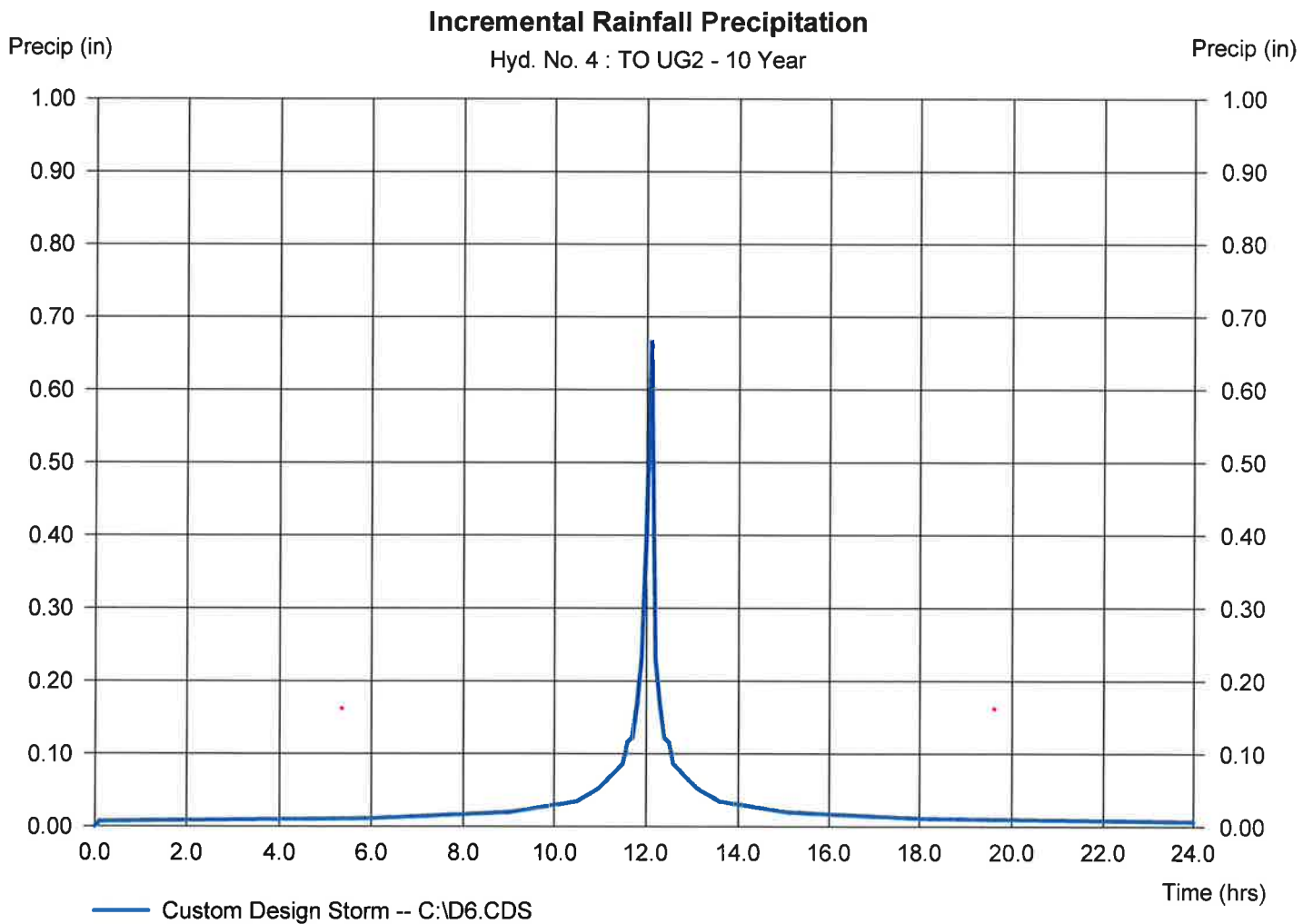


Precipitation Report

Hyd. No. 4

TO UG2

Storm Frequency	= 10 yrs	Time interval	= 6 min
Total precip.	= 6.4000 in	Distribution	= Custom
Storm duration	= C:\D6.CDS		



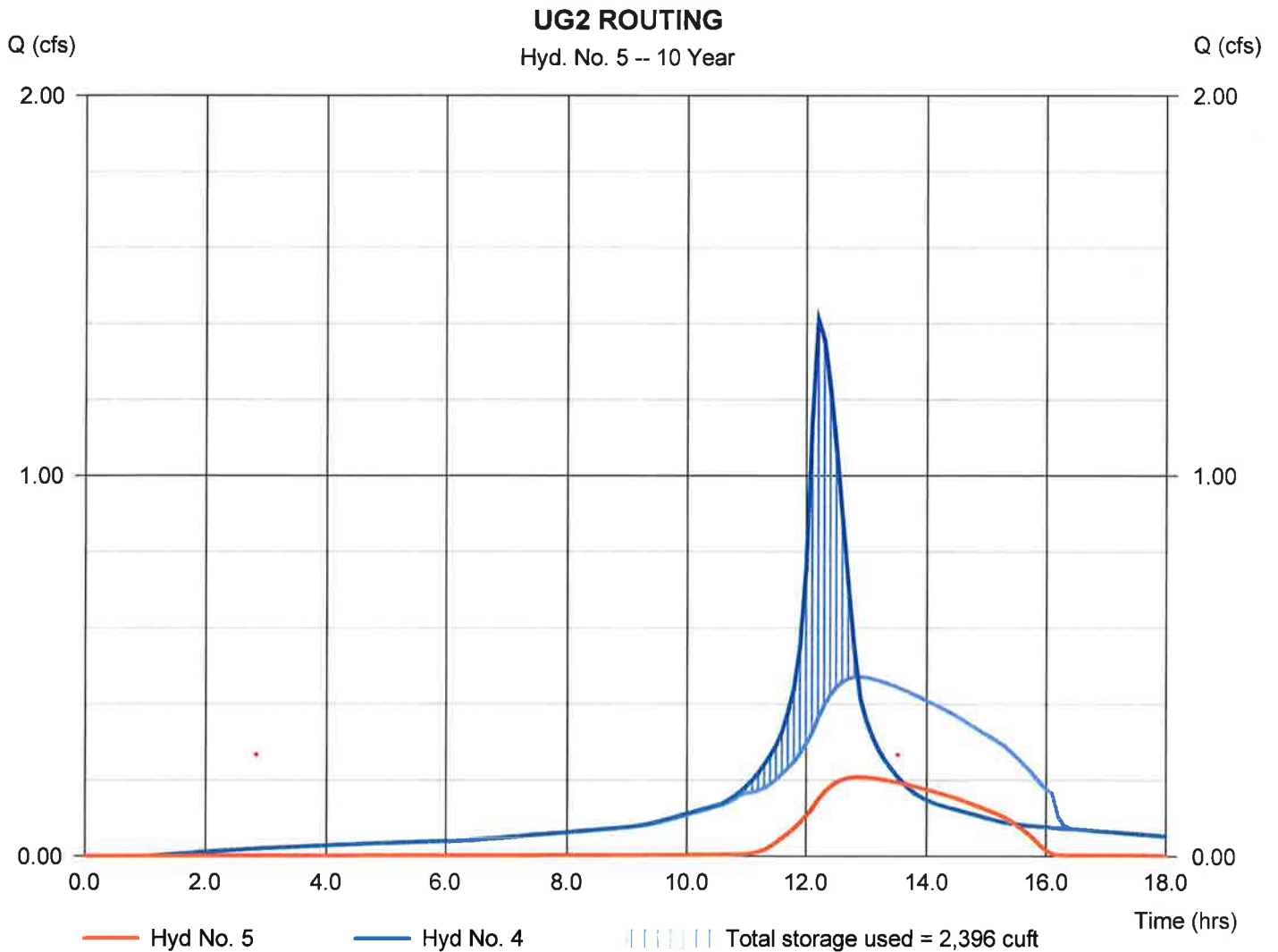
Hydrograph Report

Hyd. No. 5

UG2 ROUTING

Hydrograph type	= Reservoir	Peak discharge	= 0.208 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.90 hrs
Time interval	= 6 min	Hyd. volume	= 2,416 cuft
Inflow hyd. No.	= 4 - TO UG2	Max. Elevation	= 66.21 ft
Reservoir name	= UG2	Max. Storage	= 2,396 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



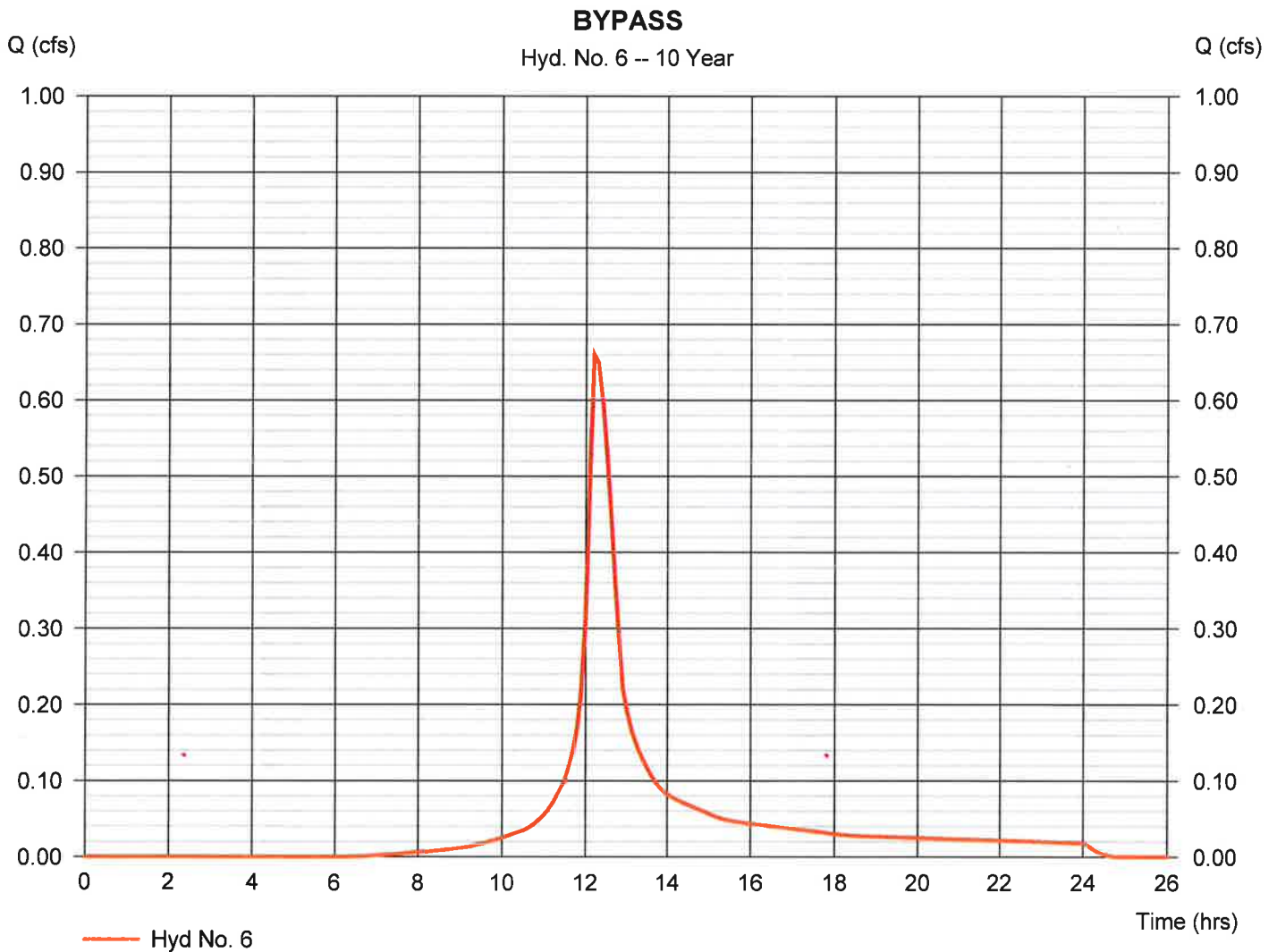
Hydrograph Report

Hyd. No. 6

BYPASS

Hydrograph type	= SCS Runoff	Peak discharge	= 0.659 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 3,974 cuft
Drainage area	= 0.280 ac	Curve number	= 78*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 6.40 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = $[(0.050 \times 98) + (0.230 \times 74)] / 0.280$



Precipitation Report

Hyd. No. 6

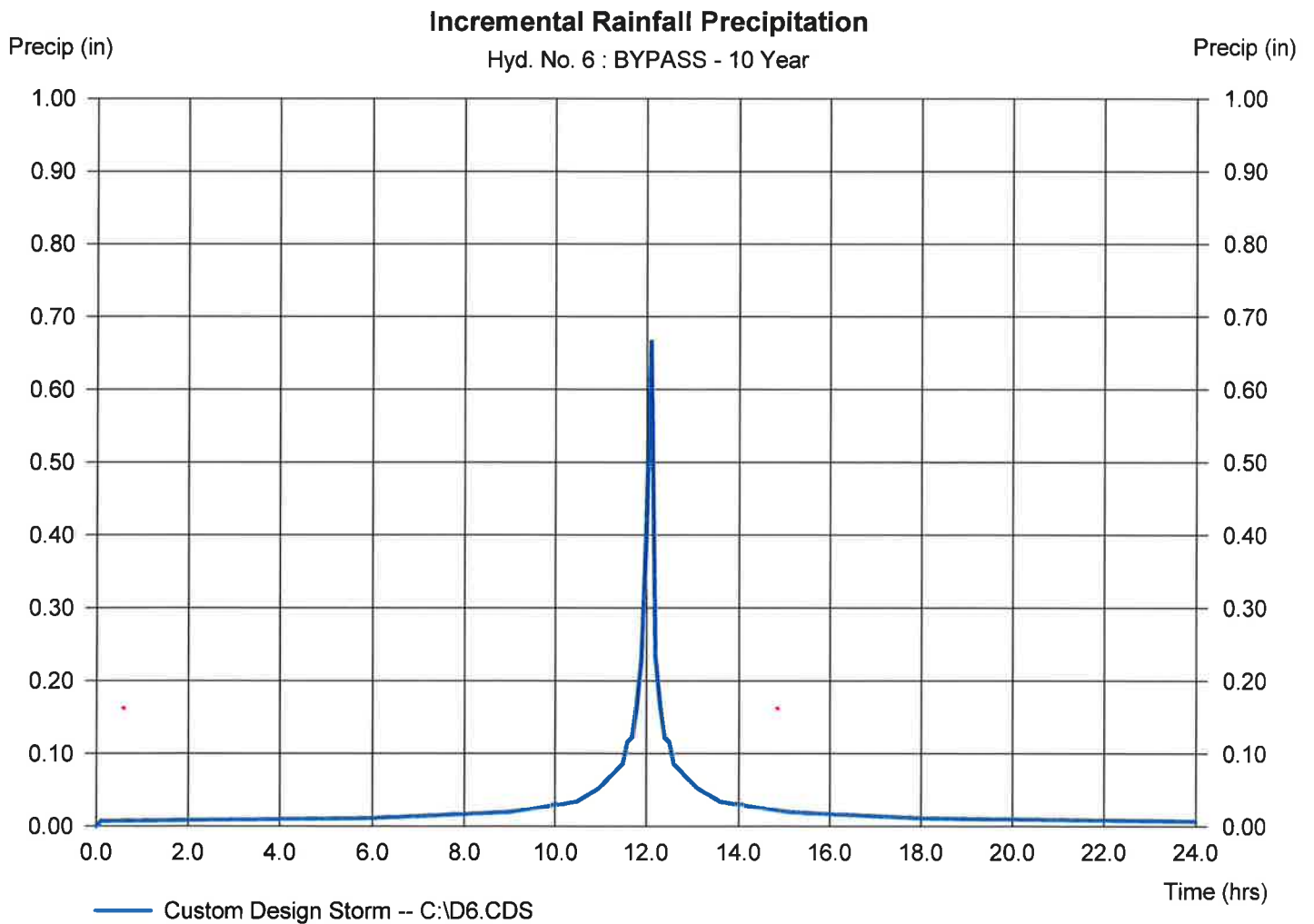
BYPASS

Storm Frequency
Total precip.
Storm duration

= 10 yrs
= 6.4000 in
= C:\D6.CDS

Time interval
Distribution

= 6 min
= Custom

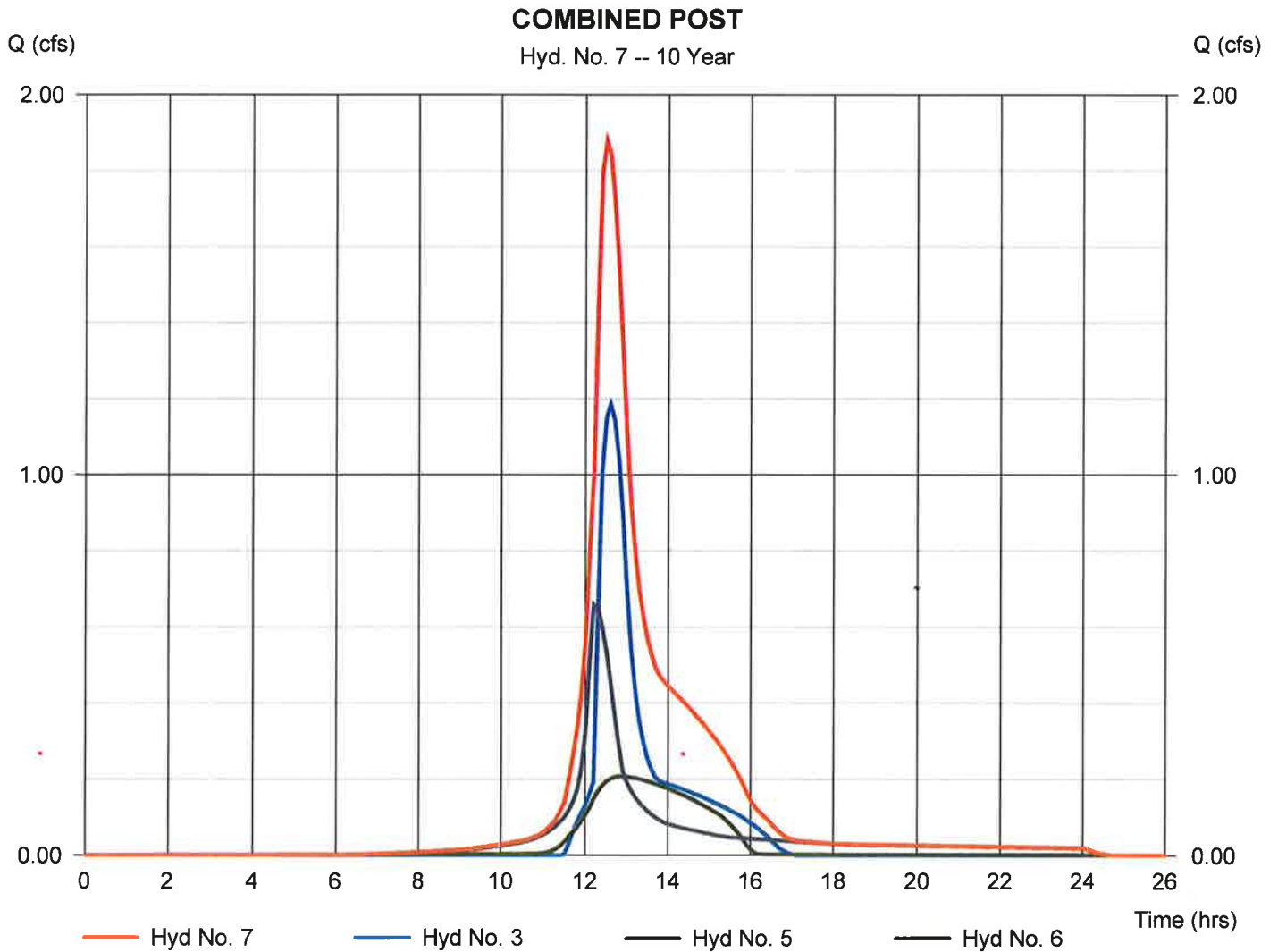


Hydrograph Report

Hyd. No. 7

COMBINED POST

Hydrograph type	= Combine	Peak discharge	= 1.878 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.50 hrs
Time interval	= 6 min	Hyd. volume	= 11,626 cuft
Inflow hyds.	= 3, 5, 6	Contrib. drain. area	= 0.280 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

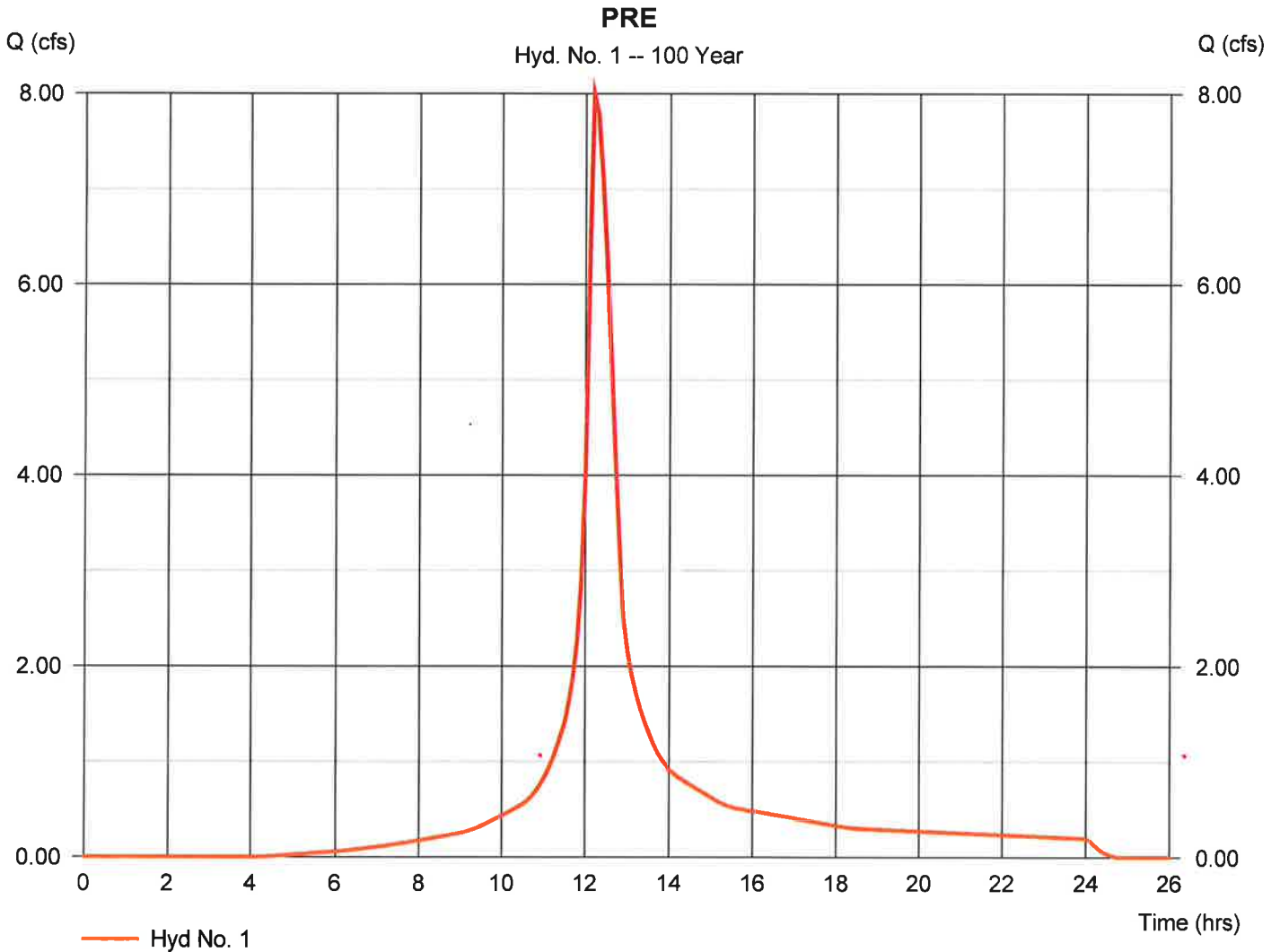
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	7.993	6	732	48,753	-----	-----	-----	PRE
2	SCS Runoff	4.775	6	732	32,003	-----	-----	-----	TO UG1
3	Reservoir	4.481	6	738	17,665	2	70.86	4,670	UG1 ROUTING
4	SCS Runoff	2.988	6	732	20,327	-----	-----	-----	TO UG2
5	Reservoir	1.366	6	762	7,095	4	68.70	6,004	UG2 ROUTING
6	SCS Runoff	1.736	6	732	10,697	-----	-----	-----	BYPASS
7	Combine	6.426	6	738	35,457	3, 5, 6	-----	-----	COMBINED POST
FRANK.gpw					Return Period: 100 Year		Thursday, 02 / 22 / 2024		

Hydrograph Report

Hyd. No. 1

PRE

Hydrograph type	= SCS Runoff	Peak discharge	= 7.993 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 48,753 cuft
Drainage area	= 1.350 ac	Curve number	= 74
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 11.50 min
Total precip.	= 13.47 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285



Precipitation Report

Hyd. No. 1

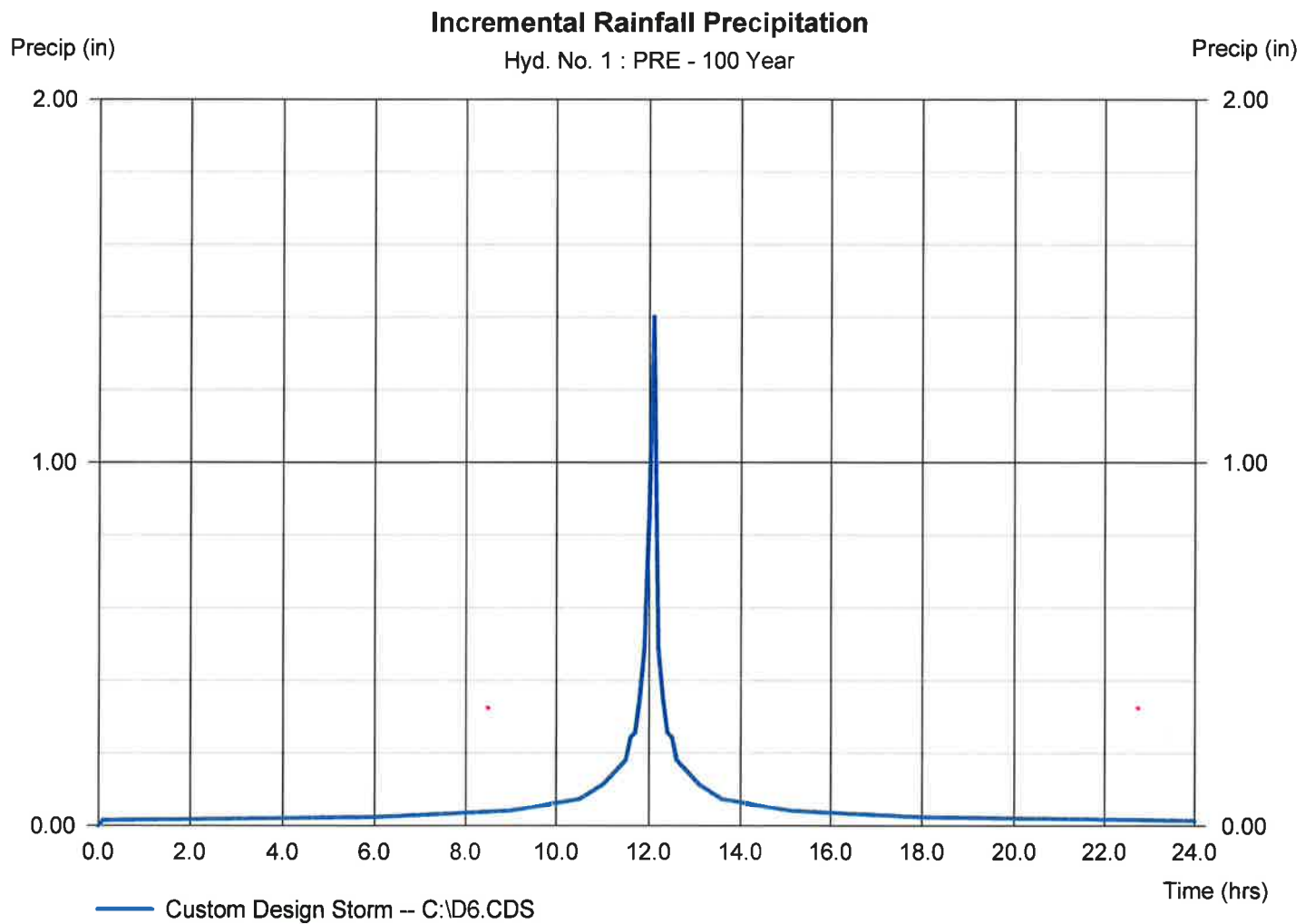
PRE

Storm Frequency
Total precip.
Storm duration

= 100 yrs
= 13.4700 in
= C:\D6.CDS

Time interval
Distribution

= 6 min
= Custom



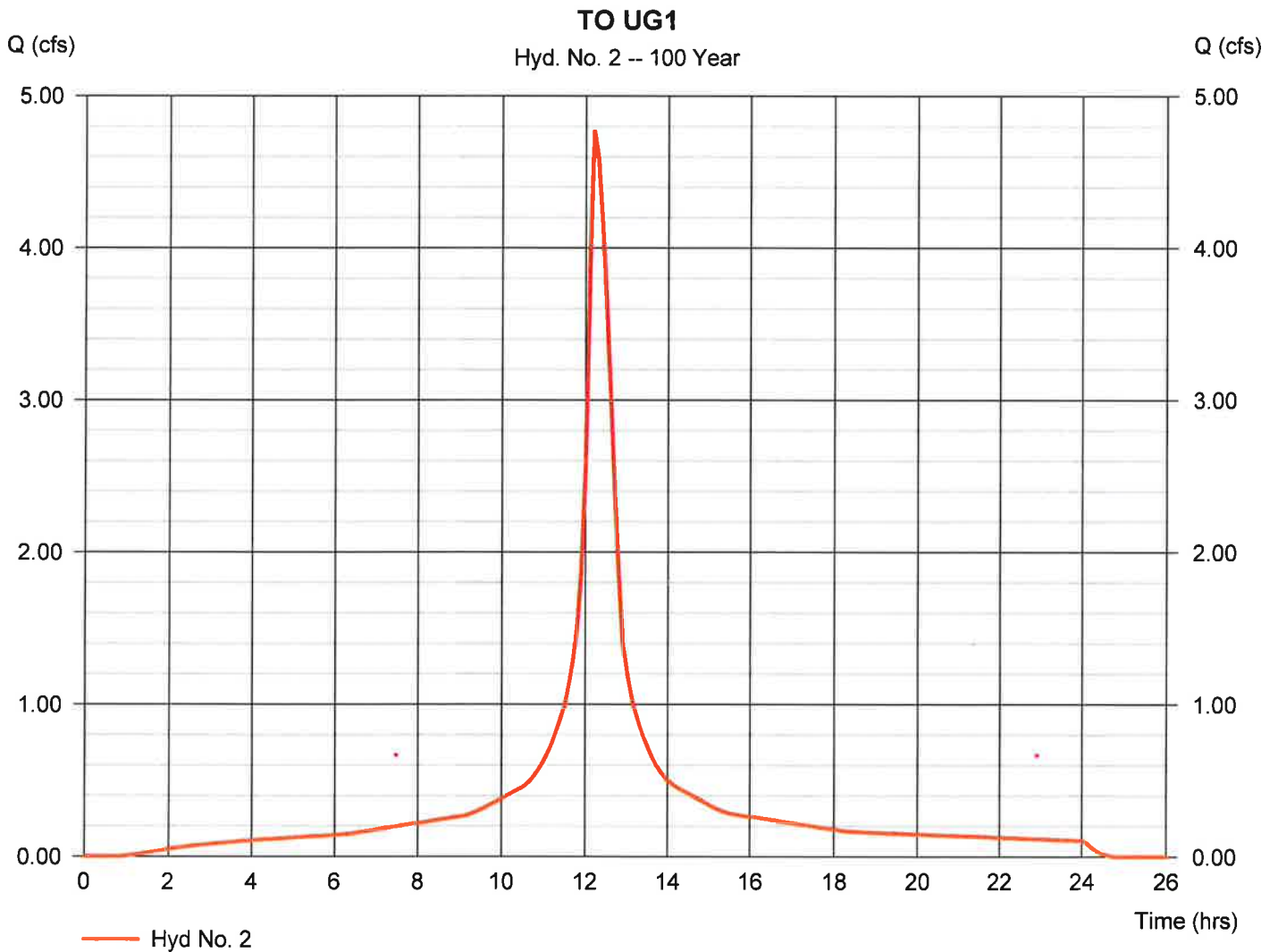
Hydrograph Report

Hyd. No. 2

TO UG1

Hydrograph type	= SCS Runoff	Peak discharge	= 4.775 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 32,003 cuft
Drainage area	= 0.690 ac	Curve number	= 95*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 13.47 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = $[(0.100 \times 74) + (0.590 \times 98)] / 0.690$

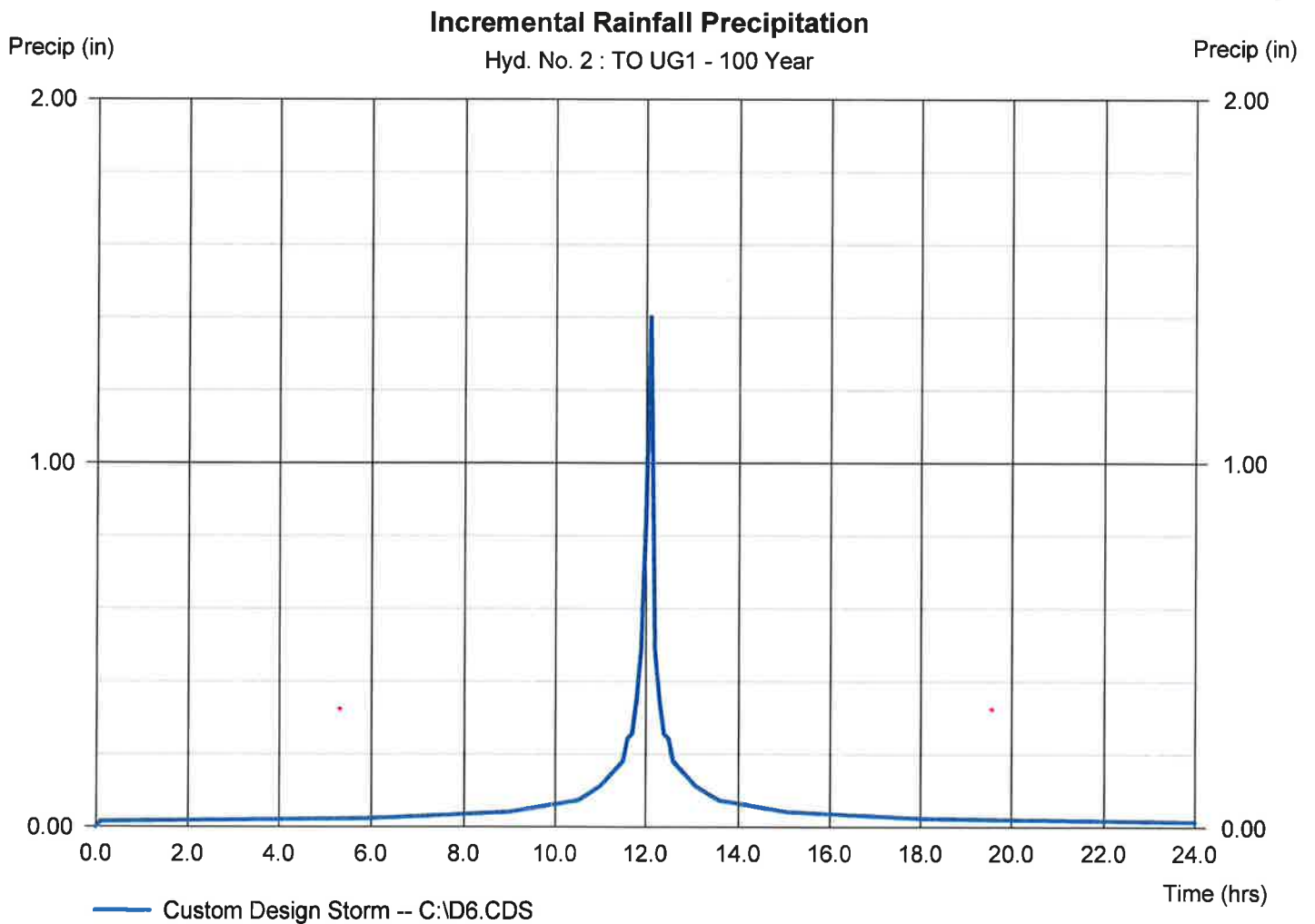


Precipitation Report

Hyd. No. 2

TO UG1

Storm Frequency	= 100 yrs	Time interval	= 6 min
Total precip.	= 13.4700 in	Distribution	= Custom
Storm duration	= C:\D6.CDS		



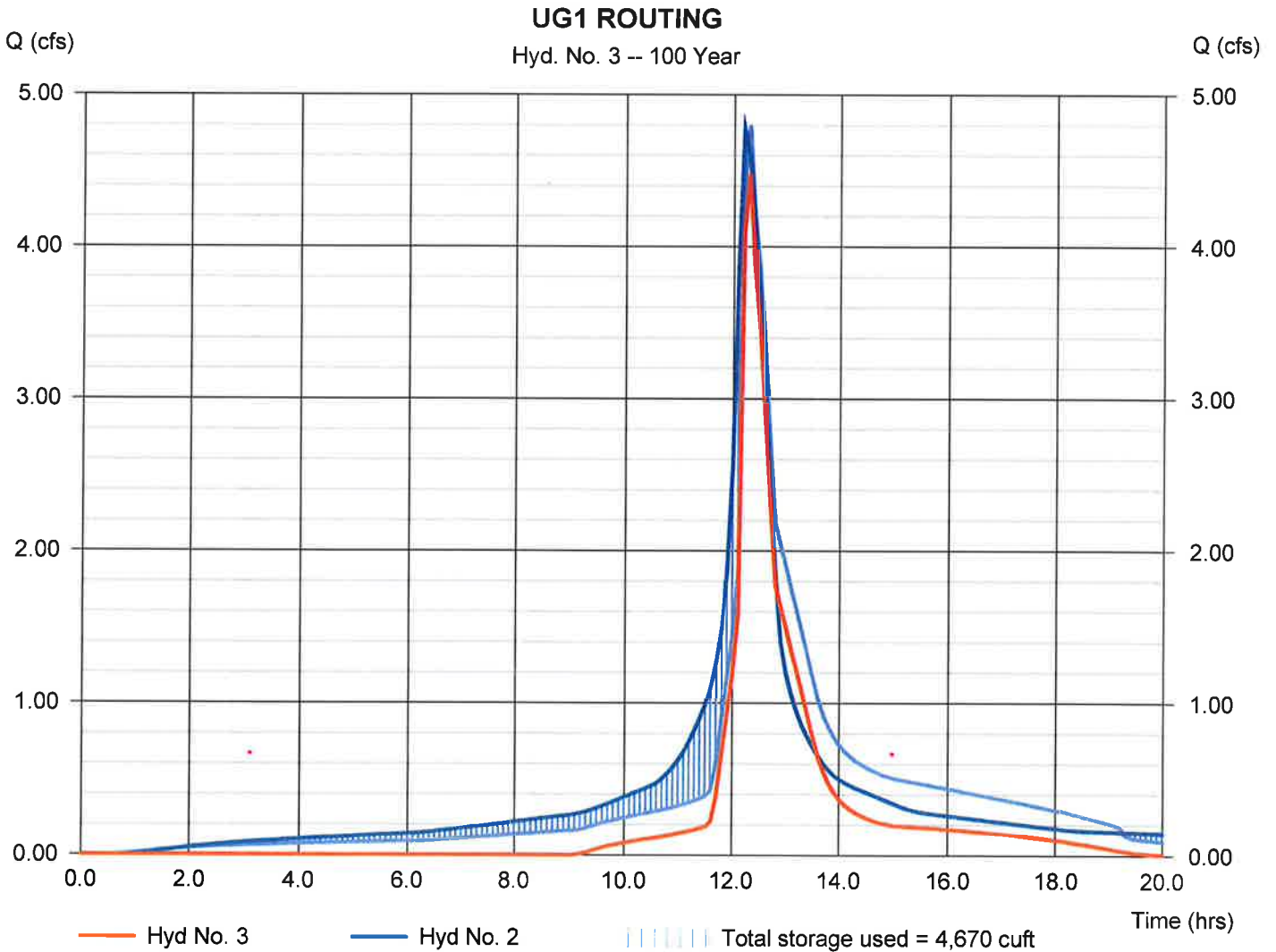
Hydrograph Report

Hyd. No. 3

UG1 ROUTING

Hydrograph type	= Reservoir	Peak discharge	= 4.481 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.30 hrs
Time interval	= 6 min	Hyd. volume	= 17,665 cuft
Inflow hyd. No.	= 2 - TO UG1	Max. Elevation	= 70.86 ft
Reservoir name	= UG1	Max. Storage	= 4,670 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



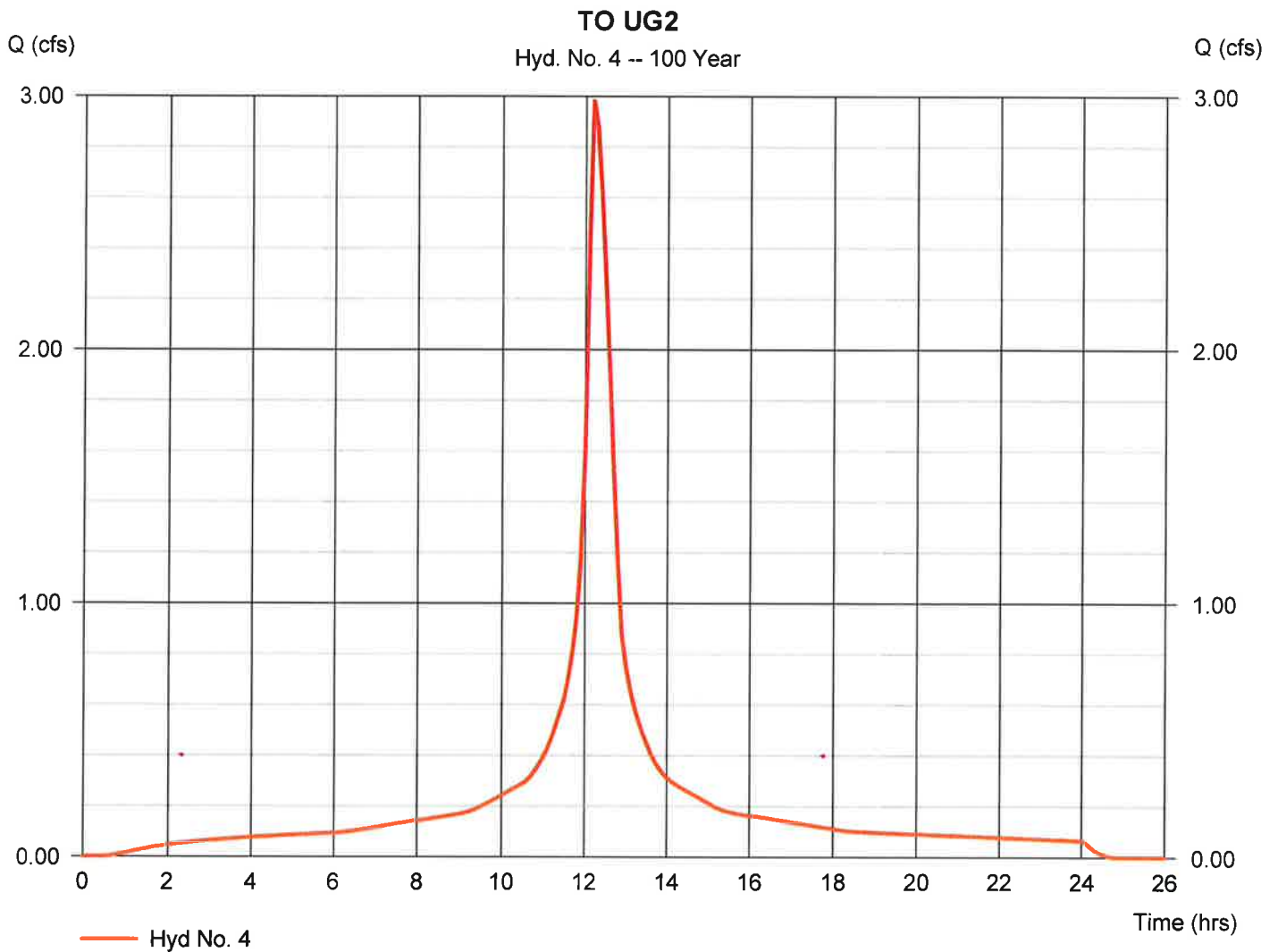
Hydrograph Report

Hyd. No. 4

TO UG2

Hydrograph type	= SCS Runoff	Peak discharge	= 2.988 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 20,327 cuft
Drainage area	= 0.430 ac	Curve number	= 97*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 13.47 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = $[(0.010 \times 74) + (0.420 \times 98)] / 0.430$

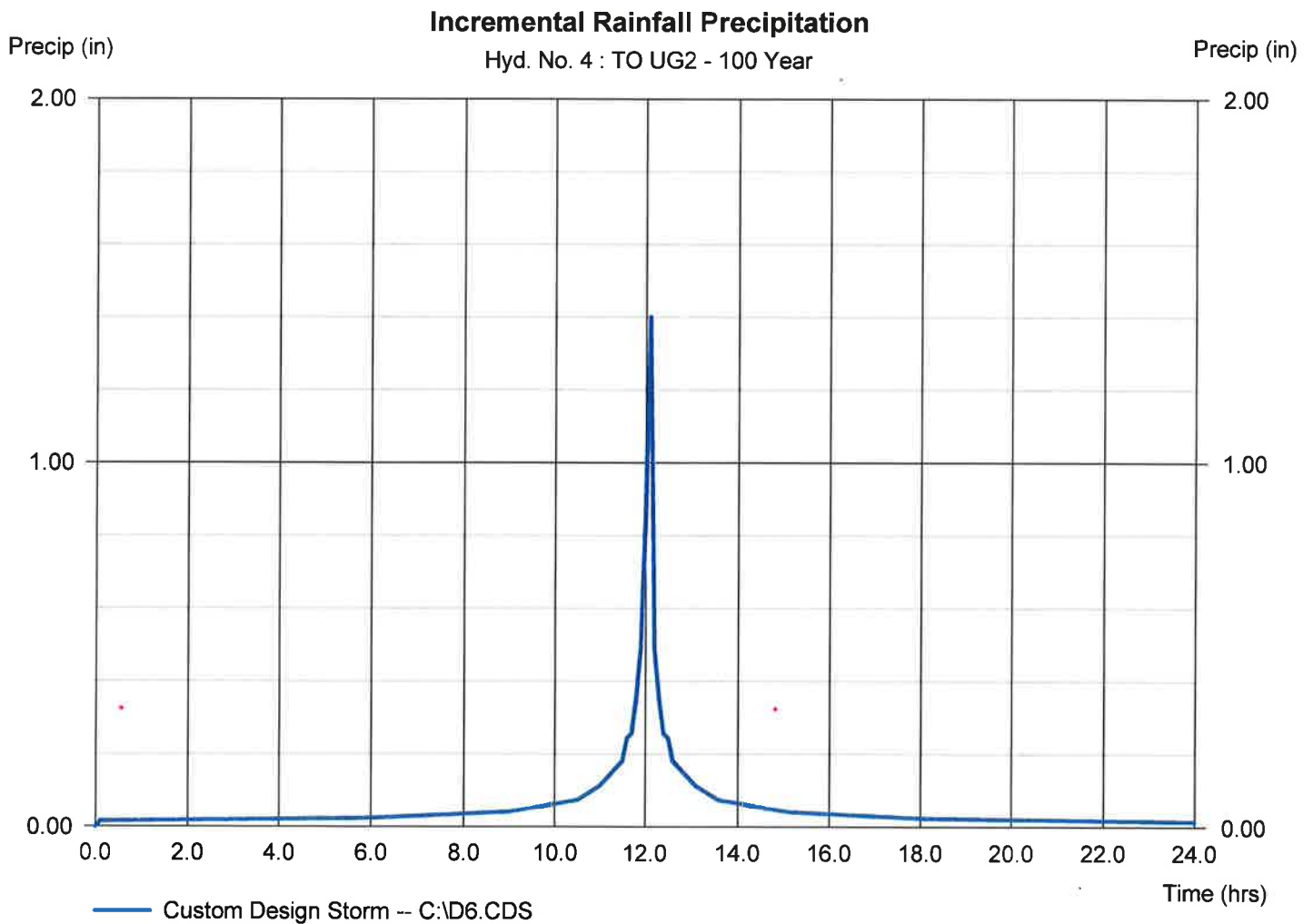


Precipitation Report

Hyd. No. 4

TO UG2

Storm Frequency	= 100 yrs	Time interval	= 6 min
Total precip.	= 13.4700 in	Distribution	= Custom
Storm duration	= C:\D6.CDS		



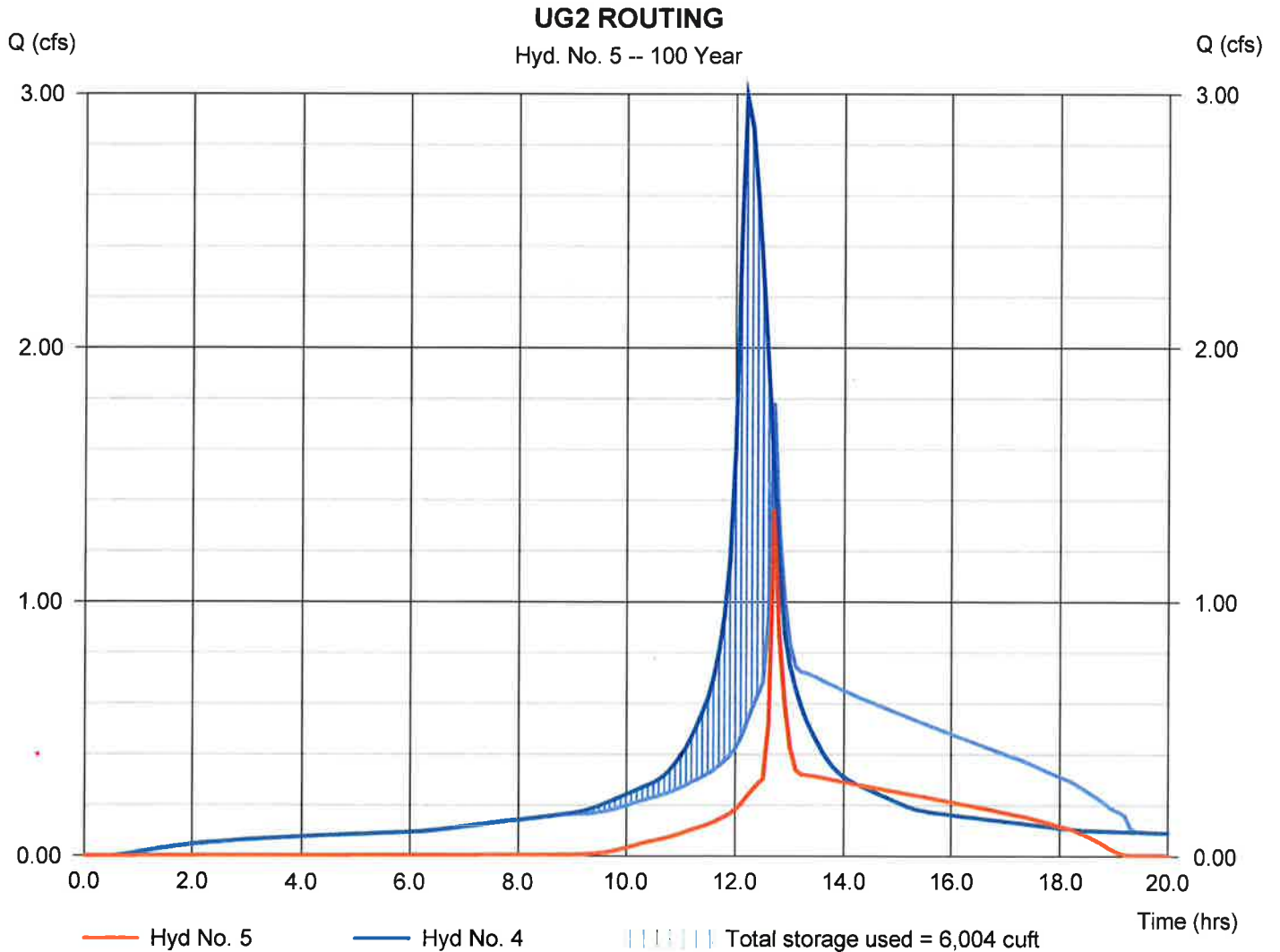
Hydrograph Report

Hyd. No. 5

UG2 ROUTING

Hydrograph type	= Reservoir	Peak discharge	= 1.366 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.70 hrs
Time interval	= 6 min	Hyd. volume	= 7,095 cuft
Inflow hyd. No.	= 4 - TO UG2	Max. Elevation	= 68.70 ft
Reservoir name	= UG2	Max. Storage	= 6,004 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



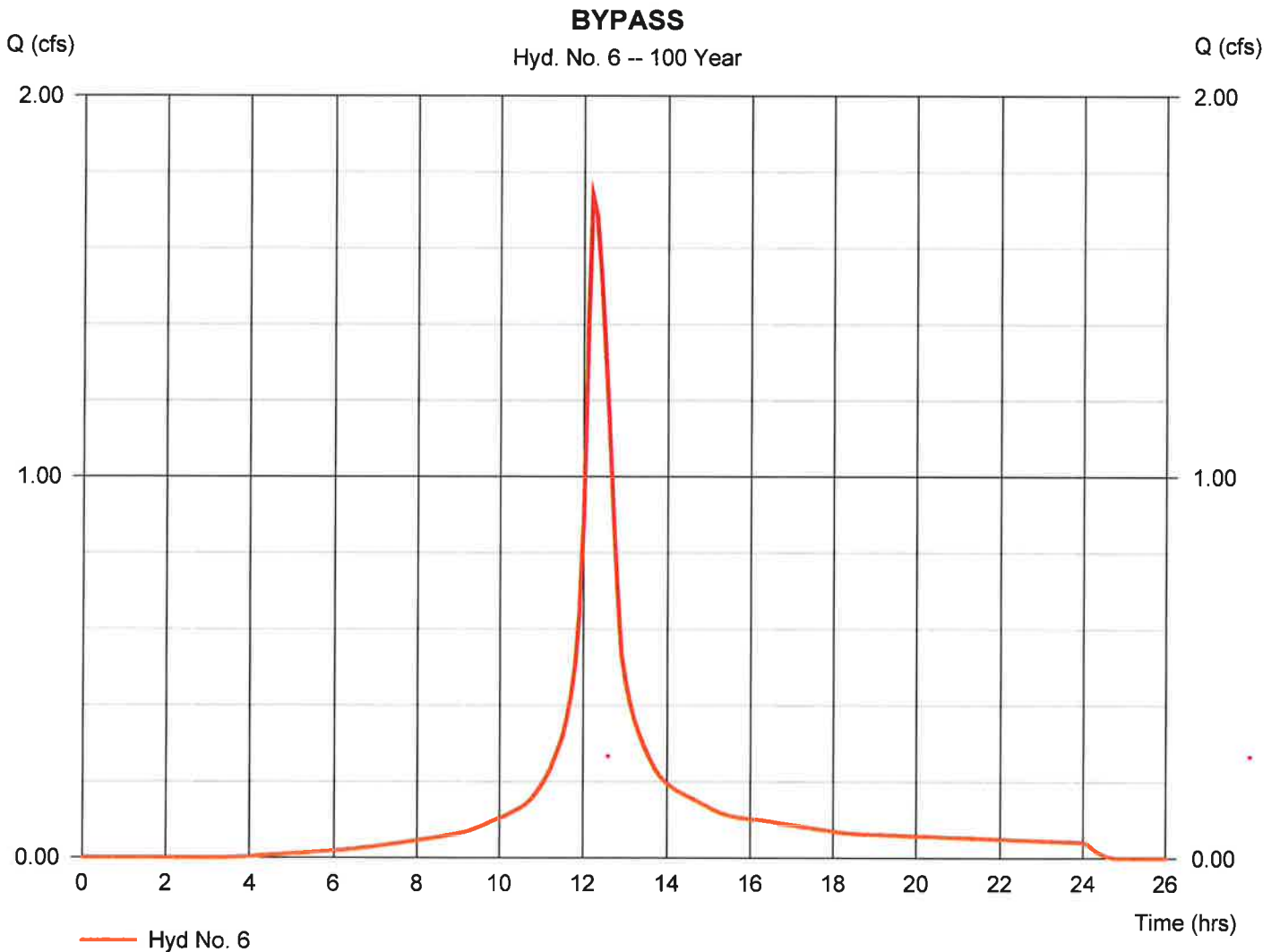
Hydrograph Report

Hyd. No. 6

BYPASS

Hydrograph type	= SCS Runoff	Peak discharge	= 1.736 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.20 hrs
Time interval	= 6 min	Hyd. volume	= 10,697 cuft
Drainage area	= 0.280 ac	Curve number	= 78*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 10.00 min
Total precip.	= 13.47 in	Distribution	= Custom
Storm duration	= C:\D6.CDS	Shape factor	= 285

* Composite (Area/CN) = $[(0.050 \times 98) + (0.230 \times 74)] / 0.280$



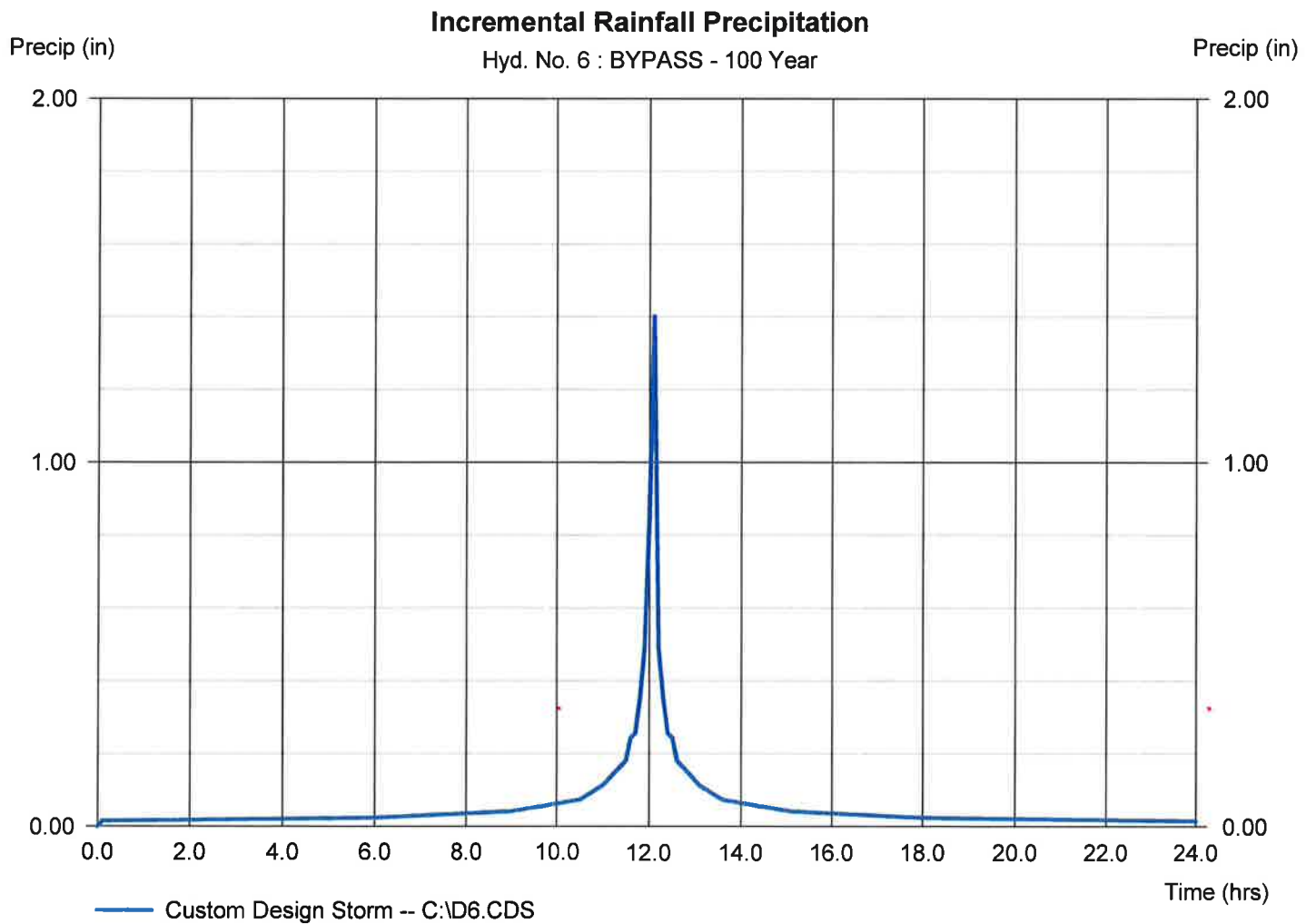
Precipitation Report

Hyd. No. 6

BYPASS

Storm Frequency = 100 yrs
Total precip. = 13.4700 in
Storm duration = C:\D6.CDS

Time interval = 6 min
Distribution = Custom

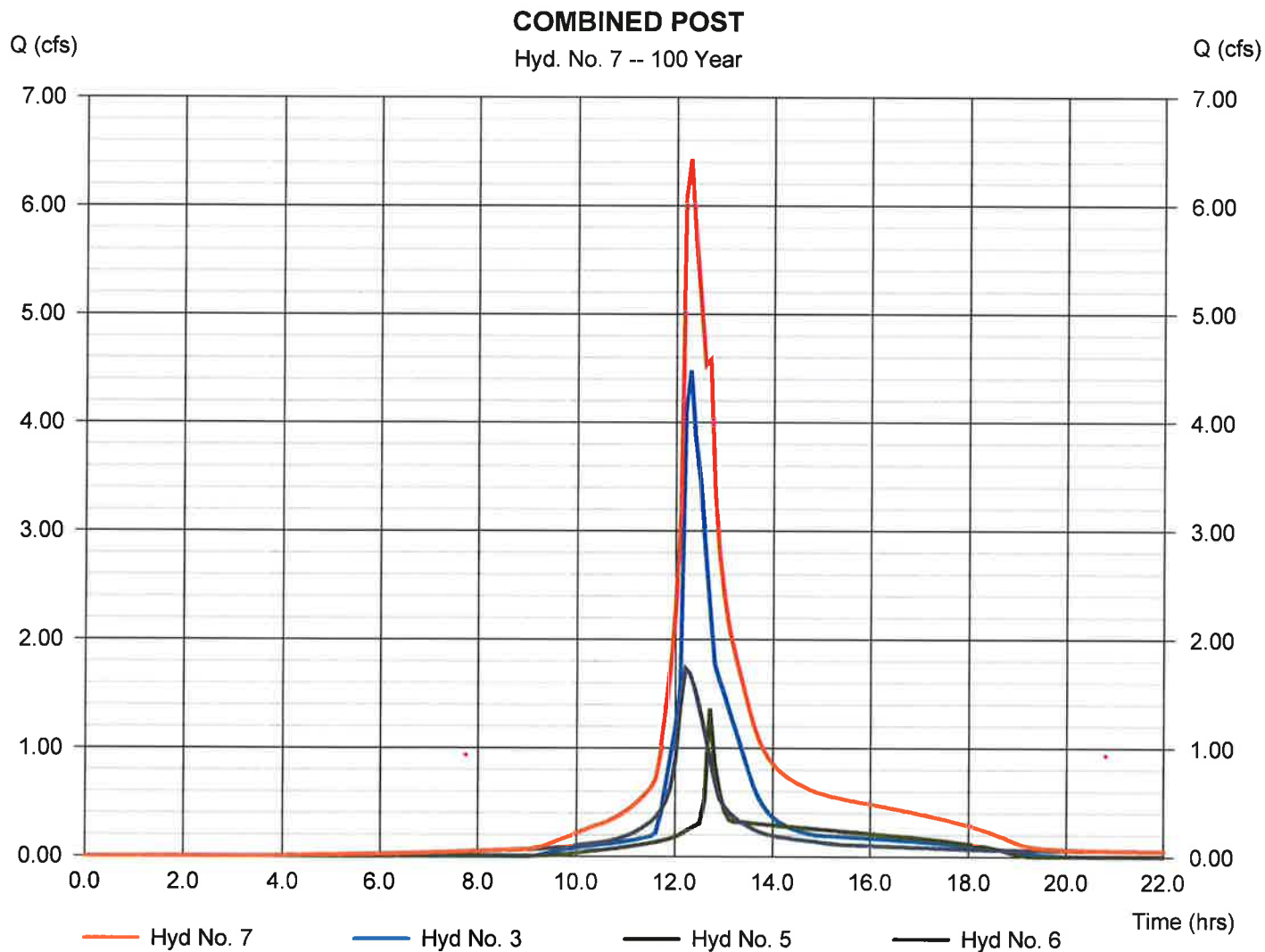


Hydrograph Report

Hyd. No. 7

COMBINED POST

Hydrograph type	= Combine	Peak discharge	= 6.426 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.30 hrs
Time interval	= 6 min	Hyd. volume	= 35,457 cuft
Inflow hyds.	= 3, 5, 6	Contrib. drain. area	= 0.280 ac



APPENDIX B:

**CONVEYANCE CAPACITY OF UNDERGROUND STORMWATER PIPES AND SCOUR
HOLE SIZING COMPUTATIONS**

Storm Sewer Tabulation

Station Line To Line	Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
		Incr (ac)	Total (ac)		Incr (min)	Total (min)	Slope (%)	Size (in)					Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	
11	End	5.000	0.00	0.00	0.00	0.00	10.0	10.0	0.0	2.20	2.89	3.59	15	0.20	67.49	67.50	68.08	68.16	0.00	0.00	OS-FES1
10	End	10.000	0.00	0.00	0.00	0.00	10.0	10.0	0.0	0.20	4.57	1.87	15	0.50	64.45	64.50	64.62	64.68	0.00	0.00	OS-FES2
9	8	57.000	0.15	0.86	0.13	0.13	10.0	10.0	6.9	0.90	4.61	2.28	15	0.51	70.25	70.54	70.82	70.91	0.00	0.00	1-2
8	6	73.000	0.09	0.94	0.08	0.21	10.0	11.3	6.7	1.43	4.60	2.51	15	0.51	69.88	70.25	70.64	70.74	0.00	0.00	2-MH
7	6	36.000	0.10	0.80	0.08	0.08	10.0	10.0	6.9	0.56	4.57	0.85	15	0.50	69.88	70.06	70.64	70.64	0.00	0.00	3-4
6	5	53.000	0.00	0.00	0.00	0.29	10.0	12.3	6.5	1.90	4.61	3.08	15	0.51	69.61	69.88	70.35	70.43	0.00	0.00	MH-4
5	4	35.000	0.07	0.99	0.07	0.36	10.0	12.9	6.4	2.32	4.63	3.78	15	0.51	69.43	69.61	70.06	70.23	0.00	0.00	4-5
4	End	86.000	0.16	0.96	0.15	0.52	10.0	13.2	6.3	3.27	7.79	4.41	15	1.45	67.50	68.75	68.23	69.48	0.00	0.00	5-UG1
3	2	63.000	0.08	0.99	0.08	0.08	10.0	10.0	6.9	0.55	4.60	2.16	15	0.51	68.49	68.81	68.87	69.10	0.00	0.00	6-MH
2	1	90.000	0.00	0.00	0.00	0.08	10.0	12.3	6.5	0.51	4.57	2.45	15	0.50	68.04	68.49	68.32	68.77	0.00	0.00	MH-7
1	End	7.000	0.35	0.98	0.34	0.42	10.0	15.7	5.9	2.50	4.88	4.00	15	0.57	64.50	64.54	65.13	65.18	0.00	0.00	7-UG2

Project File: PIPES.stm

Number of lines: 11

Run Date: 2/18/2024

NOTES: intensity = 102.61 / (Inlet time + 16.50) ^ 0.82; Return period = Yrs. 25 ; c = cir e = ellip b = box

SCOUR HOLE COMPUTATIONS AT POND 15" PIPE OUTFALL -

Variables:

Design Storm Flow for 25 Year, Q	2.20 cfs
Vertical Dimension of Outlet Pipe, D_o	15 in
Horizontal Dimension of Outlet Pipe, W_o	15 in
Tailwater Depth, TW^1	0.25 ft
Scour Hole Depth, y ($1/2 D_o$ or D_o)	11 in

Apron Dimension Calculations:

Minimum Bottom Width, $W_1 = 2W_o$	$W_1 = 2.50$ ft
Minimum Bottom Length, $L_1 = 3D_o$	$L_1 = 3.75$ ft
Minimum Top Width (max side slope of 3:1), W_2	$W_2 = 8.00$ ft
Minimum Top Length (max side slope of 3:1), L_2	$L_2 = 9.25$ ft

Rip Rap Stone Size Calculations:

Unit Discharge, $q = Q/D_o = 1.76$ cfs per foot

• **Case I: $y = 1/2 D_o$**

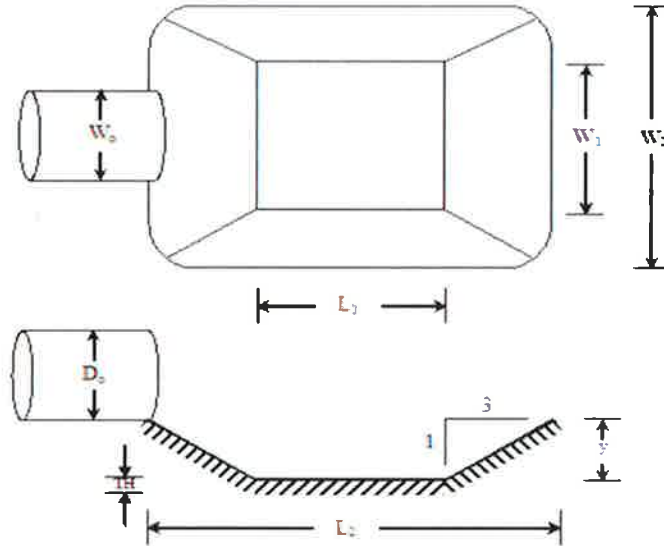
Median Stone, $d_{50} = \frac{0.0125 q^{1.33}}{TW} =$

Apron Thickness, $TH = 2 \times d_{50}$ with filter fabric

• **Case II: $y = D_o$**

Median Stone, $d_{50} = \frac{0.0082 q^{1.33}}{TW} =$

Apron Thickness, $TH = 2 \times d_{50}$ with filter fabric



Notes:

1. The side slopes shall be 3:1 or flatter.
2. The bottom grade shall be 0.0% (level).
3. There shall be no overfall at the end of the apron or at the end of the culvert.
4. Fifty (50) percent by weight of the rip-rap mixture shall be smaller than the median size stone designated as d_{50} . The largest stone size in the mixture shall be 1.5 times the d_{50} size. The rip-rap shall be reasonably well graded.
5. The thickness of the rip-rap apron may be two (2) times the median stone diameter provided that the apron is constructed on a bedding of four (4) inches of 3/4 inch clean stone on approved filter fabric material.
6. Rip-rap and filter fabric shall meet the standards of the governing Soil Conservation District as well as the requirements of the local municipality.
7. Where the scour hole is to be placed within an existing or proposed waterway:
 - a. The scour hole sidewalls should be eliminated to maintain a smooth hydraulic line along the waterway bottom to avoid inviting turbulent flow from a sudden depression in the waterway.
 - b. If the flow in the waterway is greater than the flow from the proposed outlet, the rip-rap used to construct the scour hole should be sized based on the greater flow value according to the standard rip-rap.

Footnote:

1. Tailwater depth shall be the 2 year storm if discharging into a detention basin. For areas where tailwater cannot be computed, use $TW = 0.2D_o$.

APPENDIX C:
ANNUAL GROUND WATER RECHARGE ANALYSIS WORKSHEETS AND MOUNDING
ANALYSIS

Annual Groundwater Recharge Analysis (based on GSR-32)

Project Name: 390 DAVIDSON RD
Description: MIXED USE BLDG +PARKING
Analysis Date: 02/18/24

Pre-Developed Conditions

Land Segment	Area (acres)	TR-55 Land Cover	Soil	Average Annual P (in)	Climatic Factor	Annual Recharge (in)	Annual Recharge (cu.ft)
1	1.35	Meadow, Pasture, Grassland or range	Penn	45.7	1.48	12.6	61,664
2							
3							
4							
5							
6							
7							
8							
9							
10							
11							
12							
13							
14							
15							
Total =	1.4					12.6	61,664

Post-Developed Conditions

Land Segment	Area (acres)	TR-55 Land Cover	Soil	Annual Recharge (in)	Annual Recharge (cu.ft)
1	1.24	Impervious areas	Penn	0.0	-
2	0.11	Open space	Penn	12.3	4,914
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
Total =	1.4			1.0	4,914

Annual Recharge Requirements Calculation

% of Pre-Developed Annual Recharge to Preserve = **100%**

Post-Development Annual Recharge Deficit= 56,750 (cubic feet)

RWC=	3.80	(in)	DRWC=	0.00	(in)
ERWC=	0.99	(in)	EDRWC=	0.00	(in)

Procedure to fill the Pre-Development and Post-Development Conditions Tables

For each land segment, first enter the area, then select TR-55 Land Cover, then select Soil. Start from the top of the table and proceed downward. Don't leave blank rows (with A=0) in between your segment entries. Rows with A=0 will not be displayed or used in calculations. For impervious areas outside of standard lots select "Impervious Areas" as the Land Cover. Soil type for impervious areas are only required if an infiltration facility will be built within these areas.

Recharge BMP Input Parameters		Roof Zone Water Capacity Calculated Parameters		Recharge Design Parameters			
Parameter	Symbol	Value	Unit	Parameter	Symbol	Value	Unit
BMP Area	ABMP	2154.7	sq.ft	Empty Portion of RWC under Post-D Natural Recharge	ERWC	1.49	in
BMP Effective Depth, this is the design variable Upper level of the BMP surface (negative if above ground)	dBMP	4.8	in	ERWC Modified to consider dEXC	EDRWC	0.00	in
Depth of lower surface of BMP, must be >= dBMPu	dBMPu	67.5	in	Empty Portion of RWC under Infiltration	RERWC	0.00	in
Post-development Land Segment Location of BMP	dEXC	71.5	in				
Input Zero if Location is distributed or undetermined	SegBMP	8	unitless				
				Runoff Captured Avg. over imp. Area		12.6	in

BMP Calculated Size Parameters

Parameter	Symbol	Value	Unit
Annual BMP Recharge Volume		66,750	cu.ft
Avg BMP Recharge Efficiency		100.0%	%
%Rainfall became Runoff		77.9%	%
%Runoff Infiltrated		35.4%	%
%Runoff Recharged		35.4%	%
%Rainfall Recharged		27.6%	%

Parameters from Annual Recharge Worksheet

Parameter	Symbol	Value	Unit
Post-D Deficit Recharge (or desired recharge volume)	Vdef	56,750	cu.ft
Post-D Impervious Area (or target Impervious Area)	Aimp	54,014	sq.ft
Root Zone Water Capacity	RWC	5.74	in
RWC Modified to consider dEXC	DRWC	0.00	in
Climatic Factor	C-factor	1.48	no units
Average Annual P	Pavg	45.7	in
Recharge Requirement over Imp. Area	dr	12.6	in

Calculation Check Messages

Volume Balance--> OK
dBMP Check--> dBMP must be <= dEXC-dBMPu, adjust parameters
dEXC Check--> OK
BMP Location--> Land Segment Number Selected for BMP is not Defined

OTHER NOTES

Design is accurate only after BMP dimensions are updated to make rech volume= deficit volume. The portion of BMP infiltration prior to filling and the area occupied by BMP are ignored in these calculations. Results are sensitive to dBMP, make sure dBMP selected is small enough for BMP to empty in less than 3 days. For land Segment Location of BMP if you select "impervious areas", RWC will be minimal but not zero as determined by the soil type and a shallow root zone for this Land Cover allowing consideration of lateral flow and other losses.

How to solve for different recharge volumes: By default the spreadsheet assigns the values of total deficit recharge volume "Vdef" and total proposed impervious area "Aimp" from the "Annual Recharge" sheet to "Vdef" and "Aimp" on this page. This allows solution for a single BMP to handle the entire recharge requirement assuming the runoff from entire impervious area is available to the BMP. To solve for a smaller BMP or a LID-IMP to recharge only part of the recharge requirement, set Vdef to your target value and Aimp to impervious area directly connected to your infiltration facility and then solve for ABMP or dBMP. To go back to the default configuration click the "Default Vdef & Aimp" button.

Input Values

R	3.00
Sy	0.150
Kh	25.00
x	10.000
y	40.000
t	0.63
hi(0)	10.00

Recharge rate (permeability rate) (in/hr)
 Specific yield, Sy (dimensionless)
 default value is 0.15; max value is 0.2 provided that a lab test data is submitted
 Horizontal hydraulic conductivity (in/hr)
 Kh = 5xRecharge Rate (R) in the costal plan; Kh=R outside the coastal plan
 1/2 length of basin (x direction, in feet)
 1/2 width of basin (y direction, in feet)
 Duration of infiltration period (hours)
 Initial thickness of saturated zone (feet)

h(max)	10.776
Δh(max)	0.776

Maximum thickness of saturated zone (beneath center of basin at end of infiltration period)
 Maximum groundwater mounding (beneath center of basin at end of infiltration period)

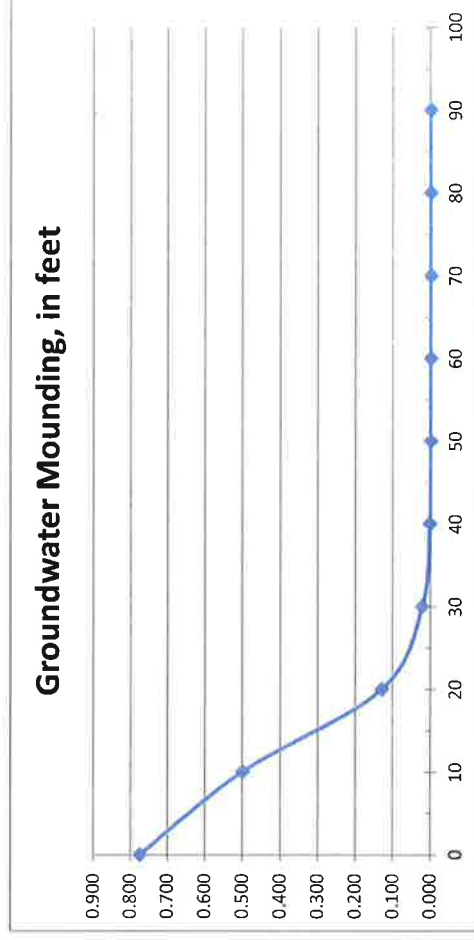
Distance from

Ground-water center of basin in x
 Mounding, in feet direction, in feet

0.776	0
0.501	10
0.131	20
0.023	30
0.003	40
0.001	50
0.000	60
0.000	70
0.000	80
0.000	90



Re-Calculate Now



Disclaimer

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

Input Values

R	3.00
Sy	0.150
Kh	25.00
x	42.500
y	12.500
t	0.63
hi(0)	10.00

Recharge rate (permeability rate) (in/hr)
 Specific yield, Sy (dimensionless)
 default value is 0.15; max value is 0.2 provided that a lab test data is submitted
 Horizontal hydraulic conductivity (in/hr)
 Kh = 5xRecharge Rate (R) in the costal plan; Kh=R outside the coastal plan
 1/2 length of basin (x direction, in feet)
 1/2 width of basin (y direction, in feet)
 Duration of infiltration period (hours)
 Initial thickness of saturated zone (feet)

h(max)	10.863
Δh(max)	0.863

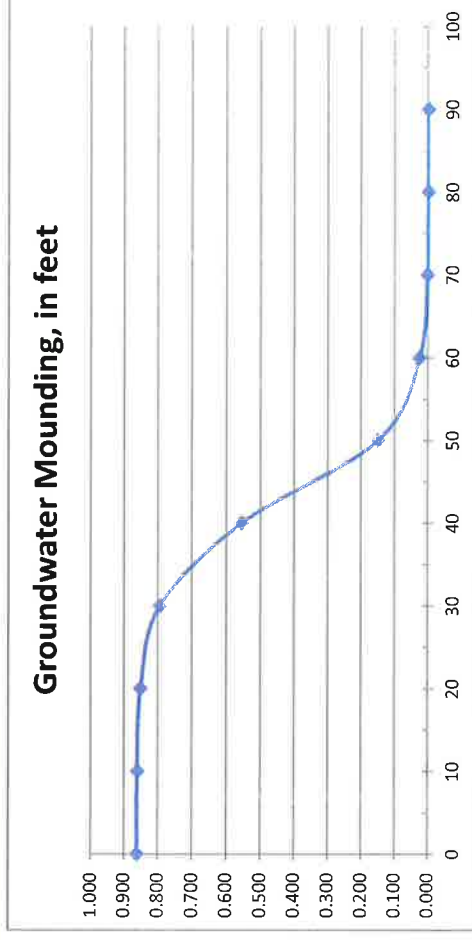
Maximum thickness of saturated zone (beneath center of basin at end of infiltration period)
 Maximum groundwater mounding (beneath center of basin at end of infiltration period)

Ground-water center of basin in x
 Mounding, in feet direction, in feet

0	0.863
10	0.862
20	0.853
30	0.795
40	0.555
50	0.152
60	0.028
70	0.004
80	0.001
90	0.000



Re-Calculate Now



Disclaimer

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

APPENDIX D:

**WATER QUALITY STORM HYDROGRAPHS AND DETAILS OF MTD DEVICES TO
REMOVED 80% TOTAL SUSPENDED SOLIDS**

Block 502.01, Lot 57.01 (MTD #1)

Franklin Twp, NJ

2/12/24

Information Provided by Engineer:

- Water quality flow rate = 0.97 cfs
- Impervious drainage area = 0.47 ac
- Pervious drainage area = 0.10 ac
- Presiding agency = NJDEP
- Required TSS removal rate = 80%

HC Kraken Filter Information and Cartridge Data:

The High-Capacity Kraken Filter Stormwater Treatment Device is a state-of-the-art stormwater filtration system utilizing pretreatment and advanced membrane filtration to ensure a high level of trash, TSS, metals, nutrients, and hydrocarbons removal. The HC Kraken Filter works by initially passing stormwater through a pretreatment chamber to capture trash, hydrocarbons, and sediments. Once runoff is pretreated, it is directed to the filter chamber where membrane filtration begins. When the water level reaches the top of the membrane filters, the treated water will then pass down the riser tube, collect in the underdrain manifold and flow to the discharge chamber. **The High-Capacity Kraken Filter has received final certification from the NJDEP for 80% TSS removal as a stand-alone treatment system.**

- HC Kraken Filter cartridge height = 10 inches (nominal)
- HC Kraken Filter cartridge surface area = 49 square feet
- HC Kraken Filter cartridge loading rate = 0.101 gallons/minute per square foot
- HC Kraken Filter cartridge treatment flow = 0.011 cfs
- **Hydraulic head required: 18.5"** (with 10-inch cartridge)

Design Summary:

The High-Capacity Kraken Filter is sized based on the NJDEP certification, which lists an approved treatment flow rate and maximum impervious acreage limit per cartridge in Table 1. The number of cartridges required based on the impervious drainage area is compared with the number of cartridges required based on the treatment flow rate; the larger number of cartridges governs the sizing.

The HC Kraken Filter for this site was sized to provide **89 cartridges** in order to meet the hydraulic load requirement (calculations shown below). To house this number of cartridges, Contech Engineered Solutions recommends a 6' x 12' precast Shallow HC Kraken Filter.

$$N_{\text{cartridges hyd.load}} = \frac{Q_{\text{treat}}}{Q_{\text{cartridge}}} = \frac{0.97 \text{ cfs}}{0.011 \text{ cfs/cartridge}} = 88.18 \Rightarrow (89) \text{ 10" Cartridges}$$

$$N_{\text{cartridges mass load}} = \frac{\text{Area}_{\text{site}}}{\text{Max Area}_{\text{cartridge}}} = \frac{0.47 \text{ acres}}{0.009 \text{ acres/cartridge}} = 52.22 \Rightarrow (53) \text{ 10" Cartridges}$$

Maintenance:

Maintenance of Stormwater best management practices is required per the New Jersey Administrative Code 7:8-5.8. Recommendations for maintenance are included in chapters 8 & 9 of the New Jersey Stormwater Best Management Practices Manual. To comply with requirements, CONTECH offers a network of Preferred Service Providers that have the capability to perform all necessary inspections, compliance reporting and cleaning services. CONTECH recommends inspecting the system annually and maintaining the system at the recommendation of the annual inspection. Full maintenance is typically required every 24-36 months. Disposal of material should be handled in accordance with local regulations. Please contact CONTECH's Maintenance Department for all questions regarding maintenance at (503) 258-3157 or visit our website at www.conteches.com/maintenance.

Thank you for the opportunity to present this information to you and your client. If you have any questions, please call me at (443-457-1529).

Sincerely,

Taylor Murdock
Stormwater Design Engineer
Contech Engineered Solutions LLC

Summary for Subcatchment 1S: Inlet #1 DA

Runoff = 0.03 cfs @ 1.16 hrs, Volume= 52 cf, Depth= 0.28"

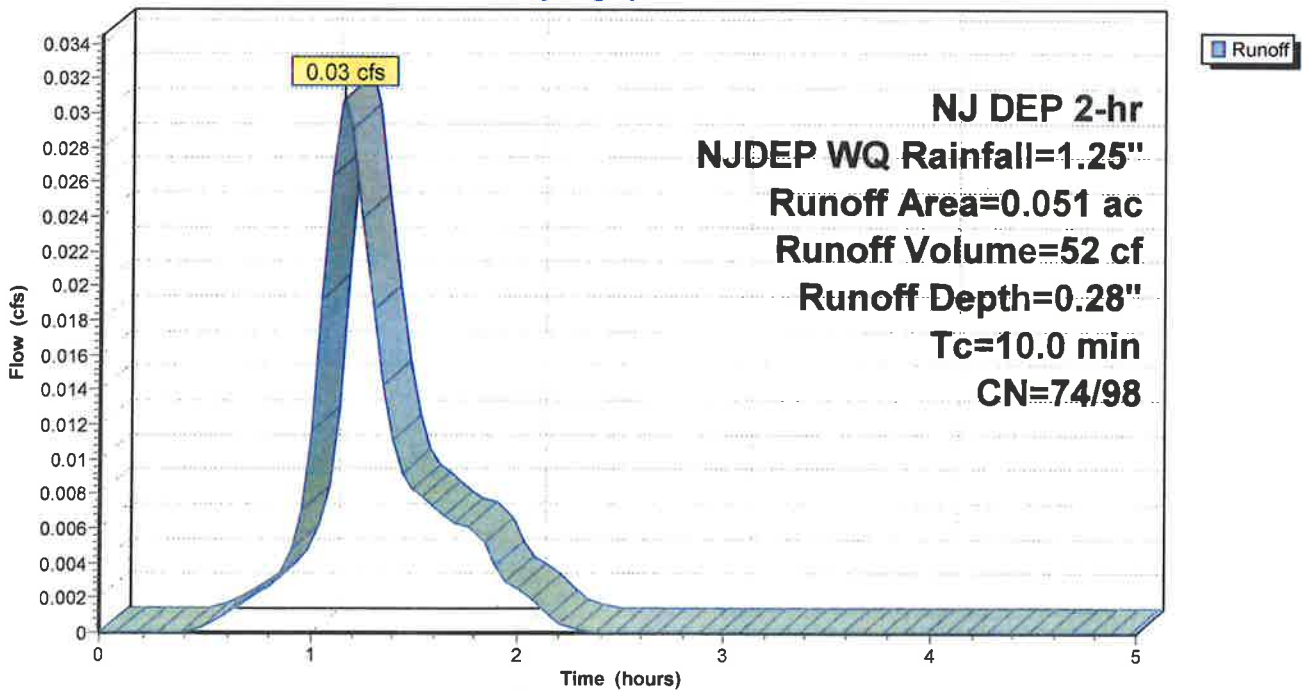
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

Area (ac)	CN	Description
* 0.011	98	
* 0.040	74	
0.051	79	Weighted Average
0.040	74	78.43% Pervious Area
0.011	98	21.57% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry,

Subcatchment 1S: Inlet #1 DA

Hydrograph



Summary for Subcatchment 2S: Inlet #2 DA

Runoff = 0.21 cfs @ 1.15 hrs, Volume= 303 cf, Depth= 0.93"

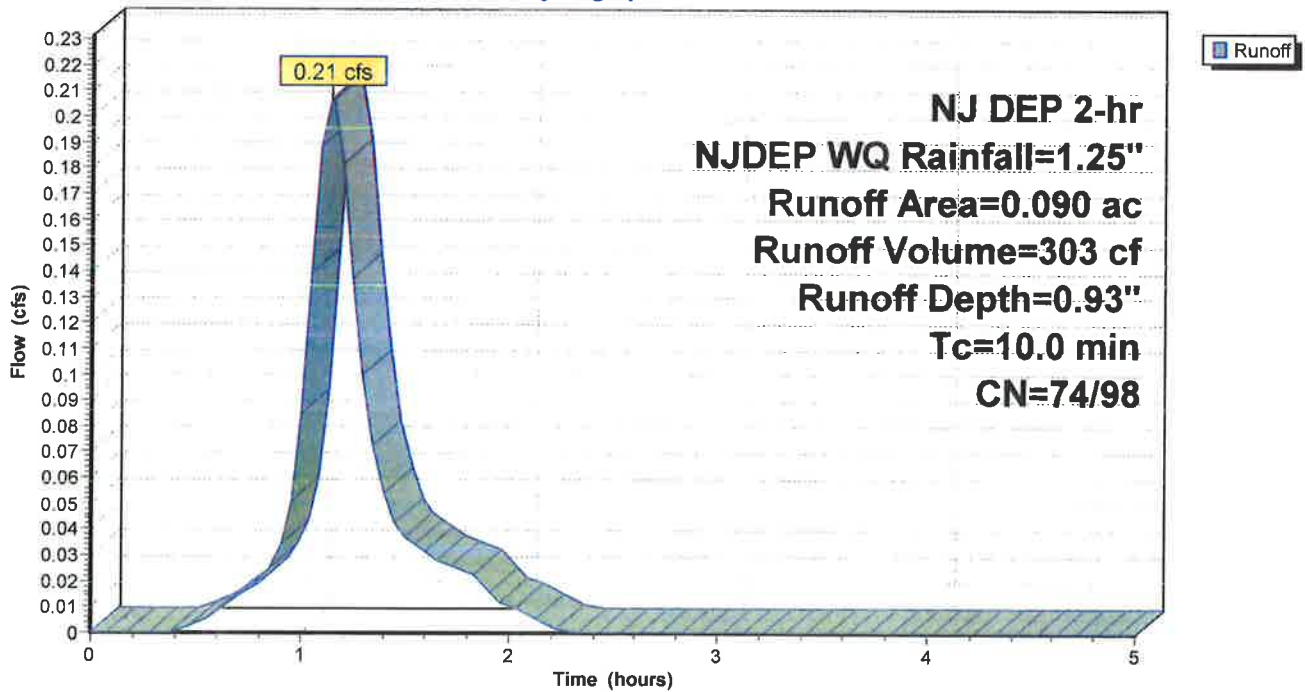
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

Area (ac)	CN	Description
* 0.080	98	
* 0.010	74	
0.090	95	Weighted Average
0.010	74	11.11% Pervious Area
0.080	98	88.89% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry,

Subcatchment 2S: Inlet #2 DA

Hydrograph



Summary for Subcatchment 3S: Inlet #3 DA

Runoff = 0.16 cfs @ 1.15 hrs, Volume= 236 cf, Depth= 0.65"

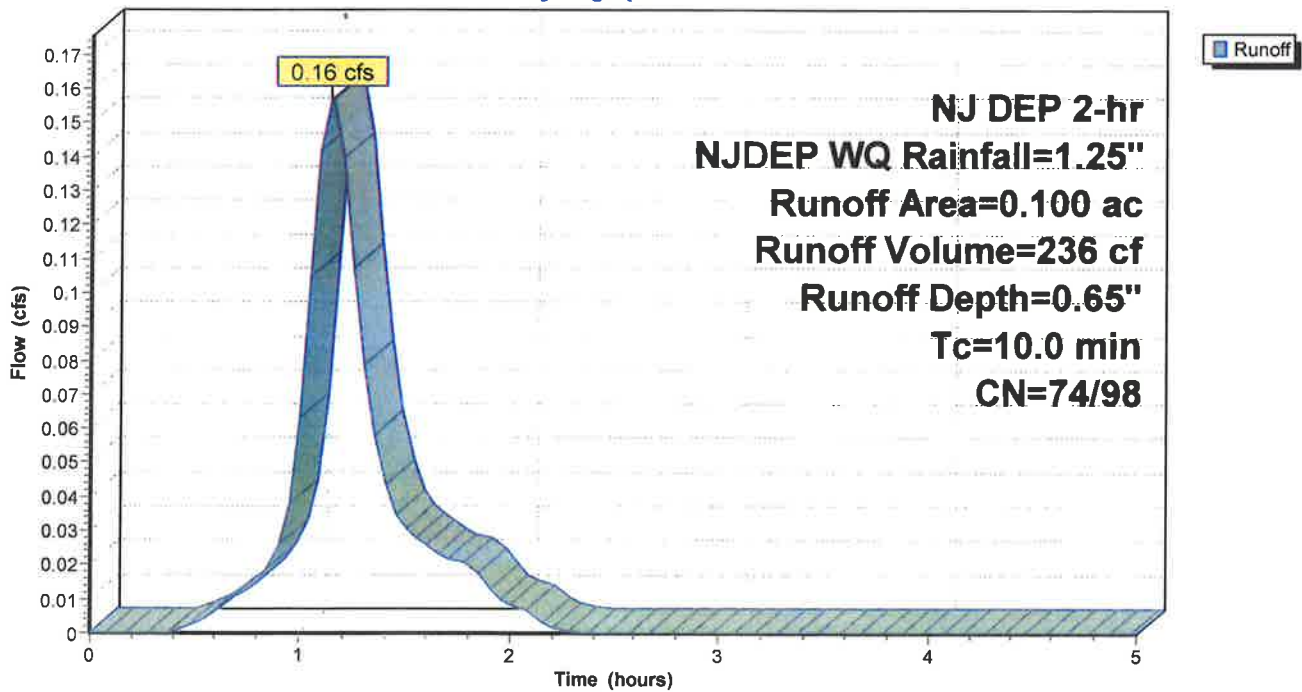
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

Area (ac)	CN	Description
* 0.060	98	
* 0.040	74	
0.100	88	Weighted Average
0.040	74	40.00% Pervious Area
0.060	98	60.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry,

Subcatchment 3S: Inlet #3 DA

Hydrograph



Summary for Subcatchment 4S: Inlet #4 DA

Runoff = 0.18 cfs @ 1.15 hrs, Volume= 263 cf, Depth= 1.03"

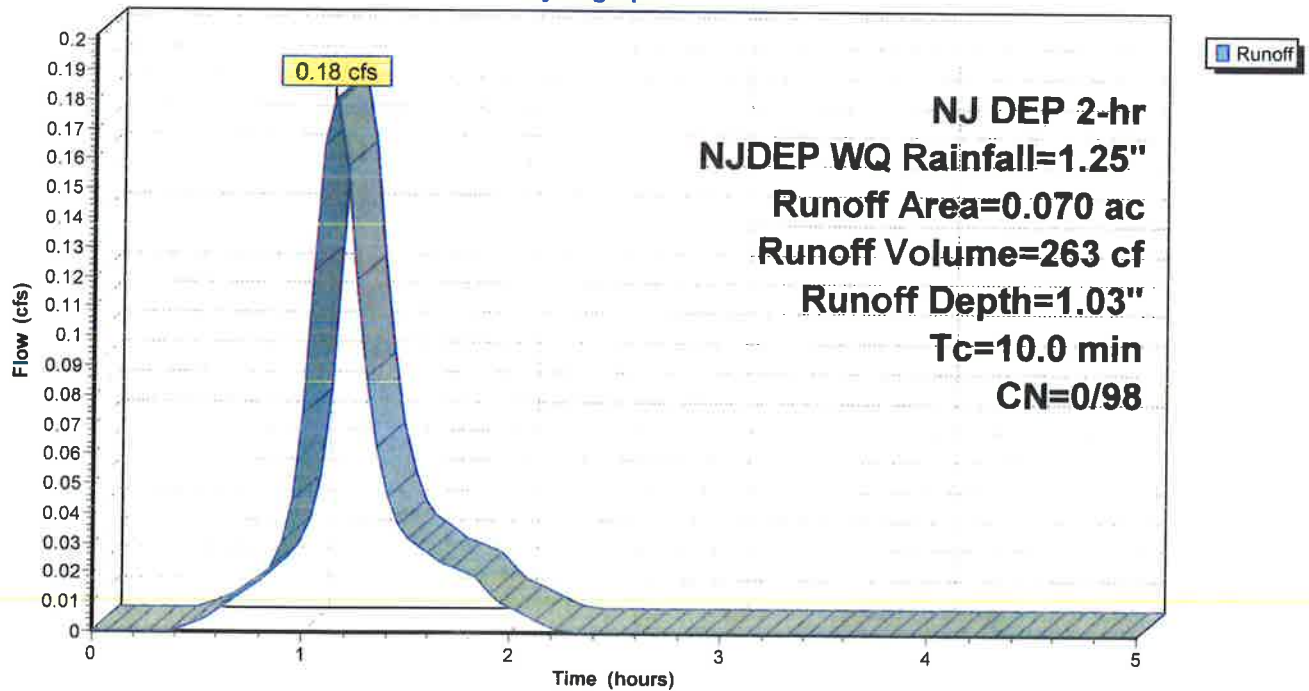
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

Area (ac)	CN	Description
* 0.070	98	
0.070	98	100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry,

Subcatchment 4S: Inlet #4 DA

Hydrograph



Summary for Subcatchment MTD1: MTD #1 Inlet DA

Runoff = 0.39 cfs @ 1.15 hrs, Volume= 566 cf, Depth= 0.97"

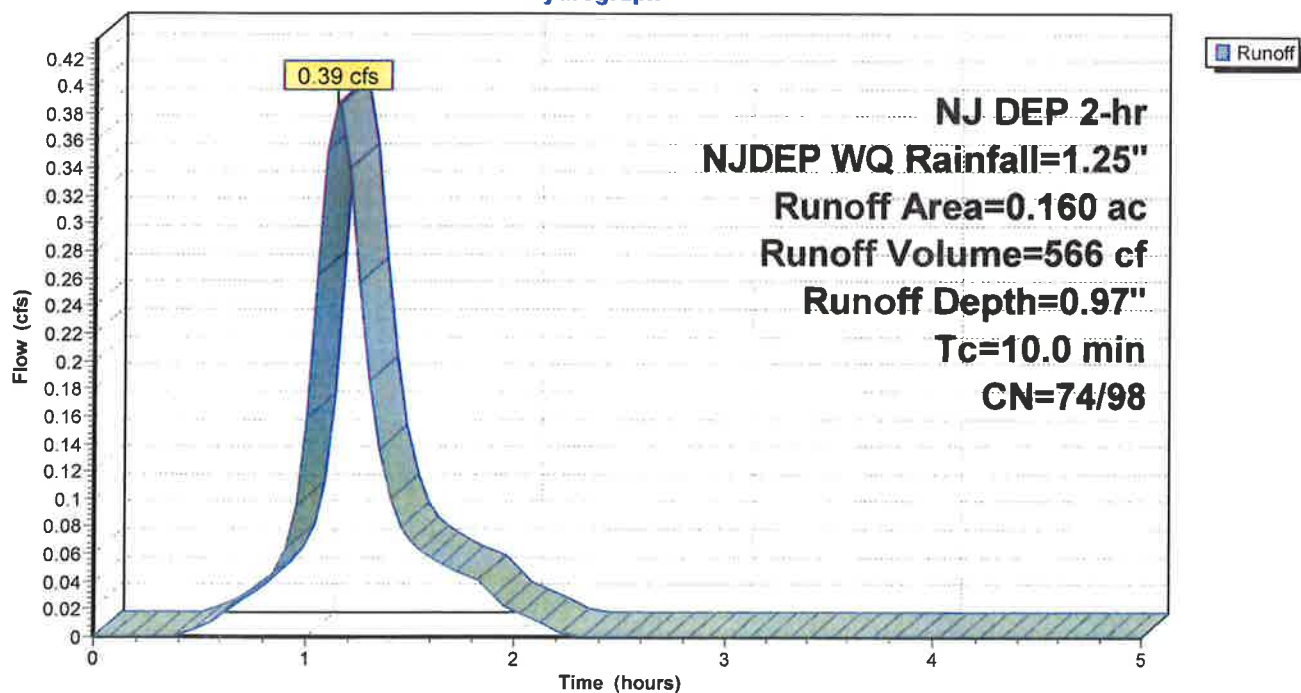
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

Area (ac)	CN	Description
* 0.150	98	
* 0.010	74	
0.160	97	Weighted Average
0.010	74	6.25% Pervious Area
0.150	98	93.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry,

Subcatchment MTD1: MTD #1 Inlet DA

Hydrograph





State of New Jersey

DEPARTMENT OF ENVIRONMENTAL PROTECTION

PHILIP D. MURPHY
Governor

DIVISION OF WATERSHED PROTECTION AND RESTORATION
BUREAU OF NJPDES STORMWATER PERMITTING & WATER QUALITY MANAGEMENT

SHAWN M. LATOURETTE
Commissioner

SHEILA Y. OLIVER
Lt. Governor

P.O. Box 420 Mail Code 501-02A
Trenton, New Jersey 08625-0420
609-633-7021 / Fax: 609-777-0432

www.njstormwater.org

November 18, 2022

Zachariha J. Kent
Vice President of Product Management
Bio Clean Environmental Services, Inc., a Quikrete Company
398 Via El Centro
Oceanside, CA 92058

Re: MTD Lab Certification
Bio Clean High Capacity Kraken Filter Stormwater Treatment Device
Online Installation

TSS Removal Rate 80%

Dear Mr. Kent:

The Stormwater Management rules under N.J.A.C. 7:8-5.2(f) and 5.2(j) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Bio Clean Environmental Services, Inc., a Quikrete company, has requested a Laboratory Certification for the Bio Clean High Capacity Kraken Filter Stormwater Treatment Device (High Capacity Kraken Filter).

The project falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advance Technology" dated January 25, 2013. The applicable protocol is the "New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated October 2022) for this device is published online at <http://www.njcat.org/uploads/newDocs/HCKrakenFilterNJCATFinalReport.pdf>.

The NJDEP certifies the use of the High Capacity Kraken Filter by Bio Clean Environmental Services, Inc. at a TSS removal rate of 80% when designed, operated, and maintained in accordance with the information provided in the Verification Appendix and the following conditions:

1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-

5.5. The MTFR is calculated based on a verified loading rate of 0.101 gpm/ft² of effective membrane filter area.

2. The High Capacity Kraken Filter shall be installed using the same configuration reviewed by NJCAT, and sized in accordance with the criteria specified in item 6 below.
3. This device cannot be used in series with another MTD or a media filter (such as a sand filter) to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
4. Additional design criteria for MTDs can be found in Chapter 11.3 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual, which can be found online at www.njstormwater.org.
5. The maintenance plan for a site using this device shall incorporate, at a minimum, the maintenance requirements for the High Capacity Kraken Filter. A copy of the maintenance plan is attached to this certification. However, it is recommended to review the maintenance website at <https://www.conteches.com/kraken> for any changes to the maintenance requirements.
6. Sizing Requirement:

The example below demonstrates the sizing procedure for the High Capacity Kraken Filter:

Example: A 0.25-acre impervious site is to be treated to 80% TSS removal using a High Capacity Kraken Filter. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs or 354.58 gpm.

The selection of the appropriate model of a High Capacity Kraken Filter is based upon both the maximum inflow drainage area and the MTFR. It is necessary to calculate the required model using both methods and to use the largest model determined by the two methods.

Inflow Drainage Area Evaluation:

The drainage area to the High Capacity Kraken Filter in this example is 0.25 acres. Based upon the information in Table 1 below, the following number of cartridges are required in a High Capacity Kraken Filter to treat the impervious area without exceeding the maximum allowable drainage area:

- a. Twenty-eight (28) 10" cartridges;
- b. Thirteen (13) 20" cartridges; or
- c. Eight (8) 30" cartridges.

Maximum Treatment Flow Rate (MTFR) Evaluation:

The site runoff (Q) was based on the following:

time of concentration = 10 minutes

$i = 3.2$ in/hr (page 74, Fig. 5-16 of Chapter 5 of the NJ Stormwater BMP Manual)

$c = 0.99$ (runoff coefficient for impervious)

$Q = ciA = 0.99 \times 3.2 \times 0.25 = 0.79$ cfs (354.58 gpm)

(Note: 1 cfs = 448.83 gpm)

Given the site runoff is 0.79 cfs and based on Table 1 below, the following minimum numbers of cartridges are required in a High Capacity Kraken Filter without exceeding the MTFR of the individual model:

- a. Seventy-two (72) 10" cartridges;
- b. Thirty-three (33) 20" cartridges; or
- c. Twenty-one (21) 30" cartridges.

The MTFR evaluation results will be used since that method results in the highest minimum configuration determined by the two methods.

The sizing table corresponding to the available system models is noted below. Additional specifications regarding each model can be found in the NJCAT Verification Report in the Verification Appendix under Table A-1.

Table 1. High Capacity Kraken Filter Cartridge MTFRs and Maximum Allowable Drainage Area

Cartridge Height (in)	Cartridge Maximum Treatment Flow Rate (MTFR) (cfs)	Maximum Allowable Drainage Area (acres)
30	0.038	0.032
20	0.024	0.020
10	0.011	0.009

Be advised a detailed maintenance plan is mandatory for any project with a Stormwater BMP subject to the Stormwater Management Rules, N.J.A.C. 7:8. The plan must include all of the items identified in the Stormwater Management Rules, N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of inspection and maintenance equipment and tools, specific corrective and preventative maintenance tasks, indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance and Retrofit of Stormwater Management Measures.

If you have any questions regarding the above information, please contact Changi Wu of my office at chang.i.wu@dep.nj.gov.

Sincerely,



Gabriel Mahon, Chief
Bureau of NJPDES Stormwater Permitting & Water Quality Management
Division of Watershed Protection and Restoration
New Jersey Department of Environmental Protection

Attachment: Maintenance Plan

cc: Richard Magee, NJCAT

Block 502.01, Lot 57.01 (MTD #2)

Franklin Twp, NJ

2/12/24

Information Provided by Engineer:

- Water quality flow rate = 1.09 cfs
- Impervious drainage area = 0.42 ac
- Pervious drainage area = 0.01 ac
- Presiding agency = NJDEP
- Required TSS removal rate = 80%

HC Kraken Filter Information and Cartridge Data:

The High-Capacity Kraken Filter Stormwater Treatment Device is a state-of-the-art stormwater filtration system utilizing pretreatment and advanced membrane filtration to ensure a high level of trash, TSS, metals, nutrients, and hydrocarbons removal. The HC Kraken Filter works by initially passing stormwater through a pretreatment chamber to capture trash, hydrocarbons, and sediments. Once runoff is pretreated, it is directed to the filter chamber where membrane filtration begins. When the water level reaches the top of the membrane filters, the treated water will then pass down the riser tube, collect in the underdrain manifold and flow to the discharge chamber. **The High-Capacity Kraken Filter has received final certification from the NJDEP for 80% TSS removal as a stand-alone treatment system.**

- HC Kraken Filter cartridge height = 20 inches (nominal)
- HC Kraken Filter cartridge surface area = 104.5 square feet
- HC Kraken Filter cartridge loading rate = 0.101 gallons/minute per square foot
- HC Kraken Filter cartridge treatment flow = 0.024 cfs
- **Hydraulic head required = 28.5"** (with 20-inch cartridge)

Design Summary:

The High-Capacity Kraken Filter is sized based on the NJDEP certification, which lists an approved treatment flow rate and maximum impervious acreage limit per cartridge in Table 1. The number of cartridges required based on the impervious drainage area is compared with the number of cartridges required based on the treatment flow rate; the larger number of cartridges governs the sizing.

The HC Kraken Filter for this site was sized to provide **46 cartridges** in order to meet the hydraulic load requirement (calculations shown below). To house this number of cartridges, Contech Engineered Solutions recommends a 6' x 8' precast Shallow HC Kraken Filter.

$$N_{\text{cartridges hyd.load}} = \frac{Q_{\text{treat}}}{Q_{\text{cartridge}}} = \frac{1.09 \text{ cfs}}{0.024 \text{ cfs/cartridge}} = 45.42 \Rightarrow (46) \text{ 20" Cartridges}$$

$$N_{\text{cartridges mass load}} = \frac{\text{Area}_{\text{site}}}{\text{Max Area}_{\text{cartridge}}} = \frac{0.42 \text{ acres}}{0.020 \text{ acres/cartridge}} = 21.00 \Rightarrow (21) \text{ 20" Cartridges}$$



HC Kraken Filter Design Summary

Maintenance:

Maintenance of Stormwater best management practices is required per the New Jersey Administrative Code 7:8-5.8. Recommendations for maintenance are included in chapters 8 & 9 of the New Jersey Stormwater Best Management Practices Manual. To comply with requirements, CONTECH offers a network of Preferred Service Providers that have the capability to perform all necessary inspections, compliance reporting and cleaning services. CONTECH recommends inspecting the system annually and maintaining the system at the recommendation of the annual inspection. Full maintenance is typically required every 24-36 months. Disposal of material should be handled in accordance with local regulations. Please contact CONTECH's Maintenance Department for all questions regarding maintenance at (503) 258-3157 or visit our website at www.conteches.com/maintenance.

Thank you for the opportunity to present this information to you and your client. If you have any questions, please call me at (443-457-1529).

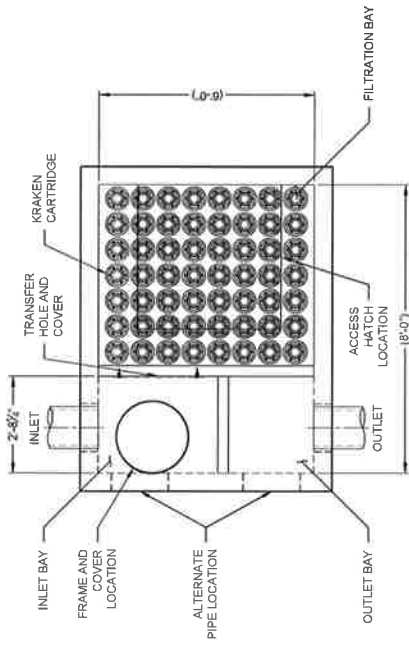
Sincerely,

Taylor Murdock
Stormwater Design Engineer
Contech Engineered Solutions LLC

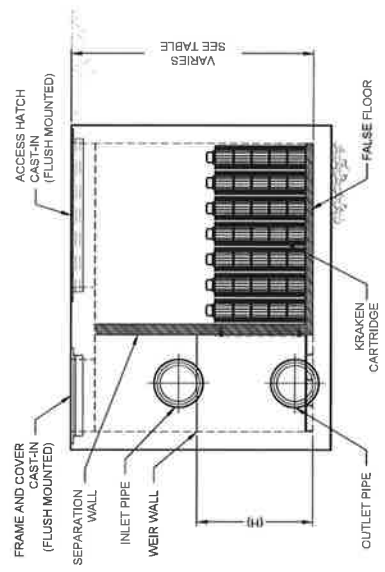
KRAKEN FILTER DESIGN NOTES

- KRAKEN FILTER TREATMENT CAPACITY VARIES BY CARTRIDGE COUNT AND LOCALLY APPROVED SURFACE AREA SPECIFIC FLOW RATE. PEAK FLOW RATE CAPACITY TO BE DETERMINED BY ENGINEER OF RECORD.
- KRAKEN FILTERS ARE SUPPLIED WITH THE MAXIMUM NUMBER OF CARTRIDGES (66) AND IS AVAILABLE IN:
 - A LEFT INLET (AS SHOWN) OR A RIGHT INLET.
 - A LEFT INLET AND RIGHT INLET.
- ALL PARTS AND INTERNAL ASSEMBLY PROVIDED BY CONTECH UNLESS NOTED OTHERWISE.

CARTRIDGE HEIGHT	30"	20"	10"
RECOMMENDED HYDRAULIC DROP (H)	38.5"	28.5"	18.5"
SPECIFIC FLOW RATE (gpm/sf)	0.10	0.10	0.10
CARTRIDGE FLOW RATE (gpm)	17	10.6	4.9



PLAN

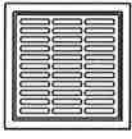


ELEVATION

SITE SPECIFIC DATA REQUIREMENTS

STRUCTURE ID	
WATER QUALITY FLOW RATE (cfs)	
PEAK FLOW RATE (cfs)	
RETURN PERIOD OF PEAK FLOW (yr)	
CARTRIDGE FLOW RATE	
CARTRIDGE SIZE (30" 20" 10")	
NUMBER OF CARTRIDGES REQUIRED	
INLET BAY RIM ELEVATION	
FILTER BAY RIM ELEVATION	
PIPE DATA	
INLET PIPE 1	
INLET PIPE 2	
OUTLET PIPE	
NOTES/SPECIAL REQUIREMENTS	

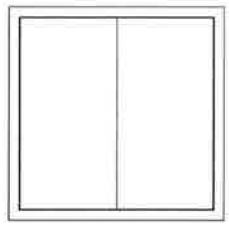
RIM TO SYSTEM INVERT		
CARTRIDGE SIZE	MIN. HEIGHT	MAX. HEIGHT
10" & 20"	3'-6"	4'-10"
30"	4'-2"	4'-10"



FRAME AND GRATE
(SIZE MAY VARY)
(NOT TO SCALE)



FRAME AND COVER
(30" ROUND)
(NOT TO SCALE)



ACCESS HATCH
(48" SQUARE)
(NOT TO SCALE)

GENERAL NOTES

- CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
 - DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
 - FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHTS. PLEASE CONTACT YOUR CONTECH REPRESENTATIVE. www.conteches.com
 - KRAKEN FILTER WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING. CONTRACTOR TO CONFIRM STRUCTURE MEETS REQUIREMENTS OF PROJECT.
 - STRUCTURE SHALL MEET AASHTO HS20 LOAD RATING. ASSUMING EARTH COVER OF 0' - 10' AND GROUNDWATER ELEVATION AT OR BELOW THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS SHALL MEET AASHTO M306 AND BE CAST WITH THE CONTECH LOGO.
- #### INSTALLATION NOTES
- ANY SUB-BASE BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
 - CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE KRAKEN FILTER STRUCTURE.
 - CONTRACTOR TO INSTALL JOINT SEALANT BETWEEN ALL SECTIONS AND ASSEMBLY STRUCTURE.
 - CONTRACTOR TO PROVIDE INSTALL AND GROUT PIPES. MATCH OUTLET PIPE INVERT WITH OUTLET BAY FLOOR.
 - CONTRACTOR TO TAKE APPROPRIATE MEASURES TO PROTECT CARTRIDGES FROM CONSTRUCTION-RELATED EROSION RUNOFF.
 - CONTRACTOR TO REMOVE THE TRANSFER OPENING COVER WHEN THE SYSTEM IS BROUGHT ONLINE.

CONTECH
ENGINEERED SOLUTIONS LLC
www.conteches.com
9100 Centre Pointe Dr., Suite 400, West Chester, OH 45388
800-338-1122 513-645-7000 513-645-7993 FAX

KFPD0608 (6' x 8')
PEAK DIVERSION KRAKEN FILTER
SHALLOW
STANDARD DETAIL

THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING US PATENTS: 8,614,601; 8,785,103; 8,949,466; 11,260,327; RELATED FOREIGN PATENTS OR OTHER PATENT PENDING

Summary for Subcatchment 5S: Inlet #5 DA

Runoff = 0.21 cfs @ 1.15 hrs, Volume= 300 cf, Depth= 1.03"

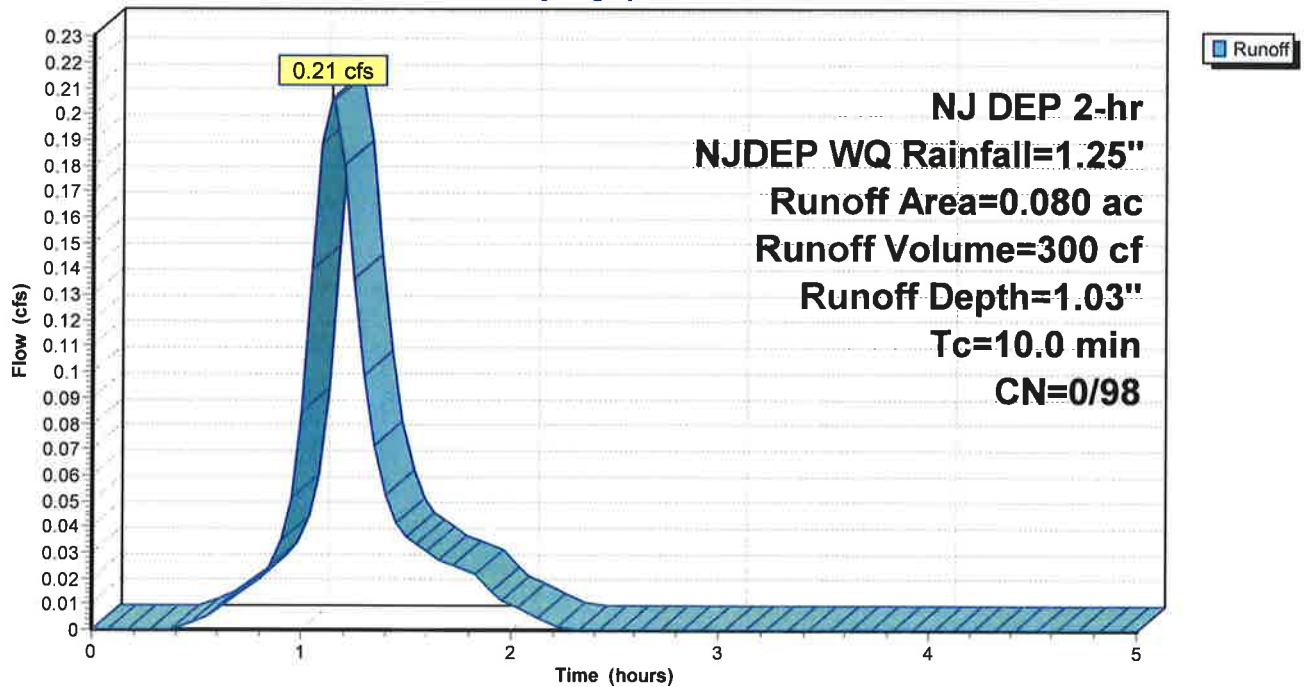
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

Area (ac)	CN	Description
* 0.080	98	
0.080	98	100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry,

Subcatchment 5S: Inlet #5 DA

Hydrograph



Summary for Subcatchment MTD2: MTD #2 Inlet DA

Runoff = 0.88 cfs @ 1.15 hrs, Volume= 1,280 cf, Depth= 1.01"

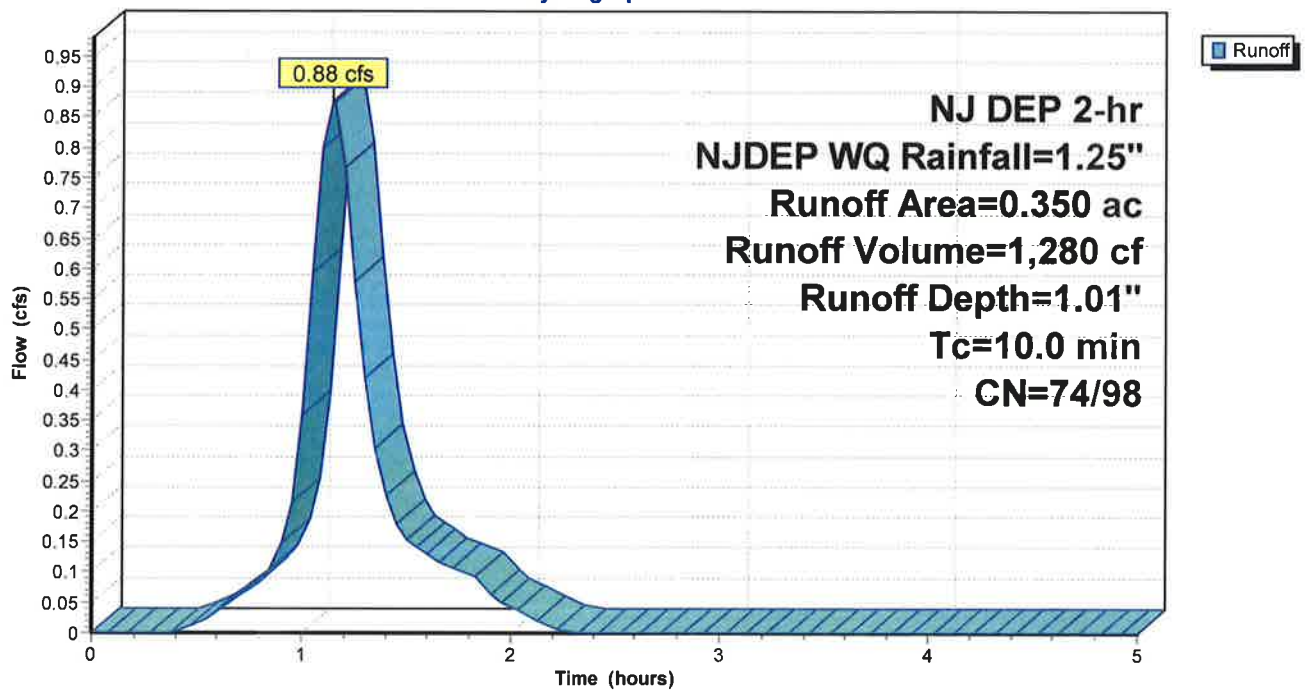
Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs
 NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

Area (ac)	CN	Description
* 0.340	98	
* 0.010	74	
0.350	97	Weighted Average
0.010	74	2.86% Pervious Area
0.340	98	97.14% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.0					Direct Entry,

Subcatchment MTD2: MTD #2 Inlet DA

Hydrograph





State of New Jersey

DEPARTMENT OF ENVIRONMENTAL PROTECTION

PHILIP D. MURPHY
Governor

DIVISION OF WATERSHED PROTECTION AND RESTORATION
BUREAU OF NJPDES STORMWATER PERMITTING & WATER QUALITY MANAGEMENT

SHAWN M. LATOURETTE
Commissioner

SHEILA Y. OLIVER
Lt. Governor

P.O. Box 420 Mail Code 501-02A
Trenton, New Jersey 08625-0420
609-633-7021 / Fax: 609-777-0432

www.njstormwater.org

November 18, 2022

Zachariha J. Kent
Vice President of Product Management
Bio Clean Environmental Services, Inc., a Quikrete Company
398 Via El Centro
Oceanside, CA 92058

Re: MTD Lab Certification
Bio Clean High Capacity Kraken Filter Stormwater Treatment Device
Online Installation

TSS Removal Rate 80%

Dear Mr. Kent:

The Stormwater Management rules under N.J.A.C. 7:8-5.2(f) and 5.2(j) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Bio Clean Environmental Services, Inc., a Quikrete company, has requested a Laboratory Certification for the Bio Clean High Capacity Kraken Filter Stormwater Treatment Device (High Capacity Kraken Filter).

The project falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advance Technology" dated January 25, 2013. The applicable protocol is the "New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated October 2022) for this device is published online at <http://www.njcat.org/uploads/newDocs/HCKrakenFilterNJCATFinalReport.pdf>.

The NJDEP certifies the use of the High Capacity Kraken Filter by Bio Clean Environmental Services, Inc. at a TSS removal rate of 80% when designed, operated, and maintained in accordance with the information provided in the Verification Appendix and the following conditions:

1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-

5.5. The MTFR is calculated based on a verified loading rate of 0.101 gpm/ft² of effective membrane filter area.

2. The High Capacity Kraken Filter shall be installed using the same configuration reviewed by NJCAT, and sized in accordance with the criteria specified in item 6 below.
3. This device cannot be used in series with another MTD or a media filter (such as a sand filter) to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
4. Additional design criteria for MTDs can be found in Chapter 11.3 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual, which can be found online at www.njstormwater.org.
5. The maintenance plan for a site using this device shall incorporate, at a minimum, the maintenance requirements for the High Capacity Kraken Filter. A copy of the maintenance plan is attached to this certification. However, it is recommended to review the maintenance website at <https://www.conteches.com/kraken> for any changes to the maintenance requirements.
6. Sizing Requirement:

The example below demonstrates the sizing procedure for the High Capacity Kraken Filter:

Example: A 0.25-acre impervious site is to be treated to 80% TSS removal using a High Capacity Kraken Filter. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs or 354.58 gpm.

The selection of the appropriate model of a High Capacity Kraken Filter is based upon both the maximum inflow drainage area and the MTFR. It is necessary to calculate the required model using both methods and to use the largest model determined by the two methods.

Inflow Drainage Area Evaluation:

The drainage area to the High Capacity Kraken Filter in this example is 0.25 acres. Based upon the information in Table 1 below, the following number of cartridges are required in a High Capacity Kraken Filter to treat the impervious area without exceeding the maximum allowable drainage area:

- a. Twenty-eight (28) 10" cartridges;
- b. Thirteen (13) 20" cartridges; or
- c. Eight (8) 30" cartridges.

Maximum Treatment Flow Rate (MTFR) Evaluation:

The site runoff (Q) was based on the following:

time of concentration = 10 minutes

i = 3.2 in/hr (page 74, Fig. 5-16 of Chapter 5 of the NJ Stormwater BMP Manual)

c = 0.99 (runoff coefficient for impervious)

$Q = ciA = 0.99 \times 3.2 \times 0.25 = 0.79 \text{ cfs (354.58 gpm)}$

(Note: 1 cfs = 448.83 gpm)

Given the site runoff is 0.79 cfs and based on Table 1 below, the following minimum numbers of cartridges are required in a High Capacity Kraken Filter without exceeding the MTFR of the individual model:

- a. Seventy-two (72) 10” cartridges;
- b. Thirty-three (33) 20” cartridges; or
- c. Twenty-one (21) 30” cartridges.

The MTFR evaluation results will be used since that method results in the highest minimum configuration determined by the two methods.

The sizing table corresponding to the available system models is noted below. Additional specifications regarding each model can be found in the NJCAT Verification Report in the Verification Appendix under Table A-1.

Table 1. High Capacity Kraken Filter Cartridge MTFRs and Maximum Allowable Drainage Area

Cartridge Height (in)	Cartridge Maximum Treatment Flow Rate (MTFR) (cfs)	Maximum Allowable Drainage Area (acres)
30	0.038	0.032
20	0.024	0.020
10	0.011	0.009

Be advised a detailed maintenance plan is mandatory for any project with a Stormwater BMP subject to the Stormwater Management Rules, N.J.A.C. 7:8. The plan must include all of the items identified in the Stormwater Management Rules, N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of inspection and maintenance equipment and tools, specific corrective and preventative maintenance tasks, indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance and Retrofit of Stormwater Management Measures.

If you have any questions regarding the above information, please contact Changi Wu of my office at chang.i.wu@dep.nj.gov.

Sincerely,

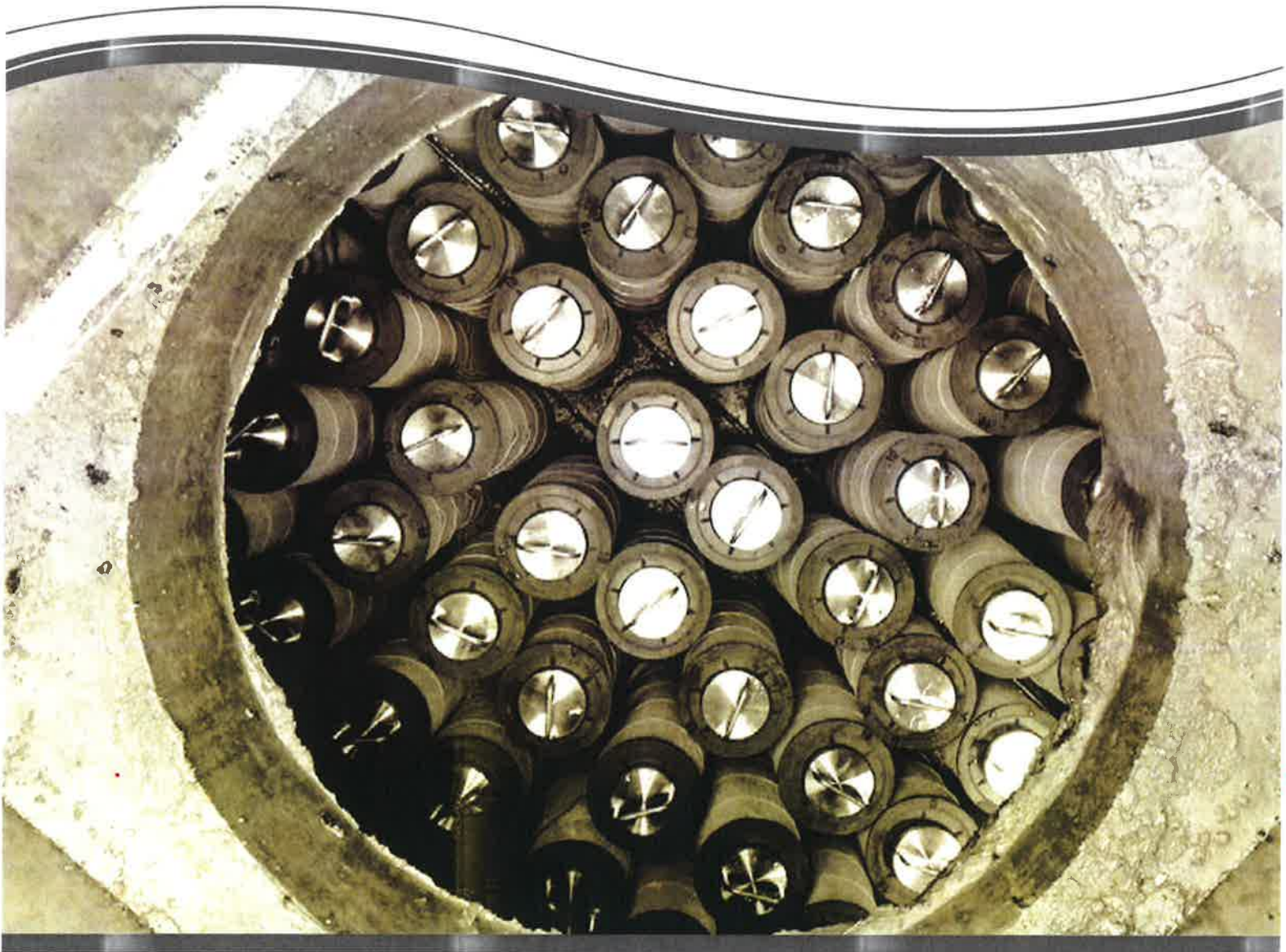


Gabriel Mahon, Chief
Bureau of NJPDES Stormwater Permitting & Water Quality Management
Division of Watershed Protection and Restoration
New Jersey Department of Environmental Protection

Attachment: Maintenance Plan

cc: Richard Magee, NJCAT

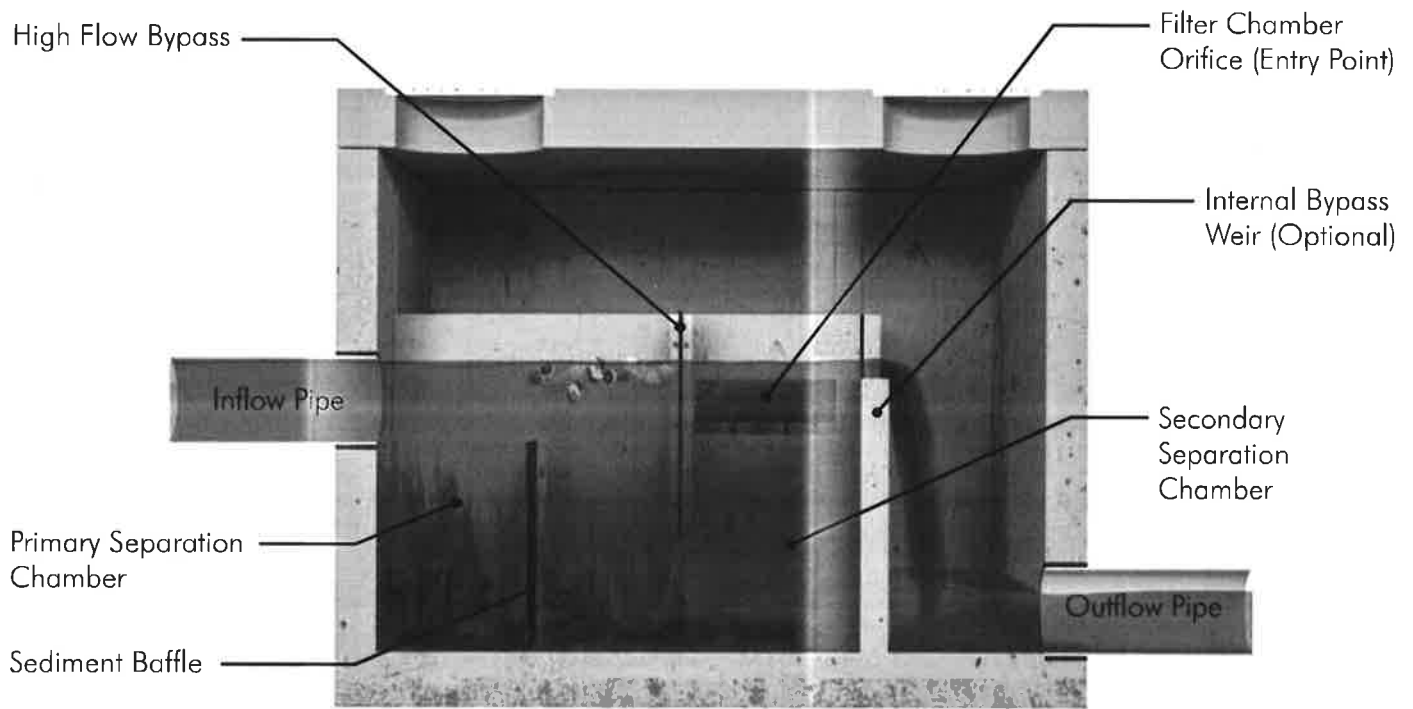
**Kraken[®] Filter
Operation & Maintenance Manual**



Operation & Maintenance

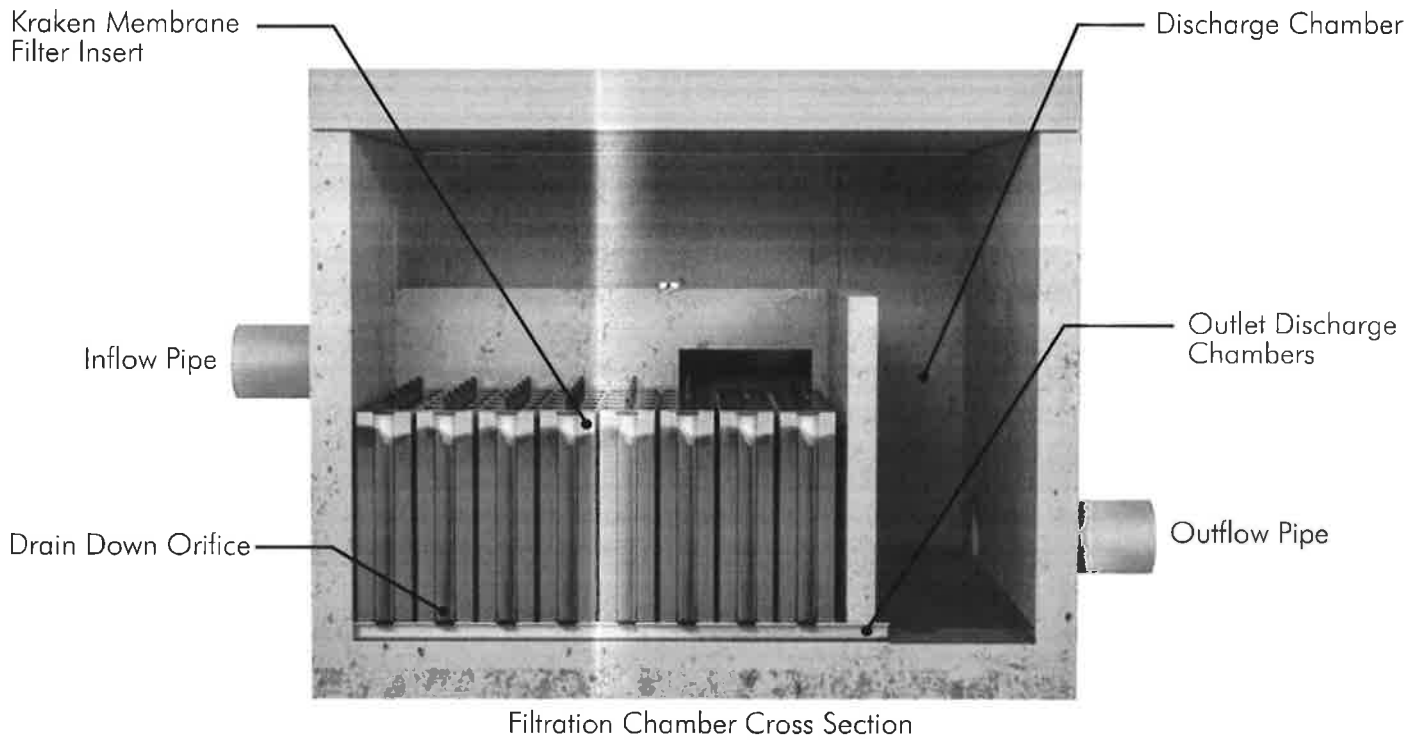
The Kraken[®] Filter is designed at a minimal loading rate of only 0.05 gpm/sq ft of media surface to maximize longevity and minimize maintenance requirements. Passive backwash and pretreatment also help to minimize system maintenance requirements. The Kraken[®] Filter is estimated to be able to handle up to at least 18 months sediment loading with no maintenance or loss of treatment capacity assuming 600 pounds of sediment per acre of impervious surface annually.

Yet, as with all stormwater BMPs, inspection and maintenance on the Kraken[®] Filter is necessary. Stormwater regulations require that all BMPs be inspected and maintained to ensure they are operating as designed to allow for effective pollutant removal and to provide protection to receiving water bodies. It is recommended that inspections be performed multiple times during the first year to assess the site specific loading conditions. This is recommended because pollutant loading and pollutant characteristics can vary greatly from site to site. Variables such as nearby soil erosion or construction sites, winter sanding on roads, amount of daily traffic and land use can increase pollutant loading on the system. Observations made during the first year of inspections can be used to estimate inspection and maintenance intervals for subsequent years to ensure appropriate maintenance is provided. Without appropriate maintenance, a BMP will exceed its storage capacity which can negatively affect its continued performance in removing and retaining captured pollutants.



Pretreatment Chamber Cross Section

Pretreatment Chamber Diagram



Filter Chamber Diagram

Inspection Equipment

Following is a list of equipment to allow for simple and effective inspection of the Kraken® Filter:

- Contech Inspection Form
- Flashlight
- Manhole hook or appropriate tools to access hatches and covers
- Appropriate traffic control signage and procedures
- Measuring pole and/or tape measure
- Protective clothing and eye protection



Inspection Steps

The core to any successful stormwater BMP maintenance program is routine inspections. The inspection steps required on the Kraken[®] Filter are quick and easy. As mentioned above, the first year should be seen as the maintenance interval establishment phase. During the first year, more frequent inspections should occur in order to gather loading data and maintenance requirements for that specific site. This information can be used to plan future inspection and maintenance intervals.

The Kraken[®] Filter can be inspected through visual observation without entry into the system. All necessary pre-inspection steps must be carried out before inspection occurs, especially traffic control and other safety measures to protect the inspector and near-by pedestrians from any dangers associated with an open access hatch or manhole. Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine inspections of the system. Once these access covers have been safely opened the inspection process can proceed:

- Prepare the inspection form by writing in the necessary information including project name, location, date & time, unit number and other info (see inspection form).
- Observe the inside of the system through the access hatches. If minimal light is available and vision into the unit is impaired, utilize a flashlight to see inside the system and all of its chambers.
- Look for any obstructions in the inflow pipe, pre-treatment chamber, filter chambers, discharge chamber or outflow pipe. Write down any observations on the inspection form.
- Through observation and/or digital photographs, estimate the amount of floatable debris accumulated in the pre-treatment chamber. Record this information on the inspection form. Next, utilizing a tape measure or measuring stick, estimate the amount of sediment accumulated in the primary and secondary sedimentation chambers. Record this depth on the inspection form. Through visual observation, inspect the condition of the filter cartridges. Look for excessive build-up of sediments on the surface and any build-up on the top of the cartridges. Record this information on the inspection form.
- Finalize inspection report for analysis by the maintenance manager to determine if maintenance is required.

Maintenance Indicators

Based upon observations made during inspection, maintenance of the system may be required based on the following indicators:

- Missing or damaged internal components or cartridges
- Obstructions in the system or its inlet or outlet
- Accumulation of floatables in the pre-treatment chambers in which the length and width of the chamber behind oil/floatables skimmer is fully impacted
- Accumulation of sediment in the primary sedimentation chamber of more than 18" in depth
- Accumulation of sediment in the secondary sedimentation chamber of more than 6" in depth
- Accumulation of sediment in the filter chambers of more than 3" on average
- Substantial build-up of sediments on the filter membrane of the filter cartridges which will have a very dark appearance indicating the membrane may be fully saturated with sediment

The Kraken Filter vault is a robust system and is designed for treating and bypassing (when required) flow rates calculated by the Engineer of Record. Under the designed conditions with routine maintenance and inspections, the Kraken Filter should function for many years. The Kraken Filter can fail under certain conditions, such as: severe damage and cracking through the vault walls, internal weir and baffle walls falling out of place, blockages of the flow path such as inlet or outlet, filters not reset properly, excessive debris or sediment accumulation within the vault and on the filters. With proper maintenance these risks can be avoided. Contech representatives are also available for troubleshooting.

Maintenance Equipment

While maintenance can be done fully by hand, it is recommended that a vacuum truck be utilized to minimize time required to maintain the Kraken® Filter:

- Contech Maintenance Form
- Flashlight
- Manhole hook or appropriate tools to access hatches and covers
- Appropriate traffic control signage and procedures
- Measuring pole and/or tape measure
- Protective clothing and eye protection
- Vacuum truck
- Trash can
- Pressure washer

Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine inspections of the system. Entry into the system will be required if it is determined the cartridge filters need washing/cleaning

Maintenance Procedures

It is recommended that maintenance occurs at least three days after the most recent rain event to allow for drain down of the system and any upstream detention systems designed to drain down over an extended period of time. Maintaining the system while flows are still entering it will increase the time and complexity required for maintenance. Cleaning of the pre-treatment chamber can be performed from finish surface without entry into the vault utilizing a vacuum truck. Once all safety measures have been set up, cleaning of the pre-treatment chamber can proceed as follows:

- Following rules for confined space entry, use a gas meter to detect the presence of any hazardous gases. If hazardous gases are present, do not enter the vault. Following appropriate confined space procedures, take steps, such as utilizing a venting system, to address the hazard. Once it is determined to be safe, enter utilizing appropriate entry equipment such as a ladder and tripod with harness.
- Once entry into the system has been established the maintenance technician should position themselves to stand in the pre-treatment chamber. From here, the removal of the cartridges can commence.
- Threaded couplings are used now, but old systems will have the pressure fitted coupling. Each cartridge that is pressure fitted in place will include a handle for easy removal. To remove a cartridge, simply grab the handle and pull straight up. It may be required to gently shift pressure from side to side while pulling up to break the pressure seal. Removal of the cartridge should be done by hand with minimal effort and requires no tools.
- Once the cartridges are removed, they should be lifted out from the vault and brought up to finish surface for cleaning. Using a large garbage can and a standard garden hose (low pressure nozzle), each cartridge should be rinsed off from the outside to remove accumulated sediments and debris. Once each cartridge is rinsed, it should be placed to the side for re-installation.

- Each filter chamber should be power washed and vacuumed clean before re-inserting the cleaned cartridges.
- After all cartridges have been washed, they can be replaced back into the vault. To replace each cartridge, simply slide cartridge over each pressure fitted coupler. Threaded couplings are used now, but old systems will have the pressure fitted coupling. Push down on the handle to ensure the cartridge has been fully seated and the bottom of the cartridge is making contact with the floor.
- The last step is to replace all access hatch lids and remove all traffic control.
- All removed debris and pollutants shall be disposed of following local and state requirements.

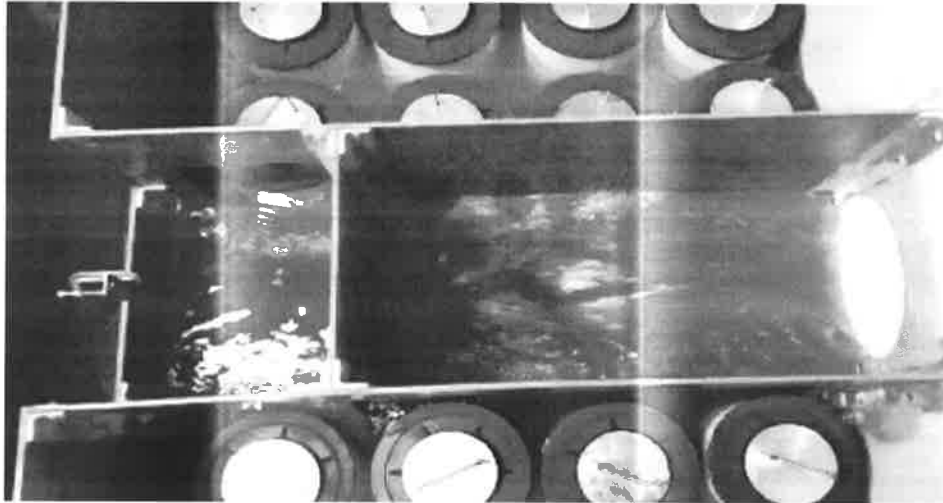
Maintenance Sequence



1. Remove access hatches set up vacuum truck to clean the pretreatment chamber.



2. Insert vacuum hose in the sedimentation chamber and vacuum out all trash, sediment and standing water.



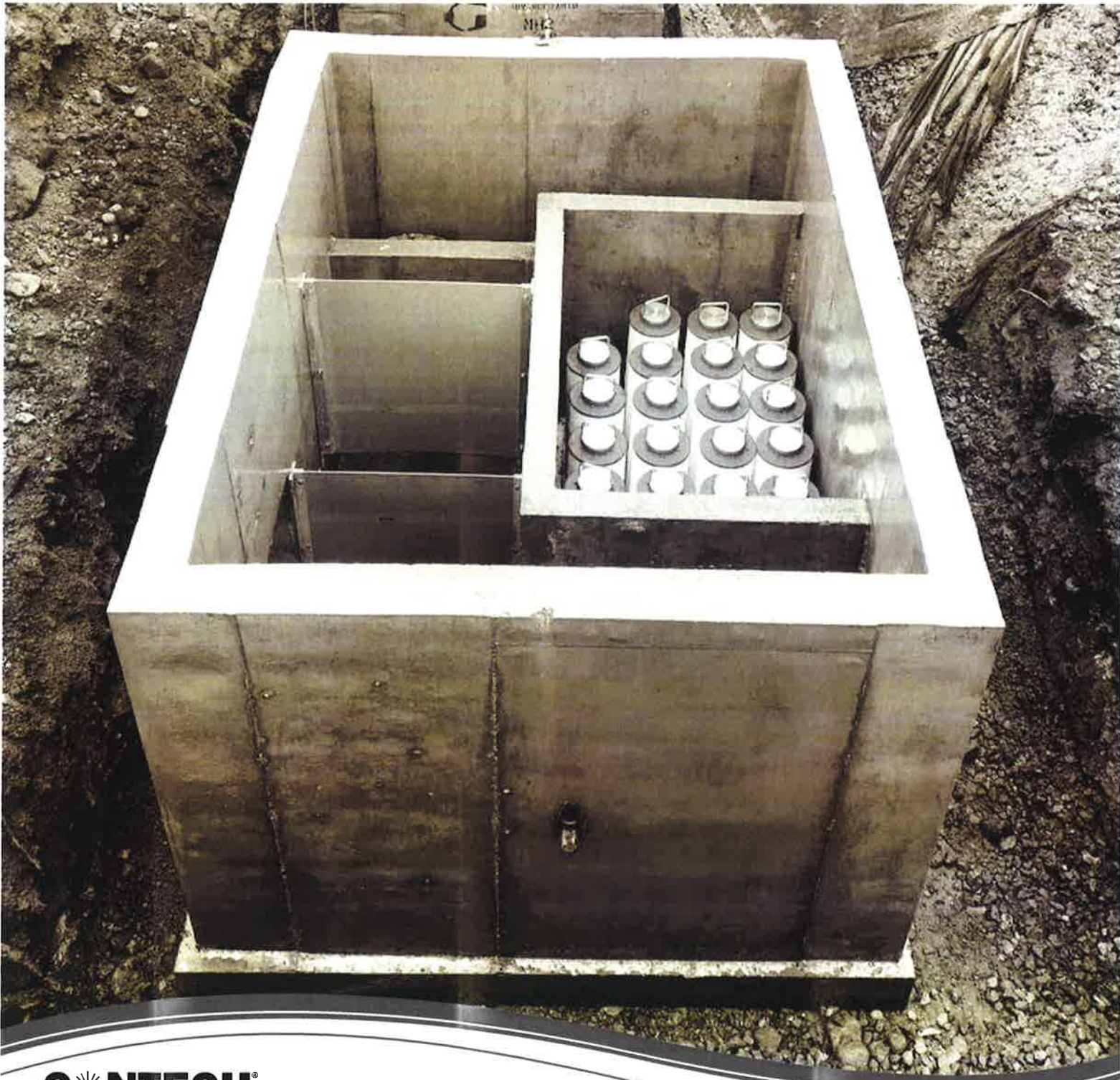
3. Assess the condition of the filter cartridges and determine if cleaning is required.



4. To wash cartridges, remove from vault. Place over trash can and use a garden hose to spray clean.



5. Once cleaned, install back into the vault. This completes maintenance. Ensure access lids are properly replaced.



CONTECH[®] ENGINEERED SOLUTIONS

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800-338-1122

WWW.CONTECHES.COM

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SUPPORT

DRAWINGS AND SPECIFICATIONS ARE AVAILABLE AT WWW.CONTECHES.COM

Kraken Maintenance Guide 08/22

APPENDIX D: PRE AND POST DEVELOPMENT DRAINAGE AREA MAP DATED 2/18/24

APPENDIX E:

SOIL PROFILES AND SOIL PERMEABILITY TEST DATA

Kashi Consulting Company, Inc.

Shrinath J Kotdawala, Ph.D., P.E.

Gary Chiang, P.E.

983 Route 33, Unit D, Monroe Township, NJ - 08831, shri@kashiinc.com
54 Oakland Mills Rd, Manalapan, NJ - 07726, Phone: (848) 203 7460

SOIL INVESTIGATION CONDUCTED FOR DETERMINING WATER TABLE AND PERMEABILITY RATINGS

Date of Investigations: 12/16/2023

Method of Excavation: Large Track Hoe, Water Tank and Helpers

Excavator: Rey Wittmann, JW Landscape Contractors Inc., 39 Minnan Street
Rahway, NJ - 07065

Weather: Sunny to Partially Sunny

Lot #1

Depth: Descriptions:

0" - 8" Top Soil (Dark Reddish Brown) - 2.5 YR (3/2), Sub Angular Blocky, Friable
8" - 34" Silty Clay, Dark Reddish Brown, Firm to Friable - 5 YR (4/4)
34" - 120" Fragmented Shale, Dark Reddish Brown (60" - 90" Depth - The shale layer is very hard)), 2.5 YR (3/6), Rippable, More than 80% non-soil shale fragments, 6" - 12" size plates with depth size increases, Water Table Observed at 7'.

Log #2

Depth: Descriptions:

0" - 6" Top Soil (Dark Reddish) - 2.5 YR (3/2)
6" - 42" Clay Loam, Dark Reddish Brown, Blocky, Friable - 5 YR (4/4)
42" - 120" Fragments Platy Shale, Dark Reddish Brown (60" - 90" Depth - The shale is very hard), More than 80% non-soil shale fragments
A PERC test conducted at the depths of 72" (From 84" and deeper - very platy structure), Water Table Observed at 7'.

Log #4

0" - 12" Top Soil (Dark Reddish), - 2.5 YR (3/2)
12" - 41" Clay Loam, Dark Reddish Brown, Blocky, Friable, - 5 YR (4/4)
41" - 132" Fragmented Platy Shale, Dark Reddish Brown (60" - 90" Depth - The shale is very hard), (24" - 48" Very Platy, 48" - 72" Very Hard Ripping, 72" - 120"), Very platy and Fragmented.

Log #5:

0" - 8" Top Soil (Dark Reddish) - 2.5 YR (3/2)
8" - 38" Clay Loam, Dark Reddish Brown, Blocky and Sub angular, Friable, 5 YR (4/4)
38" - 120" Fragmented Platy Shale, Dark Reddish Brown, Alternative Very Firm to Rippable Shale layer, With depths the size of shale increases to 8" - 12" platy and in blocks. Water Table at 72")

* The fragmented shale layers showed seams, which were hard to rip. A machine with rippable teeth required for this investigations.

(Service Provider In Areas of Civil, Environmental & Geotechnical Engineering)

Date of Test:12/16/2023 –Basin Flood*

Location of Pit – Log #1

Size of Pit – 3' x 8'

Depth of Fractured Shale: 60" (Bottom of Test Elevation) – gallons poured - 375 per fill

Time Basin Flooded (1st Fill): 15:10

Time to Empty Basin: 15:45

Time Basin Flooded (2nd Fill): 15:55

Time to Empty Basin: 16:40

Location of Pit – Log #4

Size of Pit – 3' x 8'

Depth of Fractured Shale: 78" (Bottom of Test Elevation) – gallons poured - 375 per fill

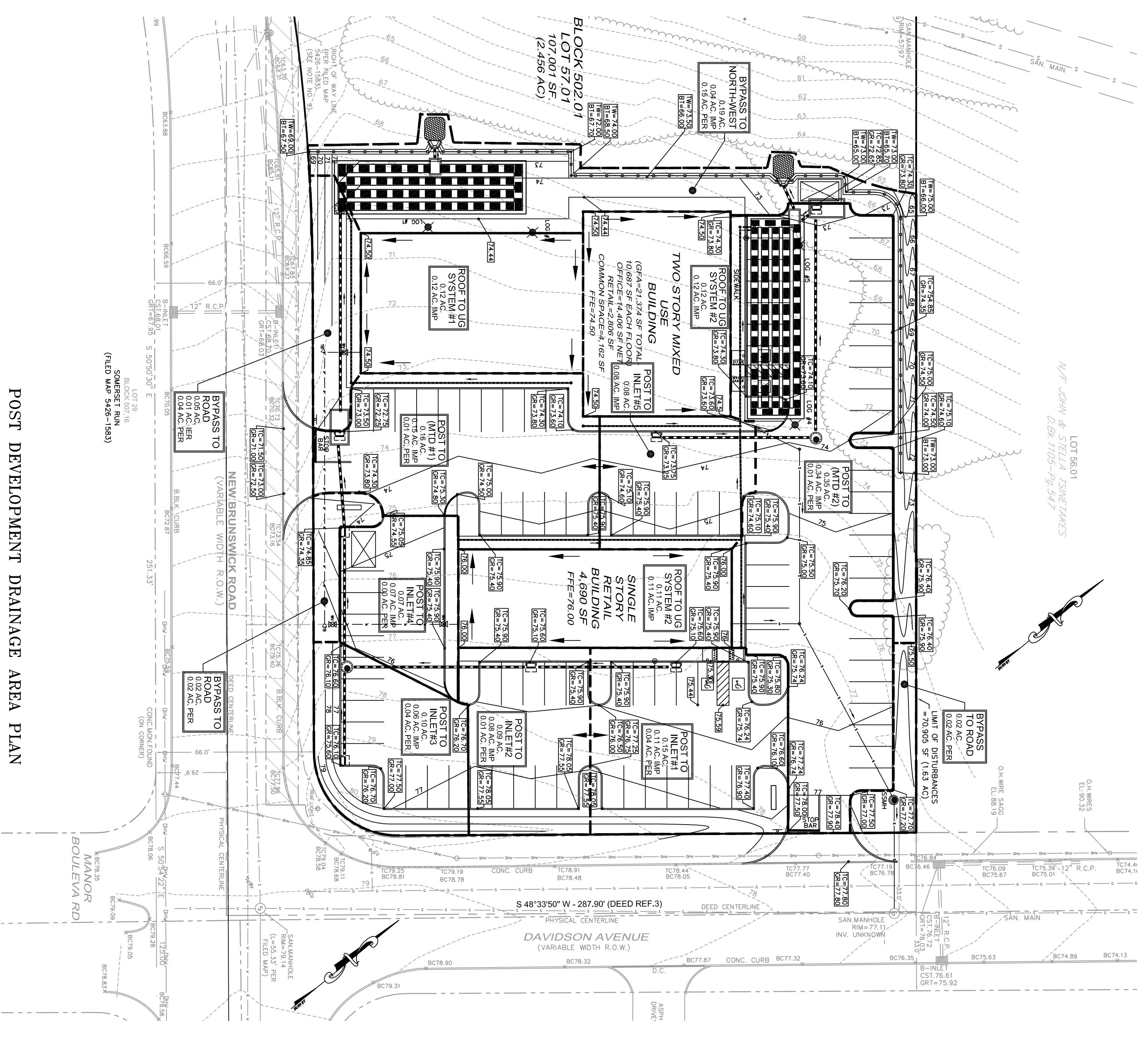
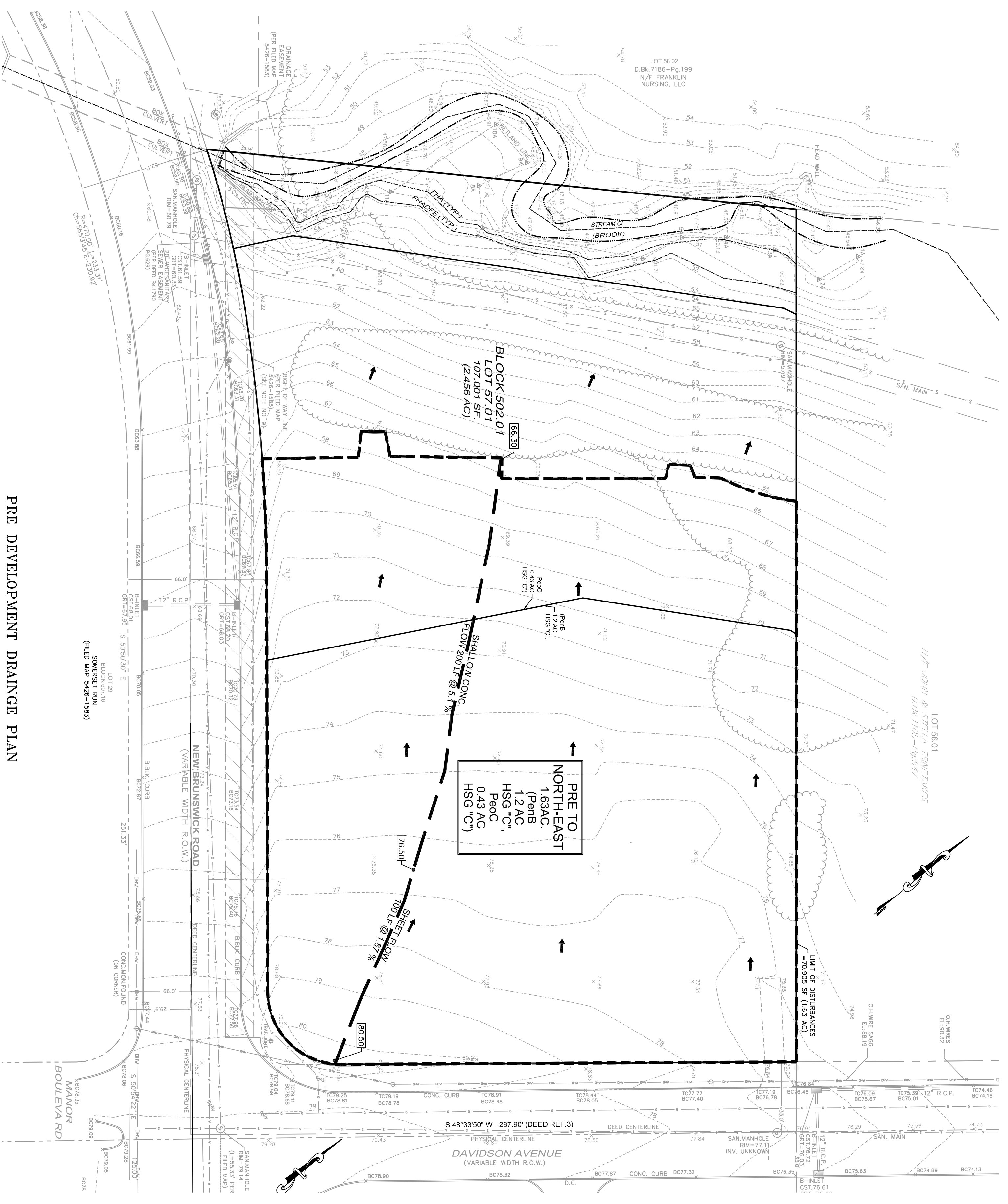
Time Basin Flooded (1st Fill): 14:07

Time to Empty Basin: 15:24

Time Basin Flooded (2nd Fill): 15:30

Time to Empty Basin: 16:20

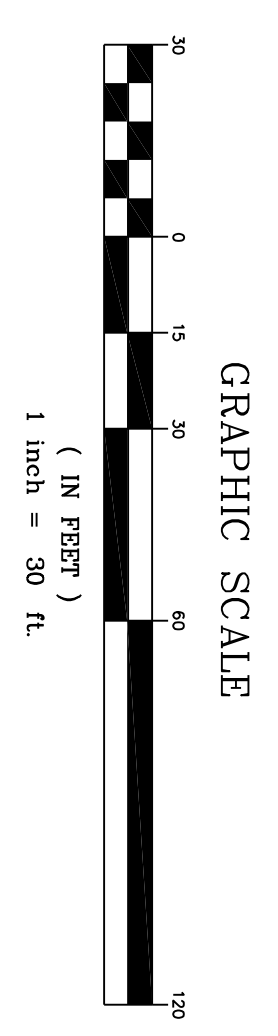
* As all the profiles have variations in fracture sizes and depths – a field test shall be done when the entire excavation for the ground Stormwater System is excavated as per the BMP manual. Two permeability tests are conducted to assist in determining the PERC value of 6.316 inch / hour. The results are enclosed.



PRE DEVELOPMENT DRAINAGE PLAN

POST DEVELOPMENT DRAINAGE AREA PLAN

SYMBOL	DESCRIPTION
[Symbol]	PILOT BOUNDARY
[Symbol]	SETBACK LINE
[Symbol]	NEW BUILDING
[Symbol]	NEW CURBS
[Symbol]	EXISTING COULTOURS
[Symbol]	UTILITY LAMP POLE
[Symbol]	UTILITY SANITARY MANHOLE
[Symbol]	UTILITY STORM INLET
[Symbol]	WETLANDS FLAG
[Symbol]	UTILITY POLE
[Symbol]	CONCRETE
[Symbol]	TREE WOOD LINE
[Symbol]	UTILITY STORM MANHOLE
[Symbol]	SANITARY LINE
[Symbol]	GAS LINE



PRE AND POST DEVELOPMENT DRAINAGE AREA MAP
 BLOCK 502.01, LOT 57.01
 TOWNSHIP OF FRANKLIN
 SOMERSET COUNTY, NJ

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REVISIONS:	DATE:	BY:
	02/01/2024 <td> </td>	

SCALE: AS SHOWN
 DRAWN BY: SJK
 CHECKED BY: SJK
 DATE: 02/01/2024
 SHEET: 1 OF 3
 PROJECT: 390 DAVIDSON AVE.
 SHRINATH J KOTDAMALA
 PROFESSIONAL ENGINEER N.J. LIC. NO. 41204

