STORMWATER MANAGEMENT REPORT

FOR

OFFICE AND RETAIL BUILDINGS AT 390 DAVIDSON AVENUE
(BLOCK 502.01, TAX LOT 57.01)
IN TOWNSHIP OF FRANKLIN,
SOMERSET COUNTY, NEW JERSEY

February 22nd 2024

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1.0 INTRODUCTION:

This report is prepared to support a Site Plan approval for two commercial buildings on land parcel known as lot 57.01 in block 502.01 in Township of Franklin, Somerset County. The site measures 2.456 acres and is located at the intersection of Davidson Avenue and New Brunswick Road. Figure 1 show the site mapped over a 2020 NJGIN aerial photograph. The following definitions are utilized for this report:

Where "MTD" means Mechanical Treatment Devices, which are certified to remove 80% of TSS from the parking lot stormwater runoff;

Where the "Rules" means Storm water Management Rules, which is known as N.J.A.C. 7:8; Where "Site "means Land Parcel in Township of Franklin known as Lot 57.01 in Block 502.01; Where "TSS" means Total Suspended Solids; and

Where "UG" means Underground Stormwater Storage System.



Figure 1: Site Mapped over a 2020 NJGIN Aerial Image

Figure 2 shows a Bound Brook USGS Quadrangle with site boundaries. Figure 3 shows the site mapped over a USDA Web Soil Survey along with the extent of the soil series. The site has three types of soil; Penn silt loam (PenB) with hydrologic soil group "C," The second one is Penn Channery silt loam (PeoC) with hydrologic soil group "C," and the third one is Rowland silt loam (RorAt) with hydrologic soil group "C." Appendix E shows the soil profiles and permeability results, which are used in determining infiltration rates and ground water mounding alalysis. Appendix F shows the Pre and Post development Drainage Area Map and locations of all the structures of proposed stormwater management system.

2.0 PRE DEVELOPMENT HYDROLOGY:

The site currently drains westerly to Raritan River Tributary. The rainfall amounts for 2, 10 and 100-year storm events are computed as:

2.1 Peak Stormwater Runoff is computed for the site based on following parameters:

2, 10, and 100 year storm event precipitation frequency is obtained from NOAA atlas 14-point precipitation frequency (a publication of Hydro meteorological design study center):

2 Year - 3.3 inches 10 year - 5.01 inches 100 year -8.35 inches

2.2 Factors for Somerset County under Table 5.5 of Stormwater Rules are described below:

2 Year 3.3 inches x 1.00 = 3.3 inches 10 year 5.01 inches x 1.03 = 5.16 inches 100 year 8.35 inches x 1.09 = 9.10 inches

2.3 Further as required under table 5.6 of the stormwater rules the precipitation amount is computed below:

2 Year 3.3 inches x 1.19 = 3.72 inches 10 year 5.16 inches x 1.24 = 6.40 inches 100 year 9.10 inches x 1.48 = 13.47 inches

Table 1 shows the pre development parameters that are used to compute peak flows:

TABLE 1: SUMMARY OF HYDROLOGIC PARAMETERS

Sub-Area	Area	Runoff	Tc
	(Ac.)	Coeff. (C)	(Min.)
Pre to North-West	1.35	74 (Hydrology Group C)	12 As computed

Appendix A shows the hydrographs for pre and post development land use for 2, 10 and 100-year storm events. Table 1A and 1B provide the compliances with the peak flow reductions in post development conditions.

3.0 POST-DEVELOPMENT HYDROLOGY:

Applicant is proposing two commercial buildings on the site and a parking lot. As the land use change is classified as major development under the rules peak flows are reduced by 50%, 25% and 20% for 2, 10 and 100-year storm events.

Proposed site improvements include construction of an Office and Retail Buildings with a parking lot. A quantitative hydrologic analysis for the disturbed areas of the site has been performed utilizing the same methodology as for the pre-development conditions. The hydrologic parameters were derived from the

same sources as the pre-development parameters. In post development conditions, the disturbed area of the site will continue to drain via the same general drainage areas as described in the pre-development hydrology.

To reduce peak flows from the site two underground (UG) storage systems are proposed. These systems include underground slotted ADS pipes and outlet structures. The outlet structures control the release of stormwater runoff to the stream. Appendix A shows the peak flow hydrographs for the post development conditions. It also shows the UG system routing and outflow volume for 2, 10 and 100-year storm event.

The pipe utilized to carry stormwater to the UG systems has capacity to handle 25-year storm event. Appendix B shows the pipe capacity computations for the all of the conveyance pipes used for the project. In addition Somerset Union County Soil Conservation District (SCD) requires the erosion protection at the stormwater discharge points. Appendix B shows the scour hole sizing computations for the anticipated stormwater runoff from the UG system.

4.0 GROUNDWATER RECHARGE AND GROUND WATER MOUNDING ANALYSIS:

In accordance with Chapter 6 of the BMP manual, compliance with one of the following two groundwater recharge standards is required:

- 1. "That 100% of the site's average annual pre-developed groundwater recharge volume be maintained after development;" or
- 2. "That 100% of the difference between the site's pre- and post-development 2-year runoff volumes be infiltrated."

The BMP areas of the site are the bottom areas of the UG systems. The Annual Groundwater Recharge Analysis (Based on GSR-32) computed the required BMP areas for the proposed development. The required BMP area is 2,155 sf while proposed BMP area for recharge is 3,795 sf. Attachment c shows the Recharge Analysis for the pre and post development conditions.

This appendix also shows the groundwater mounding analysis for proposed UG systems. Based on the results mounding due to infiltration is not negatively influencing neighboring sites. This analysis was conducted based on Hantush (1967) equation.

5. WATER QUALITY IMPROVEMENTS:

Subject project requires that the pavement area stormwater runoff is collected and filtered such that an 80% of TSS is removed prior to groundwater recharge and discharge to the stream. Two mechanical treatment devices that are certified by NJDEP are utilized to remove TSS. These device details and capacity computations are shown at appendix D. The stormwater runoff, which needs to be treated, is computed based on 1.25" rainfall in 2 hours with hydrograph distribution mentioned at the BMP manual.

6.0 NONSTRUCTURAL STRATEGIES

In addition, the stormwater management system complies with the New Jersey Stormwater Best Management Practices Manual (BMPM), dated April 2004. The site is designed in accordance with the nonstructural stormwater management strategies, to the maximum extent practical. More precisely, to achieve the required design and performance standards, the following nonstructural strategies are being applied to the design of the site:

6.1 Minimize impervious surfaces and break up or disconnect the flow of runoff over impervious surfaces.

The impervious surfaces on the site are disconnected by the provision of the proposed stormwater management basin that receives and treats the runoff from the site. The basin has been designed without a low flow channel and with a flat sand bottom to break up the flow of stormwater runoff over impervious surfaces prior to discharging to the existing drainage system within Tax Lot 57.01

- 6.2 Maximize the protection of natural drainage features and vegetation.

 The site grading and stormwater management system have been designed to maintain the existing drainage patterns of the site. This manner of development protects the natural drainage features and vegetation.
- 6.3 Minimize the decrease in the time of concentration from pre- to post-construction.

 To the maximum extent practical, the site was designed to minimize the decrease in preconstruction "time of concentration".
- 6.4 Minimize land disturbance including clearing and grading.

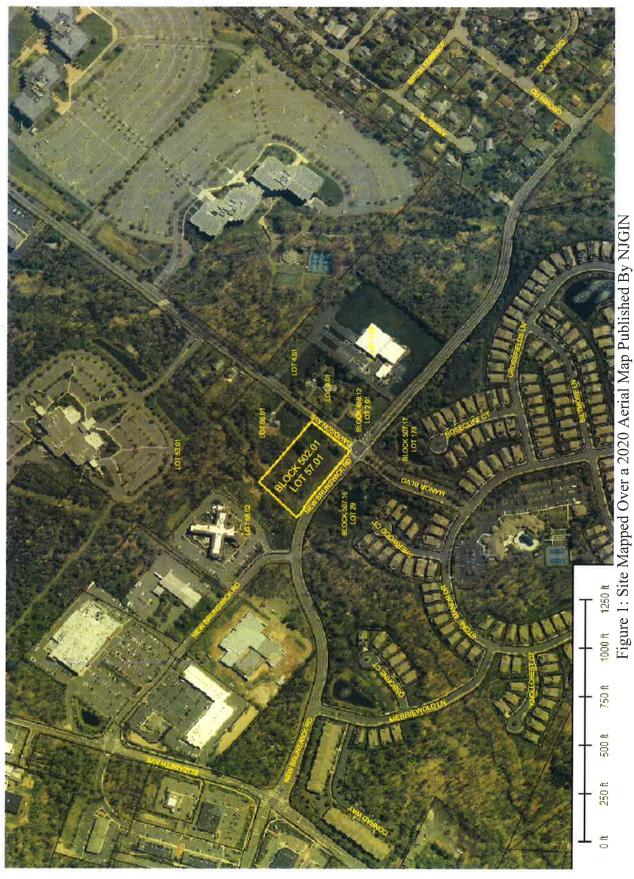
 The site has been designed to utilize a majority of the cleared site, as well as minimize the fill material needed for construction, to reduce the amount of disturbance to the site.
- 6.5 Minimize soil compaction.

 After rough grading of the site, heavy construction machinery on-site will be minimal.
- 6.6 Provide low-maintenance landscaping that encourages retention and planting of native vegetation and minimizes the use of lawns, fertilizers and pesticides.
 The site has been designed to utilize a majority of the cleared site to maintain the natural vegetation. In addition, a detailed landscape plan has been provided to supplement the existing vegetation.
- 6.7 Provide other source controls to prevent or minimize the release of pollutants into stormwater runoff.

The site is subject to and has been designed in accordance with the standards established under the Soil Erosion and Sediment Control Act.

7.0 CONCLUSIONS:

The proposed Stormwater management systems has been designed to meet the BMPM water quality, groundwater recharge standards, nonstructural Stormwater management strategy requirements, and reductions to the peak Stormwater flow rates from this development.



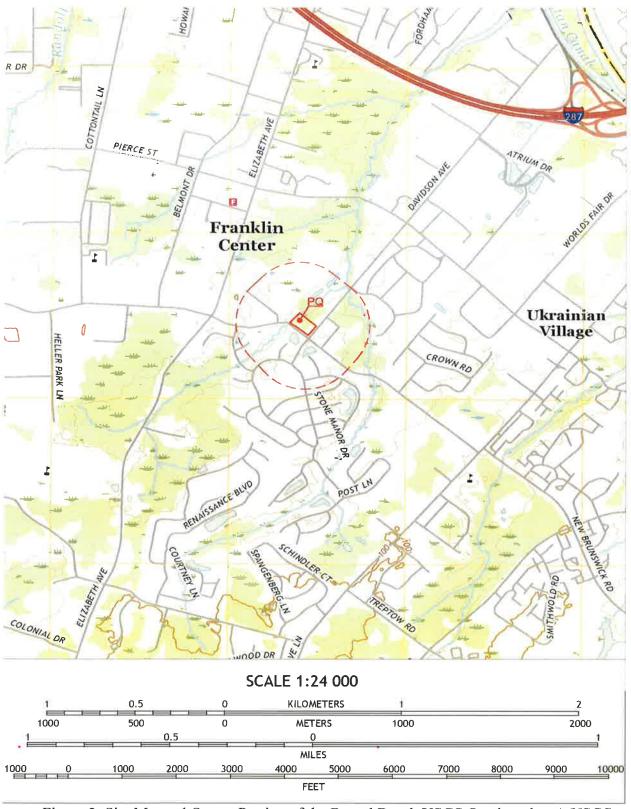


Figure 2: Site Mapped Over a Portion of the Bound Brook USGS Quadrangle - A USGS Publication

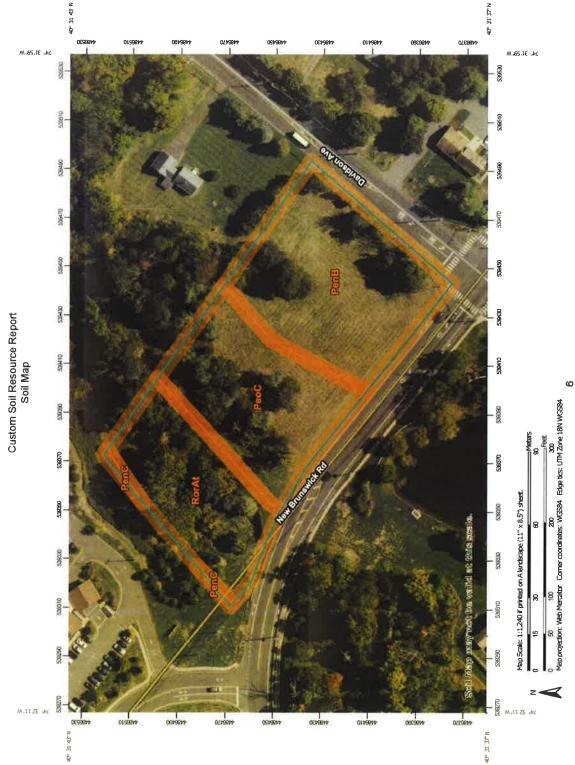


Figure 3: Site Mapped Over a Portion of Soil Survey Map (Obtained From USDA NRCS Web Site)

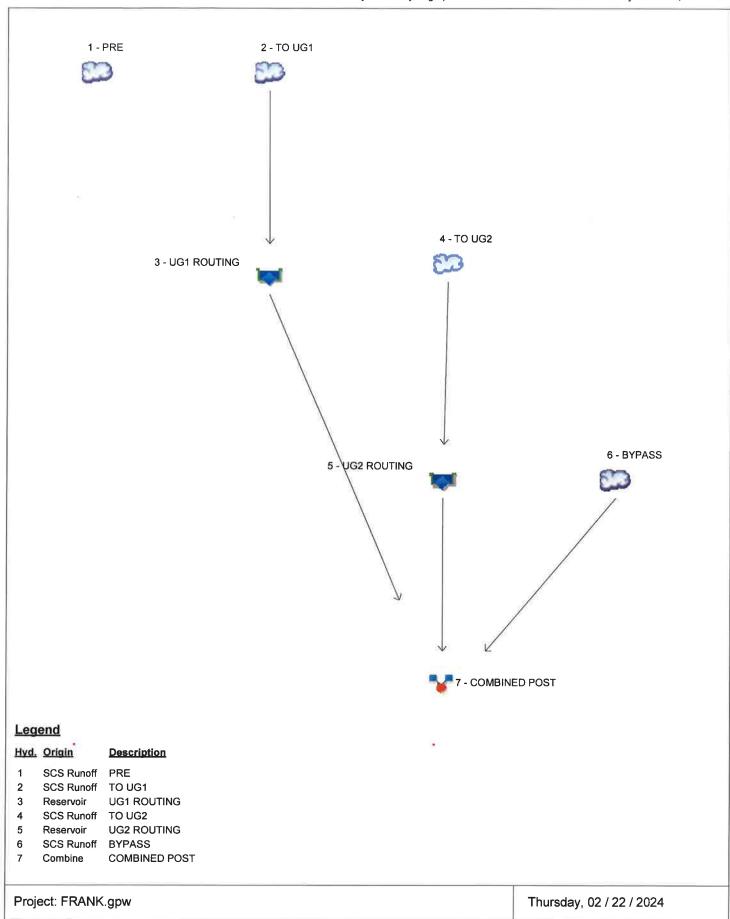
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5	UPON NEW DEVELOPMENT ON THE SITE (WHERE CFS MEANS CUBIC FEET PER SECOND)
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Table 1A- PRE DEVELOPMENT PEAK FLOW COMPUTATIONS AND DETERMINATION OF ALLOWED PEAK FLOW	
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Storm Frequency -	(B) Peak Flow (Pre Development) -		% of Peak Flow Reduction For	Maximum Peak Flow Allowed -
Years	CFS	R	Rule Compliance CFS (B -C) + D	CFS (B -C) + D
2	1.1		20.00%	9.0
10	2.8		75.00%	2.1
100	8		80:00%	6.4
		6		

Table 1B -POST		DEVELOPMENT PEAK FLOW COMPUTATIONS FROM THE DEVELOPMENT ON SITE (WHERE CFS MEANS CUBIC FEET PER SECOND)	NS FROM THE DEV PER SECOND)	ELOPMENT ON SITI	E (WHERE CFS
			Peak Flow		
Storm			Reduction		
Frequency -	Post Development	Post Development Maximum Peak Flow	Criteria		
Years	Peak Flows - CFS Allowed - CFS	Allowed - CFS	Complied		
2	0.5	9.0	0.6 YES		
10	1.9		2.1 YES		×
100	6.4		6.4 YES		

APPENDIX A:

PRE AND POST DEVELOPMENT RUNOFF CURVE NUMBER, TIME OF CONCENTRATION COMPUTATIONS AND STORM HYDROGRAPHS



Hydrograph Return Period Recap

	Hydrograph	Inflow				Peak Out	tflow (cfs)				Hydrograph
No.	type (origin)	hyd(s)	1-yr	2-yr	3-уг	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff	1111111		1,076			2.835	2.687	******	7,993	PRE
2	SCS Runoff	22222		1,247		******	2.228	2,151		4,775	TO UG1
3	Reservoir	2		0.184			1,185	1,123	******	4.481	UG1 ROUTING
4	SCS Runoff	******		0.806			1.409	1.362		2.988	TO UG2
5	Reservoir	4		0,146			0.208	0.204	900000	1.366	UG2 ROUTING
6	SCS Runoff	ARTSART.	******	0.273	2000000		0.659	0.628		1.736	BYPASS
7	Combine	3, 5, 6	20000100	0.533		u	1,878	1.781		6.426	COMBINED POST
			11								

Proj. file: FRANK.gpw

Thursday, 02 / 22 / 2024

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.076	6	738	6,788		*****	*****	PRE
2	SCS Runoff	1.247	6	732	7,853			*******	TO UG1
3	Reservoir	0.184	6	774	1,557	2	68.86	2,380	UG1 ROUTING
4	SCS Runoff	0.806	6	732	5,232	*******			TO UG2
5	Reservoir	0.146	6	768	1,027	4	65.39	1,023	UG2 ROUTING
6	SCS Runoff	0.273	6	738	1,683			******	BYPASS
7	Combine	0.533	6	744	4,268	3, 5, 6			COMBINED POST
	ù.								
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FRA	NK.gpw				Return	Period: 2 Ye	ear	Thursday,	02 / 22 / 2024

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

 $= C:\D6.CDS$

Thursday, 02 / 22 / 2024

= 285

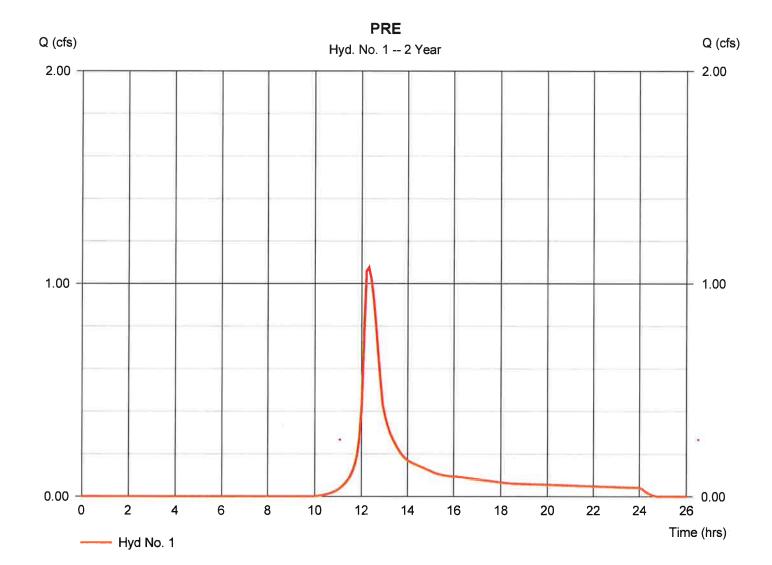
Hyd. No. 1

Storm duration

PRE

= SCS Runoff Hydrograph type Peak discharge = 1.076 cfsStorm frequency = 2 yrsTime to peak $= 12.30 \, hrs$ Time interval = 6 minHyd. volume = 6,788 cuftDrainage area = 1.350 acCurve number = 74 Basin Slope = 0.0 % Hydraulic length = 0 ftTime of conc. (Tc) Tc method = TR55 $= 11.50 \, \text{min}$ Total precip. = 3.72 inDistribution = Custom

Shape factor



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Hyd. No. 1

PRE

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.240 = 100.0 = 3.35 = 4.00		0.011 0.0 0.00 0.00	Est.	0.011 0.0 0.00 0.00		
Travel Time (min)	= 10.57	+	0.00	+	0.00	=	10.57
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 200.00 = 5.10 = Unpaved =3.64	t	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.91	+	0.00	+	0.00	=	0.91
Channel Flow							
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value	= 0.00 = 0.00 = 0.015		0.00 0.00 0.015		0.00 0.00		
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value	= 0.00 = 0.00 = 0.015		0.00 0.00 0.015		0.00 0.00 0.015		
X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.015 =0.00	+	0.00 0.00 0.015 0.00	+	0.00 0.00 0.015 0.00	=	0.00

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Thursday, 02 / 22 / 2024

Hyd. No. 1

PRE

Storm Frequency

= 2 yrs

Time interval

= 6 min

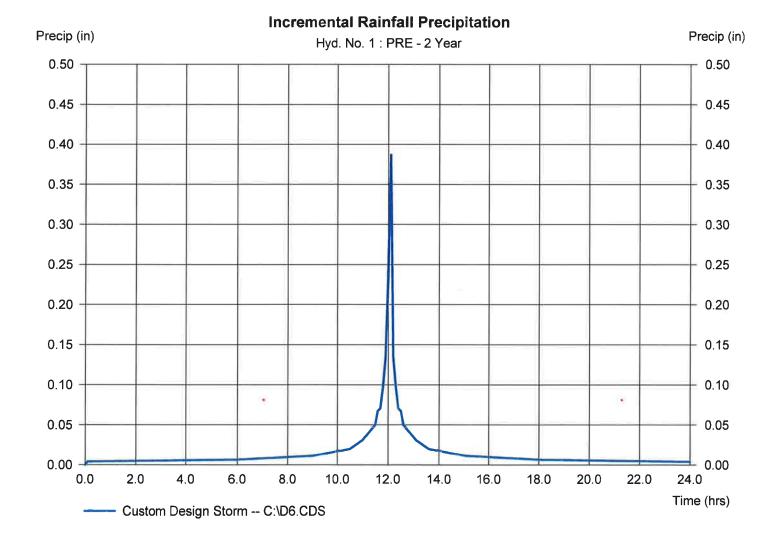
Total precip.

= 3.7200 in

Distribution

= Custom

Storm duration = C:\D6.CDS



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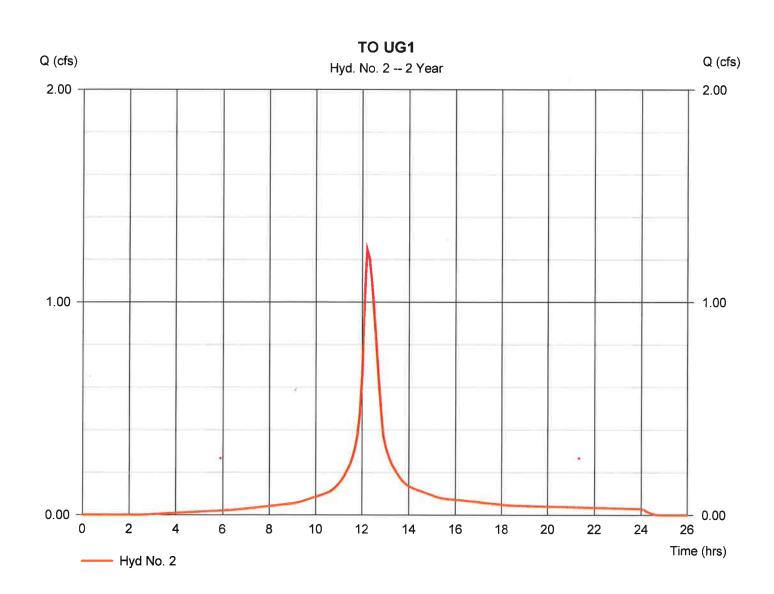
Thursday, 02 / 22 / 2024

Hyd. No. 2

TO UG1

Hydrograph type = SCS Runoff Peak discharge = 1.247 cfsStorm frequency = 2 yrs Time to peak $= 12.20 \, hrs$ Time interval = 6 min Hyd. volume = 7,853 cuftDrainage area = 0.690 acCurve number = 95* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = User Time of conc. (Tc) $= 10.00 \, \text{min}$ Total precip. = 3.72 inDistribution = Custom Storm duration $= C:\D6.CDS$ Shape factor = 285

^{*} Composite (Area/CN) = $[(0.100 \times 74) + (0.590 \times 98)] / 0.690$



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Thursday, 02 / 22 / 2024

Hyd. No. 2

TO UG1

Storm Frequency

= 2 yrs

Time interval

= 6 min

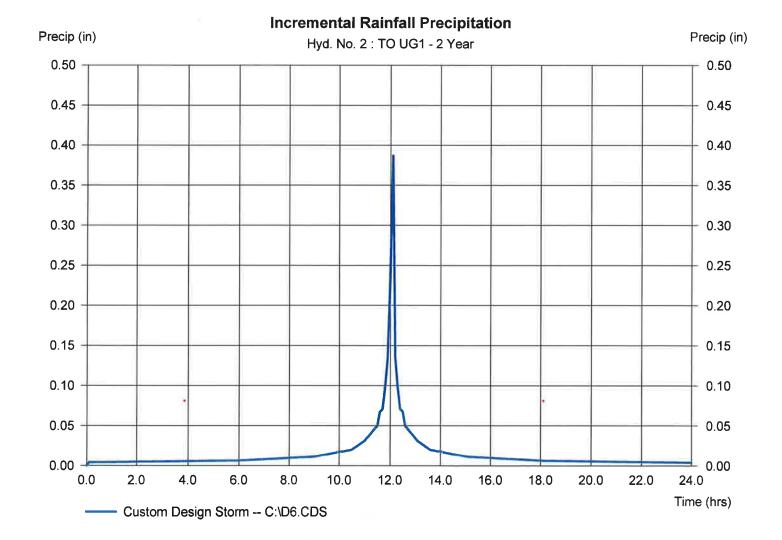
Total precip.

= 3.7200 in

Distribution

= Custom





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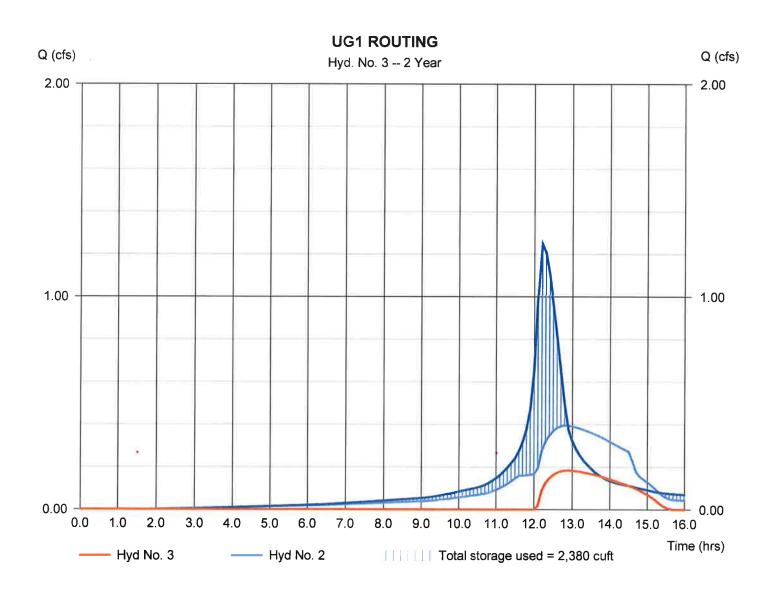
Thursday, 02 / 22 / 2024

Hyd. No. 3

UG1 ROUTING

Hydrograph type = Reservoir Peak discharge = 0.184 cfsStorm frequency = 2 yrsTime to peak $= 12.90 \, hrs$ Time interval = 6 min Hyd. volume = 1,557 cuftInflow hyd. No. = 2 - TO UG1 Max. Elevation $= 68.86 \, \mathrm{ft}$ Reservoir name = UG1 Max. Storage = 2,380 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Pond No. 1 - UG1

Pond Data

UG Chambers -Invert elev. = 67.50 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 80.00 ft, No. Barrels = 4, Slope = 0.00%, Headers = Yes **Encasement** -Invert elev. = 66.50 ft, Width = 5.00 ft, Height = 5.00 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	66.50	n/a	0	0
0.50	67.00	n/a	360	360
1.00	67.50	n/a	360	720
1.50	68.00	n/a	527	1,247
2.00	68.50	n/a	639	1,886
2.50	69.00	n/a	678	2,564
3.00	69.50	n/a	678	3,242
3.50	70.00	n/a	638	3,881
4.00	70.50	⊸ n/a	527	4,408
4.50	71.00	n/a	360	4,768
5.00	71.50	n/a	360	5,128

Culvert / Orifice Structures Weir Structures [B] [C] [A] [A] [PrfRsr] [B] [C] [D] Rise (in) = 2.507.00 0.00 0.00 Crest Len (ft) = 3.500.00 0.00 0.00 Span (in) = 2.507.00 0.00 0.00 Crest El. (ft) = 70.50 0.00 0.00 0.00 = 3.33 No. Barrels = 1 0 0 Weir Coeff. 3.33 3.33 3.33 Invert El. (ft) = 67.5069.00 0.00 0.00 Weir Type = Rect Length (ft) = 0.000.00 0.00 0.00 Multi-Stage = No No Nο Nο Slope (%) = 0.000.00 0.00 n/a N-Value = .013 .013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 3.000 (by Wet area) Multi-Stage = n/a TW Elev. (ft) No No No = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

_	_	_											
Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	66.50	0.00	0.00	3 4114 1	***	0.00	***		***	0.000	***	0.000
0.50	360	67.00	0.00	0.00	***	ener I	0.00				0.142		0.142
1.00	720	67.50	0.00 ic	0.00			0.00	2000			0.165	***	0.165
1.50	1,247	68.00	0.10 ic	0.00			0.00		***	***	0.189	-	0.292
2.00	1,886	68.50	0.16 ic	0.00	***	***	0.00			***	0.212		0.368
2.50	2,564	69.00	0.19 ic	0.00 ic	S444	***	0.00				0.236		0.430
3.00	3,242	69.50	0.23 ic	0.59 ic	***		0.00		***		0.260		1.074
3.50	3,881	70.00	0.25 ic	1.08 ic	***	777	0.00	TTT:	Certe:		0.283		1.621
4.00	4,408	70.50	0.28 ic	1.41 ic	***	***	0.00	99.5	(market		0.307		2.001
4.50	4,768	71.00	0.30 ic	1.68 ic		022	4.13	2012			0.331	***	6.445
5.00	5,128	71.50	0.32 ic	1.91 ic	5 75 5	****	11.67	222	***	H22	0.354		14.26

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

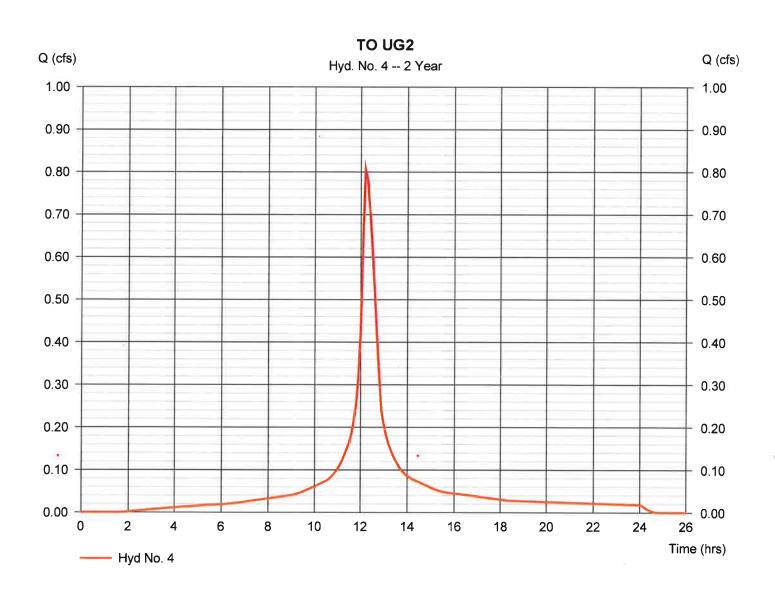
Thursday, 02 / 22 / 2024

Hyd. No. 4

TO UG2

Hydrograph type = SCS Runoff Peak discharge = 0.806 cfsStorm frequency = 2 yrs Time to peak $= 12.20 \, hrs$ Time interval = 6 min Hyd. volume = 5,232 cuftDrainage area = 0.430 acCurve number = 97* Basin Slope = 0.0 %Hydraulic length = 0 ftTime of conc. (Tc) Tc method = User $= 10.00 \, \text{min}$ Total precip. = 3.72 inDistribution = Custom Storm duration $= C:\D6.CDS$ Shape factor = 285

^{*} Composite (Area/CN) = $[(0.010 \times 74) + (0.420 \times 98)] / 0.430$



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Thursday, 02 / 22 / 2024

Hyd. No. 4

TO UG2

Storm Frequency

= 2 yrs

Time interval

= 6 min

Total precip.

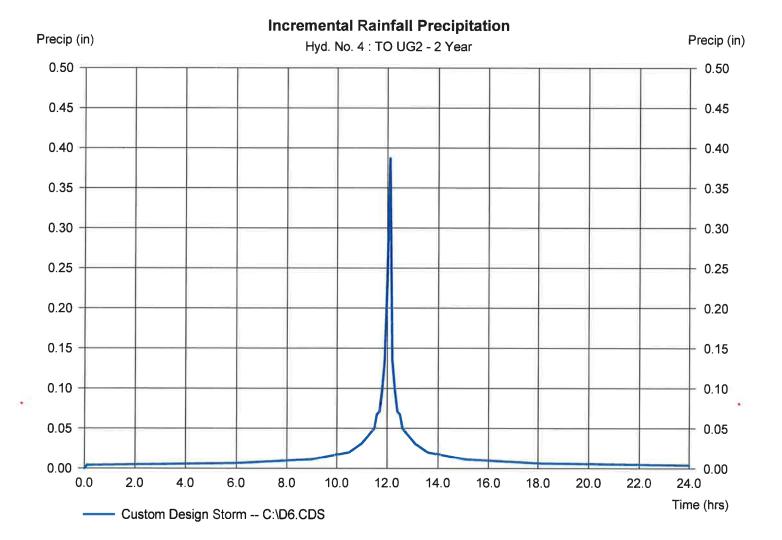
= 3.7200 in

Distribution

= Custom

Storm duration

 $= C:\D6.CDS$



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Thursday, 02 / 22 / 2024

= 1,023 cuft

Hyd. No. 5

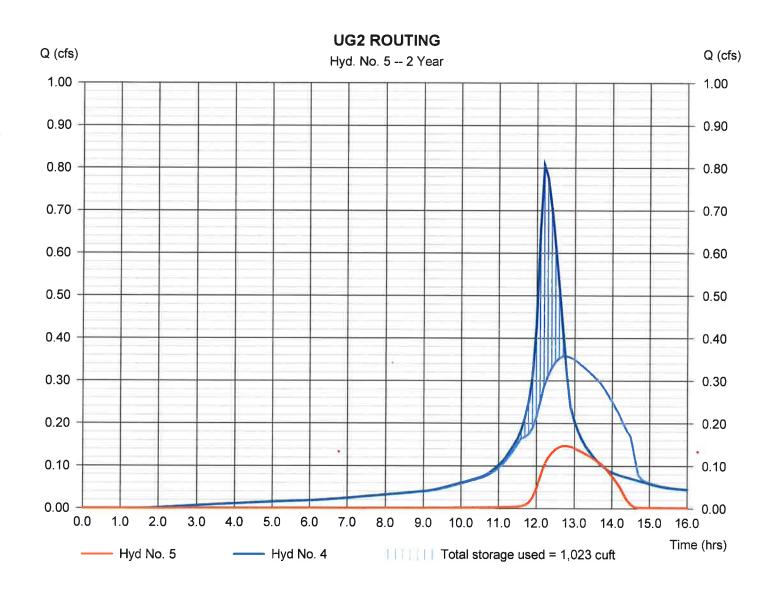
UG2 ROUTING

Hydrograph type = Reservoir
Storm frequency = 2 yrs
Time interval = 6 min
Inflow hyd. No. = 4 - TO UG2
Reservoir name = UG2

Peak discharge = 0.146 cfs
Time to peak = 12.80 hrs
Hyd. volume = 1,027 cuft
Max. Elevation = 65.39 ft

Max. Storage

Storage Indication method used. Exfiltration extracted from Outflow.



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Pond No. 3 - UG2

Pond Data

UG Chambers -Invert elev. = 65.00 ft, Rise x Span = 3.00 x 3.00 ft, Barrel Len = 85.00 ft, No. Barrels = 5, Slope = 0.00%, Headers = Yes Encasement -Invert elev. = 64.50 ft, Width = 5.00 ft, Height = 5.00 ft, Voids = 40.00%

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	64.50	n/a	0 :	0
0.50	65.00	n/a	475	475
1.00	65.50	n/a	696	1,171
1.50	66,00	n/a	843	2,013
2.00	66.50	n/a	895	2,908
2.50	67.00	n/a	895	3,803
3.00	67.50	n/a	842	4,645
3.50	68.00	n/a	696	5,341
4.00	68.50	n/a	475	5,816
4.50	69.00	n/a	475	6,291
5.00	69.50	n/a	475	6,766

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [C] [B] [D] Rise (in) = 2.500.00 0.00 0.00 Crest Len (ft) = 3.500.00 0.00 0.00 Span (in) = 2.500.00 0.00 0.00 Crest El. (ft) = 68.500.00 0.00 0.00 No. Barrels = 1 Weir Coeff. 0 0 0 = 3.333.33 3.33 3.33 invert El. (ft) = 64.500.00 0.00 0.00 Weir Type = Rect Length (ft) = 0.000.00 0.00 0.00 Multi-Stage = No No Nο Νo Slope (%) = 0.000.00 0.00 n/a N-Value = .013.013 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 3.000 (by Wet area) = 0.00 Multi-Stage = n/aNo No No TW Elev. (ft)

Note: Culvert/Onlice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for onlice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	CIv A cfs	CIV B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	64.50	0.00				0.00	777		***	0.000		0.000
0.50	475	65.00	0.10 ic	***	***	Here:	0.00	****	***	***	0.187		0.291
1.00	1,171	65.50	0.16 ic			2000	0.00		***		0.219		0.374
1.50	2,013	66.00	0.19 ic	-	***	***	0.00				0.250	***	0.444
2.00	2,908	66.50	0.23 ic	100	Sene:		0.00	555	***		0.281	***	0.507
2.50	3,803	67.00	0.25 ic	***	***	H445	0.00	***	***		0.312		0.567
3.00	4,645	67.50	0.28 ic			Massivi	0.00	2022	***	***	0.344	***	0.623
3.50	5,341	68.00	0.30 ic		***	777	0.00	555			0.375	esta.	0.677
4.00	5,816	68.50	0.32 ic	***	***	9991	0.00	***			0.406		0.730
4.50	6,291	69.00	0.34 ic	1010	222	322	4.13	-	***		0.438		4.912
5.00	6,766	69.50	0.36 ic		***	***	11.67	707			0.469		12,50

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

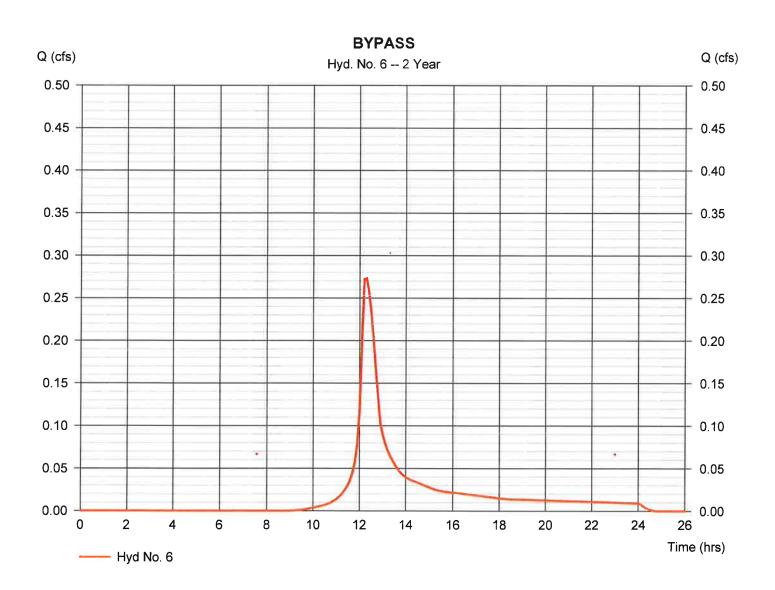
Thursday, 02 / 22 / 2024

Hyd. No. 6

BYPASS

Hydrograph type = SCS Runoff Peak discharge = 0.273 cfsStorm frequency = 2 yrsTime to peak = 12.30 hrsTime interval = 6 min Hyd. volume = 1,683 cuft Drainage area = 0.280 acCurve number = 78* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = User Time of conc. (Tc) $= 10.00 \, \text{min}$ Total precip. = 3.72 inDistribution = Custom Storm duration $= C:\D6.CDS$ Shape factor = 285

^{*} Composite (Area/CN) = [(0.050 x 98) + (0.230 x 74)] / 0.280



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Thursday, 02 / 22 / 2024

Hyd. No. 6

BYPASS

Storm Frequency

= 2 yrs

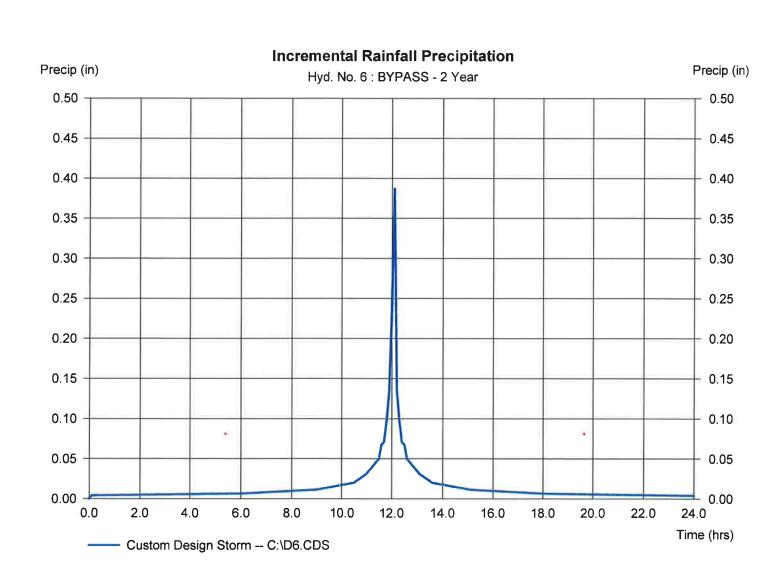
Time interval

= 6 min

Total precip.
Storm duration

= 3.7200 in = C:\D6.CDS Distribution

= Custom



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 7

COMBINED POST

Hydrograph type

= Combine

Peak discharge

= 0.533 cfs

Storm frequency

= 2 yrs

Time to peak

= 12.40 hrs

Time interval

= 6 min

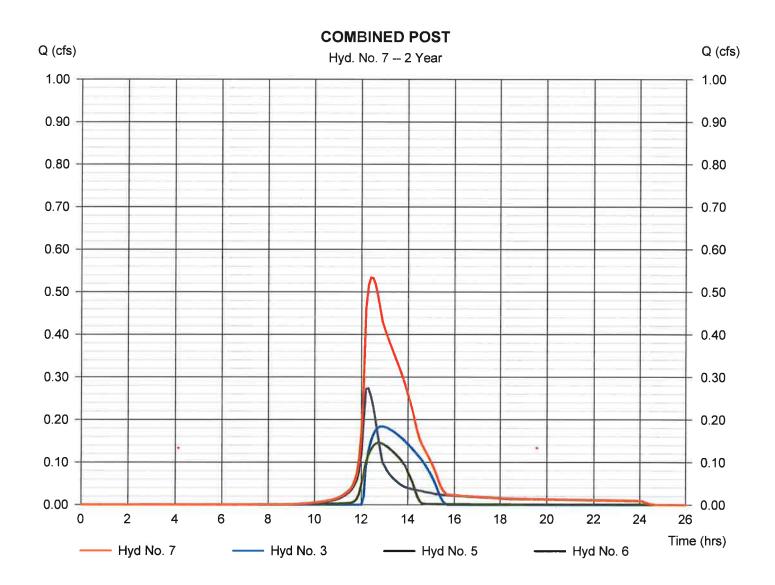
Hyd. volume

= 4,268 cuft

Inflow hyds.

= 3, 5, 6

Contrib. drain. area = 0.280 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.835	6	732	17,160	# 115511 6	3 113115 .		PRE
2	SCS Runoff	2.228	6	732	14,458		21.001		TO UG1
3	Reservoir	1.185	6	756	5,236	2	69.83	3,658	UG1 ROUTING
4	SCS Runoff	1.409	6	732	9,373		•••••	******	TO UG2
5	Reservoir	0.208	6	774	2,416	4	66.21	2,396	UG2 ROUTING
6	SCS Runoff	0.659	6	732	3,974		3*****	(B. 1874)	BYPASS
	1	•						*	
			I						
FRA	NK.gpw				Return F	Period: 10 Y	ear/	Thursday, 0	02 / 22 / 2024

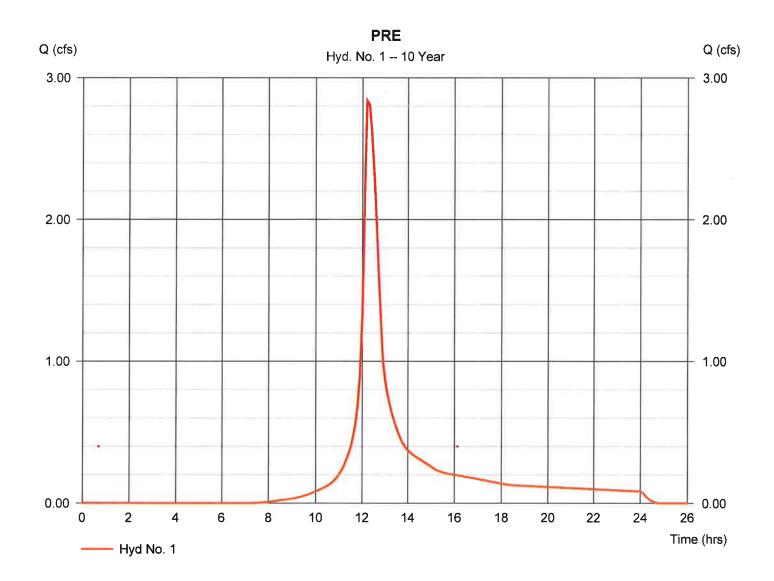
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 1

PRE

Hydrograph type = SCS Runoff Peak discharge = 2.835 cfsStorm frequency Time to peak = 10 yrs $= 12.20 \, hrs$ Time interval = 6 min Hyd. volume = 17,160 cuftDrainage area = 1.350 acCurve number = 74 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method = TR55 Time of conc. (Tc) $= 11.50 \, \text{min}$ Total precip. = 6.40 inDistribution = Custom Storm duration $= C:\D6.CDS$ Shape factor = 285



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Thursday, 02 / 22 / 2024

Hyd. No. 1

PRE

Storm Frequency

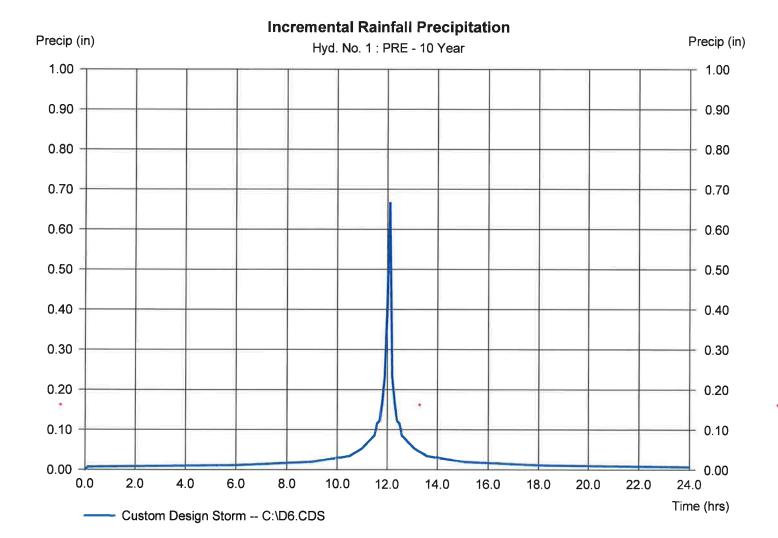
= 10 yrs

Time interval

= 6 min

Total precip.
Storm duration

= 6.4000 in = C:\D6.CDS Distribution = Custom



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

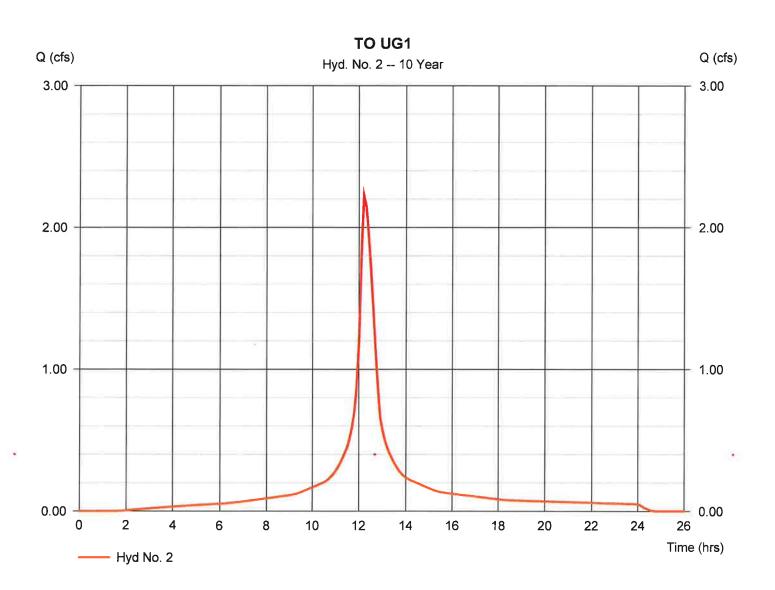
Thursday, 02 / 22 / 2024

Hyd. No. 2

TO UG1

Hydrograph type = SCS Runoff Peak discharge = 2.228 cfsStorm frequency Time to peak = 10 yrs= 12.20 hrsTime interval = 6 min Hyd. volume = 14,458 cuft Drainage area = 0.690 acCurve number = 95* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 10.00 \, \text{min}$ Total precip. = 6.40 inDistribution = Custom Storm duration $= C:\D6.CDS$ Shape factor = 285

^{*} Composite (Area/CN) = $[(0.100 \times 74) + (0.590 \times 98)] / 0.690$



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 2

TO UG1

Storm Frequency

= 10 yrs

Time interval

= 6 min

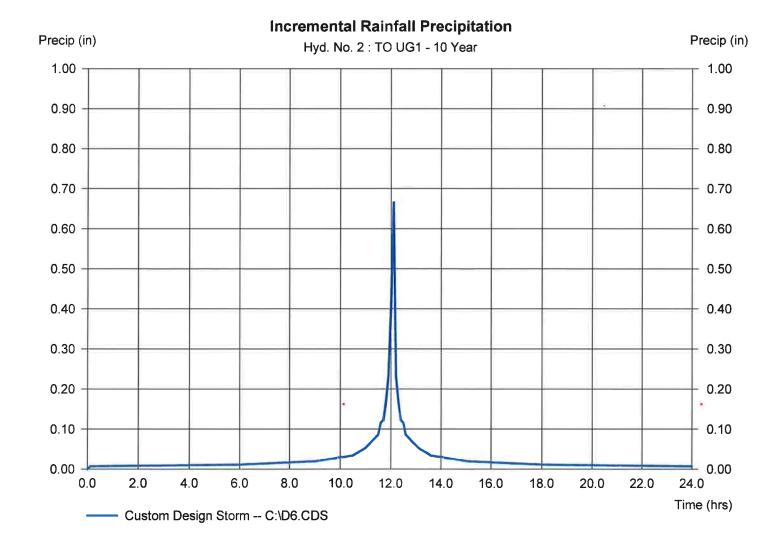
Total precip.

= 6.4000 in

Distribution

= Custom





Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

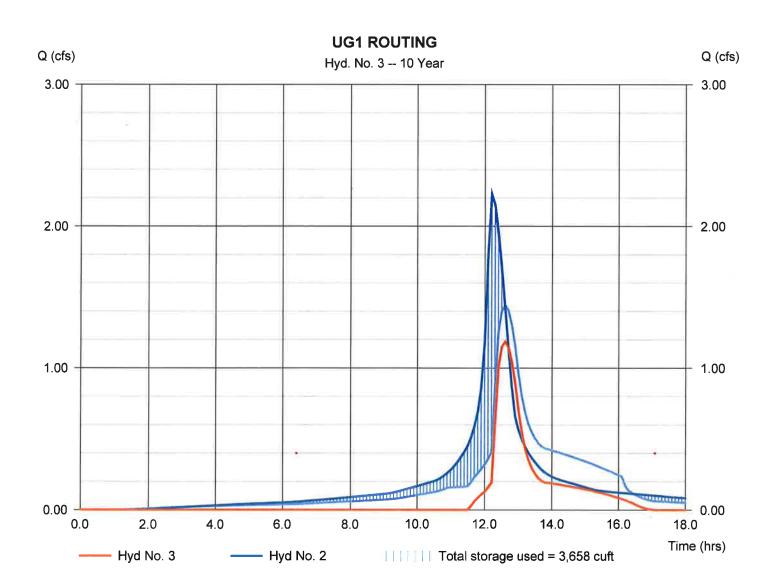
Thursday, 02 / 22 / 2024

Hyd. No. 3

UG1 ROUTING

Hydrograph type = Reservoir Peak discharge = 1.185 cfsStorm frequency Time to peak = 10 yrs $= 12.60 \, hrs$ Time interval = 6 min Hyd. volume = 5,236 cuftMax. Elevation Inflow hyd. No. = 2 - TO UG1 $= 69.83 \, \text{ft}$ Reservoir name = UG1 Max. Storage = 3,658 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

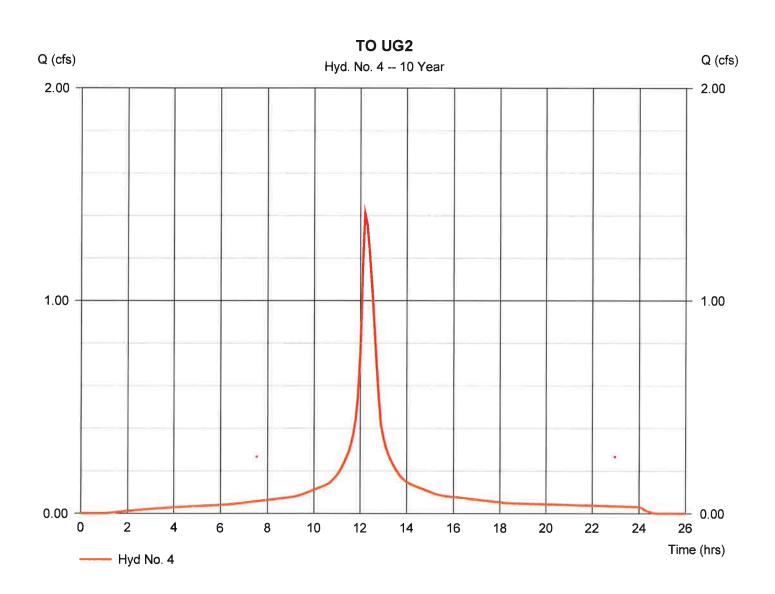
Thursday, 02 / 22 / 2024

Hyd. No. 4

TO UG2

Hydrograph type = SCS Runoff Peak discharge = 1.409 cfsStorm frequency = 10 vrsTime to peak $= 12.20 \, hrs$ Time interval = 6 min Hyd. volume = 9,373 cuftDrainage area = 0.430 acCurve number = 97* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 10.00 \, \text{min}$ Total precip. = 6.40 inDistribution = Custom Storm duration = C:\D6.CDS Shape factor = 285

^{*} Composite (Area/CN) = [(0.010 x 74) + (0.420 x 98)] / 0.430



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 4

TO UG2

Storm Frequency

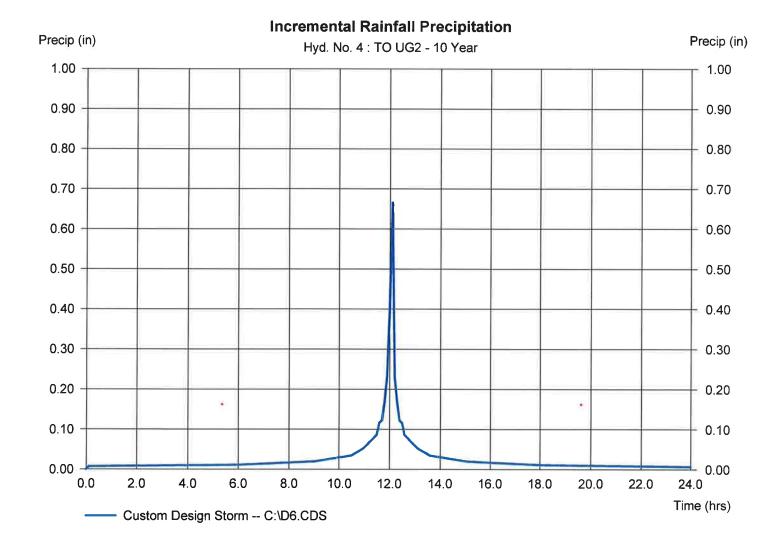
= 10 yrs

Time interval

= 6 min

Total precip.
Storm duration

= 6.4000 in = C:\D6.CDS Distribution = Custom



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

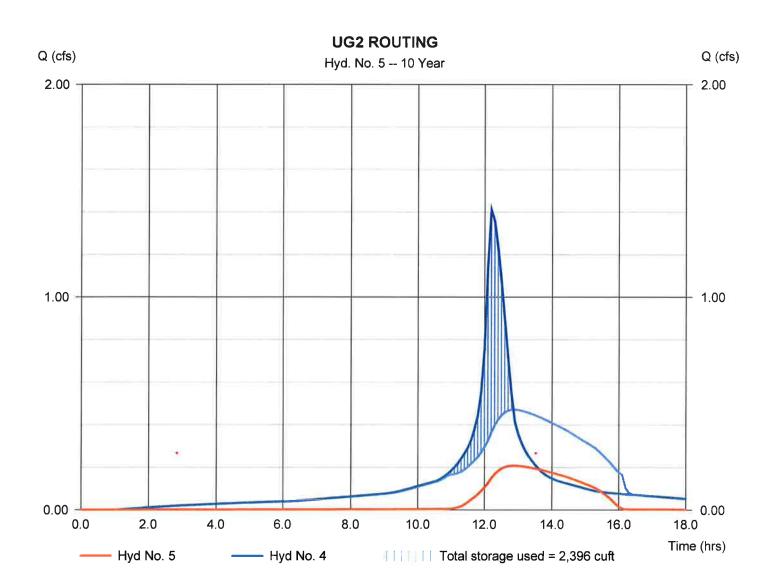
Thursday, 02 / 22 / 2024

Hyd. No. 5

UG2 ROUTING

Hydrograph type = Reservoir Peak discharge = 0.208 cfsStorm frequency = 10 yrsTime to peak $= 12.90 \, hrs$ Time interval = 6 min Hyd. volume = 2,416 cuftInflow hyd. No. = 4 - TO UG2 Max. Elevation $= 66.21 \, \mathrm{ft}$ Reservoir name = UG2 Max. Storage = 2,396 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

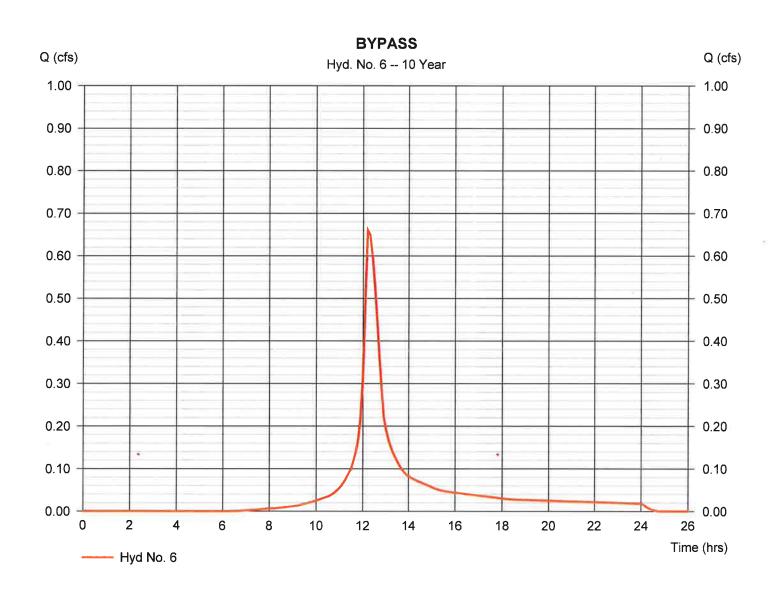
Thursday, 02 / 22 / 2024

Hyd. No. 6

BYPASS

Peak discharge Hydrograph type = SCS Runoff = 0.659 cfsStorm frequency = 10 yrsTime to peak $= 12.20 \, hrs$ Time interval = 6 min Hyd. volume = 3,974 cuftDrainage area = 0.280 acCurve number = 78* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 10.00 \, \text{min}$ Total precip. = 6.40 inDistribution = Custom Storm duration $= C:\D6.CDS$ Shape factor = 285

^{*} Composite (Area/CN) = [(0.050 x 98) + (0.230 x 74)] / 0.280



Precipitation Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 6

BYPASS

Storm Frequency

= 10 yrs

Time interval

= 6 min

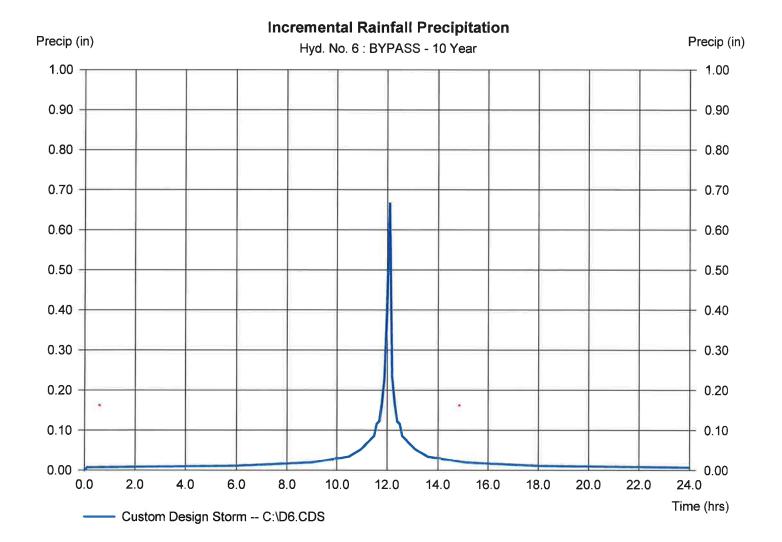
Total precip.

= 6.4000 in

Distribution

= Custom





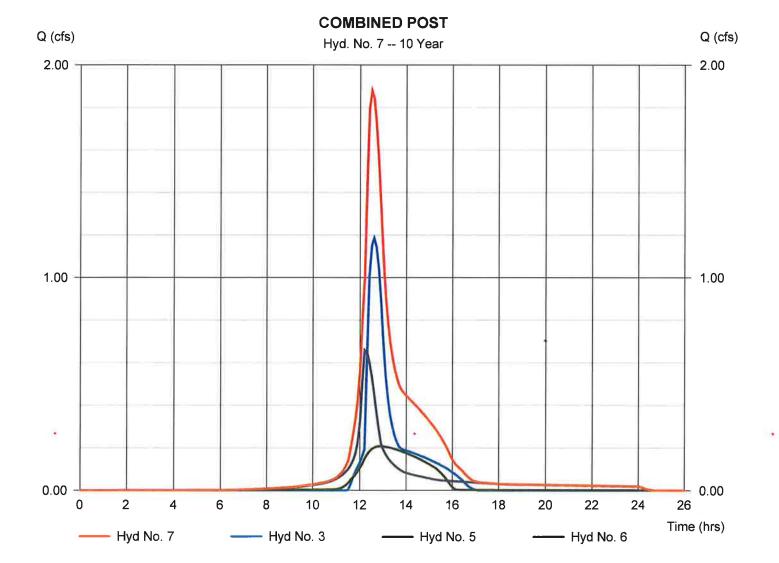
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 7

COMBINED POST

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 6 min Inflow hyds. = 3, 5, 6 Peak discharge = 1.878 cfs
Time to peak = 12.50 hrs
Hyd. volume = 11,626 cuft
Contrib. drain. area = 0.280 ac



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	7.993	6	732	48,753	STATE OF THE STATE		: 48254 3	PRE
2	SCS Runoff	4.775	6	732	32,003				TO UG1
3	Reservoir	4.481	6	738	17,665	2	70.86	4,670	UG1 ROUTING
4	SCS Runoff	2.988	6	732	20,327			******	TO UG2
5	Reservoir	1.366	6	762	7,095	4	68.70	6,004	UG2 ROUTING
6	SCS Runoff	1.736	6	732	10,697			i siese i,	BYPASS
7	Combine	6.426	6	738	35,457	3, 5, 6			COMBINED POST
						(*)			•
FRA	NK.gpw				Return P	eriod: 100	Year	Thursday, 0	2 / 22 / 2024

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 1

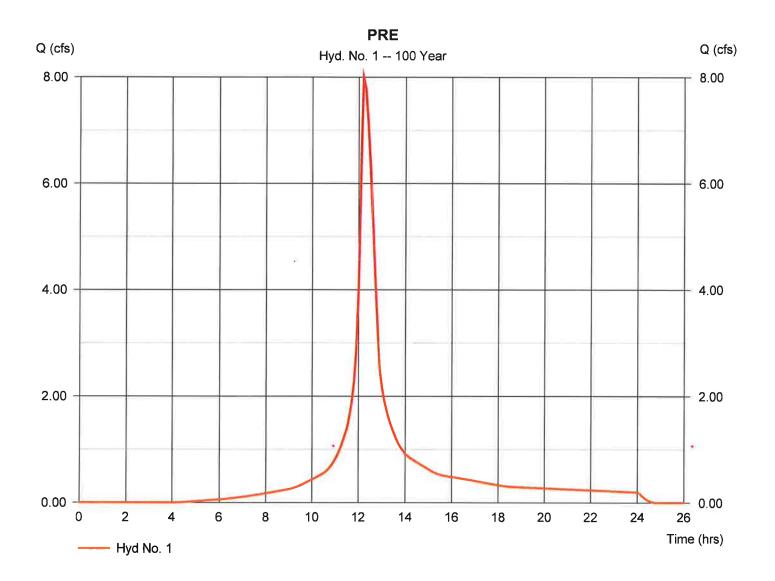
PRE

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 6 min Drainage area = 1.350 acBasin Slope = 0.0 %Tc method = TR55 Total precip. = 13.47 inStorm duration $= C:\D6.CDS$

Peak discharge = 7.993 cfs
Time to peak = 12.20 hrs
Hyd. volume = 48,753 cuft
Curve number = 74

Curve number = 74 Hydraulic length = 0 ft

Time of conc. (Tc) = 11.50 min
Distribution = Custom
Shape factor = 285



Precipitation Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 1

PRE

Storm Frequency

= 100 yrs

Time interval

= 6 min

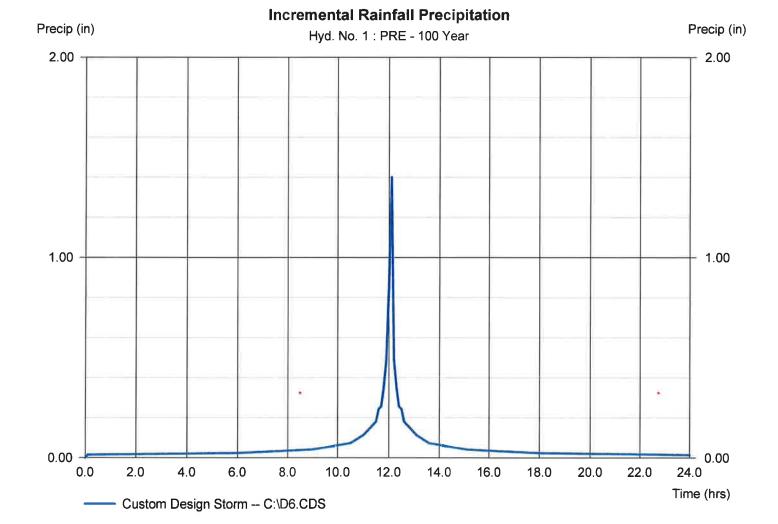
Total precip.

= 13.4700 in

Distribution

= Custom





Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

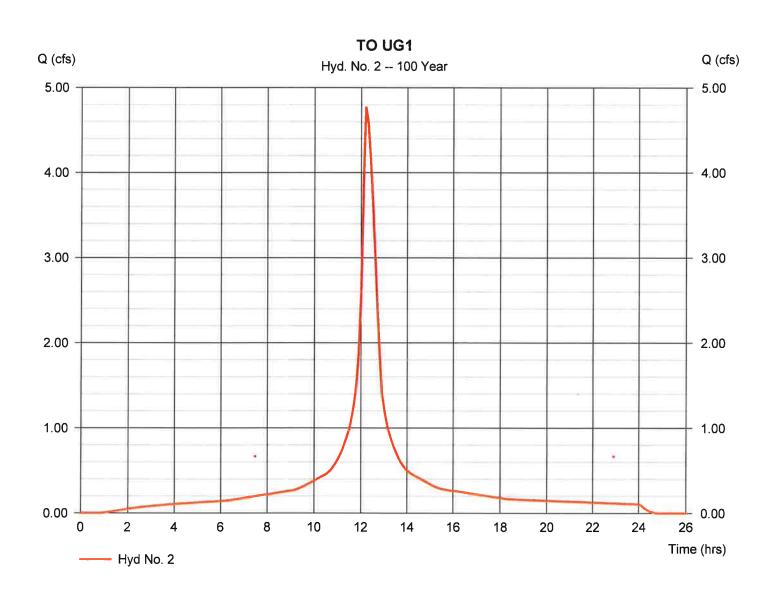
Thursday, 02 / 22 / 2024

Hyd. No. 2

TO UG1

Hydrograph type = SCS Runoff Peak discharge = 4.775 cfsStorm frequency = 100 yrsTime to peak = 12.20 hrs Time interval = 6 min Hyd. volume = 32,003 cuft Drainage area = 0.690 acCurve number = 95* Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = User Time of conc. (Tc) $= 10.00 \, \text{min}$ Total precip. = 13.47 inDistribution = Custom Storm duration $= C:\D6.CDS$ Shape factor = 285

^{*} Composite (Area/CN) = [(0.100 x 74) + (0.590 x 98)] / 0,690



Precipitation Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 2

TO UG1

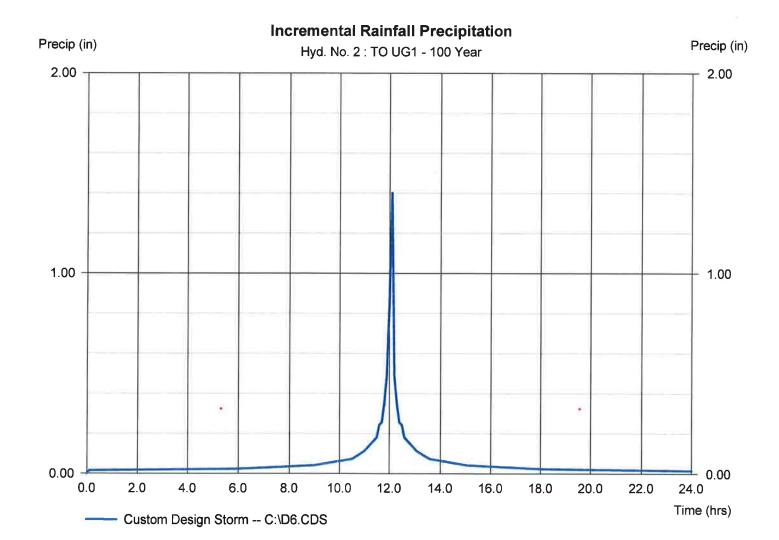
Storm Frequency

= 100 yrs

Time interval

= 6 min

Total precip. Storm duration = 13.4700 in = C:\D6.CDS Distribution = Custom



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

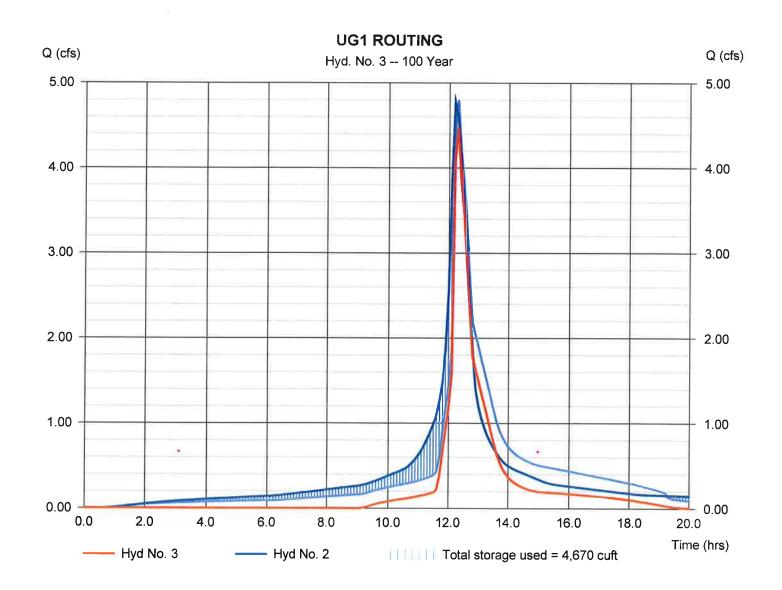
Thursday, 02 / 22 / 2024

Hyd. No. 3

UG1 ROUTING

Hydrograph type = Reservoir Peak discharge = 4.481 cfsStorm frequency = 100 yrsTime to peak = 12.30 hrsTime interval = 6 min Hyd. volume = 17,665 cuft Inflow hyd. No. = 2 - TO UG1 Max. Elevation $= 70.86 \, \text{ft}$ Reservoir name = UG1 Max. Storage = 4,670 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

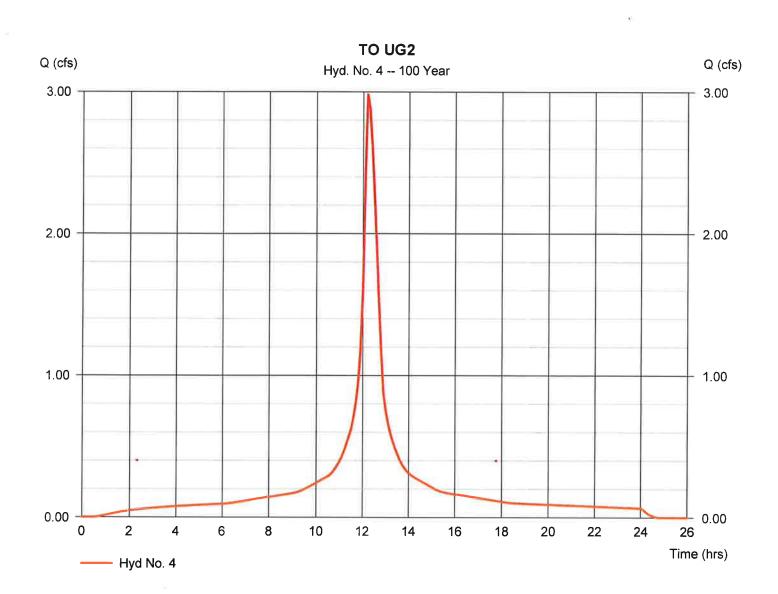
Thursday, 02 / 22 / 2024

Hyd. No. 4

TO UG2

Hydrograph type = SCS Runoff Peak discharge = 2.988 cfsStorm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval $= 6 \, \text{min}$ Hyd. volume = 20,327 cuftDrainage area = 0.430 acCurve number = 97* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = User Time of conc. (Tc) $= 10.00 \, \text{min}$ Total precip. = 13.47 inDistribution = Custom = C:\D6.CDS Storm duration Shape factor = 285

^{*} Composite (Area/CN) = $[(0.010 \times 74) + (0.420 \times 98)] / 0.430$



Precipitation Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 4

TO UG2

Storm Frequency

= 100 yrs

Time interval

= 6 min

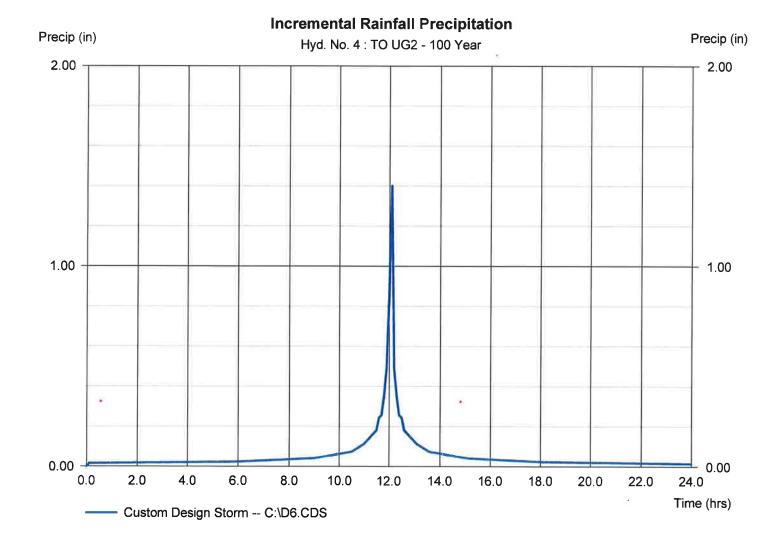
Total precip.

= 13.4700 in

Distribution

= Custom





Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

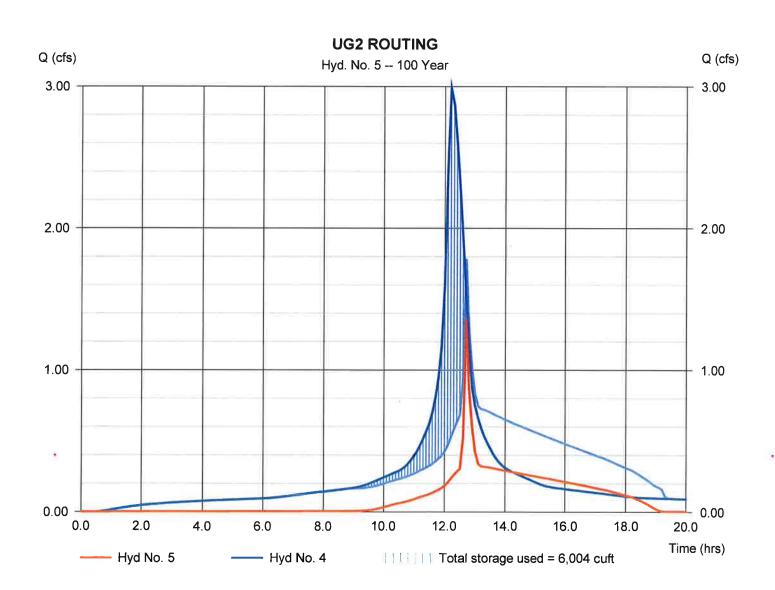
Thursday, 02 / 22 / 2024

Hyd. No. 5

UG2 ROUTING

Hydrograph type = Reservoir Peak discharge = 1.366 cfsStorm frequency = 100 yrsTime to peak $= 12.70 \, hrs$ Time interval = 6 min Hyd. volume = 7,095 cuftMax. Elevation Inflow hyd. No. = 4 - TO UG2 $= 68.70 \, \text{ft}$ Reservoir name = UG2 Max. Storage = 6,004 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

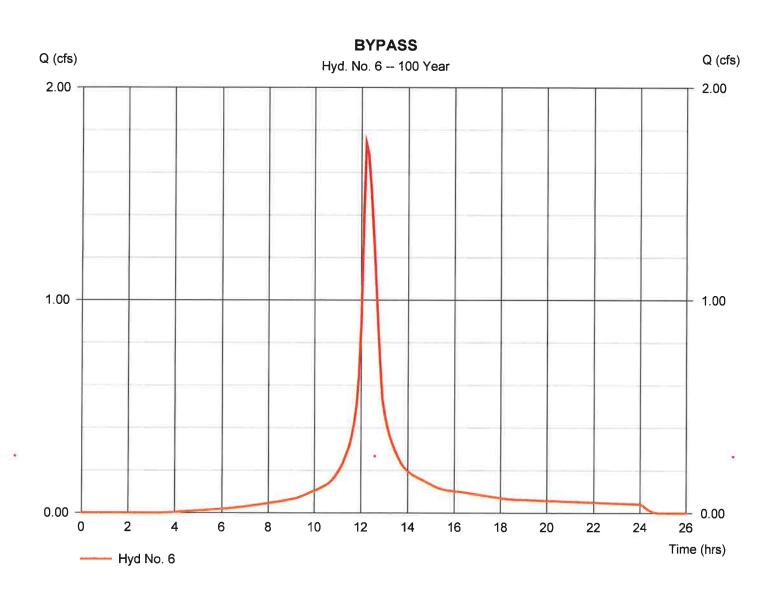
Thursday, 02 / 22 / 2024

Hyd. No. 6

BYPASS

Hydrograph type = SCS Runoff Peak discharge = 1.736 cfsStorm frequency = 100 yrsTime to peak $= 12.20 \, hrs$ Time interval = 6 min Hyd. volume = 10,697 cuftDrainage area = 0.280 acCurve number = 78* Basin Slope = 0.0 %Hydraulic length = 0 ftTc method = User Time of conc. (Tc) $= 10.00 \, \text{min}$ Total precip. = 13.47 inDistribution = Custom Storm duration = 285 $= C:\D6.CDS$ Shape factor

^{*} Composite (Area/CN) = [(0.050 x 98) + (0.230 x 74)] / 0.280



Precipitation Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 6

BYPASS

Storm Frequency

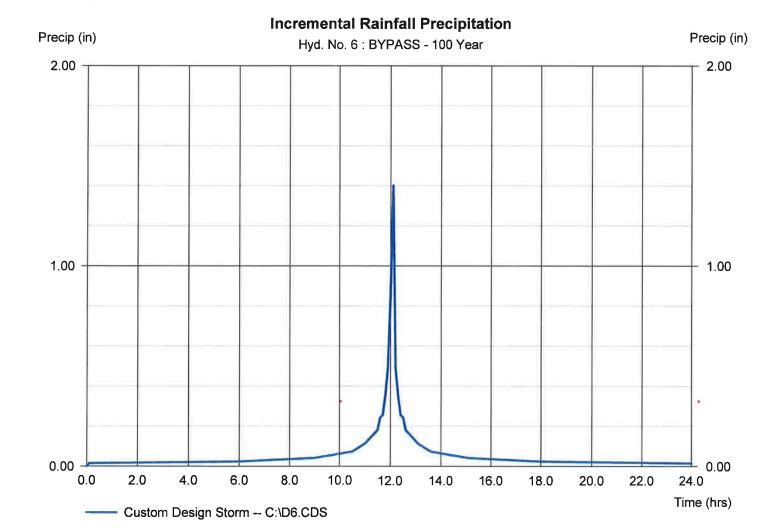
= 100 yrs

Time interval

= 6 min

Total precip.
Storm duration

= 13.4700 in = C:\D6.CDS Distribution = Custom



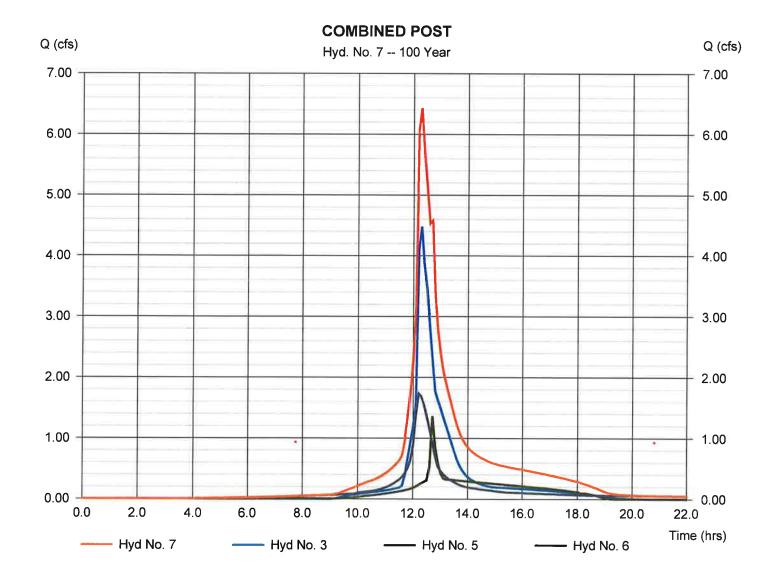
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Thursday, 02 / 22 / 2024

Hyd. No. 7

COMBINED POST

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 6 min Inflow hyds. = 3, 5, 6 Peak discharge = 6.426 cfs
Time to peak = 12.30 hrs
Hyd. volume = 35,457 cuft
Contrib. drain. area = 0.280 ac



APPENDIX B:

CONVEYANCE CAPACITY OF UNDERGROUND STORMWATER PIPES AND SCOUR HOLE SIZING COMPUTATIONS

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St	Station	Le	Drng Area	rea	Rnoff	Area x C	ပ	JC		Rain	Total	Cap	le Vel	Pipe		invert Elev	2	HGL Elev	>	Grnd / Rim Elev	m Elev	Line ID
Line	e To		Incr	Total		lncr	Total	Inlet	Syst				,	Size	Slope	Du	д	-G	ď	۵	ď	
		£	(ac)	(ac)	(0)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(£/\s)	(ii)	(%)	(#)	(#)	(H)	£)	(£)	(£)	
7	П	2,000	9	• 00	0	0	00	5	5	6	600	9	0	ů	5	04 40	0	0	9	8	6	200
9			00 0	000	000	000	8 6	2 0	5 6		200	20.4	2.0			64. 70 74. 74	06.70	00.00	00.10	0 0	9 6	OS-FEST
თ			0.15	0.15	0.86	0.13	0.13	100	10.0		06.0	19.4	2 %			70.25	70.54	70.82	70.94	8 6	8 6	US-rES2
00	φ	73.000	0.09	0.24	0.94	0.08	0.21	10.0	11.3		1.43	4.60	2.51			88 69	70.25	70.64	70.74		8 8	2-MH
7	φ	36.000	0.10	0.10	0.80	0.08	90.0	10.0	10.0		0.56	4.57	0.85			69.88	70.06	70.64	70.64	000	00.0	34
9	5	53.000	0.00	0.34	0.00	0.00	0.29	10.0	12.3	6.5	1.90	19.4	3.08	15	0,51	69.61	69.88	70.35	70.43	0.00	0.00	MH-4
c)	4	35.000	0.07	0.41	0.99	0.07	0.36	10.0	12.9	6.4	2.32	4.63	3.78	15	0.51	69.43	69.61	70.06	70.23	00.00	00.00	4-5
4	End	86.000	0.16	0.57	96'0	0.15	0.52	10.0	13.2	6,3	3.27	62.7	4.41	15	1.45	67.50	68.75	68.23	69.48	0.00	0.00	5-UG1
က	2	63.000	80.0	0.08	66.0	90.0	90.0	10.0	10.0	6.9	0.55	4.60	2.16	15	0.51	68.49	68.81	68.87	69.10	0.00	0.00	9-МН
7	-	90.000	00.00	90.0	00'0	00.00	90.0	10.0	12.3	6.5	0.51	4.57	2.45	15	0.50	68.04	68.49	68.32	68.77	0.00	0.00	MH-7
-	End	7.000	0.35	0.43	0.98	0.34	0,42	10.0	15.7	5.9	2.50	4.88	4.00	15	0.57	64.50	64.54	65.13	65.18	00.00	0.00	7-UG2
				140														¥i				
ሷ	Project File: PIPES.stm	PIPES.	stm													Number	Number of lines: 11	_		Run Dat	Run Date: 2/18/2024	54

NOTES:Intensity = 102.61 / (Inlet time + 16.50) ^ 0.82; Return period = Yrs, 25; c = cir e = ellip b = box

Storm Sewers v2024,00

SCOUR HOLE COMPUTATIONS AT POND 15" PIPE OUTFALL -

Variables:

Design Storm Flow for 25 Year, Q	2.20 cfs
Vertical Dimension of Outlet Pipe, D o	15 in
Horizontal Dimension of Outlet Pipe, Wo	15 in
Tailwater Depth, TW ¹	0.25 ft
Scour Hole Depth, y (1/2 D _o or D _o)	11 in

Apron Dimension Calculations:

Minimum Bottom Width, $W_1 = 2W_0$	$W_1 = 2.50 \text{ ft}$
Minimum Bottom Length, $L_1 = 3D_0$	$L_1 = 3.75 \text{ft}$
Minimum Top Width (max side slope of 3:1), W ₂	$W_2 = 8.00 \text{ ft}$
Minimum Top Length (max side slope of 3:1), L ₂	$L_2 = 9.25 \text{ft}$

Rip Rap Stone Size Calculations:

Unit Dicharge, $q = Q/D_0 = 1.76$ cfs per foot

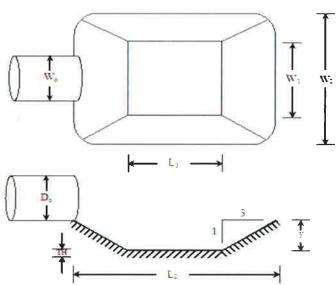
• Case I:
$$y = D_0$$

Median Stone, $d_{50} = \frac{0.0125 \, q^{1.33}}{TW} =$

Apron Thickness, $TH = 2 \times d_{50}$ with filter fabric

Median Stone,
$$d_{50} = \frac{0.0082 \, q^{1.33}}{TW} =$$

Apron Thickness, $TH = 2 \times d_{50}$ with filter fabric



Notes:

- 1. The side slopes shall be 3:1 or flatter.
- 2. The bottom grade shall be 0.0% (level).
- 3. There shall be no overfall at the end of the apron or at the end of the culvert.
- 4. Fifty (50) percent by weight of the rip-rap mixture shall be smaller than the median size stone designated as d₅₀. The largest stone size in the mixture shall be 1.5 times the d₅₀ size. The rip-rap shall be reasonably well graded.
- 5. The thickness of the rip-rap apron may be two (2) times the median stone diameter provided that the apron is constructed on a bedding of four (4) inches of 3/4 inch clean stone on approved filter fabric material.
- Rip-rap and filter fabric shall meet the standards of the governing Soil Conservation District as well as the requirements of the local municipality.
- 7. Where the scour hole is to be placed within an existing or proposed waterway:
 - a. The scour hole sidewalls should be eliminated to maintain a smooth hydraulic line along the waterway bottom to avoid inviting turbulent flow from a sudden depression in the waterway.
 - b. If the flow in the waterway is greater than the flow from the proposed outlet, the rip-rap used to construct the scour hole should be sized based on the greater flow value according to the standard rip-rap.

Footnote

1. Tailwater depth shall be the 2 year storm if discharging into a detention basin. For areas where tailwater cannot be computed, use TW = 0.2D_n.

APPENDIX C:

ANNUAL GROUND WATER RECHARGE ANALYSIS WORKSHEETS AND MOUNDING ANALYSIS

New Jersey	sey	Annual Groundwater Recharge Analysis (based on GSR-32)	rae An	alysis	based on G	3SR-32)			Project Name:	390 DAVIDSON RD	ON RD	
Groundwater	water		Average			/						
Recharge Spreadsheet Version 2.0	je iheet 0	Select Township ↓ Ai	Annual P (in)	Climatic Factor					Description:	MIXED USE BLDG +PARKING	BLDG +P	ARKING
November 2003	2003	SOMERSET CO., FRANKLIN TWP	45.7	1.48					Analysis Date:	02/18/24		
		Pre-Developed Conditions			=				Post-Developed Conditions	ditions		
Land Segment	Area (acres)	TR-55 Land Cover	Soil	Annual Recharge (in)	Annual Recharge (cu.ft)	Land Segment		Area (acres)	TR-55 Land Cover	Soil	Annual Recharge (in)	Annual Recharge (cu.ft)
-	1.35	Meadow, Pasture, Grassland or range	Penn	12.6	61,664		-	1.24	Impervious areas	Penn	0.0	
2							2	0.11	Open space	Penn	12.3	4,914
3							m					
4							4		7.4			
10							S					
9							9					
7							7					
8							80					
6							6					
10							10					
11							11					
12							12					
13							13					
14							14					
15							15					
ļ				Total Annual	Total Annual						Annual	Total
10131	4.1			Recharge (in)	Recharge (cu-ft)	Total	=	1.4			Recharge (in)	Recharge (cu.ft)
				12.6	61,664		Annu	al Rech	Annual Recharge Requirements Calculation		1.0	4,914
2000							:				Total	
ווחתפתחו	111 PM	Procedure to this the Pre-Development and Post-Development Conditions Tables	Signies		81	of Pre-Develo	ped And	nai Kecr	% of Pre-Developed Annual Recharge to Preserve =	100%	Area (sq.ft)	54,014

Procedure to fill the Pre-Development and Post-Development Conditions Tables

displayed or used in calculations. For impervious areas outside of standard lots select "Impervious Areas" as the Land Cover. For each land segment, first enter the area, then select TR-55 Land Cover, then select Soil. Start from the top of the table and proceed downward. Don't leave blank rows (with A=0) in between your segment entries, Rows with A=0 will not be Soil type for impervious areas are only required if an infiltration facility will be built within these areas,

Rech	large l	Efficienc	y Parameters Calculations (area averages)	
RWC= 3.80		(in)	DRWC= 0.00	(in)
ERWC = 0.99		(iii)	EDRWC= 0.00	(j)

56,750 (cubic feet)

Post-Development Annual Recharge Deficit= % of Pre-Developed Annual Recharge to Preserve =

Project Name		Description	no		Analysis Date	Date	BMP or LID Type	ID Type				
390 DAVIDSON RD		MIXED U	MIXED USE BLDG +PAR	+PARKING	02/18/24							
Recharge BMP Input Parameters	arameters			Root Zone Water capacity Calculated Parameters	pacity Calcu	lated Paran	neters	Recharge Design Parameters	ameters		Γ	
Parameter	Symbol	Value	Unit	Parameter	Symbol	Value	Unit	Parameter	Symbol	Value	Chit	
BMP Area	ABMP	2154.7	sq.ft	Empty Portion of RWC under Post-D Natural Recharge	ERWC	1.49	u	Inches of Runoff to capture	Qdesign	0.19		
BMP Effective Depth, this is the design variable	dBMP	4.8	LI.	ERWC Modified to consider dEXC	EDRWC	00.00	£	Inches of Rainfall to capture	Pdesign	0.27	, <u>s</u>	
Upper level of the BMP surface (negative if above ground)	dBMPu	67.5	:,⊑	Empty Portion of RWC under Infilt. BMP	RERWC	0.00	Ē	Recharge Provided Avg. over Imp. Area	,	12.6	Ę	
Depth of lower surface of BMP, must be>=dBMPu	dEXC	71.5	E					Runoff Captured Avg. over imp. Area		12.6	5	
Post-development Land Segment Location of BMP	SegBMP	80	unitless									
Input Zero if Location is distributed or undetermined												
				BMP Calculated Size Parameters	Parameter	S		CALCULATION CH	CHECK MESSAGES	SAGES		
				ABMP/Aimp	Aratio	0.04	unitless	Volume Balance-> OK)X			
				BMP Volume	VBMP	862	cu.ft	dBMP Check> dBMP must be<=dEXC-dBMPu, adjust parameters	JBMP must I	pe<=dEXC-	dBMPu, ac	ijust parameters
Parameters from Annual		Recharge Worksheet		System Performance Calculated Parameters	Calculated	Parameters		dEXC Check> OK	OK			
Post-D Deficit Recharge (or desired recharge volume)	Vdef	56,750	cu.ft	Annual BMP Recharge Volume		56,750 cu.ft	cu.ft	BMP Location> L	and Segme-	nt Number	Selected f	BMP Location> Land Segment Number Selected for BMP is not Defined
Post-D Impervious Area (or target Impervious Area)	Aimp	54,014	sq.ft	Avg BMP Recharge Efficiency		100.0%	Represents % Infiltration Recharged	OTHER NOTES				
Root Zone Water Capacity	RWC	5.74	Ľ.	%Rainfall became Runoff		77.9%	%	Pdesign is accurate only after B	3MP dimensions	are updated to	make rechive	Pdesign is accurate only after BMP dimensions are updated to make rech volume deficit volume. The portion
RWC Modified to consider dEXC	DRWC	00.0	ŗ.	%Runoff Infiltrated		35.4%	%	of BMP infiltration prior to filling	and the area oc	cupied by BMF	are ignored ii	of BMP infiltration prior to filling and the area occupied by BMP are ignored in these calculations. Results are
Climatic Factor	C-factor	1.48	no units	%Runoff Recharged		35.4%	%	sensetive to dBMP, make sure of	dBMP selected i	s small enough	for BMP to e	sensetive to dBMP, make sure dBMP selected is small enough for BMP to emoty in less than 3 days. For land
Average Annual P	Pavg	45.7	, <u>c</u>	%Rainfall Recharged		27.6%	%	Segment Location of BMP if you	u select "impervi	ous areas" RW	/C will be mini	Segment Location of BMP if you select "impervious areas" RWC will be minimal but not zero as determined by
Recharge Requirement over Imp. Area	dr	12.6	. <u>⊆</u>	Recharge Requirement dr 12.6 in the soil type				the soil type and a shallow root	zone for this Lar	nd Cover allow	ing consideration of lat	the soil type and a shallow root zone for this Land Cover allowing consideration of lateral flow and other losses.

How to solve for different recharge volumes: By default the spreadsheet assigns the values of total deficit recharge volume "Vdef" and total proposed impervious area "Aimp" from the "Annual Recharge" sheet to "Vdef" and "Aimp" on this page. This allows solution for a single BMP to handle the entire recharge requirement assuming the runoff from entire impervious area is available to the BMP.
To solve for a smaller BMP or a LID-IMP to recharge only part of the recharge requirement, set Vdef to your target value and Aimp to impervious area directly connected to your infiltration facility and then solve for ABMP or dBMP. To go back to the default configuration clik the "Default Vdef & Aimp" button.

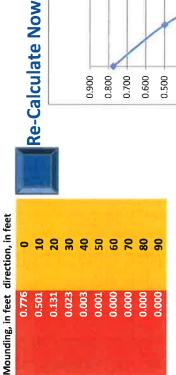
3.00 R Recharge rate (permeability rate) (in/hr) Specific yield, Sy (dimensionless) 0.150 Sy default value is 0.15; max value is 0.2 provided that a lab test data is sub Horizontal hydraulic conductivity (in/hr) Kh = 5xRecharge Rate (R) in the costal plan; Kh=R outside the coastal plan 10.000 x 1/2 length of basin (x direction, in feet) y 1/2 width of basin (y direction, in feet) t Duration of infiltration period (hours) hi(0) Initial thickness of saturated zone (feet)	input values		
S, Kh X, Y, t t t t t t t t t t t t t t t t t t	3.00	R	Recharge rate (permeability rate) (in/hr)
S, KY X Y			Specific yield, Sy (dimensionless)
유 × × 차 j.	0.150	Sy	default value is 0.15; max value is 0.2 provided that a lab test data is submitted
문 × × + (i)			Horizontal hydraulic conductivity (in/hr)
hi(0)	25.00	ĸ	Kh = 5xRecharge Rate (R) in the costal plan; Kh=R outside the coastal plan
t t hi(0)	10.000	×	1/2 length of basin (x direction, in feet)
t hi(0)	40.000	>	1/2 width of basin (y direction, in feet)
hi(0)	0.63		Duration of infiltration period (hours)
	10.00	hi(0)	Initial thickness of saturated zone (feet)

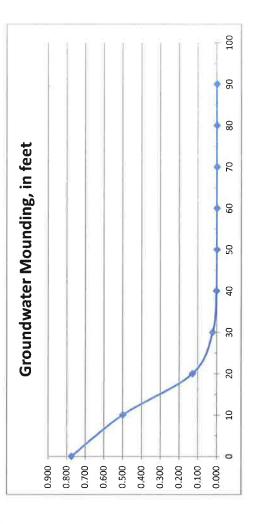
Maximum thickness of saturated zone (beneath center of basin at end of infiltration period) Maximum groundwater mounding (beneath center of basin at end of infiltration period)

center of basin in x

Ground-water

10.77





Disclaimer

as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to for documenting the changes and justifying the results and conclusions.

10.863 h(max) Maximum thic

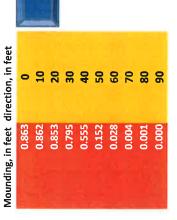
center of basin in x

Ground-water

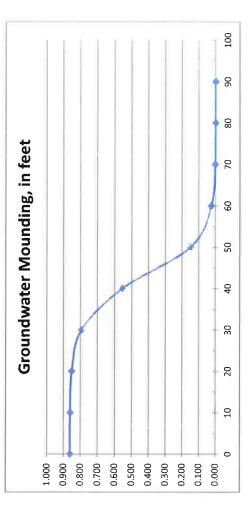
Δh(max) Distance from

0.863

Maximum thickness of saturated zone (beneath center of basin at end of infiltration period) Maximum groundwater mounding (beneath center of basin at end of infiltration period)



Re-Calculate Now



Disclaimer

as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to for documenting the changes and justifying the results and conclusions.

APPENDIX D:

WATER QUALITY STROM HYDROGRAPHS AND DETAILS OF MTD DEVICES TO REMOVED 80% TOTAL SUSPENDED SOLIDS



HC Kraken Filter Design Summary

Block 502.01, Lot 57.01 (MTD #1) Franklin Twp, NJ 2/12/24

Information Provided by Engineer:

- Water quality flow rate = 0.97 cfs
- Impervious drainage area = 0.47 ac
- Pervious drainage area = 0.10 ac
- Presiding agency = NJDEP
- Required TSS removal rate = 80%

HC Kraken Filter Information and Cartridge Data:

The High-Capacity Kraken Filter Stormwater Treatment Device is a state-of-the-art stormwater filtration system utilizing pretreatment and advanced membrane filtration to ensure a high level of trash, TSS, metals, nutrients, and hydrocarbons removal. The HC Kraken Filter works by initially passing stormwater through a pretreatment chamber to capture trash, hydrocarbons, and sediments. Once runoff is pretreated, it is directed to the filter chamber where membrane filtration begins. When the water level reaches the top of the membrane filters, the treated water will then pass down the riser tube, collect in the underdrain manifold and flow to the discharge chamber. The High-Capacity Kraken Filter has received final certification from the NJDEP for 80% TSS removal as a stand-alone treatment system.

- HC Kraken Filter cartridge height = 10 inches (nominal)
- HC Kraken Filter cartridge surface area = 49 square feet
- HC Kraken Filter cartridge loading rate = 0.101 gallons/minute per square foot
- HC Kraken Filter cartridge treatment flow = 0.011 cfs
- Hydraulic head required: 18.5" (with 10-inch cartridge)

Design Summary:

The High-Capacity Kraken Filter is sized based on the NJDEP certification, which lists an approved treatment flow rate and maximum impervious acreage limit per cartridge in Table 1. The number of cartridges required based on the impervious drainage area is compared with the number of cartridges required based on the treatment flow rate; the larger number of cartridges governs the sizing.

The HC Kraken Filter for this site was sized to provide **89 cartridges** in order to meet the hydraulic load requirement (calculations shown below). To house this number of cartridges, Contech Engineered Solutions recommends a 6' x 12' precast Shallow HC Kraken Filter.

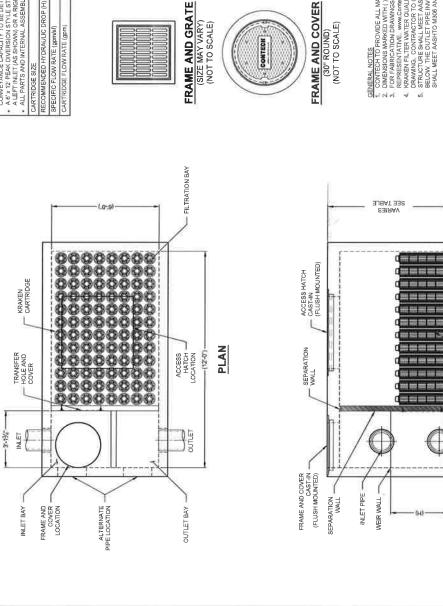
$$N_{cartridges\ hyd.load} = \frac{Q_{treat}}{Q_{cartridge}} = \frac{0.97\ cfs}{0.011\ ^{cfs}/_{cartridge}} = 88.18 \Rightarrow (89)\ 10"\ Cartridges$$

$$N_{cartridges\;mass\;load} = \frac{Area_{site}}{Max\;Area_{cartridge}} = \frac{0.47\;acres}{0.009\;acres/cartridge} = 52.22 \Rightarrow (53)\;10"\;Cartridges$$

7037 Ridge Road, Suite 350 | Hanover, MD 21076

Fax: 410-740-8492

Office: 443-457-1500



KRAKEN FILTER DESIGN NOTES

- RAMEN FILTER TREATMENT CAPACITY VARIES BY CARTRIDGE COUNT AND LOCALLY APPROVED SURFACE AREA SPECIFIC FLOWRATE, PEAK
 CONNETANCE CAPACITY TO BE DETERMINED BY REACHED.

 CONNETANCE CAPACITY TO BE DETERMINED BY REACHED.

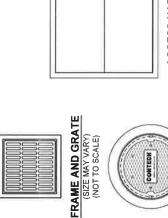
 A LEAT IN THE STORMINE TREATMENT OF THE SHOWN WITH THE MAJANUM NUMBER OF CARTRIDGES (98) AND IS AVAILABLE IN
 A LEATH THE TIME SHOWN OR A REPORT INLET CONFIGURATION.

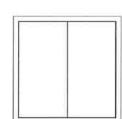
 ALL PARTS AND INTERNAL ASSEMBLY PROVIDED BY CONTICE HULLESS NOTED OTHERWISE

CARTRIDGE SIZE	30"	20.	101
RECOMMENDED HYDRAULIC DROP (H)	38.5"	28.5"	18.5"
SPECIFIC FLOW RATE (gpm/sf)	0 10	0,10	0,10
CARTRIDGE FLOW RATE (gpm)	17	10.6	4.9

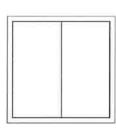
DATA REQUIREMENTS

SITE SPECIFIC









MATERIAL

INVERT

FILTER BAY RIM EL

CARTRIDGE HEIGHT (SEE TABLE ABOVE)

PEAK FLOW (yrs)



MAX, HEIGHT 4-10 4-10 RIM TO SYSTEM INVERT MIN, HEIGHT 3.6 4.2 CARTRIDGE SIZE 10" 8 20" 30,

- GENERAL NOTES

 LOONING TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.

 2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.

 2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS AND WEIGHTS. PLEASE CONTACT YOUR CONTECH

 3. FOR ARRENTATIVE. WAS CONTACTURE SHALL BE INACCORDANCE WITH ALL DESIGNS DATA AND INFORMATION CONTAINED IN THIS

 DRAWING. CONTRACTOR TO CONFIGN STRUCTURE, BETTS REQUIREMENTS OF PROJECT.

 5. STRUCTURE SHALL MEET AASHTO HESD LOAD RATING, ASSUMING EARTH COVER OF 0'-10' AND GROUNDWATER ELEVATION AT, OR BELLOW THE OUTLET PHER UNRET ELEVATION. ENGINEER RELOATIONS SHALL MEET AASHTO MISS AND BE CAST WITH THE CONTECT HERE AASHTO MISS AND BE CAST WITH THE AASHTO MISS AND BE CAST WITH THE CONTECT HERE AASHTO MISS AND BE CAST WITH THE CONTECT HERE AASHTO MISS AND BE CAST WITH THE CONTECT HERE AASHTO MISS AND TO CONTECT HERE AASHTO MISS AND TO CONTECT HERE AASHTO MISS AND T

FALSE FLOOR

ELEVATION

OUTLET PIPE

- INSTALLATION NOTES

 A. ANY SIDEBAGE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE
 A. ANY SIDEBAGE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVIDER OF RECORD,
 B. CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LITTING AND REACH CAPACITY TO LIFT AND SET THE KRAKEN FILTER
 B. CONTRACTOR TO DINING LALAND BETWEEN ALL SECTIONS AND ASSENDER. STRUCTURE.
 D. CONTRACTOR TO INSTALL AND GROUP ITHESES, MATCH OUTLET PRE INVEST WITH OUTLET BAY FLOOR.
 E. CONTRACTOR TO PROVIDE. INSTALL AND GROUP ITHESES, MATCH OUTLET PRE INVEST WITH OUTLET BAY FLOOR.
 E. CONTRACTOR TO REMOVE THE TRANSFER DEPUNG COVER WHEN THE SYSTEM IS BROUGHT ONLINE.

KFPD0612 (6' × 12') PEAK DIVERSION KRAKEN FILTER STANDARD DETAIL SHALLOW

THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING US PATENTS: 9604,601;0,1557,551,10,389,496,11,280,321; RELATED FOREIGN PATENTS OR OTHER PATENT PENDING

9100 Centre Pointe Dr., Suite 400, West Chester, OH 45069 ann. cyr., 3000 513-645-7000 513-645-7035 FAX CAN NIECH ENGINEERED SOLUTIONS LLC



HC Kraken Filter Design Summary

Maintenance:

Maintenance of Stormwater best management practices is required per the New Jersey Administrative Code 7:8-5.8. Recommendations for maintenance are included in chapters 8 & 9 of the New Jersey Stormwater Best Management Practices Manual. To comply with requirements, CONTECH offers a network of Preferred Service Providers that have the capability to perform all necessary inspections, compliance reporting and cleaning services. CONTECH recommends inspecting the system annually and maintaining the system at the recommendation of the annual inspection. Full maintenance is typically required every 24-36 months. Disposal of material should be handled in accordance with local regulations. Please contact CONTECH's Maintenance Department for all questions regarding maintenance at (503) 258-3157 or visit our website at www.conteches.com/maintenance.

Thank you for the opportunity to present this information to you and your client. If you have any questions, please call me at (443-457-1529).

Sincerely,

Taylor Murdock Stormwater Design Engineer Contech Engineered Solutions LLC

Summary for Subcatchment 1S: Inlet #1 DA

Runoff

=

0.03 cfs @

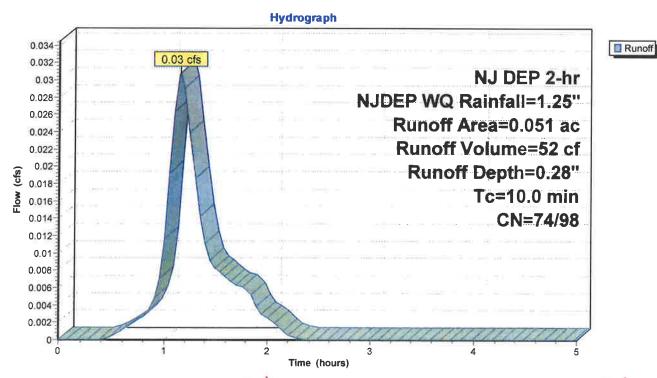
1.16 hrs, Volume=

52 cf, Depth= 0.28"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

-	Area (ac)	CN	Desc	cription			
*	0.011	98					
*	0.040	74					
	0.051	79	Weig	hted Aver	age		
	0.040	74		3% Pervio			
	0.011	98	21.5	7% Imperv	vious Area		
	Tc Leng	_	Slope	Velocity	Capacity	Description	
_	(min) (fe	et)	(ft/ft)	(ft/sec)	(cfs)		
	10.0					Direct Entry,	

Subcatchment 1S: Inlet #1 DA



Summary for Subcatchment 2S: Inlet #2 DA

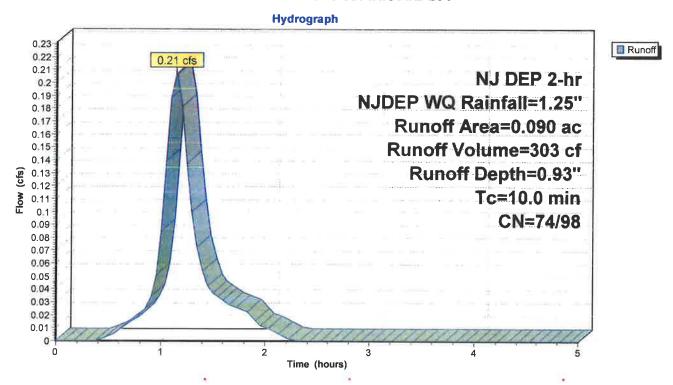
Runoff = 0.21 cfs @ 1.15 hrs, Volume=

303 cf, Depth= 0.93"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

	Area (ac) CN	Desc	cription			
*	0.080	98					
*	0.010	74					
7	0.090	95	Weig	hted Aver	age		
	0.010	74		1% Pervio			
	0.080	98	88.89	9% Imper	vious Area		
		_	Slope	Velocity	Capacity	Description	
_	(min) ((feet)	(ft/ft)	(ft/sec)	(cfs)		
	10.0					Direct Entry.	

Subcatchment 2S: Inlet #2 DA



Summary for Subcatchment 3S: Inlet #3 DA

Runoff

= 0

0.16 cfs @

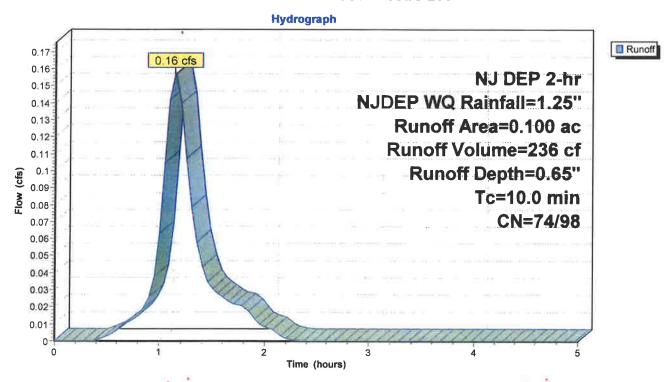
1.15 hrs, Volume=

236 cf, Depth= 0.65"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

	Area (ac)	CN	Desc	ription			
*	0.060	98					
*	0.040	74					
	0.100	88	Weig	hted Aver	age		
	0.040	74	40.00	% Pervio	us Area		
	0.060	98	60.00)% Imper	rious Area		
	Tc Len	_	Slope	Velocity	Capacity	Description	
_	(min) (fe	et)	(ft/ft)	(ft/sec)	(cfs)		_
	10.0					Direct Entry,	

Subcatchment 3S: Inlet #3 DA



Page 4

Summary for Subcatchment 4S: inlet #4 DA

Runoff

= 0.18 cfs @

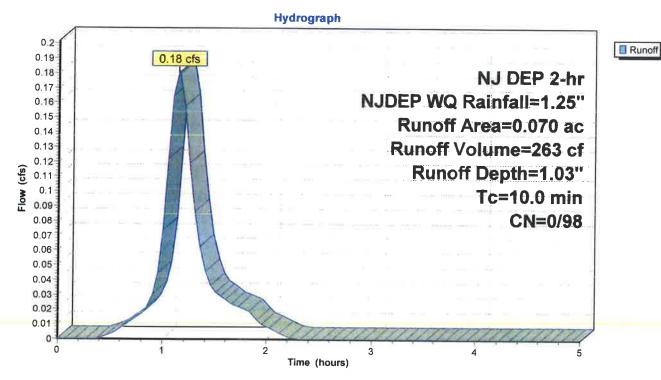
1.15 hrs, Volume=

263 cf, Depth= 1.03"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

-	Area	(ac)	CN	Desc	cription				
*	0.	070	98						
	0.	070	98	100.	00% Impe	rvious Area		8	
_	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	10.0						Direct Entry,		

Subcatchment 4S: Inlet #4 DA



Summary for Subcatchment MTD1: MTD #1 Inlet DA

Runoff

=

0.39 cfs @

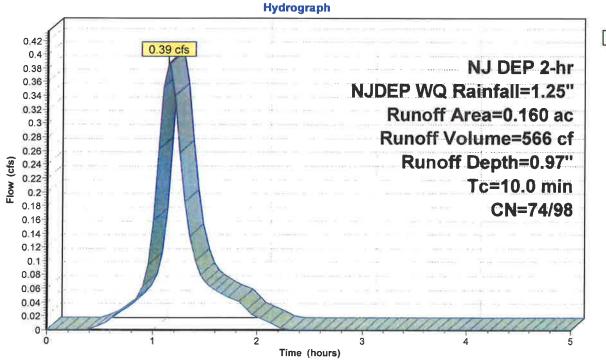
1.15 hrs, Volume=

566 cf, Depth= 0.97"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

_	Area (a	c) CN	Desc	cription		
*	0.15	50 98				
*	0.01	10 74				
	0.16	30 97	Weig	ghted Avei	age	
	0.01	10 74	6.25	% Perviou	s Ārea	
	0.15	50 98	93.7	5% Imper	ious Area	
-	Tc L (min)	ength	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7	10.0	77			······································	Direct Entry,

Subcatchment MTD1: MTD #1 Inlet DA







State of New Jersey

DEPARTMENT OF ENVIRONMENTAL PROTECTION

PHILIP D. MURPHY Governor

DIVISION OF WATERSHED PROTECTION AND RESTORATION BUREAU OF NJPDES STORMWATER PERMITTING & WATER QUALITY MANAGEMENT P.O. Box 420 Mail Code 501-02A Trenton, New Jersey 08625-0420

SHAWN M. LATOURETTE Commissioner

SHEILA Y. OLIVER Lt. Governor

609-633-7021 / Fax: 609-777-0432 www.nistormwater.org

November 18, 2022

Zachariha J. Kent Vice President of Product Management Bio Clean Environmental Services, Inc., a Quikrete Company 398 Via El Centro Oceanside, CA 92058

Re: MTD Lab Certification

Bio Clean High Capacity Kraken Filter Stormwater Treatment Device

Online Installation

TSS Removal Rate 80%

Dear Mr. Kent:

The Stormwater Management rules under N.J.A.C. 7:8-5.2(f) and 5.2(i) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Bio Clean Environmental Services, Inc., a Quikrete company, has requested a Laboratory Certification for the Bio Clean High Capacity Kraken Filter Stormwater Treatment Device (High Capacity Kraken Filter).

The project falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advance Technology" dated January 25, 2013. The applicable protocol is the "New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated October 2022) for this device is published online at http://www.njcat.org/uploads/newDocs/HCKrakenFilterNJCATFinalReport.pdf.

The NJDEP certifics the use of the High Capacity Kraken Filter by Bio Clean Environmental Services, Inc. at a TSS removal rate of 80% when designed, operated, and maintained in accordance with the information provided in the Verification Appendix and the following conditions:

1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-

- 5.5. The MTFR is calculated based on a verified loading rate of 0.101 gpm/ft² of effective membrane filter area.
- 2. The High Capacity Kraken Filter shall be installed using the same configuration reviewed by NJCAT, and sized in accordance with the criteria specified in item 6 below.
- 3. This device cannot be used in series with another MTD or a media filter (such as a sand filter) to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
- 4. Additional design criteria for MTDs can be found in Chapter 11.3 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual, which can be found online at www.njstormwater.org.
- 5. The maintenance plan for a site using this device shall incorporate, at a minimum, the maintenance requirements for the High Capacity Kraken Filter. A copy of the maintenance plan is attached to this certification. However, it is recommended to review the maintenance website at https://www.conteches.com/kraken for any changes to the maintenance requirements.

6. Sizing Requirement:

The example below demonstrates the sizing procedure for the High Capacity Kraken Filter:

Example:

A 0.25-acre impervious site is to be treated to 80% TSS removal using a High Capacity Kraken Filter. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs or 354.58 gpm.

The selection of the appropriate model of a High Capacity Kraken Filter is based upon both the maximum inflow drainage area and the MTFR. It is necessary to calculate the required model using both methods and to use the largest model determined by the two methods.

Inflow Drainage Area Evaluation:

The drainage area to the High Capacity Kraken Filter in this example is 0.25 acres. Based upon the information in Table 1 below, the following number of cartridges are required in a High Capacity Kraken Filter to treat the impervious area without exceeding the maximum allowable drainage area:

- a. Twenty-eight (28) 10" cartridges;
- b. Thirteen (13) 20" cartridges; or
- c. Eight (8) 30" cartridges.

Maximum Treatment Flow Rate (MTFR) Evaluation:

```
The site runoff (Q) was based on the following:

time of concentration = 10 minutes

i = 3.2 in/hr (page 74, Fig. 5-16 of Chapter 5 of the NJ Stormwater BMP Manual)

c = 0.99 (runoff coefficient for impervious)

Q = ciA = 0.99 \times 3.2 \times 0.25 = 0.79 \text{ cfs } (354.58 \text{ gpm})

(Note: 1 cfs = 448.83 gpm)
```

Given the site runoff is 0.79 cfs and based on Table 1 below, the following minimum numbers of cartridges are required in a High Capacity Kraken Filter without exceeding the MTFR of the individual model:

- a. Seventy-two (72) 10" cartridges;
- b. Thirty-three (33) 20" cartridges; or
- c. Twenty-one (21) 30" cartridges.

The MTFR evaluation results will be used since that method results in the highest minimum configuration determined by the two methods.

The sizing table corresponding to the available system models is noted below. Additional specifications regarding each model can be found in the NJCAT Verification Report in the Verification Appendix under Table A-1.

Table 1. High Capacity Kraken Filter Cartridge MTFRs and Maximum Allowable

Drainage Area

Cartridge Height (in)	Cartridge Maximum Treatment Flow Rate (MTFR) (cfs)	Maximum Allowable Drainage Area (acres)		
30	0.038	0.032		
20	0.024	0.020		
10	0.011	0.009		

Be advised a detailed maintenance plan is mandatory for any project with a Stormwater BMP subject to the Stormwater Management Rules, N.J.A.C. 7:8. The plan must include all of the items identified in the Stormwater Management Rules, N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of inspection and maintenance equipment and tools, specific corrective and preventative maintenance tasks, indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance and Retrofit of Stormwater Management Measures.

If you have any questions regarding the above information, please contact Changi Wu of my office at chang.i.wu@dep.nj.gov.

Labriel Mahon

Sincerely,

Gabriel Mahon, Chief

Bureau of NJPDES Stormwater Permitting & Water Quality Management Division of Watershed Protection and Restoration

New Jersey Department of Environmental Protection

Attachment: Maintenance Plan

cc: Richard Magee, NJCAT



HC Kraken Filter Design Summary

Block 502.01, Lot 57.01 (MTD #2) Franklin Twp, NJ 2/12/24

Information Provided by Engineer:

- Water quality flow rate = 1.09 cfs
- Impervious drainage area = 0.42 ac
- Pervious drainage area = 0.01 ac
- Presiding agency = NJDEP
- Required TSS removal rate = 80%

HC Kraken Filter Information and Cartridge Data:

The High-Capacity Kraken Filter Stormwater Treatment Device is a state-of-the-art stormwater filtration system utilizing pretreatment and advanced membrane filtration to ensure a high level of trash, TSS, metals, nutrients, and hydrocarbons removal. The HC Kraken Filter works by initially passing stormwater through a pretreatment chamber to capture trash, hydrocarbons, and sediments. Once runoff is pretreated, it is directed to the filter chamber where membrane filtration begins. When the water level reaches the top of the membrane filters, the treated water will then pass down the riser tube, collect in the underdrain manifold and flow to the discharge chamber. The High-Capacity Kraken Filter has received final certification from the NJDEP for 80% TSS removal as a stand-alone treatment system.

- HC Kraken Filter cartridge height = 20 inches (nominal)
- HC Kraken Filter cartridge surface area = 104.5 square feet
- HC Kraken Filter cartridge loading rate = 0.101 gallons/minute per square foot
- HC Kraken Filter cartridge treatment flow = 0.024 cfs
- Hydraulic head required = 28.5" (with 20-inch cartridge)

Design Summary:

The High-Capacity Kraken Filter is sized based on the NJDEP certification, which lists an approved treatment flow rate and maximum impervious acreage limit per cartridge in Table 1. The number of cartridges required based on the impervious drainage area is compared with the number of cartridges required based on the treatment flow rate; the larger number of cartridges governs the sizing.

The HC Kraken Filter for this site was sized to provide **46 cartridges** in order to meet the hydraulic load requirement (calculations shown below). To house this number of cartridges, Contech Engineered Solutions recommends a 6' x 8' precast Shallow HC Kraken Filter.

$$N_{cartridges\ hyd.load} = \frac{Q_{treat}}{Q_{cartridge}} = \frac{1.09\ cfs}{0.024\ cfs/_{cartridge}} = 45.42 \Rightarrow (46)\ 20"\ Cartridges$$

$$N_{cartridges\; mass\; load} = \frac{Area_{site}}{Max\; Area_{cartridge}} = \frac{0.42\; acres}{0.020\; acres/cartridge} = 21.00 \Rightarrow (21)\; 20"\; Cartridges$$

7037 Ridge Road, Suite 350 | Hanover, MD 21076 Office: 443-457-1500 Fax: 410-740-8492



HC Kraken Filter Design Summary

Maintenance:

Maintenance of Stormwater best management practices is required per the New Jersey Administrative Code 7:8-5.8. Recommendations for maintenance are included in chapters 8 & 9 of the New Jersey Stormwater Best Management Practices Manual. To comply with requirements, CONTECH offers a network of Preferred Service Providers that have the capability to perform all necessary inspections, compliance reporting and cleaning services. CONTECH recommends inspecting the system annually and maintaining the system at the recommendation of the annual inspection. Full maintenance is typically required every 24-36 months. Disposal of material should be handled in accordance with local regulations. Please contact CONTECH's Maintenance Department for all questions regarding maintenance at (503) 258-3157 or visit our website at www.conteches.com/maintenance.

Thank you for the opportunity to present this information to you and your client. If you have any questions, please call me at (443-457-1529).

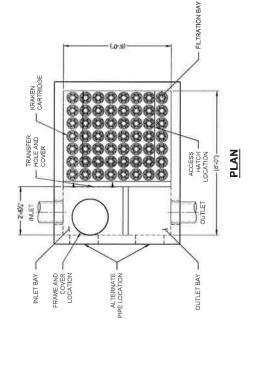
7037 Ridge Road, Suite 350 | Hanover, MD 21076

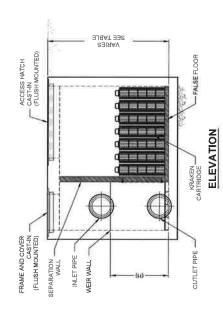
Fax: 410-740-8492

Office: 443-457-1500

Sincerely,

Taylor Murdock
Stormwater Design Engineer
Contech Engineered Solutions LLC





KRAKEN FILTER DESIGN NOTES

- KRANEN FLIER TREATMENT CARACTIFT VARIES BY CARTRIDGE COLAIT AND LOCALLY APPROVED SURFACE AREA SPECIFIC FLOW RATE, PEAK
 CONVEYANCE CAPACITY TO BE DETERMINED BY ENGINEER OF RECORD CONVEYANCE OF CARTRIDGES (58) AND IS AVAILABLE IN
 A LEFT IMETIVE ASSOCIATION STYLE KRANEN FLITER IS SHOWN WITH THE MAXIMUM NUMBER OF CARTRIDGES (58) AND IS AVAILABLE IN
 A LEFT IMETIVE ASSOCIATION STYLE KRANEN FROVIDED BY CONTINUED SYNOTED OTHERWISE

CARTRIDGE HEIGHT	30"	20"	10
RECOMMENDED HYDRAULIC DROP (H)	38.5"	28.5"	18,5"
SPECIFIC FLOW RATE (gpm/sf)	0,10	0,10	0,10
CARTRIDGE FLOW RATE (gpm)	17	10.6	4.9

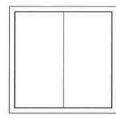


DATA REQUIREMENTS

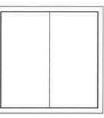
RETURN PERIOD OF PEAK FLOW lyns

STRUCTURE ID
WATER QUALITY FLOW RATE (cm)

SITE SPECIFIC



(SIZE MAY VARY) (NOT TO SCALE)





CONTECH









MAX HEIGHT 4-10

MIN HEIGHT

CARTRIDGE SIZE 10" & 20" 30.

3,-6 4'-2"

RIM TO SYSTEM INVERT

4-10

FRAME AND COVER (30" ROUND) (NOT TO SCALE)

- GENERAL NOTES

 LO ONICHOT PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.

 2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS, ACTUAL DIMENSIONS MAY VARY,

 3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH
- REPRESENTATIVE, www.combedieS.com
 4. KRAKEN PLIER WARTE QUALITY. STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS
 DRAWMING, CONTRACTOR OF STRUCTURE SHALL MEETS REQUIREMENTS OF PROJECT.
 5. STRUCTURE SHALL MEET AASHTO HS20 LOAD RATING, ASSUMING EARTH COVER OF 0°-10° AND GROUNDWATER ELEVATION AT, OR BELOW.
 THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS SHALL MEET
 AASHTO MSOS AND BE CAST WITH THE CONTECH LOGG.

- INSTALLATION NOTES.
 A. APT SUB-BASE, ENCKELL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE
 A. APT SUB-BASE, ENCKELL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS OF SECURITY OF LIFT AND SET THE KRAKEN FILTER SITUCTURE.
 B. CONTRACTIOR TO REVISIONE USE OF SECURITY SET ANTI BETWEEN ALL SECTIONS AND ASSEMBLE STRUCTURE.
 D. CONTRACTIOR TO REVOID IN INSTALL, AND SOFTON PIPES. MATHOUTE PIPE INVEST WITH OUTLIF THE YELOOR.
 E. CONTRACTIOR TO TAKE APPROPRIATE MASSINES TO PROVIDE INSTALL CHAIR SOFTON PARES.
 E. CONTRACTION TO THE AREA SHEES TO PROVIDE INSTALL CHAIR SOFTON CONSTRUCTION. RELATED EROSION RUNOFF.
 F. CONTRACTOR TO REMOUS THE TRANSFER OPENING COVER WHEN THE SYSTEM IS BROUGHT ONLINE.

THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING US PATENTS: 9604,160;10,145,785,10,369,496;11,280,321, RELATED FOREIGN PATENTS OR OTHER PATENT PENDING



PEAK DIVERSION KRAKEN FILTER STANDARD DETAIL KFPD0608 (6' x 8') SHALLOW

Summary for Subcatchment 5S: Inlet #5 DA

Runoff

=

0.21 cfs @

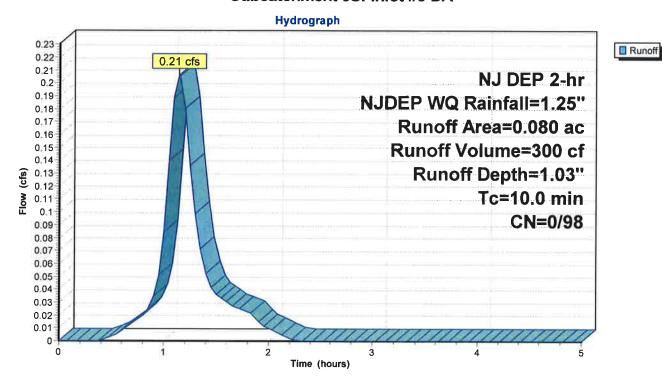
1.15 hrs, Volume=

300 cf, Depth= 1.03"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

	Area	(ac)	CN	Desc	cription		
*	0.	080	98				
	0.	080	98	100.	00% Impe	rvious Area	a
	Tc (min)	Leng (fee		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
=	10.0	(100	,,	(IUIL)	(10360)	(015)	Direct Entry,

Subcatchment 5S: Inlet #5 DA



Summary for Subcatchment MTD2: MTD #2 Inlet DA

Runoff

= 0.88 cfs @

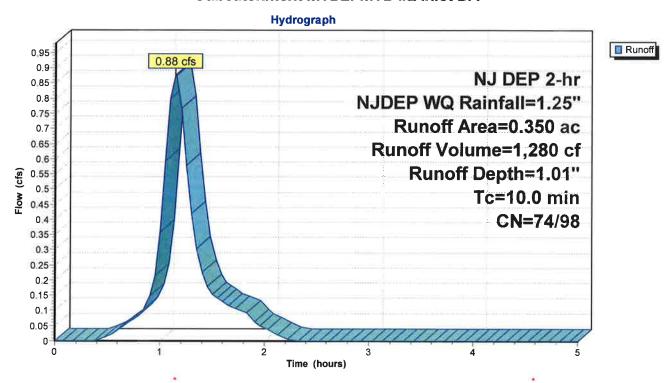
1.15 hrs, Volume=

1,280 cf, Depth= 1.01"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 0.00-5.00 hrs, dt= 0.05 hrs NJ DEP 2-hr NJDEP WQ Rainfall=1.25"

	Area (ac)	CN	Desc	ription			
*	0.340	98					
*	0.010	74					
	0.350	97	Weig	hted Aver	age		
	0.010	74	2.869	% Perviou	s Area		
	0.340	98	97.14	l% Imperv	vious Area		
	Tc Leng	gth	Slope	Velocity	Capacity	Description	
_	(min) (fe	et)	(ft/ft)	(ft/sec)	(cfs)		
	10.0					Direct Entry.	

Subcatchment MTD2: MTD #2 Inlet DA





State of New Jersey

DEPARTMENT OF ENVIRONMENTAL PROTECTION

PHILIP D. MURPHY
Governor

DIVISION OF WATERSHED PROTECTION AND RESTORATION
BUREAU OF NJPDES STORMWATER PERMITTING & WATER QUALITY MANAGEMENT
P.O. Box 420 Mail Code 501-02A

SHAWN M. LATOURETTE Commissioner

SHEILA Y. OLIVER
Lt. Governor

Trenton, New Jersey 08625-0420 609-633-7021 / Fax: 609-777-0432 www.nistormwater.org

November 18, 2022

Zachariha J. Kent Vice President of Product Management Bio Clean Environmental Services, Inc., a Quikrete Company 398 Via El Centro Oceanside, CA 92058

Re:

MTD Lab Certification

Bio Clean High Capacity Kraken Filter Stormwater Treatment Device

Online Installation

TSS Removal Rate 80%

Dear Mr. Kent:

The Stormwater Management rules under N.J.A.C. 7:8-5.2(f) and 5.2(j) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Bio Clean Environmental Services, Inc., a Quikrete company, has requested a Laboratory Certification for the Bio Clean High Capacity Kraken Filter Stormwater Treatment Device (High Capacity Kraken Filter).

The project falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advance Technology" dated January 25, 2013. The applicable protocol is the "New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated October 2022) for this device is published online at http://www.njcat.org/uploads/newDocs/HCKrakenFilterNJCATFinalReport.pdf.

The NJDEP certifies the use of the High Capacity Kraken Filter by Bio Clean Environmental Services, Inc. at a TSS removal rate of 80% when designed, operated, and maintained in accordance with the information provided in the Verification Appendix and the following conditions:

1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-

- 5.5. The MTFR is calculated based on a verified loading rate of 0.101 gpm/ft² of effective membrane filter area.
- 2. The High Capacity Kraken Filter shall be installed using the same configuration reviewed by NJCAT, and sized in accordance with the criteria specified in item 6 below.
- 3. This device cannot be used in series with another MTD or a media filter (such as a sand filter) to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
- 4. Additional design criteria for MTDs can be found in Chapter 11.3 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual, which can be found online at www.njstormwater.org.
- 5. The maintenance plan for a site using this device shall incorporate, at a minimum, the maintenance requirements for the High Capacity Kraken Filter. A copy of the maintenance plan is attached to this certification. However, it is recommended to review the maintenance website at https://www.conteches.com/kraken for any changes to the maintenance requirements.
- 6. Sizing Requirement:

The example below demonstrates the sizing procedure for the High Capacity Kraken Filter:

Example:

A 0.25-acre impervious site is to be treated to 80% TSS removal using a High Capacity Kraken Filter. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs or 354.58 gpm.

The selection of the appropriate model of a High Capacity Kraken Filter is based upon both the maximum inflow drainage area and the MTFR. It is necessary to calculate the required model using both methods and to use the largest model determined by the two methods.

Inflow Drainage Area Evaluation:

The drainage area to the High Capacity Kraken Filter in this example is 0.25 acres. Based upon the information in Table 1 below, the following number of cartridges are required in a High Capacity Kraken Filter to treat the impervious area without exceeding the maximum allowable drainage area:

- a. Twenty-eight (28) 10" cartridges;
- b. Thirteen (13) 20" cartridges; or
- c. Eight (8) 30" cartridges.

Maximum Treatment Flow Rate (MTFR) Evaluation:

The site runoff (Q) was based on the following: time of concentration = 10 minutes i = 3.2 in/hr (page 74, Fig. 5-16 of Chapter 5 of the NJ Stormwater BMP Manual) c = 0.99 (runoff coefficient for impervious) $Q = ciA = 0.99 \times 3.2 \times 0.25 = 0.79 \text{ cfs (354.58 gpm)}$ (Note: 1 cfs = 448.83 gpm) Given the site runoff is 0.79 cfs and based on Table 1 below, the following minimum numbers of cartridges are required in a High Capacity Kraken Filter without exceeding the MTFR of the individual model:

- a. Seventy-two (72) 10" cartridges;
- b. Thirty-three (33) 20" cartridges; or
- c. Twenty-one (21) 30" cartridges.

The MTFR evaluation results will be used since that method results in the highest minimum configuration determined by the two methods.

The sizing table corresponding to the available system models is noted below. Additional specifications regarding each model can be found in the NJCAT Verification Report in the Verification Appendix under Table A-1.

Table 1. High Capacity Kraken Filter Cartridge MTFRs and Maximum Allowable
Drainage Area

Cartridge Height (in)	Cartridge Maximum Treatment Flow Rate (MTFR) (cfs)	Maximum Allowable Drainage Area (acres)
30	0.038	0.032
20	0.024	0.020
10	0.011	0.009

Be advised a detailed maintenance plan is mandatory for any project with a Stormwater BMP subject to the Stormwater Management Rules, N.J.A.C. 7:8. The plan must include all of the items identified in the Stormwater Management Rules, N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of inspection and maintenance equipment and tools, specific corrective and preventative maintenance tasks, indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance and Retrofit of Stormwater Management Measures.

If you have any questions regarding the above information, please contact Changi Wu of my office at chang.i.wu@dep.nj.gov.

Labriel Mahor

Sincerely,

Gabriel Mahon, Chief

Bureau of NJPDES Stormwater Permitting & Water Quality Management Division of Watershed Protection and Restoration

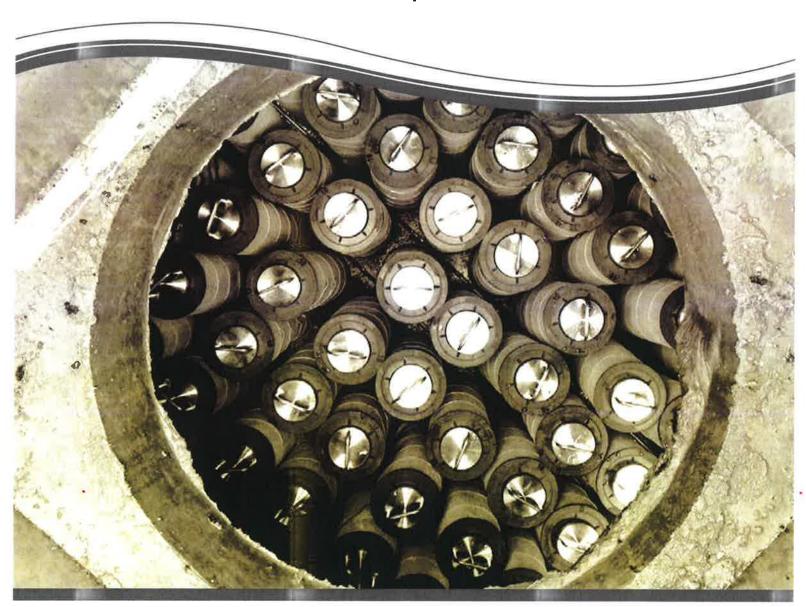
New Jersey Department of Environmental Protection

Attachment: Maintenance Plan

cc: Richard Magee, NJCAT



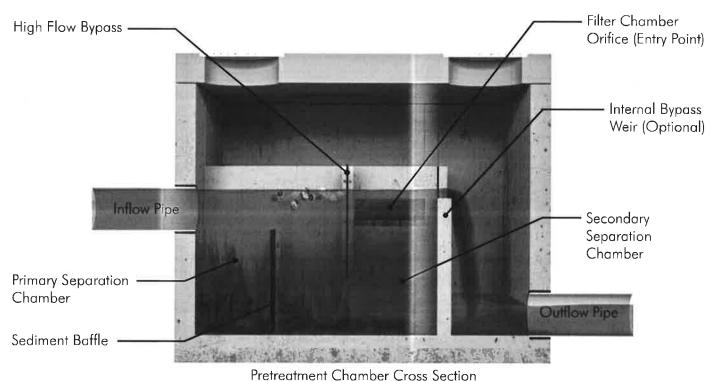
Kraken® Filter Operation & Maintenance Manual



Operation & Maintenance

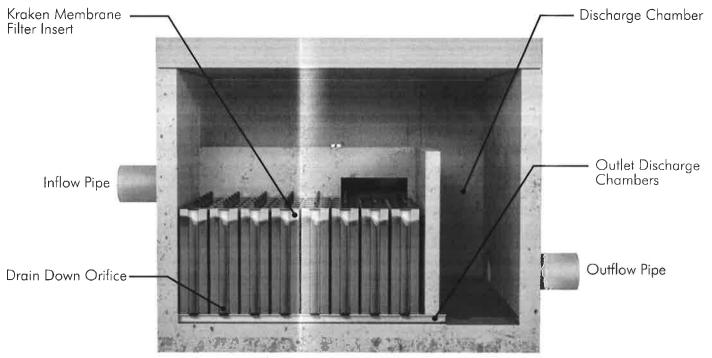
The Kraken® Filter is designed at a minimal loading rate of only 0.05 gpm/sq ft of media surface to maximize longevity and minimize maintenance requirements. Passive backwash and pretreatment also help to minimize system maintenance requirements. The Kraken® Filter is estimated to be able to handle up to at least 18 months sediment loading with no maintenance or loss of treatment capacity assuming 600 pounds of sediment per acre of impervious surface annually.

Yet, as with all stormwater BMPs, inspection and maintenance on the Kraken[®] Filter is necessary. Stormwater regulations require that all BMPs be inspected and maintained to ensure they are operating as designed to allow for effective pollutant removal and to provide protection to receiving water bodies. It is recommended that inspections be performed multiple times during the first year to assess the site specific loading conditions. This is recommended because pollutant loading and pollutant characteristics can vary greatly from site to site. Variables such as nearby soil erosion or construction sites, winter sanding on roads, amount of daily traffic and land use can increase pollutant loading on the system. Observations made during the first year of inspections can be used to estimate inspection and maintenance intervals for subsequent years to ensure appropriate maintenance is provided. Without appropriate maintenance, a BMP will exceed its storage capacity which can negatively affect its continued performance in removing and retaining captured pollutants.



rrefrediment Chamber Cross Section

Pre-Treatment Chamber Diagram



Filtration Chamber Cross Section

Filter Chamber Diagram

Inspection Equipment

Following is a list of equipment to allow for simple and effective inspection of the Kraken® Filter:

- Contech Inspection Form
- Flashlight
- Manhole hook or appropriate tools to access hatches and covers
- Appropriate traffic control signage and procedures
- Measuring pole and/or tape measure
- Protective clothing and eye protection

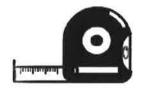












Inspection Steps

The core to any successful stormwater BMP maintenance program is routine inspections. The inspection steps required on the Kraken[®] Filter are quick and easy. As mentioned above, the first year should be seen as the maintenance interval establishment phase. During the first year, more frequent inspections should occur in order to gather loading data and maintenance requirements for that specific site. This information can be used to plan future inspection and maintenance intervals.

The Kraken® Filter can be inspected through visual observation without entry into the system. All necessary pre-inspection steps must be carried out before inspection occurs, especially traffic control and other safety measures to protect the inspector and near-by pedestrians from any dangers associated with an open access hatch or manhole. Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine inspections of the system. Once these access covers have been safely opened the inspection process can proceed:

- Prepare the inspection form by writing in the necessary information including project name, location, date & time, unit number and other info (see inspection form).
- Observe the inside of the system through the access hatches. If minimal light is available and vision into the unit is impaired, utilize a flashlight to see inside the system and all of its chambers.
- Look for any obstructions in the inflow pipe, pre-treatment chamber, filter chambers, discharge chamber or outflow pipe. Write down any observations on the inspection form.
- Through observation and/or digital photographs, estimate the amount of floatable debris accumulated in the pretreatment chamber. Record this information on the inspection form. Next, utilizing a tape measure or measuring stick, estimate the amount of sediment accumulated in the primary and secondary sedimentation chambers. Record this depth on the inspection form. Through visual observation, inspect the condition of the filter cartridges. Look for excessive build-up of sediments on the surface and any build-up on the top of the cartridges. Record this information on the inspection form.
- Finalize inspection report for analysis by the maintenance manager to determine if maintenance is required.

Maintenance Indicators

Based upon observations made during inspection, maintenance of the system may be required based on the following indicators:

- Missing or damaged internal components or cartridges
- Obstructions in the system or its inlet or outlet
- Accumulation of floatables in the pre-treatment chambers in which the length and width of the chamber behind oil/floatables skimmer is fully impacted
- Accumulation of sediment in the primary sedimentation chamber of more than 18" in depth
- Accumulation of sediment in the secondary sedimentation chamber of more than 6" in depth
- Accumulation of sediment in the filter chambers of more than 3" on average
- Substantial build-up of sediments on the filter membrane of the filter cartridges which will have a very dark appearance indicating the membrane may be fully saturated with sediment

The Kraken Filter vault is a robust system and is designed for treating and bypassing (when required) flow rates calculated by the Engineer of Record. Under the designed conditions with routine maintenance and inspections, the Kraken Filter should function for many years. The Kraken Filter can fail under certain conditions, such as: severe damage and cracking through the vault walls, internal weir and baffle walls falling out of place, blockages of the flow path such as inlet or outlet, filters not reset properly, excessive debris or sediment accumulation within the vault and on the filters. With proper maintenance these risks can be avoided. Contech representatives are also available for troubleshooting.

Maintenance Equipment

While maintenance can be done fully by hand, it is recommended that a vacuum truck be utilized to minimize time required to maintain the Kraken® Filter:

- Contech Maintenance Form
- Flashlight
- Manhole hook or appropriate tools to access hatches and covers
- Appropriate traffic control signage and procedures
- Measuring pole and/or tape measure
- Protective clothing and eye protection
- Vacuum truck
- Trash can
- Pressure washer

Note: entering a confined space requires appropriate safety and certification. It is generally not required for routine inspections of the system. Entry into the system will be required if it is determined the cartridge filters need washing/cleaning

Maintenance Procedures

It is recommended that maintenance occurs at least three days after the most recent rain event to allow for drain down of the system and any upstream detention systems designed to drain down over an extended period of time. Maintaining the system while flows are still entering it will increase the time and complexity required for maintenance. Cleaning of the pre-treatment chamber can be performed from finish surface without entry into the vault utilizing a vacuum truck. Once all safety measures have been set up, cleaning of the pre-treatment chamber can proceed as follows:

- Following rules for confined space entry, use a gas meter to detect the presence of any hazardous gases. If hazardous gases are present, do not enter the vault. Following appropriate confined space procedures, take steps, such as utilizing a venting system, to address the hazard. Once it is determined to be safe, enter utilizing appropriate entry equipment such as a ladder and tripod with harness.
- Once entry into the system has been established the maintenance technician should position themselves to stand in the pre-treatment chamber. From here, the removal of the cartridges can commence.
- Threaded couplings are used now, but old systems will have the pressure fitted coupling. Each cartridge that is pressure fitted in place will include a handle for easy removal. To remove a cartridge, simply grab the handle and pull straight up. It may be required to gently shift pressure from side to side while pulling up to break the pressure seal. Removal of the cartridge should be done by hand with minimal effort and requires no tools.
- Once the cartridges are removed, they should be lifted out from the vault and brought up to finish surface for cleaning. Using a large garbage can and a standard garden hose (low pressure nozzle), each cartridge should be rinsed off from the outside to remove accumulated sediments and debris. Once each cartridge is rinsed, it should be placed to the side for re-installation.

- Each filter chamber should be power washed and vacuumed clean before re-inserting the cleaned cartridges.
- After all cartridges have been washed, they can be replaced back into the vault. To replace each cartridge, simply slide cartridge over each pressure fitted coupler. Threaded couplings are used now, but old systems will have the pressure fitted coupling. Push down on the handle to ensure the cartridge has been fully seated and the bottom of the cartridge is making contact with the floor.
- The last step is to replace all access hatch lids and remove all traffic control.
- All removed debris and pollutants shall be disposed of following local and state requirements.

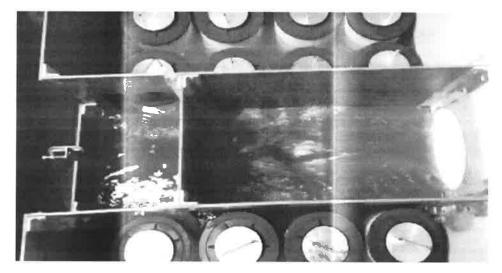
Maintenance Sequence



1. Remove access hatches set up vacuum truck to clean the pretreatment chamber.



2. Insert vacuum hose in the sedimentation chamber and vacuum out all trash, sediment and standing water.



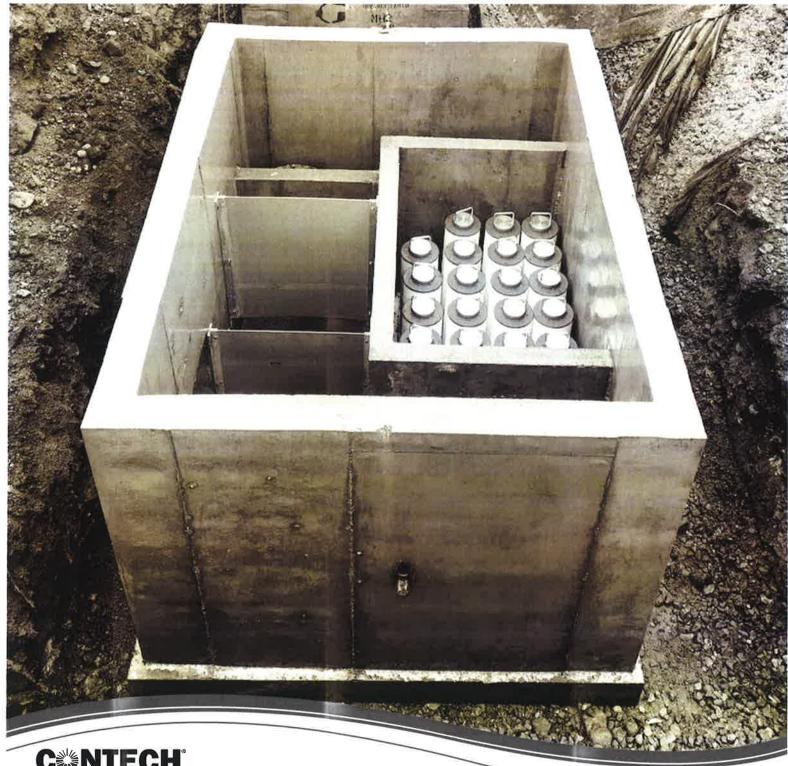
3. Assess the condition of the filter cartridges and determine if cleaning is required.



4. To wash cartridges, remove from vault. Place over trash can and use a garden hose to spray clean.



5. Once cleaned, install back into the vault. This completes maintenance. Ensure access lids are properly replaced.



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Kraken Maintenance Guide 08/22

APPENDIX D: PRE AND POST DEVELOPMENT DRAINAGE AREA MAP DATED 2/18/24

APPENDIX E:

SOIL PROFILES AND SOIL PERMEABILITY TEST DATA

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SOIL INVESTIGATION CONDUCTED FOR DETERMINING WATER TABLE AND PERMEABILITY RATINGS

Date of Investigations: 12/16/2023

Method of Excavation: Large Track Hoe, Water Tank and Helpers

Excavator: Rey Wittmann, JW Landscape Contractors Inc., 39 Minnan Street

Rahway, NJ – 07065

Weather: Sunny to Partially Sunny

Lot #1

Depth:	Descriptions:
0" – 8"	Top Soil (Dark Reddish Brown) – 2.5 YR (3/2), Sub Angular Blocky, Friable
8 " – 34"	Silty Clay, Dark Reddish Brown, Firm to Friable - 5 YR (4/4)
34" – 120"	Fragmented Shale, Dark Reddish Brown (60" – 90" Depth – The shale layer is
	very hard)), 2.5 YR (3/6), Rippable, More than 80% non-soil shale fragments, 6"
	- 12" size plates with depth size increases, Water Table Observed at 7'.
Log #2	
Depth:	Descriptions:
0"-6"	Top Soil (Dark Reddish) - 2.5 YR (3/2)
6" – 42"	Clay Loam, Dark Reddish Brown, Blocky, Friable - 5 YR (4/4)
42" – 120"	Fragments Platy Shale, Dark Reddish Brown (60" – 90" Depth – The shale is
	very hard), More than 80% non-soil shale fragments
	A PERC test conducted at the depths of 72" (From 84" and deeper - very platy
	structure), Water Table Observed at 7'.
Log #4	<i>"</i>
0"-12"	Top Soil (Dark Reddish), - 2.5 YR (3/2)
12" - 41"	Clay Loam, Dark Reddish Brown, Blocky, Friable, - 5 YR (4/4)
41" – 132"	Fragmented Platy Shale, Dark Reddish Brown (60" – 90" Depth – The shale is
	very hard), (24" – 48" Very Platy, 48" – 72" Very Hard Ripping, 72" – 120"),
	Very platy and Fragmented.
Log #5:	
0" - 8"	Top Soil (Dark Reddish) – 2.5 YR (3/2)
8"-38"	
38" – 120"	
0" - 8" 8" - 38"	Top Soil (Dark Reddish) – 2.5 YR (3/2) Clay Loam, Dark Reddish Brown, Blocky and Sub angular, Friable, 5 YR (4/4) Fragmented Platy Shale, Dark Reddish Brown, Alternative Very Firm to Rippable Shale layer, With depths the size of shale increases to 8" – 12" platy and in blocks. Water Table at 72")

^{*} The fragmented shale layers showed seams, which were hard to rip. A machine with rippable teeth required for this investigations.

Date of Test:12/16/2023 -Basin Flood*

Location of Pit - Log #1

Size of Pit -3' x 8'

Depth of Fractured Shale: 60" (Bottom of Test Elevation) – gallons poured - 375 per fill

Time Basin Flooded (1st Fill): 15:10 Time to Empty Basin: 15:45 Time Basin Flooded (2nd Fill): 15.55 Time to Empty Basin: 16:40

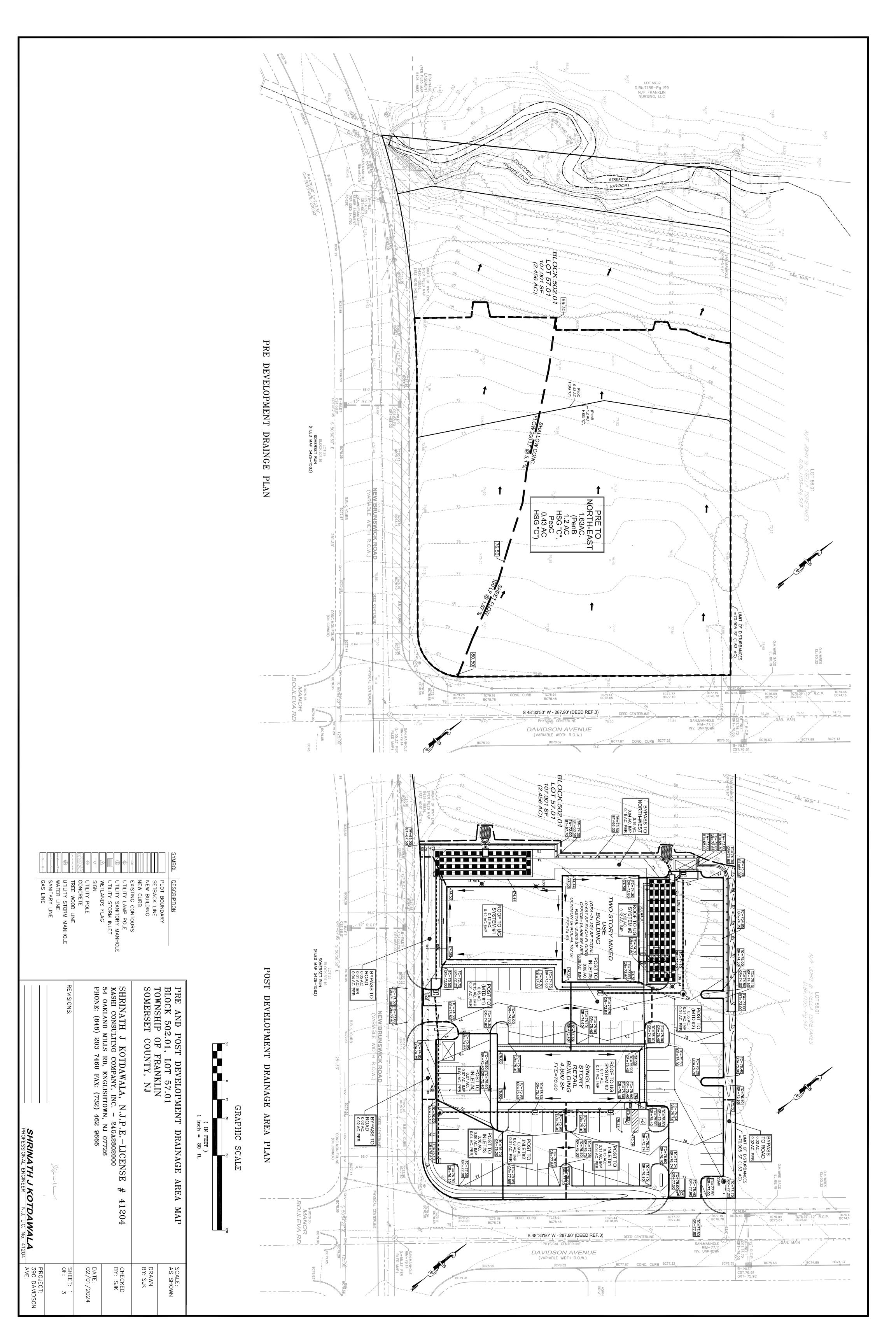
Location of Pit - Log #4

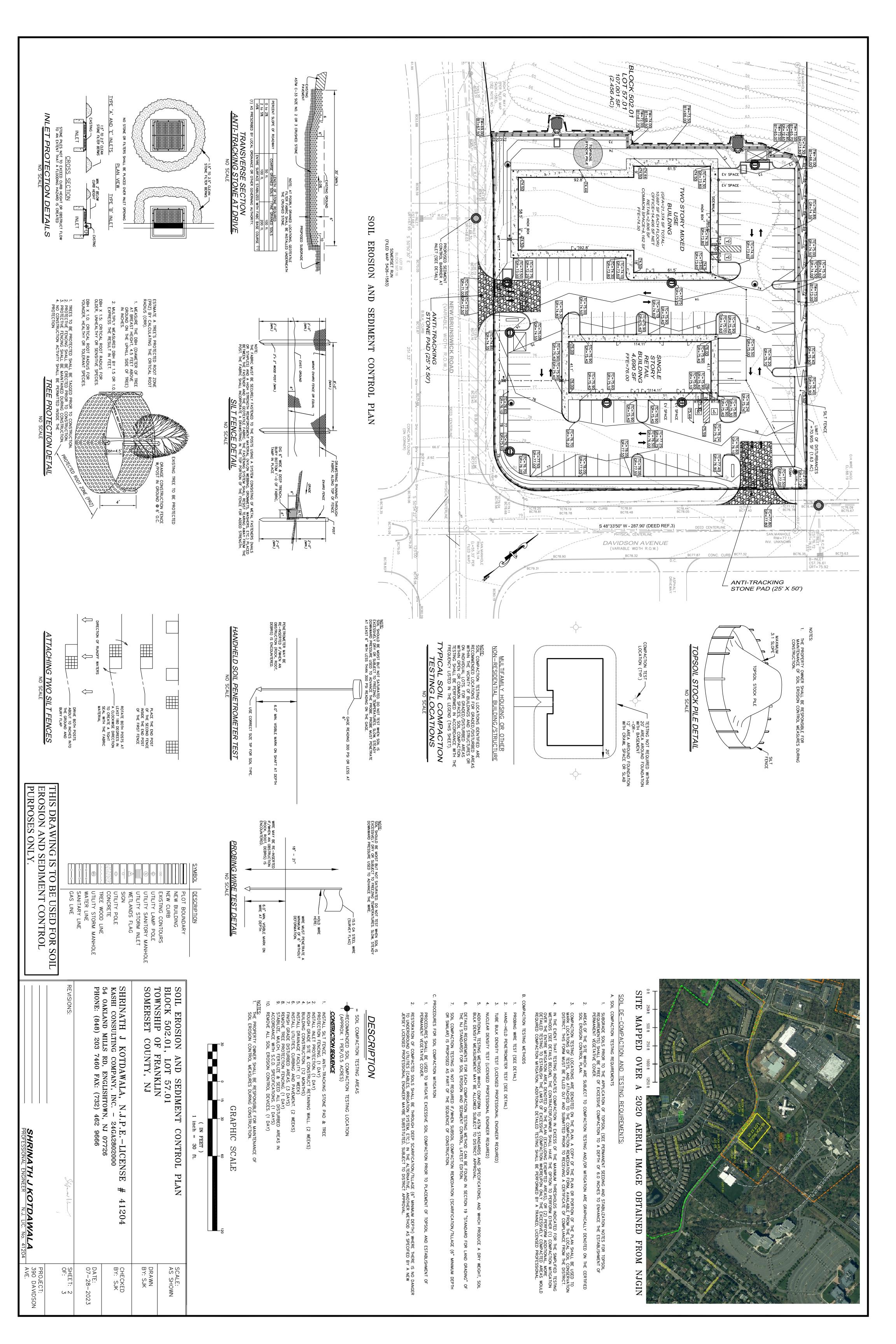
Size of Pit -3' x 8'

Depth of Fractured Shale: 78" (Bottom of Test Elevation) – gallons poured - 375 per fill

Time Basin Flooded (1st Fill): 14:07 Time to Empty Basin: 15:24 Time Basin Flooded (2nd Fill): 15.30 Time to Empty Basin: 16:20

^{*} As all the profiles have variations in fracture sizes and depths – a field test shall be done when the entire excavation for the ground Stormwater System is excavated as per the BMP manual. Two permeability tests are conducted to assist in determining the PERC value of 6.316 inch / hour. The results are enclosed.





PERMANENT VEGETATIVE COVER FOR SOIL STABILIZATION:

- GRADE AS NEEDED AND FEASIBLE TO PERMIT THE USE OF CONVENTIONAL EQUIPMENT FOR SEEDBED PREPARATION, SEEDING, MULCH APPLICATION, AND MULCH ANCHORING. ALL GRADING SHOULD BE DONE IN ACCORDANCE WITH STANDARD FOR LAND GRADING.
- IMMEDIATELY PRIOR TO SEEDING AND TOPSOIL APPLICATION, THE SUBSOIL SHALL BE EVALUATED FOR COMPACTION IN ACCORDANCE WITH THE STANDARD FOR LAND GRADING.

 TOPSOIL SHOULD BE HANDLED ONLY WHEN IT IS DRY ENOUGH TO WORK WITHOUT DAMAGING THE SOIL STRUCTURE. A UNIFORM APPLICATION TO A DEPTH OF 5 INCHES (UNSETTLED) IS REQUIRED ON ALL SITES. TOPSOIL SHALL BE AMENDED WITH ORGANIC MATTER, AS NEEDED, IN ACCORDANCE WITH THE STANDARD FOR TOPSOILING.
- SEEDBED PREPARATION
 UNIFORMLY APPLY GF INSTALL NEEDED EROSION CONTROL PRACTICES OR FACILITIES SUCH AS DIVERSIONS, GRADE STABILIZATION STRUCTURES, CHANNEL STABILIZATION MEASURES, SEDIMENT BASINS, AND WATERWAYS.
- UNIFORMLY APPLY GROUND LIMESTONE AND FERTILIZER TO TOPSOIL WHICH HAS BEEN SPREAD AND FIRMED, ACCORDING TO SOIL TEST RECOMMENDATIONS SUCH AS OFFERED BY RUTGERS CO-OPERATIVE EXTENSION. SOIL SAMPLE MAILERS ARE AVAILABLE FROM THE LOCAL RUTGERS COOPERATIVE EXTENSION OFFICES (https://njacs.rutgers.edu/county/). FERTILIZER SHALL BE APPLIED AT THE RATE OF 500 POUNDS PER ACRE OR 11 POUNDS PER 1,000 SQUARE FEET OF 10-10 OR EQUIVALENT WITH 50% WATER INSOLUBLE NUTROGEN UNLESS A SOIL TEST INDICATES OTHERWISE AND INCORPORATED INTO THE SURFACE 4 INCHES. IF FERTILIZER IS NOT INCORPORATED, APPLY ONE HALF THE RATE DESCRIBED ABOVE DURING SEEDBED PREPARATION AND REPEAT ANOTHER ONE HALF RATE APPLICATION OF THE SAME FERTILIZER WITHIN 3 TO 5 WEEKS AFTER SEEDING.
- WORK LIME AND FERTILIZER INTO THE TOPSOIL AS NEARLY AS PRACTICAL TO A DEPTH OF 4 INCHES WITH A DISC, SPRINGTOOTH HARROW, OR OTHER SUITABLE EQUIPMENT. THE FINAL HARROWING OR DISKING OPERATION SHOULD BE ON THE GENERAL CONTOUR. CONTINUE TILLAGE UNTIL A REASONABLE UNIFORM SEEDBED IS PREPARED.

 HIGH ACID PRODUCING SOIL. SOILS HAVING A PH OF 4 OR LESS OR CONTAINING IRON SULFIDE SHALL BE COVERED WITH A MINIMUM OF 12 INCHES OF SOIL HAVING A PH OF 5 OR MORE BEFORE INITIATING SEEDBED PREPARATION. SEE STANDARD FOR MANAGEMENT OF HIGH ACID PRODUCING SOILS FOR SPECIFIC REQUIREMENTS.
- SELECT A MIXTURE FROM TABLE 4-3 OR USE MIXTURE RECOMMENDED BY RUTGERS COOPERATIVE EXTENSION OR NATURAL RESOURCES CONSERVATION SERVICE WHICH IS APPROVED BY THE SOIL CONSERVATION DISTRICT. SEED GERMINATION SHALL HAVE BEEN TESTED WITHIN 12 MONTHS OF THE PLANTING DATE. NO SEED SHALL BE ACCEPTED A GERMINATION TEST DATE MORE THAN 12 MONTHS OLD UNLESS RETESTED.
- SEEDING RATES SPECIFIED ARE REQUIRED WHEN A REPORT OF COMPLIANCE IS REQUESTED PRIOR TO ACTUAL ESTABLISHMENT OF PERMANENT VEGETATION. UP TO 50% REDUCTION IN RATES MAY BE USED WHEN PERMANENT VEGETATION IS ESTABLISHED PRIOR TO A REPORT OF COMPLIANCE INSPECTION. THESE RATES APPLY TO ALL METHODS OF SEEDING. ESTABLISHING PERMANENT VEGETATION MEANS 80% VEGETATIVE COVERAGE WITH THE SPECIFIED SEED MIXTURE FOR THE SEEDED AREA AND MOWED ONCE.
- WARM SEASON MIXTURES ARE GRASSES AND LEGUMES WHICH MAXIMIZE GROWTH AT HIGH TEMPERATURES, GENERALLY 850 F AND ABOVE. SEE TABLE 4–3 MIXTURES 1 TO 7. PLANTING RATES FOR WARM SEASON GRASSES SHALL BE THE AMOUNT OF PURE LIVE SEED (PLS) AS DETERMINED BY GERMINATION TESTING RESULTS.
- COOL SEASON MIXTURES ARE GRASSES AND LEGUMES WHICH MAXIMIZE GROWTH AT TEMPERATURES BELOW 850 F. MANY GRASSES BECOME ACTIVE AT 650 F. SEE TABLE 4-3, MIXTURES 8-20. ADJUSTMENT OF PLANTING RATES TO COMPENSATE FOR THE AMOUNT OF PURE LIVE SEED IS NOT REQUIRED FOR COOL SEASON GRASSES. CONVENTIONAL SEEDING IS PERFORMED BY APPLYING SEED UNIFORMLY BY HAND, CYCLONE (CENTRIFUGAL) SEEDER, DROP SEEDER, DRILL OR CULTIPACKED SEEDINGS, SEED SHALL BE INCORPORATED INTO THE SOIL WITHIN 24 HOURS OF SEEDBED PREPARATION TO A DEPTH OF 1/4 TO 1/2 INCH, BY RAKING OR DRAGGING. DEPTH OF SEED PLACEMENT MAY BE 1/4 INCH DEEPER ON COARSE TEXTURED SOIL.
- HYDROSEEDING IS A BROADCAST SEEDING METHOD USUALLY INVOLVING A TRUCK OR TRAILER MOUNTED TANK, WITH AN AGITATION SYSTEM AND HYDRAULIC PUMP FOR MIXING SEED, WATER AND FERTILIZER AND SPRAYING THE MIX ONTO THE PREPARED SEEDBED. MULCH SHALL NOT BE INCLUDED IN THE TANK WITH SEED. SHORT FIBERED MULCH MAY BE APPLIED WITH A HYDROSEEDER FOLLOWING SEEDING. (ALSO SEE SECTION 4-MULCHING BELOW). HYDROSEEDING IS NOT A PREFERRED SEEDING METHOD BECAUSE SEED AND FERTILIZER ARE APPLIED TO THE SURFACE AND NOT INCORPORATED PROPERTY. THE SOIL. WHEN POOR SEED TO SOIL CONTACT OCCURS, THERE IS A REDUCED SEED GERMINATION AND GROWTH. AFTER SEEDING, FIRMING THE SOIL WITH A CORRUGATED ROLLER WILL ASSURE GOOD SEED—TO—SOIL CONTACT, RESTORE CAPILLARITY, AND IMPROVE SEEDLING EMERGENCE. THIS IS THE PREFERRED METHOD. WHEN PERFORMED ON THE CONTOUR, SHEET EROSION WILL BE MINIMIZED AND WATER CONSERVATION ON SITE WILL BE MAXIMIZED.
- MULCHING IS REQUIRED ON ALL SEEDING. MULCH WILL INSURE AGAINST EROSION BEFORE GRASS IS ESTABLISHED AND WILL PROMOTE FASTER AND EARLIER ESTABLISHMENT. THE EXISTENCE OF VEGETATION SUFFICIENT TO CONTROL SOIL EROSION SHALL BE DEEMED COMPLIANCE WITH THIS MULCHING REQUIREMENT.
- STRAW OR HAY. UNROTTED SMALL GRAIN STRAW, HAY FREE OF SEEDS, TO BE APPLIED AT THE RATE OF 1-1/2 TO 2 TONS PER ACRE (70 TO 90 POUNDS PER 1,000 SQUARE FEET), EXCEPT THAT WHERE A CRIMPER IS USED INSTEAD OF A LIQUID MULCH-BINDER (TACKIFYING OR ADHESIVE AGENT), THE RATE OF APPLICATION IS 3 TONS PER ACRE. MULCH CHOPPER-BLOWERS MUST NOT GRIND THE MULCH. HAY MULCH IS NOT RECOMMENDED FOR ESTABLISHING FINE TURF OR LAWNS DUE TO THE PRESENCE OF WEED SEED. APPLICATION - SPREAD MULCH UNIFORMLY BY HAND OR MECHANICALLY SO THAT AT LEAST 85% OF THE SOIL SURFACE IS COVERED. FOR UNIFORM DISTRIBUTION OF HAND-SPREAD MULCH, DIVIDE AREA INTO APPROXIMATELY 1,000 SQUARE FEET SECTIONS AND DISTRIBUTE 70 TO 90 POUNDS WITHIN EACH SECTION. ANCHORING SHALL BE ACCOMPLISHED IMMEDIATELY AFTER PLACEMENT TO MINIMIZE LOSS BY WIND OR WATER. THIS MAY BE DONE BY ONE OF THE FOLLOWING METHODS, DEPENDING UPON THE SIZE OF THE AREA, STEEPNESS OF SLOPES, AND COSTS.
- PEG AND TWINE. DRIVE 8 TO 10 INCH WOODEN PEGS TO WITHIN 2 TO 3 INCHES OF THE SOIL SURFACE EVERY 4 FEET IN ALL DIRECTIONS. STAKES MAY BE DRIVEN BEFORE OR AFTER APPLYING MULCH. SECURE MULCH TO SOIL SURFACE BY STRETCHING TWINE BETWEEN PEGS IN A CRISS-CROSS AND A SQUARE PATTERN. SECURE TWINE AROUND EACH PEG WITH TWO OR MORE ROUND TURNS.
- MULCH NETTINGS STAPLE PAPER, JUTE, COTTON, OR PLASTIC NETTINGS TO THE NETTING IN AREAS TO BE MOWED. SOIL SURFACE. USE A DEGRADABLE
- CRIMPER (MULCH ANCHORING COULTER TOOL) A TRACTOR-DRAWN IMPLEMENT, SOMEWHAT LIKE A DISC HARROW, ESPECIALLY DESIGNED TO PUSH OR CUT SOME OF THE BROADCAST LONG FIBER MULCH 3 TO 4 INCHES INTO THE SOIL SO AS TO ANCHOR IT AND LEAVE PART STANDING UPRIGHT. THIS TECHNIQUE IS LIMITED TO AREAS TRAVERSABLE BY A TRACTOR, WHICH MUST OPERATE ON THE CONTOUR OF SLOPES. STRAW MULCH RATE MUST BE 3 TONS PER ACRE. NO TACKIFYING OR ADHESIVE AGENT IS REQUIRED.
- $\widehat{\succeq}$ APPLICATIONS SHOULD BE HEAVIER AT EDGES WHERE WIND MAY CATCH THE MULCH, IN VALLEYS, AND AT CRESTS OF BANKS. THE REMAINDER OF THE AREA SHOULD BE UNIFORM IN APPEARANCE. - MAY BE USED TO ANCHOR SALT HAY, HAY OR STRAW MULCH.
- (B) USE ONE OF THE FOLLOWING:
- RGANIC AND VEGETABLE BASED BINDERS NATURALLY OCCURRING, POWDER BASED, HYDROPHILIC MATERIALS WHEN INXED WITH WATER FORMULATES A GEL AND WHEN APPLIED TO MULCH UNDER SATISFACTORY CURING CONDITIONS WILL ORM MEMBRANED NETWORKS OF INSOLUBLE POLYMERS. THE VEGETABLE GEL SHALL BE PHYSIOLOGICALLY HARMLESS AND OT RESULT IN A PHYTOTOXIC EFFECT OR IMPEDE GROWTH OF TURF GRASS. USE AT RATES AND WEATHER CONDITIONS IS RECOMMENDED BY THE MANUFACTURER TO ANCHOR MULCH MATERIALS. MANY NEW PRODUCTS ARE AVAILABLE, SOME WHICH MAY NEED FURTHER EVALUATION FOR USE IN THIS STATE.
- 2) SYNTHETIC BINDERS - HIGH POLYMER SYNTHETIC EMULSION, MISCIBLE WITH WATER WHEN DILUTED AND FOLLOWING APPLICATION TO MULCH, DRYING AND CURING SHALL NO LONGER BE SOLUBLE OR DISPERSIBLE IN WATER. IT SHALL APPLIED AT RATES RECOMMENDED BY THE MANUFACTURER AND REMAIN TACKY UNTIL GERMINATION OF GRASS. NOTE: ALL NAMES GIVEN ABOVE ARE REGISTERED TRADE NAMES. THIS DOES NOT CONSTITUTE THESE PRODUCTS TO THE EXCLUSION OF OTHER PRODUCTS. A RECOMMENDATION OF
- WOOD-FIBER OR PAPER-FIBER MULCH SHALL BE MADE FROM WOOD, PLANT FIBERS OR PAPER CONTAINING NO GROWTH OR GERMINATION INHIBITING MATERIALS, USED AT THE RATE OF 1,500 POUNDS PER ACRE (OR AS RECOMMENDED BY THE PRODUCT MANUFACTURER) AND MAY BE APPLIED BY A HYDROSEEDER. MULCH SHALL NOT BE MIXED IN THE TANK WITH SEED. USE IS LIMITED TO FLATTER SLOPES AND DURING OPTIMUM SEEDING PERIODS IN SPRING AND FALL.
- PELLETIZED MULCH COMPRESSED AND EXTRUDED PAPER AND/OR WOOD FIBER PRODUCT, WHICH MAY CONTAIN CO-POLYMERS, TACKIFIERS, FERTILIZERS AND COLORING AGENTS. THE DRY PELLETS, WHEN APPLIED TO A SEEDED AREA AND WATERED, FORM A MULCH MAT. PELLETIZED MULCH SHALL BE APPLIED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS. MULCH MAY BE APPLIED BY HAND OR MECHANICAL SPREADER AT THE RATE OF 60-75 LBS/1,000 SQUARE FEET AND ACTIVATED WITH 0.2 TO 0.4 INCHES OF WATER. THIS MATERIAL HAS BEEN FOUND TO BE BENEFICIAL FOR USE ON SMALL LAWN OR RENOVATION AREAS, SEEDED AREAS WHERE WEED-SEED FREE MULCH IS DESIRED OR ON SITES WHERE STRAW MULCH AND TACKIFIER AGENT ARE NOT PRACTICAL OR DESIRABLE. APPLYING THE FULL 0.2 TO 0.4 INCHES OF WATER AFTER SPREADING PELLETIZED MULCH ON THE SEED BED IS EXTREMELY IMPORTANT FOR SUFFICIENT ACTIVATION AND EXPANSION OF THE MULCH TO PROVIDE SOIL COVERAGE.
- SATION (WHERE FEASIBLE)
- IF SOIL MOISTURE IS DEFICIENT, AND MULCH IS NOT USED, SUPPLY NEW SEEDING WITH ADEQUATE WATER (A MINIMUM 1/4 INCH APPLIED UP TO TWICE A DAY UNTIL VEGETATION IS WELL ESTABLISHED). THIS IS ESPECIALLY TRUE WHEN SEEDINGS ARE MADE IN ABNORMALLY DRY OR HOT WEATHER OR ON DROUGHTY SITES.
- SINCE SOIL ORGANIC MATTER CONTENT AND SLOW RELEASE NITROGEN FERTILIZER (WATER INSOLUBLE) ARE PRESCRIBED IN SECTION 2A SEEDBED PREPARATION IN THIS STANDARD, NO FOLLOW-UP OF TOPDRESSING IS MANDATORY. AN EXCEPTION MAY BE MADE WHERE GROSS NITROGEN DEFICIENCY EXISTS IN THE SOIL TO THE EXTENT THAT TURF FAILURE MAY DEVELOP. IN THAT INSTANCE, TOPDRESS WITH 10-10-10 OR EQUIVALENT AT 300 POUNDS PER ACRE OR 7 POUNDS PER 1,000 SQUARE FEET EVERY 3 TO 5 WEEKS UNTIL THE GROSS NITROGEN DEFICIENCY IN THE TURF IS AMELIORATED.
- THE QUALITY OF PERMANENT VEGETATION RESTS WITH THE CONTRACTOR. THE TIMING OF SEEDING, PREPARING THE SEEDBED, APPLYING NUTRIENTS, MULCH AND OTHER MANAGEMENT ARE ESSENTIAL. THE SEED APPLICATION RATES IN TABLE 4—3 ARE REQUIRED WHEN A REPORT OF COMPLIANCE IS REQUESTED PRIOR TO ACTUAL ESTABLISHMENT OF PERMANENT VEGETATION. UP TO 50% REDUCTION IN APPLICATION RATES MAY BE USED WHEN PERMANENT VEGETATION IS ESTABLISHED PRIOR TO REQUESTING A REPORT OF COMPLIANCE FROM THE DISTRICT. THESE RATES APPLY TO ALL METHODS OF SEEDING. ESTABLISHING PERMANENT VEGETATION MEANS 80% VEGETATIVE COVER (OF THE SEEDED SPECIES) AND MOWED ONCE. NOTE THIS DESIGNATION OF MOWED ONCE DOES NOT GUARANTEE THE PERMANENCY OF THE TURF SHOULD OTHER MAINTENANCE FACTORS BE NEGLECTED OR OTHERWISE MISMANAGED.

Permanent	Table 4-2 Stabilization Mixtu	Table 4-2 Permanent Stabilization Mixtures for Various Uses	•
	PLANTING M	PLANTING MIXTURES BY SOIL DRAINAGE CLASS (1) (SEE TABLE 4-3)	AINAGE CLASS (1)
APPLICATION	EXCESSIVELY DRAINED	WELL TO MODERATELY WELL DRAINED	SOMEWHAT POORLY POORLY DRAINED
RESIDENTIAL/COMMERCIAL LOTS	10, 12, 15	6, 10, 12, 13, 14, 15	16
POND AND CHANNEL BANKS, DIKES, BERMS AND DAMS	2, 5, 6, 10	5, 6, 7, 8, 9, 15	2, 8, 16, 17
DRAINAGE DITCHES, SWALES, DETENTION BASINS	2, 9, 11	2, 7, 9, 11, 12, 17	2, 9, 16, 17
FILTER STRIPS	12	11, 12	11, 12
GRASSES WATERWAY, SPILLWAYS	2, 3, 9, 10, 12	6, 7, 9, 10, 11, 12	2, 9, 11, 12
RECREATION AREAS, ATHLETIC FIELDS	5, 12, 15, 18	12, 13, 14, 15, 18	16
SPECIAL PROBLEM SITES,STEEP SLOPES AND BANKS, ROADSIDES, BORROW AREAS	2, 3, 4, 6	2, 3, 5, 7, 8, 9, 10, 15, 18	2, 9, 10, 11, 12
SAND AND GRAVEL PITS, SANITARY LANDFILLS	1, 2, 3, 4, 6, 20	1, 2, 3, 4, 5, 6, 8, 15, 20	2, 8
DREDGED MATERIAL, SPOILBANKS, BORROW AREAS	2, 3, 6, 20	2, 3, 6, 11	2, 8
STREAMBANKS & SHORELINES (2)	2 8 20 212	2 8 105 20 212 215	2 8 102 212 b 2

1. REFER TO SOIL SURVEYS FOR DRAINAGE CLASS DESCRIPTIONS. 2. REFER TO SOIL BIOENGINEERING STANDARD FOR ADDITIONAL SEED MIXTU 3. SPILLWAYS ONLY. 4. SEE APPENDIX E FOR DESCRIPTION OF TURF GRASSES AND CULTIVARS. TEMPORARY VEGETATIVE COVER FOR SOIL STABILIZATION: _ SEED MIXTURES

- INSTALL NEEDED EROSION CONTROL PRACTICES OR FACILITIES SUCH AS DIVERSIONS, GRADE STABILIZATION STRUCTURES, CHANNEL STABILIZATION MEASURES, SEDIMENT BASINS, AND WATERWAYS. SEE STANDARDS 11 THROUGH 42. CONVENTIONAL EQUIPMENT FOR SEEDBED PREPARATION, DE DONE IN ACCORDANCE WITH THE STANDARDS FOR GRADING, PG 19-1.
- IMMEDIATELY PRIOR TO SEEDING, THE SURFACE SHOULD BE PRACTICE IS PERMISSIBLE ONLY WHERE THERE IS NO DANGE SEEDBED PREPARATION
- œ APPLY GROUND LIMESTONE AND FERTILIZER ACCORDING TO SCIO-OPERATIVE EXTENSION. SOIL SAMPLE MAILERS ARE AVAILED-OPERATIVE EXTENSION. SOIL SAMPLE MAILERS ARE AVAILED AT THE RATE OF 500 POUND EQUIVALENT WITH 50% WATER INSOLUBLE NITROGEN UNLESS VIA SOIL TESTING. CALCIUM CARBONATE IS THE EQUIVALENT NEUTRALIZE SOIL ACIDITY AND SUPPLY CALCIUM AND MAGNE
- INSPECT SEEDBED JUST BEFORE SEEDING. IF TRAFFIC HAS LEFT THE SOIL COMPACTED, THE AREA MUST BE RETILLED IN ACCORDANCE WITH THE ABOVE. WORK LIME AND FERTILIZER INTO THE SOIL AS NEARLY AS FOR OTHER SUITABLE EQUIPMENT. THE FINAL HARROWING OR TILLAGE UNTIL A REASONABLE UNIFORM SEEDBED IS PREPARTICLE. RACTICAL TO A DEPTH OF 4 INCHES WITH A DISC, SPRINGTOOTH HARROW DISKING OPERATION SHOULD BE ON THE GENERAL CONTOUR. CONTINUE SED.
- SOILS HIGH IN SULFIDES OR HAVING A PH OF 4 OR LESS REFER TO STANDARD FOR MANAGEMENT OF HIGH ACID PRODUCING SOILS.

SELECT SEED FROM RECOMMENDATIONS IN TABLE 7–2 BELOW. TABLE 7–2 TEMPORARY VEGETATIVE STABILIZATION GRASSES. TEMPORARY VEGETATIVE STABILIZATION

		SEEDINI (pou	SEEDING RATE ^(†) (pounds)	OPTIMUN Based c	OPTIMUM SEEDING DATE (2) Based on Plant Hordiness Zone ⁽³⁾	(2) ss Zone ⁽³⁾
	SEED SELECTIONS	Per Acre	Per 1000 Sq. Ft.	ZONE 5b, 6s	ZONE 6b	ZONE 7a, b
COOL S	COOL SEASON GRASSES	•	10	3/15-6/1	3/1-5/15	2/15-5
	 Perennial ryegrass 	100	1.0	3/15-6/1 8/1-9/15	3/1-5/15 8/15-10/1	2/15-5/1 8/15-10/15
	2. Spring oats	86	2.0	3/15-6/1 8/1-9/15	3/1-5/15 8/15-10/1	2/15-5/1 8/15-10/15
بب	Winter Barley	96	2.2	8/1-9/15	8/15-10/1	8/15-10/15
4.	4. Annual ryegrass	100	1.0	3/15-6/1 8/1-9/15	3/15-6/1 8/1-9/15	2/15-5/1 8/15-10/15
<u>,</u> 5	Winter Cereal Rye	112	2.8	8/1 - 11/1	8/1 - 11/15 8/1 - 12/15	8/1 - 12
WARM S	WARM SEASON GRASSES 6. Pearl millet	20	0.5	6/1-8/1	5/18-8/15	5/1-9/1
7.	7. Millet (German or Hungarian)	30	0.7	6/1-8/1	5/15-8/15 5/1-9/1	5/1-9/1

- 1 SEEDING RATE FOR WARM SEASON GRASS, SELECTIONS 5 7 SHALL BE ADJUSTED TO REFLECT THE AMOUNT OF PURE LIVE SEED (PLS) AS DETERMINED BY A GERMINATION TEST RESULT. NO ADJUSTMENT IS REQUIRED FOR COOL SEASON GRASSES.
 2 MAY BE PLANTED THROUGHOUT SUMMER IF SOIL MOISTURE IS ADEQUATE OR SEEDED AREA CAN BE IRRIGATED.
 3 PLANT HARDINESS ZONE
 4 TWICE THE DEPTH FOR SANDY SOILS
- CYCLONE (CENTRIFUGAL) SEEDER, DROP SEEDER, DRILL OR CULTIPACKER ED SEEDINGS, SEED SHALL BE INCORPORATED INTO THE SOIL, TO A DEPTH SEED PLACEMENT MAY BE 1/4 INCH DEEPER ON COARSE TEXTURED SOIL.
- HYDROSEEDING IS A BROADCAST SEEDING METHOD USUALLY INVOLVING A TRUCK OR TRAILER MOUNTED TANK, WITH AN AGITATION SYSTEM AND HYDRAULIC PUMP FOR MIXING SEED, WATER AND FERTILIZER AND SPRAYING THE MIX ONTO THE PREPARED SEEDBED. MULCH SHALL NOT BE INCLUDED IN THE TANK WITH SEED. SHORT FIBERED MULCH MAY BE APPLIED WITH A HYDROSEEDER FOLLOWING SEEDING. (ALSO SEE SECTION4-MULCHING). HYDROSEEDING IS NOT A PREFERRED SEEDING METHOD BECAUSE SEED AND FERTILIZER ARP APPLIED TO THE SURFACE AND NOT INCORPORATED INTO THE SOIL BECAUSE POOR SEED TO SOIL CONTACT REDUCES SEED GERMINATION AND GROWTH.
- AFTER SEEDING, FIRMING THE SOIL WITH A CORRUGATED ROLLER WILL ASSURE GOOD SEED—TO—SOIL CONTACT, RESTORE CAPILLARITY, AND IMPROVE SEEDLING EMERGENCE. THIS IS THE PREFERRED METHOD. WHEN PERFORMED ON THE CONTOUR, SHEET EROSION WILL BE MAXIMIZED AND WATER CONSERVATION ON SITE WILL BE MAXIMIZED. MULCHING IS REQUIRED ON ALL SEEDING. MULCH WILL INSURE AGAINST EROSION BEFORE GRASS IS ESTABLISHED AND WILL PROMOTE FASTER AND EARLIER ESTABLISHMENT. THE EXISTENCE OF VEGETATION SUFFICIENT TO CONTROL SOIL EROSION SHALL BE DEEMED COMPLIANCE WITH THIS MULCHING REQUIREMENT.
- (1) PEG AND TWINE. DRIVE 8 TO 10 INCH WOODEN PEGS TO DIRECTIONS. STAKES MAY BE DRIVEN BEFORE OR AFTER TWINE BETWEEN PEGS IN A CRIS-CROSS AND A SQUARE TURNS. ANCHORING SHALL BE ACCOMPLISHED IMMEDIATELY AFTER PLACEMENT TO MINIMIZE LOSS BY WIND OR WATER. THIS MAY BE DONE BY ONE OF THE FOLLOWING METHODS, DEPENDING UPON THE SIZE OF THE AREA, STEEPNESS OF SLOPES, AND COSTS. APPLICATION: SPREAD MULCH UNIFORMLY BY HAND OR MECHANICALLY SO THAT APPROXIMATELY 95% OF THE SOIL SURFACE WILL BE COVERED. FOR UNIFORM DISTRIBUTION OF HAND-SPREAD MULCH, DIVIDE AREA INTO APPROXIMATELY 1,000 SQUARE FEET SECTIONS AND DISTRIBUTE 70 TO 90 POUNDS WITHIN EACH SECTION. STRAW OR HAY, UNROTTED SMALL GRAIN STRAW, HAY FREE OF SEEDS, APPLIED AT THE RATE OF 1-1/2 TO 2 TONS PER ACRE (70 TO 90 POUNDS PER 1,000 SQUARE FEET), EXCEPT THAT WHERE A CRIMPER IS USED INSTEAD OF A LIQUID MULCH-BINDER (TACKIFYING OR ADHESIVE AGENT), THE RATE OF APPLICATION IS 3 TONS PER ACRE. MULCH CHOPPER-BLOWERS MUST NOT GRIND THE MULCH. HAY MULCH IS NOT RECOMMENDED FOR ESTABLISHING FINE TURF OR LAWNS DUE TO THE PRESENCE OF WEED SEED. WITHIN 2 TO 3 INCHES OF THE SOIL SURFACE EVERY 4 FEET IN ALL APPLYING MULCH. SECURE MULCH TO SOIL SURFACE BY STRETCHING PATTERN. SECURE TWINE AROUND EACH PEG WITH TWO OR MORE ROUND
- (3) CRIMPER (MULCH ANCHORING COULTER DESIGNED TO PUSH OR CUT SOME OF AND LEAVE PART STANDING UPRIGHT. ON THE CONTOUR OF SLOPES. STRAW I REQUIRED. (2) MULCH NETTINGS, STAPLE PAPER, JUTE, COTTON, OR PLAREAS TO BE MOWED. TOOL). A TRACTOR-DRAWN IMPLEMENT, SOMEWHAT LIKE A DISC HARROW, ESPECIALLY THE BROADCAST LONG FIBER MULCH 3 TO 4 INCHES INTO THE SOIL SO AS TO ANCHOR IT THIS TECHNIQUE IS LIMITED TO AREAS TRAVERSABLE BY A TRACTOR, WHICH MUST OPERATE MULCH RATE MUST BE 3 TONS PER ACRE. NO TACKIFYING OR ADHESIVE AGENT IS

ASTIC NETTINGS TO THE SOIL SURFACE. USE DEGRADABLE NETTING IN

(B) USE ONE OF THE FOLLOWING: (A) APPLICATIONS SHOULD BE HEAVIER AT EDGES WHERE THE REMAINDER OF THE AREA SHOULD BE UNIFORM TO ANCHOR H. WIND MAY CATCH I APPEARANCE. CRESTS OF BANKS

 \exists

ORGANIC AND VEGETABLE BASED BINDERS — NATURALLY WATER FORMULATES A GEL AND WHEN APPLIED TO MULC NETWORKS OF INSOLUBLE POLYMERS. THE VEGETABLE GE PHYTOTOXIC EFFECT OR IMPEDE GROWTH OF TURFGRASS. MANUFACTURER TO ANCHOR MULCH MATERIALS. MANY NEVALUATION FOR USE IN THIS STATE.

MIXED WITH

- (2) SYNTHETIC BINDERS HIGH POLYMER SYNTHETIC EMULSION, MISCIBLE WITH WATER WHEN DILUTED AND FOLLOWING APPLICATION TO MULCH, DRYING AND CURING SHALL NO LONGER BE SOLUBLE OR DISPERSIBLE IN WATER. IT SHALL BE APPLIED AT RATES RECOMMENDED BY THE MANUFACTURER AND REMAIN TACKY UNTIL GERMINATION OF GRASS. NOTE: ALL NAMES GIVEN ABOVE ARE REGISTERED TRADE NAMES. THIS DOES NOT CONSTITUTE A COMMENDATIONS PRODUCTS TO THE EXCLUSION OF OTHER PRODUCTS.
- WOOD-FIBER OR PAPER-FIBER MULCH. SHALL BE MADE FROM WOOD, PLANT FIBERS OR PAPER CONTAINING NO GROWTH OR GERMINATION INHIBITING MATERIALS, USED AT THE RATE OF 1,500 POUNDS PER ACRE (OR AS RECOMMENDED BY THE PRODUCT MANUFACTURER) AND MAPPLIED BY A HYDROSEEDER. THIS MULCH SHALL NOT BE MIXED IN THE TANK WITH SEED. USE IS LIMITED TO FLATTER SLOPES AND DURIN OPTIMUM SEEDING PERIODS IN SPRING AND FALL.

T0

- APPLYING THE FULL 0.2 TO 0.4 INCHES OF WATER AFTER SPREADING PELLETIZED MULCH ON THE SEED BED IS EXTREMELY IMPORTANT FOF SUFFICIENT ACTIVATION AND EXPANSION OF THE MULCH TO PROVIDE SOIL COVERAGE.

		<u> </u>				· <u> </u>	l	
Hard fescue and/or Chewing fescue and/or Strong creeping red fescue Perennial ryegrass Ky, bluegrass (blend)	COOL SEASON SEED MIXTURES					SEED MIXTURB)	PERMANENT VEGETATIVE MIXTURES, PLANTINGS RATES AND PLANTINGS DATES	
175 45 45		lbs/acre sq. ft. 5/31 7/31 10/1		KA /	PLANTING		ETATIV	
4.0 1.0 1.0		165/1000 sq. ft.		£ (3)	ING.		'E MIX	
>		3/15- 5/31	Z		0=0¢		TURES	
A		6/1 <u>-</u> 7/31	Zone 5b, 6a		0=0ptimal Planting period		, PLAN	
A		8/1-	50	PLA	Planting		ITINGS	2
0		3/1- 4/30		NT H	period	PLAN1	RATE	1000
A ⁵ A		2/1 ₋	Zone 6b	ARDINI		PLANTING DATES	S AND	(
0		3/1- 5/1- 8/15- 2/1- 4/30 8/14 10/15 4/30		PLANT HARDINESS ZONES	A=Acceptable Planting period	ATES	PLAN	
		2/1- 4/30	12	ZONES	ble Pla		TINGS	
_ს		5/1- 8/14 10/30	Zone 7a, 7b		nting p		DATE	
		8/15-	7 _b		eriod		ီ	
A-C		M. LE	AIN T VEL	TENA (4)	NCE	=		
General lawn/recreation.				REMARKS			(3)	

TO IMPROVE THE SOIL MEDIUM FOR PLANT ESTABLISHMENT AND MAINTENANCE

B. TOPSOIL SUBSTITUTE IS A SOIL MATERIAL WHICH MAY HAVE BEEN AMENDED WITH SAND, SILT, CLAY, ORGANIC MATTER, FERTILIZER OF LIME AND HAS THE APPEARANCE OF TOPSOIL. TOPSOIL SUBSTITUTES MAY BE UTILIZED ON SITES WITH INSUFFICIENT TOPSOIL FOR ESTABLISHING PERMANENT VEGETATION. ALL TOPSOIL SUBSTITUTE MATERIALS SHALL MEET THE REQUIREMENTS OF TOPSOIL NOTED ABOVE. SOIL TESTS SHALL BE PERFORMED TO DETERMINE THE COMPONENTS OF SAND, SILT, CLAY, ORGANIC MATTER, SOLUBLE SALTS AND PHLEVEL. A. TOPSOIL SHOULD BE FRIABLE1, LOAMY2, FREE OF DEBRIS, OBJECTIONABLE WEEDS AND STONES, AND CONTAIN NO TOXIC SUBSTANCE OR ADVERSE CHEMICAL OR PHYSICAL CONDITION THAT MAY BE HARMFUL TO PLANT GROWTH. SOLUBLE SALTS SHOULD NOT BE EXCESSIVE (CONDUCTIVITY LESS THAN 0.5 MILLIMHOS PER CENTIMETER. MORE THAN 0.5 MILLIMHOS MAY DESICCATE SEEDLINGS AND ADVERSELY IMPACT GROWTH). IMPORTED TOPSOIL SHALL HAVE A MINIMUM ORGANIC MATTER CONTENT OF 2.75 PERCENT. ORGANIC MATTER CONTENT MAY BE RAISED BY ADDITIVES.

FIELD EXPLORATION SHOULD BE MADE TO DETERMINE WHETHER QUANTITY AND OR QUALITY OF SURFACE SOIL STRIPPING SHALL BE CONFINED TO THE IMMEDIATE CONSTRUCTION AREA. THE SOIL PH

F. STOCKPILES SHOULD BE VEGETATED IN ACCORDANCE WITH STANDARDS PREVIOUSLY DESCRIBED HEREIN; SEE STANDARDS FOR PERMANENT (PG. 4-1) OR TEMPORARY (PG.7-1) VEGETATIVE COVER FOR SOIL STABILIZATION. WEEDS SHOULD NOT BE ALLOWED TO GROVON STOCKPILES. D. A 4-6 INCH STRIPPING DEPTH IS COMMON, BUT MAY VARY DEPENDING ON THE PARTICULAR SOIL.

E. STOCKPILES OF TOPSOIL SHOULD BE SITUATED SO AS NOT TO OBSTRUCT NATURAL DRAINAGE OR CAUSE OFF-SITE ENVIRONMENTAL DAMAGE.

A. GRADE AT THE ONSET OF THE OPTIMAL SEEDING PERIOD SO AS TO MINIMIZE THE DURATION AND AREA OF EXPOSURE OF DISTURBED SOIL TO EROSION. IMMEDIATELY PROCEED TO ESTABLISH VEGETATIVE COVER IN ACCORDANCE WITH THE SPECIFIED SEED MIXTURE. TIME IS OF THE ESSENCE

C. PURSUANT TO THE REQUIREMENTS IN SECTION 7 OF THE STANDARD FOR PERMANENT VEGETATIVE STABILIZATION, THE CONTRACTOR IS RESPONSIBLE TO ENSURE THAT PERMANENT VEGETATIVE COVER BECOMES ESTABLISHED ON AT LEAST 80% OF THE SOILS TO BE STABILIZED WITH VEGETATION. FAILURE TO ACHIEVE THE MINIMUM COVERAGE MAY REQUIRE ADDITIONAL WORK TO BE PERFORMED BY THE CONTRACTOR TO INCLUDE SOME OR ALL OF THE FOLLOWING: SUPPLEMENTAL SEEDING, RE-APPLICATION OF LIME AND FERTILIZERS, AND/OR THE ADDITION OF ORGANIC MATTER (I.E. COMPOST) AS A TOP DRESSING. SUCH ADDITIONAL MEASURES SHALL BE BASED ON SOIL TESTS SUCH AS THOSE OFFERED BY RUTGERS COOPERATIVE EXTENSION SERVICE OR OTHER APPROVED LABORATORY FACILITIES QUALIFIED TO TEST SOIL SAMPLES FOR AGRONOMIC PROPERTIES.

- SEEDING MIXTURES AND/OR RATES NOT LISTED ABOVE MAY BE USED IF RECOMMENDED BY THE LOCAL SOIL CONSERVATION DISTRICT, NATURAL RESOURCES CONSERVATION SERVICE; RECOMMENDATIONS OF RUTGERS COOPERATIVE EXTENSION MAY BE USED IF APPROVED BY THE SOIL CONSERVATION DISTRICT. LEGUMES (WHITE CLOVER, FLATPEA, LESPEDEZA) SHOULD BE MIXED WITH PROPER INNOCULANT PRIOR TO PLANTING.
- A: INTENSIVE MOWING, (2-4 DAYS), FERTILIZATION, LIME, PEST CONTROL COMMERCIAL AND RECREATION AREAS, PUBLIC FACILITIES). FREQUENT MOWING, (4-7 DAYS), OCCASIONAL FERTILIZATION, LIME AND WEED CONTROL (EXAMPLES HOOL SITES). PERIODIC MOWING (7-14 DAYS), OCCASIONAL FERTILIZATION AND LIME (EXAMPLES - HOME LAWNS, PARKS). AND IRRIGATION (EXAMPLES SITES,
- IC MATERIALS WHEN MIXED WITH ONS WILL FORM MEMBRANED AND NOT RESULT IN A US AS RECOMMENDED BY THE WHICH MAY NEED FURTHER SUMMER SEEDINGS SHOULD ONLY BE CONDUCTED WHEN SITE IS IRRIGATED. MIXES INCLUDING WHITE CLOVER REQ WEEKS OF GROWING SEASON REMAIN AFTER SEEDING TO ENSURE ESTABLISHMENT BEFORE FREEZING CONDITIONS. PLANT HARDINESS ZONE — PROPERTY IN QUESTION IS WITHIN ZONE 6B.

- PELLETIZED MULCH. COMPRESSED AND EXTRUDED PAPER AND/OR WOOD FIBER PRODUCT, WHICH MAY CONTAIN CO-POLYMERS, TACKIFIERS, FERTILIZERS AND COLORING AGENTS. THE DRY PELLETIS, WHEN APPLIED TO A SEEDED AREA AND WATERED, FORM A MULCH MAT. PELLETIZED MULCH SHALL BE APPLIED IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS. MULCH MAY BE APPLIED BY HAND OR MECHANICAL SPREADER AT THE RATE OF 60-75 LBS/1,000 SQUARE FEET AND ACTIVATED WITH 0.2 TO 0.4 INCHES OF WATER. THIS MATERIAL HAS BEEN FOUND TO BE BENEFICIAL FOR USE ON SMALL LAWN OR RENOVATION AREAS, SEEDED AREAS WHERE WEED-SEED FREE MULCH IS DESIRED OR ON SITES WHERE STRAW MULCH AND TACKIFIER AGENT ARE NOT PRACTICAL OR DESIRABLE.

PERMANENT VEGETATIVE MIXTURES, PLANTINGS RATES AND PLANTINGS DATES	ETATIVE MIX	TURES	, PLAN	ITINGS	RATE	SAND	PLAN	TINGS	DATE	S		(3)
SEED MIXTIES					PLAN	PLANTING DATES)ATES				•	
	PLANTING		timal I	Planting	perioc	/ A=,	O=Optimal Planting period A=Acceptable Planting period	ble Pla	nting p		NCE	
	RATE (3)			PLA	NT h	IARDIN	PLANT HARDINESS ZONES	ZONES			ENA (4)	REMARKS
		7.0	Zone 5b, 6a	60		Zone 6b		7.	Zone 7a, 7b		VEL	
<i>1</i>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 3/15- 5/31	6/1- 7/31	8/1- -1/8	3/1- 4/30	5/1- 8/14	8/15- 10/15	2/1- 4/30	5/1- 8/14 8/15- 10/30	8/15- 10/30	M. LE	
COOL SEASON SEED MIXTURES												
Hard fescue and/or Chewing fescue and/or	175 4.0		ħ			ħ			n n		A-C	General
Strong creeping red fescue Perennial ryegrass Ky, bluegrass (blend)	45 1.0 1.0	>	Ö	A A	0	A	0		Ú			lawn/recreation.

STANDARD NOTES FOR TOPSOILING:

ING ENTAILS THE DISTRIBUTION OF SUITABLE QUALITY SOIL

WATER QUALITY ENHANCEMENT:

TOPSOIL SHALL BE USED WHERE SOILS ARE TO BE DISTURBED AND WILL BE REVEGETATED

METHODS AND MATERIALS

PING AND STOCKPILING

C. WHERE FEASIBLE, LIME MAY BE APPLIED BEFORE STRIPPING APPROXIMATELY 6.5. AT A RATE DETERMINED BY SOIL TESTS TO

E. EMPLOY NEEDED EROSION CONTROL PRACTICES SUCH AS DIVERSIONS, GRADE STABILIZATION STRUCTUMEASURES, SEDIMENTATION BASINS, AND WATERWAYS. SEE STANDARDS 11 THROUGH 42. C. AS GUIDANCE FOR IDEAL CONDITIONS, SUBSOIL SHOULD BE TESTED FOR LIME REQUIREMENT. LIMESTONE, IF NEEDED, SHOULD BE APPLIED TO BRING SOIL TO A PH OF APPROXIMATELY 6.5 AND INCORPORATED INTO THE SOIL AS NEARLY AS PRACTICAL TO A DEPTH OF 4 INCHES. B. GRADE AS NEEDED AND FEASIBLE TO PERMIT THE USE OF CONVENTIONAL EQUIPMENT FOR SEEDBED PREPARATION, SEEDING, MULCH APPLICATION AND ANCHORING, AND MAINTENANCE. SEE THE STANDARD FOR LAND GRADING, PG. 19—1. OR TO TOPSOILING, THE SUBSOIL SHALL BE IN COMPLIANCE WITH THE STANDARD FOR LAND GRADING, P.G.

B. A UNIFORM APPLICATION TO AN AVERAGE DEPTH OF 5.0 INCHES, MINIMUM OF 4 INCHES, FIRMED IN PLACE IS REQUIRED. ALTERNATIVE DEPTHS MAY BE CONSIDERED WHERE SPECIAL REGULATORY AND/OR INDUSTRY DESIGN STANDARDS ARE APPROPRIATE SUCH AS ON GOLF COURSES, SPORTS FIELDS, LANDFILL CAPPING, ETC.. SOILS WITH A PH OF 4.0 OR LESS OR CONTAINING IRON SULFIDE SHALL BE COVERED WITH A MINIMUM DEPTH OF 12 INCHES OF SOIL HAVING A PH OF 5.0 OR MORE, IN ACCORDANCE WITH THE STANDARD FOR MANAGEMENT OF HIGH ACID PRODUCING SOIL (PG. 1-1). A. TOPSOIL SHOULD BE HANDLED ONLY WHEN IT IS DRY ENOUGH TO WORK WITHOUT DAMAGING SOIL STRUCTURE; I.E., LESS THAN FIELD CAPACITY (SEE GLOSSARY).

FOOTNOTES:

- SEE APPENDIX B OF THE STANDARDS FOR SOIL EROSION AND SEDIMENT CONTROL IN NEW JERSEY FOR DESCRIPTIONS OF TURF GRASS MIXTURES AND CULIVARS. THE ACTUAL AMOUNT OF WARM SEASON GRASS MIXTURE USED IN TABLE 3 (SEED MIX 1-7) SHALL BE ADJUSTED TO REFLECT THE AMOUNT OF PURE LIVE SEED (PLS) AS DETERMINED BY GERMINATION TESTING RESULTS. NO ADJUSTMENT IS REQUIRED FOR COOL SEASON GRASSES (SEED MIXTURES 8-20).
- SEEDING RATES SPECIFIED ARE REQUIRED WHEN A REPORT OF COMPLIANCE IS REQUESTED PRIOR TO ACTUAL ESTABLISHMENT OF PERMANENT VEGETATION. UP TO 50% REDUCTION IN RATES MAY BE USED WHEN PERMANENT VEGETATION IS ESTABLISHED PRIOR TO REPORT OF COMPLIANCE INSPECTION. THESE RATES APPLY TO ALL METHODS OF SEEDING. ESTABLISHING PERMANENT VEGETATION ME/% VEGETATIVE COVERAGE OF THE SEEDED AREA AND MOWED ONCE. GRASS SEED MIXTURE CHECKED BY THE STATE SEED ANALYST, N JERSEY DEPARTMENT OF AGRICULTURE, TRENTON, NEW JERSEY, WILL ASSURE THE PURCHASER THAT THE MIXTURE OBTAINED IS THE N ORDERED, PURSUANT TO THE N.J. STATE SEED LAW, N.J.S.A. 4:8-17.13 ET. SEQ.

- INFREQUENT OR NO MOWING, FERTILIZATION AND LIME THE FIRST YEAR OF ESTABLISHMENT (EXAMPLES BLIC OPEN SPACES). AREAS,

AND SEDIMENT CONTROL NOTES:

1. ALL SOIL EROSION AND SEDMENT CONTROL PRACTICES SHALL DE INSTALLED PRIOR TO ANY MAJOR SOIL DISTURBANCES, OR IN THEIR PROPER
2 SOLVENEY AND INSTALLAND MAINTAINED WINL PERMANENT PROTECTION IS ESTABLISHED.
2 ANY DISTURBED AREAS THAT WILL BE LEFT EXPOSED MORE HAN SO JON'S AND NOT SUBJECT TO CONSTRUCTION TRAFFIC, WILL IMMEDIATELY
2 RECEIVE A TEMPORARY SEEDING. IF THE EXPOSED MORE HAN SO JON'S AND NOT SUBJECT TO CONSTRUCTION TRAFFIC, WILL IMMEDIATELY
3 FERMANENT VICETATION SHALL BE SEEDED OR SOIDED ON ALL EXPOSED MARE. ACCROSONIC ON A STATE STANDARDS.
3 FERMANENT VICETATION SHALL BE SEEDED OR SOIDED ON ALL EXPOSED MARE. ACCROSONIC ON A STATE STANDARD.
4 MAIN WARK SHALL BE SEEDED OR SOIDED ON ALL EXPOSED MARE. ACCROSONIC ON A STATE STANDARD.
5 AS USED AND SOID FOR ACCROSONIC ON A STATE STANDARD STATE STANDARD.
6 MANEDIATELY FOLLOWING MINITAL DISTURBANCE OR ROUGH GRADING ALL EXTREME HAN A STATE SUB-BASE COMES WILL BE APPLIED MADE STANDARD.
7 ANY STEED SLOPES RECEIVE A TEMPORARY SEEDING IN COMBINATION WITH STRAW MULLOW OR A SUTABLE COUNTRUIT. A RATE OF TWO (2) TON'S EPR ACRE, ACCROSONIC ON THE MASS THAT STANDARDS.
7 ANY STEED SLOPES RECEIVED AND EXPLAINED MEDIA TO THE MASS THAT STANDARDS.
8 MANEDIATELY FOLLOWING MINITAL DISTURBANCE FOR ROUGH GRADING AND STANDARD STANDARD.
9 THE SUBJECT AND STANDARD STANDARD.
10 THE SUBJECT AND STANDARD STANDARD.
11 THAT MASS THE SUBJECT AND STANDARD STANDARD.
12 THE SUBJECT AND STANDARD STAND

STABILIZATION WITH MULCH ONLY:

. GRADE AS NEEDED AND FEASIBLE TO PERMIT THE USE OF CONVENTIONAL EQUIPMENT FOR SEEDBED PREPARATION, SEEDING, MULCH APPLICATION, AND MULCH ANCHORING. ALL GRADING SHOULD BE DONE IN ACCORDANCE WITH THE STANDARDS FOR SOIL EROSION & SEDIMENT CONTROL FOR LAND GRADING. INSTALL NEEDED EROSION CONTROL PRACTICES OR FACILITIES SUCH AS DIVERSIONS, GRADE STABILIZATION STRUCTURES, CHANNEL STABILIZATION MEASURES, SEDIMENT BASINS, AND WATERWAYS. SEE STANDARDS 11 THROUGH 42 OF STANDARDS FOR SOIL EROSION AND SEDIMENT CONTROL IN NEW JERSEY.

C. SYNTHETIC OR ORGANIC SOIL STABILIZERS MAY BE USED UNDER SUITABLE CONDITIONS AND IN QUANTITIES AS RECOMMENDED BY THE MANUFACTURER. . ASPHALT EMULSION IS RECOMMENDED AT THE RATE OF 600 TO 1,200 GALLONS PER ACRE. THIS IS SUITABLE FOR A LIMITED PERIOD OF TIME WHERE TRAVEL BY PEOPLE, ANIMALS, OR MACHINES IS NOT A PROBLEM. UNROTTED SMALL-GRAIN STRAW AT 2.0 TO 2.5 TONS PER ACRE IS SPREAD UNIFORMLY AT 90 TO 115 POUNDS PER 1,000 SQUARE FEET AND ANCHORED WITH A MULCH ANCHORING TOOL, LIQUID MULCH BINDERS, OR NETTING TIE DOWN. OTHER SUITABLE MATERIALS MAY BE USED IF APPROVED BY THE SOIL CONSERVATION DISTRICT. THE APPROVED RATES ABOVE HAVE BEEN MET WHEN THE MULCH COVERS THE GROUND COMPLETELY UPON VISUAL INSPECTION, I.E. THE SOIL CANNOT BE SEEN BELOW THE MULCH.

E. MULCH NETTING, SUCH AS PAPER JUTE, EXCELSIOR, COTTON, OR PLASTIC, MAY BE USED. F. WOOD CHIPS APPLIED UNIFORMLY TO A MINIMUM DEPTH OF 2 INCHES MAY BE USED. WOOD CHIPS WILL NOT BE USED ON AREAS WHER FLOWING WATER COULD WASH THEM INTO AN INLET AND PLUG IT. . WOOD-FIBER OR PAPER-FIBER MULCH AT THE RATE OF 1,500 POUNDS PER ACRE (OR ACCORDING TO THE MANUFACTURER'S REQUIREMENTS) MAY BE APPLIED BY A HYDROSEEDER. GRAVEL, CRUSHED STONE, OR SLAG AT THE RATE OF 9 CUBIC YARDS PER 1,000 SQ. FT. APPLIED UNIFORMLY TO A MINIMUM DEPTH OF 3 INCHES MAY BE USED. SIZE 2 OR 3 (ASTM C-33) IS RECOMMENDED.

A. PEG AND TWINE - DRIVE 8 TO 10 INCH WOODEN PEGS TO WITHIN 2 TO 3 INCHES OF THE SOIL SURFACE EVERY 4 FEET IN ALL DIRECTIONS. STAKES MAY BE DRIVEN BEFORE OR AFTER APPLYING MULCH. SECURE MULCH TO SOIL SURFACE BY STRETCHING TWINE BETWEEN PEGS IN A CRIS-CROSS AND A SQUARE PATTERN. SECURE TWINE AROUND EACH PEG WITH TWO OR MORE ROUND TURNS.

B. MULCH NETTINGS - STAPLE PAPER, COTTON, OR PLASTIC NETTINGS OVER MULCH. USE A DEGRADABLE NETTING IN AREA TO BE MOWED. NETTING IS USUALLY AVAILABLE IN ROLLS 4 FEET WIDE AND UP TO 300 FEET LONG. MULCH ANCHORING — SHOULD BE ACCOMPLISHED IMMEDIATELY AFTER PLACEMENT OF HAY OR STRAW MULCH TO MINIMIZE LOSS BY WIND OR WATER THIS MAY BE DONE BY ONE OF THE FOLLOWING METHODS, DEPENDING UPON THE SIZE OF THE AREA AND STEEPNESS OF SLOPES.

APPLICATIONS SHOULD BE HEAVIER AT EDGES WHERE WIND CATCHES THE MULCH, IN VALLEYS, AND AT CRESTS OF BANKS. SHOULD BE UNIFORM IN APPEARANCE. . CRIMPER MULCH ANCHORING COULTER TOOL - A TRACTOR-DRAWN IMPLEMENT ESPECIALLY DESIGNED TO PUNCH AND ANCHOR MULCH INTO THE SOIL SURFACE. THIS PRACTICE AFFORDS MAXIMUM EROSION CONTROL, BUT ITS USE IS LIMITED TO THOSE SLOPES UPON WHICH THE TRACTOR CAN OPERATE SAFELY. SOIL PENETRATION SHOULD BE ABOUT 3 TO 4 INCHES. ON SLOPING LAND, THE OPERATION SHOULD BE ON THE CONTOUR.

ORGANIC AND VEGETABLE BASED BINDERS — NATURALLY OCCURRING, POWDER BASED, HYDROPHILIC MATERIALS THAT MIXED WITH WATER FORMULATES A GEL AND WHEN APPLIED TO MULCH UNDER SATISFACTORY CURING CONDITIONS WILL FORM MEMBRANED NETWORKS OF INSOLUBLE POLYMERS. THE VEGETABLE GEL SHALL BE PHYSIOLOGICALLY HARMLESS AND NOT RESULT IN A PHYTOTOXIC EFFECT OR IMPEDE GROWTH OF TURFGRASS. VEGETABLE BASED GELS SHALL BE APPLIED AT RATES AND WEATHER CONDITIONS RECOMMENDED BY THE MANUFACTURER. USE ONE OF THE FOLLOW

B. SYNTHETIC BINDERS – HIGH POLYMER SYNTHETIC EMULSION, MISCIBLE WITH WATER WHEN DILUTED AND FOLLOWING APPLICATION TO MULCH, DRYING AND CURING SHALL NO LONGER BE SOLUBLE OR DISPERSIBLE IN WATER. IT SHALL BE APPLIED AT RATES AND WEATHER CONDITIONS RECOMMENDED BY THE MANUFACTURER AND REMAIN TACKY UNTIL GERMINATION OF GRASS.

STANDARDS FOR MANAGEMENT OF HIGH ACID PRODUCING SOILS:

1. LIMIT THE EXCAVATION AREA AND EXPOSURE TIME WHEN HIGH ACID-PRODUCING SOILS ARE ENCOUNTERED.

2. TOPSOIL STRIPPED FROM THE SITE SHALL BE STORED SEPARATELY FROM TEMPORARILY STOCKPILED HIGH ACID-PRODUCING SOILS.

3. STOCKPILES OF HIGH ACID-PRODUCING SOIL SHOULD BE LOCATED ON LEVEL LAND TO MINIMIZE ITS MOVEMENT, ESPECIALLY WHEN THIS MATERIAL HAS A HIGH CLAY CONTENT.

HIGH ACID-PRODUCING SOILS WITH A PH OF 4.0 OR LESS OR CONTAINING IRON SULFIDE (INCLUDING BORROW FROM CUTS OR DREDGED SEDIMENT) SHALL BE ULTIMATELY PLACED OR BURIED WITH LIMESTONE APPLIED AT THE RATE OF 10 TONS PER ACRE (OR 450 POUNDS PER 1,000 SQUARE FEET OF SURFACE AREA) AND COVERED WITH A MINIMUM OF 12 INCHES OF SETTLED SOIL WITH A PH OF 5.0 OR MORE EXCEPT AS FOLLOWS:

a. AREAS WHERE TREES OR SHRUBS ARE TO BE PLANTED SHALL BE COVERED WITH A MINIMUM OF 24 INCHES OF SOIL WITH A PH OR 5 OR MORE.
b. DISPOSAL AREAS SHALL NOT BE LOCATED WITHIN 24 INCHES OF ANY SURFACE OF A SLOPE OR BANK, SUCH AS BERMS, STREAM BANKS, DITCHES, AND OTHERS, TO PREVENT POTENTIAL LATERAL LEACHING DAMAGES. TEMPORARILY STOCKPILED HIGH ACID-PRODUCING SOIL MATERIAL TO BE STORED MORE THAN 48 HOURS SHOULD BE COVERED WITH PROPERLY ANCHORED, HEAVY GRADE SHEETS OF POLYETHYLENE WHERE POSSIBLE. IF NOT POSSIBLE, STOCKPILES SHALL BE COVERED WITH A MINIMUM OF 3 TO 6 INCHES OF WOOD CHIPS TO MINIMIZE EROSION OF THE STOCKPILE. SILT FENCE SHALL BE INSTALLED AT THE TOE OF THE SLOPE TO CONTAIN MOVEMENT OF THE STOCKPILED MATERIAL. TOPSOIL SHALL NOT BE APPLIED TO THE STOCKPILES TO PREVENT TOPSOIL CONTAMINATION WITH HIGH ACID-PRODUCING SOIL.

EQUIPMENT USED FOR MOVEMENT OF HIGH ACID-PRODUCING SOILS SHOULD BE CLEANED AT THE END OF EACH DAY TO PREVENT SPREADING OF HIGH ACID-PRODUCING SOIL MATERIALS TO OTHER PARTS OF THE SITE, INTO STREAMS OR STORMWATER CONVEYANCES, AND TO PROTECT MACHINERY FROM ACCELERATED RUSTING. ON-VEGETATIVE EROSION CONTROL PRACTICES (STONE TRACKING PADS, STRATEGICALLY PLACED LIMESTONE CHECK DAM, SEDIMENT ARRIER, WOOD CHIPS) SHOULD BE INSTALLED TO LIMIT THE MOVEMENT OF HIGH ACID-PRODUCING SOILS FROM, AROUND, OR OFF THE TF

FOLLOWING BURIAL OR REMOVAL OF HIGH ACID-PRODUCING SOIL, TOPSOILING AND SEEDING OF THE SITE (SEE TEMPORARY VEGETATIVE COVER FOR SOIL STABILIZATION, PERMANENT VEGETATIVE COVER FOR SOIL STABILIZATION, AND TOPSOILING), MONITORING MUST CONTINUE FOR A MINIMUM OF 6 MONTHS TO ENSURE THERE IS ADEQUATE STABILIZATION AND THAT NO HIGH ACID-PRODUCING SOIL PROBLEMS EMERGE. IF PROBLEMS STILL EXIST, THE AFFECTED AREA MUST BE TREATED AS INDICATED ABOVE TO CORRECT THE PROBLEM.

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PROJECT: 390 DAVIDSON AVE.	SHEET: 3 OF: 3	DATE: 07-28-2023	CHECKED BY: SJK	DRAWN BY: SJK	SCALE: AS SHOWN